

**REGIONE  
PUGLIA**



**CUP: E75G19000040005**

**PIANO DEGLI INTERVENTI AIP 2020-2023 DI CUI ALLA DELIBERA N.6 DEL 22/02/2021  
CON COPERTURA FINANZIARIA " FONDI DERIVANTI DA PROVENTI TARIFFARI"**

**PROGETTO DEFINITIVO  
POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E DEL RECAPITO FINALE  
A SERVIZIO DELL'AGGLOMERATO DEL COMUNE DI SQUINZANO (LE)**

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*Elaborato*

**R.37.13**

**TABULATI DI CALCOLO STRUTTURALE  
-BASAMENTI BTK1-BTK2-BTK3 -**

**Codice Intervento P1370**

**Codice SAP  
210000023391**

**Prot. N. 27346  
Data 23/04/2021**

**Scala:**

00	MAG.2021	Emesso per Progetto DEFINITIVO			
N. Rev.	Data	Descrizione	Disegnato	Controllato	Approvato



	<b>POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E DEL RECAPITO FINALE DI SQUINZANO (LE) PROGETTO DEFINITIVO <u>Tabulati di calcolo strutturale-Basamenti BTK1-BTK2- BTK3</u></b>	<b>R.37.13</b>
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## 1. AZIONE SISMICA RELATIVA AGLI ELEMENTI NON STRUTTURALI: BIOTRICKLING

L'azione sismica delle masse relative ai biofiltri è stata determinata mediante la seguente relazione riportata nel paragrafo 7 delle NTC 2018:

$$F_a = (S_a \cdot W_a) / q_a \quad [7.2.1]$$

Ossia, la domanda sismica sugli elementi non strutturali è stata determinata applicando loro una forza orizzontale  $F_a$ , con

$F_a$  è la forza sismica orizzontale distribuita o agente nel centro di massa dell'elemento non strutturale, nella direzione più sfavorevole, risultante delle forze distribuite proporzionali alla massa;

$S_a$  è l'accelerazione massima, adimensionalizzata rispetto a quella di gravità, che l'elemento non strutturale subisce durante il sisma e corrisponde allo stato limite in esame;

$W_a$  è il peso dell'elemento; si è assunto un peso pari a 26.350 daN per il BTK1 e 15.500 daN per il BTK2 e il BTK3, con altezza dei biofiltri pari a 3,30 m.

$q_a$  è il fattore di comportamento dell'elemento assunto pari a 2.

In merito alla determinazione dell'accelerazione  $S_a$ , le NTC 2018 permettono di utilizzare, in assenza di analisi più accurate, la seguente formula riportata nelle NTC 2008:

$$S_a = \alpha \cdot S \cdot \left[ \frac{3 \cdot (1 + Z/H)}{1 + (1 - T_a/T_1)^2} - 0,5 \right] \quad (7.2.2 \text{ N.T.C. } 2008)$$

dove:

$\alpha$  è il rapporto tra l'accelerazione massima del terreno ag su sottosuolo tipo A da considerare nello stato limite in esame (v. § 3.2.1) e l'accelerazione di gravità  $g$ ;

$S$  è il coefficiente che tiene conto della categoria di sottosuolo e delle condizioni topografiche secondo quanto riportato nel § 3.2.3.2.1;

$T_a$  è il periodo fondamentale di vibrazione dell'elemento non strutturale;

$T_1$  è il periodo fondamentale di vibrazione della costruzione nella direzione considerata;

$Z$  è la quota del baricentro dell'elemento non strutturale misurata a partire dal piano di fondazione (v. § 3.2.2);

$H$  è l'altezza della costruzione misurata a partire dal piano di fondazione (altezza muri).

Nel caso in esame si ha:

$T_a / T_1 = 1,00$  (a favore di sicurezza)

$Z/H = 2,45 \text{ m} / 0,80 \text{ m} = 3,06$

$\alpha = 0,056$  allo SLV,  $\alpha = 0,022$  allo SLD e  $\alpha = 0,017$  allo SLO;

$S = 1,20$  essendo il terreno di Categoria B

Per cui si ha:

$S_a = 0,056 \cdot 1,20 \cdot [(3 \cdot (1 + 3,06) / (1 + (1 - 1)^2) - 0,5)] = 0,784$  allo SLV

$S_a = 0,022 \cdot 1,20 \cdot [(3 \cdot (1 + 3,06) / (1 + (1 - 1)^2) - 0,5)] = 0,308$  allo SLD

$S_a = 0,017 \cdot 1,20 \cdot [(3 \cdot (1 + 3,06) / (1 + (1 - 1)^2) - 0,5)] = 0,238$  allo SLO

Considerando  $q_a = 2,0$  risulta

$S_a/q_a = 0,392$  allo SLV

$S_a/q_a = 0,154$  allo SLD

$S_a/q_a = 0,119$  allo SLO

La forza sismica da applicare al baricentro di ciascun elemento secondario in funzione del suo peso  $W_a$  è pari a:

SLV

BTK1:  $F_a = 0,3927 \cdot 26350 \text{ daN} = 10350 \text{ daN}$

BTK2:  $F_a = 0,3927 \cdot 15500 \text{ daN} = 6100 \text{ daN}$

BTK3:  $F_a = 0,3927 \cdot 15500 \text{ daN} = 6100 \text{ daN}$

SLD

BTK1:  $F_a = 0,154 \cdot 26350 \text{ daN} = 4065 \text{ daN}$

BTK2:  $F_a = 0,154 \cdot 15500 \text{ daN} = 2395 \text{ daN}$

BTK3:  $F_a = 0,154 \cdot 15500 \text{ daN} = 2395 \text{ daN}$

SLO

BTK1:  $F_a = 0,154 \cdot 26350 \text{ daN} = 3145 \text{ daN}$

BTK2:  $F_a = 0,154 \cdot 15500 \text{ daN} = 1850 \text{ daN}$

BTK3:  $F_a = 0,154 \cdot 15500 \text{ daN} = 1850 \text{ daN}$

	<b>POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E DEL RECAPITO FINALE DI SQUINZANO (LE) PROGETTO DEFINITIVO <u>Tabulati di calcolo strutturale-Basamenti BTK1-BTK2- BTK3</u></b>	<b>R.37.13</b>
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## 2. DATI COMUNI PER IL PROGETTO E LA VERIFICA DEI BASAMENTI PER BIOTRICKLING

La costruzione in oggetto è definita dalla seguente tipologia (p.to 2.4 delle NT):

Vita della struttura	
Tipo	Opere ordinarie (50-100)
Vita nominale VN [anni]	50.0
Classe d'uso	III
Coefficiente d'uso CU	1.500
Periodo di riferimento VR [anni]	75.000
Probabilità di superamento PVR allo Stato limite di esercizio - SLO	81.0%
Probabilità di superamento PVR allo Stato limite di esercizio - SLD	63.0%
Probabilità di superamento PVR allo Stato limite ultimo - SLV	10.0%
Periodo di ritorno TR SLO [anni]	45.2
Periodo di ritorno TR SLD [anni]	75.4
Periodo di ritorno TR SLV [anni]	711.8

Materiali impiegati e resistenze di calcolo

Per la realizzazione dell'opera in oggetto saranno impiegati i seguenti materiali, di cui si riportano nell'ordine le proprietà meccaniche adottate nel calcolo elastico e le resistenze di calcolo per le verifiche di sicurezza:

Materiali		
C35/45		
Peso specifico	daN/m <sup>3</sup>	2500.00
Modulo di Young E	MPa	3.41E04
Modulo di Poisson n		0.13
Coefficiente di dilatazione termica l	1/°C	1e-05

Caratteristiche dei materiali delle parti in calcestruzzo armato		
Classe calcestruzzo		Classe C35/45
Resistenza cubica Rck	MPa	45.00
Resistenza di calcolo fcd	MPa	21.16
Resistenza a trazione di calcolo fctd	MPa	1.56
Resistenza cilindrica fck	MPa	37.35
Resistenza a trazione media fctm	MPa	3.35
Classe acciaio barre longitudinali		Acciaio barre B450C
Resistenza allo snervamento fyk	MPa	>=450.00
Resistenza alla rottura barre fitk	MPa	>=540.00
Classe acciaio staffe		Acciaio barre B450C
Resistenza allo snervamento fyk	MPa	>=450.00
Resistenza alla rottura barre fitk	MPa	>=540.00

Impalcati ( a vantaggio di sicurezza, si è considerata l'altezza di calcolo dei muretti pari a 1,00 m anziché 0,80 m)

N°	Quota	Rigido	Incr.Soll.Pil	Incr.Soll.Par.
	m	m		
0	0.000	No	1.000	1.000
1	1.000	Si	1.000	1.000

Percentuali Spostamento masse impalcato

Posizione	% Spostamento direzione X	% Spostamento direzione Y
1	0	-5
2	5	0
3	0	5
4	-5	0



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Combinazioni del Sisma in X e Y e Verticale

Comb.	Pos. SismaX	Pos. SismaY	Fx	Fy	Fz
1	1	2	1	0.3	0.3
2	1	2	0.3	1	0.3
3	1	2	0.3	0.3	1
4	1	4	1	0.3	0.3
5	1	4	0.3	1	0.3
6	1	4	0.3	0.3	1
7	3	2	1	0.3	0.3
8	3	2	0.3	1	0.3
9	3	2	0.3	0.3	1
10	3	4	1	0.3	0.3
11	3	4	0.3	1	0.3
12	3	4	0.3	0.3	1

Comb. Numero di combinazione dei sismi  
Pos. SismaX Posizione in cui viene scelto il sisma in direzione X  
Pos. SismaY Posizione in cui viene scelto il sisma in direzione Y  
Fx Fattore con cui il sisma X partecipa  
Fy Fattore con cui il sisma Y partecipa  
Fz Fattore con cui il sisma Verticale partecipa (quando richiesto)

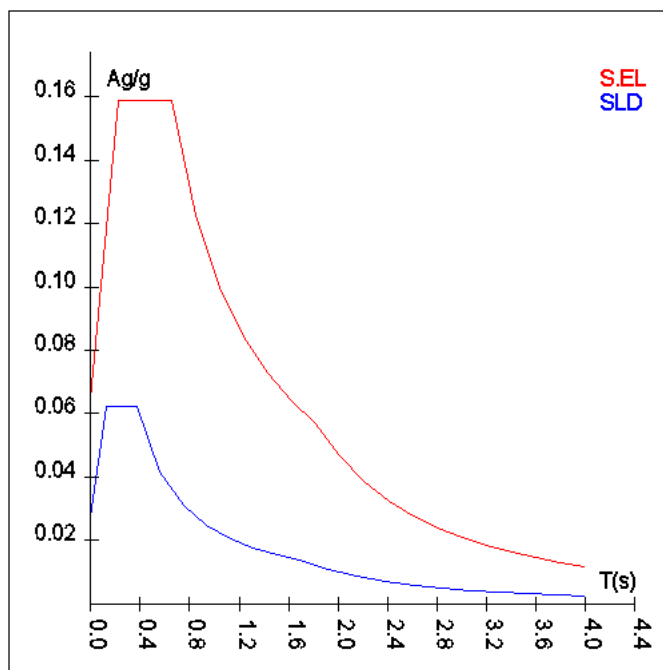
Spettri di risposta

Spettro: SpettroNT\_2018

Il calcolo degli spettri e del fattore di comportamento sono stati calcolati per la seguente tipologia di terreno e struttura.

<b>Vita della struttura</b>	
Tipo	Opere ordinarie (50-100)
Vita nominale VN [anni]	50.0
Classe d'uso	III
Coefficiente d'uso CU	1.500
Periodo di riferimento VR [anni]	75.000
Probabilità di superamento PVR allo Stato limite di esercizio - SLD	63.0%
Probabilità di superamento PVR allo Stato limite ultimo - SLV	10.0%
Periodo di ritorno TR SLD [anni]	75.4
Periodo di ritorno TR SLV [anni]	711.8
<b>Parametri del sito</b>	
Comune	Squinzano (LE)
Longitudine	18.0458
Latitudine	40.4344
Id reticolo del sito	34590-34591-34812-34813
<b>Valori di riferimento del sito</b>	
Accelerazione orizzontale massima del sito Ag/g - SLD (TR=75.4)	0.0225
Fattore di amplificazione dello spettro Fo - SLD (TR=75.4)	2.2984
Periodo di riferimento di inizio del tratto a velocità costante T <sub>C</sub> [s] - SLD (TR=75.4)	0.259
Accelerazione orizzontale massima del sito Ag/g - SLV (TR=711.8)	0.0536
Fattore di amplificazione dello spettro Fo - SLV (TR=711.8)	2.4663
Periodo di riferimento di inizio del tratto a velocità costante T <sub>C</sub> [s] - SLV (TR=711.8)	0.523
Coefficiente Amplificazione Topografica St	1.000
Categoria terreno	B
<b>Stato limite SLV</b>	
Coefficiente di amplificazione stratigrafica Ss	1.20
Periodo di inizio del tratto ad accelerazione costante dello spettro TB [s]	0.22
Periodo di inizio del tratto a velocità costante dello spettro TC [s]	0.65
Periodo di inizio del tratto a spostamento costante dello spettro TD [s]	1.81
<b>Stato limite SLD</b>	
Coefficiente di amplificazione stratigrafica Ss	1.20
Periodo di inizio del tratto ad accelerazione costante dello spettro TB [s]	0.12
Periodo di inizio del tratto a velocità costante dello spettro TC [s]	0.37
Periodo di inizio del tratto a spostamento costante dello spettro TD [s]	1.69
<b>Spettro Elastico</b>	
Smorzamento viscoso %	5.0

T El. [s]	Sd El. [a/g]	T SLD [s]	Sd SLD [a/g]
0.00000	0.06437	0.00000	0.02706
0.21825	0.15877	0.12459	0.06219
0.65475	0.15877	0.37377	0.06219
0.84805	0.12258	0.56183	0.04137
1.04136	0.09982	0.74989	0.03100
1.23466	0.08419	0.93795	0.02478
1.42797	0.07280	1.12601	0.02064
1.62128	0.06412	1.31407	0.01769
1.81458	0.05729	1.50213	0.01547
2.01326	0.04654	1.69019	0.01375
2.21193	0.03855	1.92117	0.01064
2.41061	0.03246	2.15215	0.00848
2.60928	0.02771	2.38313	0.00692
2.80795	0.02392	2.61411	0.00575
3.00663	0.02087	2.84509	0.00485
3.20530	0.01836	3.07608	0.00415
3.40398	0.01628	3.30706	0.00359
3.60265	0.01453	3.53804	0.00314
3.80133	0.01305	3.76902	0.00277
4.00000	0.01179	4.00000	0.00246



Percentuali Spostamento masse impalcati

Posizione	% Spostamento direzione X	% Spostamento direzione Y
1	0	-5
2	5	0
3	0	5
4	-5	0

Combinazioni del Sisma in X e Y e Verticale

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
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Comb.	Pos. SismaX	Pos. SismaY	Fx	Fy	Fz
1	1	2	1	0.3	0.3
2	1	2	0.3	1	0.3
3	1	2	0.3	0.3	1
4	1	4	1	0.3	0.3
5	1	4	0.3	1	0.3
6	1	4	0.3	0.3	1
7	3	2	1	0.3	0.3
8	3	2	0.3	1	0.3
9	3	2	0.3	0.3	1
10	3	4	1	0.3	0.3
11	3	4	0.3	1	0.3
12	3	4	0.3	0.3	1

Comb. Numero di combinazione dei sismi

Pos. SismaX Posizione in cui viene scelto il sisma in direzione X

Pos. SismaY Posizione in cui viene scelto il sisma in direzione Y

Fx Fattore con cui il sisma X partecipa

Fy Fattore con cui il sisma Y partecipa

Fz Fattore con cui il sisma Verticale partecipa (quando richiesto)

**Azioni sulla struttura**

Descrizione	Tipo
Peso Proprio	Automatica
NEVE	Utente
biofiltro	Utente
vento y	Utente
accidentali	Utente
vento x	Utente
azione sismica SLV y	Utente
azione sismica SLV x	Utente
azione sismica SLD y	Utente
azione sismica SLD x	Utente
serbatoio	Utente
ventilatore	Utente
4100	Utente

**Scenario di calcolo**

Scenario : ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO

Combinazione n° 1: **Peso proprio**

Tipo: STR+GEO

Spettro: n.a.

Fattore sisma: n.a.

Angolo ingresso sisma [°]: n.a.

Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1.3	Si	n.a.	n.a.
NEVE	1	No	n.a.	n.a.
biofiltro	1	No	n.a.	n.a.
vento y	1	No	n.a.	n.a.
accidentali	1	No	n.a.	n.a.
vento x	1	No	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1	No	n.a.	n.a.
ventilatore	1	No	n.a.	n.a.
4100	1	No	n.a.	n.a.

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**Combinazione n° 2:** Solo Permanenti  
Tipo: STR+GEO  
Spettro: n.a.  
Fattore sisma: n.a.  
Angolo ingresso sisma [°]: n.a.  
Kmod: 0.60

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1.3	Si	n.a.	n.a.
NEVE	1.3	No	n.a.	n.a.
biofiltro	1.5	Si	n.a.	n.a.
vento y	1	No	n.a.	n.a.
accidentali	1	No	n.a.	n.a.
vento x	1	No	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1.5	Si	n.a.	n.a.
ventilatore	1.5	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 3:** Solo Permanenti  
Tipo: STR+GEO  
Spettro: n.a.  
Fattore sisma: n.a.  
Angolo ingresso sisma [°]: n.a.  
Kmod: 0.60

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1.3	Si	n.a.	n.a.
NEVE	1.3	No	n.a.	n.a.
biofiltro	1.5	No	n.a.	n.a.
vento y	1	No	n.a.	n.a.
accidentali	1	No	n.a.	n.a.
vento x	1	No	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1.5	No	n.a.	n.a.
ventilatore	1.5	No	n.a.	n.a.
4100	1.5	Si	n.a.	n.a.

**Combinazione n° 4:** SLU1  
Tipo: STR+GEO  
Spettro: n.a.  
Fattore sisma: n.a.  
Angolo ingresso sisma [°]: n.a.  
Kmod: 0.90

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1.3	Si	n.a.	n.a.
NEVE	0.75	Si	n.a.	n.a.
biofiltro	1.5	Si	n.a.	n.a.
vento y	1.5	No	n.a.	n.a.
accidentali	1.5	Si	n.a.	n.a.
vento x	1	No	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1.5	Si	n.a.	n.a.
ventilatore	1.5	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 5:** SLU2  
 Tipo: STR+GEO  
 Spettro: n.a.  
 Fattore sisma: n.a.  
 Angolo ingresso sisma [°]: n.a.  
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1.3	Si	n.a.	n.a.
NEVE	0.75	Si	n.a.	n.a.
biofiltro	1.5	Si	n.a.	n.a.
vento y	0.9	Si	n.a.	n.a.
accidentali	1.5	Si	n.a.	n.a.
vento x	1	No	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1.5	Si	n.a.	n.a.
ventilatore	1.5	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 6:** SLU3  
 Tipo: STR+GEO  
 Spettro: n.a.  
 Fattore sisma: n.a.  
 Angolo ingresso sisma [°]: n.a.  
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1.3	Si	n.a.	n.a.
NEVE	0.75	Si	n.a.	n.a.
biofiltro	1.5	Si	n.a.	n.a.
vento y	0.75	No	n.a.	n.a.
accidentali	1.5	Si	n.a.	n.a.
vento x	0.9	Si	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1.5	Si	n.a.	n.a.
ventilatore	1.5	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 7:** SLU4  
 Tipo: STR+GEO  
 Spettro: n.a.  
 Fattore sisma: n.a.  
 Angolo ingresso sisma [°]: n.a.  
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1.3	Si	n.a.	n.a.
NEVE	1.5	Si	n.a.	n.a.
biofiltro	1.5	Si	n.a.	n.a.
vento y	0.9	Si	n.a.	n.a.
accidentali	1.5	Si	n.a.	n.a.
vento x	0.75	No	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1.5	Si	n.a.	n.a.

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Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
ventilatore	1.5	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

Combinazione n° 8: **SLU5**  
 Tipo: STR+GEO  
 Spettro: n.a.  
 Fattore sisma: n.a.  
 Angolo ingresso sisma [°]: n.a.  
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1.3	Si	n.a.	n.a.
NEVE	1.5	Si	n.a.	n.a.
biofiltro	1.5	Si	n.a.	n.a.
vento y	0.9	No	n.a.	n.a.
accidentali	1.5	Si	n.a.	n.a.
vento x	0.9	Si	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1.5	Si	n.a.	n.a.
ventilatore	1.5	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

Combinazione n° 9: **SLU6**  
 Tipo: STR+GEO  
 Spettro: n.a.  
 Fattore sisma: n.a.  
 Angolo ingresso sisma [°]: n.a.  
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1.3	Si	n.a.	n.a.
NEVE	0.75	Si	n.a.	n.a.
biofiltro	1.5	Si	n.a.	n.a.
vento y	1.5	No	n.a.	n.a.
accidentali	1.5	Si	n.a.	n.a.
vento x	1.5	Si	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1.5	Si	n.a.	n.a.
ventilatore	1.5	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

Combinazione n° 10: **SLU7**  
 Tipo: STR+GEO  
 Spettro: n.a.  
 Fattore sisma: n.a.  
 Angolo ingresso sisma [°]: n.a.  
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1.3	Si	n.a.	n.a.
NEVE	0.75	Si	n.a.	n.a.
biofiltro	1.5	Si	n.a.	n.a.
vento y	1.5	Si	n.a.	n.a.
accidentali	1.5	Si	n.a.	n.a.
vento x	1.5	No	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.

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Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1.5	Si	n.a.	n.a.
ventilatore	1.5	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 11:** **SLU8**  
 Tipo: STR+GEO  
 Spettro: n.a.  
 Fattore sisma: n.a.  
 Angolo ingresso sisma [°]: n.a.  
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1.3	Si	n.a.	n.a.
NEVE	0.75	No	n.a.	n.a.
biofiltro	1.5	Si	n.a.	n.a.
vento y	1.5	Si	n.a.	n.a.
accidentali	1.5	No	n.a.	n.a.
vento x	1.5	No	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1.5	Si	n.a.	n.a.
ventilatore	1.5	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 12:** **SISMAxSLV**  
 Tipo: Modale STR+GEO  
 Spettro: SpettroNT\_2018  
 Fattore sisma: 1.00  
 Angolo ingresso sisma [°]: 0  
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	Si	1
NEVE	1	No	No	1
biofiltro	1	Si	Si	1
vento y	1	No	No	1
accidentali	0.8	Si	Si	1
vento x	1	No	No	1
azione sismica SLV y	1	No	Si	1
azione sismica SLD y	1	No	Si	1
azione sismica SLD x	1	No	Si	1
serbatoio	1	Si	Si	1
ventilatore	1	Si	Si	1
4100	1	No	No	1

**Combinazione n° 13:** **SISMAySLV**  
 Tipo: Modale STR+GEO  
 Spettro: SpettroNT\_2018  
 Fattore sisma: 1.00  
 Angolo ingresso sisma [°]: 90  
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	Si	1
NEVE	1	No	No	1
biofiltro	1	Si	Si	1

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Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
vento y	1	No	No	1
accidentali	0.8	Si	Si	1
vento x	1	No	No	1
azione sismica SLV y	1	Si	Si	1
azione sismica SLV x	1	No	Si	1
azione sismica SLD y	1	No	Si	1
azione sismica SLD x	1	No	Si	1
serbatoio	1	Si	Si	1
ventilatore	1	Si	Si	1
4100	1	No	No	1

**Combinazione n° 14:** **SISMAx1SLV**  
 Tipo: Modale STR+GEO  
 Spettro: SpettroNT\_2018  
 Fattore sisma: 1.00  
 Angolo ingresso sisma [°]: 0  
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	Si	1
NEVE	1	No	No	1
biofiltro	1	Si	Si	1
vento y	1	No	No	1
accidentali	0.8	No	Si	1
vento x	1	No	No	1
azione sismica SLV y	1	No	Si	1
azione sismica SLV x	1	Si	Si	1
azione sismica SLD y	1	No	Si	1
azione sismica SLD x	1	No	Si	1
serbatoio	1	Si	Si	1
ventilatore	1	Si	Si	1
4100	1	No	No	1

**Combinazione n° 15:** **SISMAy1SLV**  
 Tipo: Modale STR+GEO  
 Spettro: SpettroNT\_2018  
 Fattore sisma: 1.00  
 Angolo ingresso sisma [°]: 90  
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	Si	1
NEVE	1	No	No	1
biofiltro	1	Si	Si	1
vento y	1	No	No	1
accidentali	0.8	No	Si	1
vento x	1	No	No	1
azione sismica SLV y	1	Si	Si	1
azione sismica SLV x	1	No	Si	1
azione sismica SLD y	1	No	Si	1
azione sismica SLD x	1	No	Si	1
serbatoio	1	Si	Si	1
ventilatore	1	Si	Si	1
4100	1	No	No	1

**Combinazione n° 16:** **RARA1**  
 Tipo: SLE Rara  
 Spettro: n.a.  
 Fattore sisma: n.a.  
 Angolo ingresso sisma [°]: n.a.  
 Kmod: 1.00



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Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
NEVE	0.5	Si	n.a.	n.a.
biofiltro	1	Si	n.a.	n.a.
vento y	0.6	Si	n.a.	n.a.
accidentali	1	Si	n.a.	n.a.
vento x	1	No	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1	Si	n.a.	n.a.
ventilatore	1	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 17:** **RARA2**  
 Tipo: SLE Rara  
 Spettro: n.a.  
 Fattore sisma: n.a.  
 Angolo ingresso sisma [°]: n.a.  
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
NEVE	0.5	Si	n.a.	n.a.
biofiltro	1	Si	n.a.	n.a.
vento y	0.2	No	n.a.	n.a.
accidentali	1	Si	n.a.	n.a.
vento x	0.6	Si	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1	Si	n.a.	n.a.
ventilatore	1	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 18:** **RARA3**  
 Tipo: SLE Rara  
 Spettro: n.a.  
 Fattore sisma: n.a.  
 Angolo ingresso sisma [°]: n.a.  
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
NEVE	0.5	Si	n.a.	n.a.
biofiltro	1	Si	n.a.	n.a.
vento y	1	Si	n.a.	n.a.
accidentali	1	Si	n.a.	n.a.
vento x	1	No	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1	Si	n.a.	n.a.
ventilatore	1	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 19:** **RARA4**  
 Tipo: SLE Rara  
 Spettro: n.a.  
 Fattore sisma: n.a.  
 Angolo ingresso sisma [°]: n.a.  
 Kmod: 1.00

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Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
NEVE	0.5	Si	n.a.	n.a.
biofiltro	1	Si	n.a.	n.a.
vento y	1	No	n.a.	n.a.
accidentali	1	Si	n.a.	n.a.
vento x	1	Si	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1	Si	n.a.	n.a.
ventilatore	1	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 20:** **RARA5**  
 Tipo: SLE Rara  
 Spettro: n.a.  
 Fattore sisma: n.a.  
 Angolo ingresso sisma [°]: n.a.  
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
NEVE	1	Si	n.a.	n.a.
biofiltro	1	Si	n.a.	n.a.
vento y	1	No	n.a.	n.a.
accidentali	1	Si	n.a.	n.a.
vento x	0.6	Si	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1	Si	n.a.	n.a.
ventilatore	1	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 21:** **RARA6**  
 Tipo: SLE Rara  
 Spettro: n.a.  
 Fattore sisma: n.a.  
 Angolo ingresso sisma [°]: n.a.  
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
NEVE	1	Si	n.a.	n.a.
biofiltro	1	Si	n.a.	n.a.
vento y	0.6	Si	n.a.	n.a.
accidentali	1	Si	n.a.	n.a.
vento x	0.6	No	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1	Si	n.a.	n.a.
ventilatore	1	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 22:** **RARA7**  
 Tipo: SLE Rara  
 Spettro: n.a.  
 Fattore sisma: n.a.

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Angolo ingresso sisma [°]: n.a.  
Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
NEVE	1	No	n.a.	n.a.
biofiltro	1	Si	n.a.	n.a.
vento y	1	Si	n.a.	n.a.
accidentali	1	No	n.a.	n.a.
vento x	0.6	No	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1	Si	n.a.	n.a.
ventilatore	1	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 23:** FREQUENTE 1  
Tipo: SLE Freq.  
Spettro: n.a.  
Fattore sisma: n.a.  
Angolo ingresso sisma [°]: n.a.  
Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
NEVE	0.2	No	n.a.	n.a.
biofiltro	1	Si	n.a.	n.a.
vento y	1	No	n.a.	n.a.
accidentali	0.9	Si	n.a.	n.a.
vento x	0.2	No	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1	Si	n.a.	n.a.
ventilatore	1	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 24:** FREQUENTE 2  
Tipo: SLE Freq.  
Spettro: n.a.  
Fattore sisma: n.a.  
Angolo ingresso sisma [°]: n.a.  
Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
NEVE	0.2	Si	n.a.	n.a.
biofiltro	1	Si	n.a.	n.a.
vento y	1	No	n.a.	n.a.
accidentali	0.9	Si	n.a.	n.a.
vento x	0.2	No	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1	Si	n.a.	n.a.
ventilatore	1	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 25:** FREQUENTE 3  
Tipo: SLE Freq.

Spettro: n.a.  
Fattore sisma: n.a.  
Angolo ingresso sisma [°]: n.a.  
Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
NEVE	1	No	n.a.	n.a.
biofiltro	1	Si	n.a.	n.a.
vento y	1	No	n.a.	n.a.
accidentali	0.9	Si	n.a.	n.a.
vento x	0.2	Si	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1	Si	n.a.	n.a.
ventilatore	1	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 26: FREQUENTE 4**  
Tipo: SLE Freq.  
Spettro: n.a.  
Fattore sisma: n.a.  
Angolo ingresso sisma [°]: n.a.  
Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
NEVE	1	No	n.a.	n.a.
biofiltro	1	Si	n.a.	n.a.
vento y	0.2	Si	n.a.	n.a.
accidentali	0.9	Si	n.a.	n.a.
vento x	0.2	No	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1	Si	n.a.	n.a.
ventilatore	1	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 27: FREQUENTE 5**  
Tipo: SLE Freq.  
Spettro: n.a.  
Fattore sisma: n.a.  
Angolo ingresso sisma [°]: n.a.  
Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
NEVE	1	No	n.a.	n.a.
biofiltro	1	Si	n.a.	n.a.
vento y	0.2	Si	n.a.	n.a.
accidentali	0.9	No	n.a.	n.a.
vento x	0.2	No	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1	Si	n.a.	n.a.
ventilatore	1	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

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**Combinazione n° 28:** **Quasi P1**  
Tipo: SLE Q.Perm.  
Spettro: n.a.  
Fattore sisma: n.a.  
Angolo ingresso sisma [°]: n.a.  
Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
NEVE	1	No	n.a.	n.a.
biofiltro	1	Si	n.a.	n.a.
vento y	1	No	n.a.	n.a.
accidentali	0.8	Si	n.a.	n.a.
vento x	1	No	n.a.	n.a.
azione sismica SLV y	1	No	n.a.	n.a.
azione sismica SLV x	1	No	n.a.	n.a.
azione sismica SLD y	1	No	n.a.	n.a.
azione sismica SLD x	1	No	n.a.	n.a.
serbatoio	1	Si	n.a.	n.a.
ventilatore	1	Si	n.a.	n.a.
4100	1	No	n.a.	n.a.

**Combinazione n° 29:** **Sisma x SLD**  
Tipo: Modale SLE  
Spettro: SpettroNT\_2018  
Fattore sisma: 1.00  
Angolo ingresso sisma [°]: 0  
Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	Si	1
NEVE	1	No	No	1
biofiltro	1	Si	Si	1
vento y	1	No	No	1
accidentali	0.8	Si	Si	1
vento x	1	No	No	1
azione sismica SLV y	1	No	Si	1
azione sismica SLV x	1	No	Si	1
azione sismica SLD y	1	No	Si	1
azione sismica SLD x	1	Si	Si	1
serbatoio	1	Si	Si	1
ventilatore	1	Si	Si	1
4100	1	No	No	1

**Combinazione n° 30:** **Sisma Y SLD**  
Tipo: Modale SLE  
Spettro: SpettroNT\_2018  
Fattore sisma: 1.00  
Angolo ingresso sisma [°]: 90  
Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	Si	1
NEVE	1	No	No	1
biofiltro	1	Si	Si	1
vento y	1	No	No	1
accidentali	0.8	Si	Si	1
vento x	1	No	No	1
azione sismica SLV y	1	No	Si	1
azione sismica SLV x	1	No	Si	1
azione sismica SLD y	1	Si	Si	1
azione sismica SLD x	1	No	Si	1
serbatoio	1	Si	Si	1
ventilatore	1	Si	Si	1
4100	1	No	No	1

Combinazione n° 31: Sisma x1 SLD  
Tipo: Modale SLE  
Spettro: SpettroNT\_ 2018  
Fattore sisma: 1.00  
Angolo ingresso sisma [°]: 0  
Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	Si	1
NEVE	1	No	No	1
biofiltro	1	Si	Si	1
vento y	1	No	No	1
accidentali	0.8	No	Si	1
vento x	1	No	No	1
azione sismica SLV y	1	No	Si	1
azione sismica SLV x	1	No	Si	1
azione sismica SLD y	1	No	Si	1
azione sismica SLD x	1	Si	Si	1
serbatoio	1	Si	Si	1
ventilatore	1	Si	Si	1
4100	1	No	No	1

Combinazione n° 32: Sisma Y1 SLD  
Tipo: Modale SLE  
Spettro: SpettroNT\_ 2018  
Fattore sisma: 1.00  
Angolo ingresso sisma [°]: 90  
Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	Si	1
NEVE	1	No	No	1
biofiltro	1	Si	Si	1
vento y	1	No	No	1
accidentali	0.8	No	Si	1
vento x	1	No	No	1
azione sismica SLV y	1	No	Si	1
azione sismica SLV x	1	No	Si	1
azione sismica SLD y	1	Si	Si	1
azione sismica SLD x	1	No	Si	1
serbatoio	1	Si	Si	1
ventilatore	1	Si	Si	1
4100	1	No	No	1

#### Criteri di verifica

CLS_Platee_ND		
Generici		
Resistenza caratteristica Rck	MPa	45.00
Tensione caratteristica snervamento acciaio barre fyk	MPa	450.00
Tensione caratteristica snervamento acciaio staffe fyk	MPa	450.00
Deformazione unitaria ec0		0.002
Deformazione ultima ecu		0.0035
efu (solo incrudimento)		0.002
Modulo elastico E acciaio	MPa	2.10E05
Copriferro di calcolo	cm	5.6
Copriferro di disegno	cm	5.0
Coefficiente di sicurezza gCIs		1.5
Coefficiente di sicurezza gAcc		1.15
Riduzione fcd calcestruzzo		0.85

Usa staffe minime di normativa in assenza di sisma		Si
Usa staffe minime di normativa in presenza di sisma		No
Generici N.T.		
Inclinazione bielle compresse cotg(q)		1.00
Modello acciaio		Incrudente
Incrudimento Ey/E0		0.000
Elemento esistente		No
Generici D.M. 96 T.A.		
Tensione ammissibile sc	MPa	13.50
Tensione ammissibile sc in trazione	MPa	4.02
Tensione ammissibile sc acciaio	MPa	260.00
Tensione tangenziale ammissibile tc0	MPa	0.80
Tensione tangenziale massima tc1	MPa	2.26
Coefficiente di omogeneizzazione n		15
Coefficiente di omogeneizzazione n in trazione		0.5
Sezione interamente reagente		No
Fessurazioni		
Verifica a decompressione		No
Verifica formazione fessure		No
Verifica aperture fessure		Si
Classe di esposizione		XC4
Tipo armatura		Poco sensibile
Combinazione Rara		No
Combinazione QP		Si
W ammissibile Combinazione QP	mm	0.200
Combinazione Freq.		Si
W ammissibile Combinazione Freq.	mm	0.300
Valore caratteristico apertura fessure wk(*wm)		1
Resistenza media a trazione fctm	MPa	3.4
Coefficiente di breve o lunga durata kt		0.40
Coefficiente di aderenza kl		0.80
Tensioni ammissibili di esercizio		
Verifica Combinazione Rara		Si
Tensione ammissibile sCls	MPa	22.41
Tensione ammissibile sAcciaio	MPa	360.00
Verifica Combinazione QP		Si
Tensione ammissibile sCls	MPa	16.81
Tensione ammissibile sAcciaio	MPa	360.00
Verifica Combinazione Freq.		No
Coefficienti di omogeneizzazione		
Acciaio - Cls compresso		15
Cls tesoro - Cls compresso		0.5
Armatura muri		
Minima percentuale armatura rispetto al Cls in direzione X	%	0.1
Minima percentuale armatura rispetto al Cls in direzione Y	%	0.1
Massima percentuale armatura rispetto al Cls in direzione X	%	2
Massima percentuale armatura rispetto al Cls in direzione Y	%	2
Verifica muri		
Step incremento armatura	cmq	0.01
Verifica muri come pareti		No

<b>CLS_Muri_ND</b>		
Generici		
Resistenza caratteristica Rck	MPa	45.00
Tensione caratteristica snervamento acciaio barre fyk	MPa	450.00
Tensione caratteristica snervamento acciaio staffe fyk	MPa	450.00
Deformazione unitaria ec0		0.002
Deformazione ultima ecu		0.0035
efu (solo incrudimento)		0.002
Modulo elastico E acciaio	MPa	2.10E05
Copriferro di calcolo	cm	5.6
Copriferro di disegno	cm	5.0
Coefficiente di sicurezza gCls		1.5
Coefficiente di sicurezza gAcc		1.15
Riduzione fed calcestruzzo		0.85

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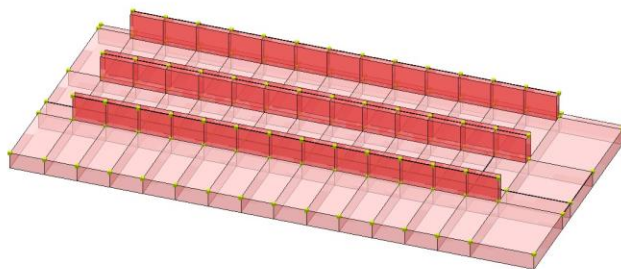
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Usa staffe minime di normativa in assenza di sisma		Si
Usa staffe minime di normativa in presenza di sisma		No
Generici N.T.		
Inclinazione bielle compresse cotg(q)		1.00
Modello acciaio		Incrudente
Incrudimento Ey/E0		0.000
Elemento esistente		No
Generici D.M. 96 T.A.		
Tensione ammissibile sc	MPa	13.50
Tensione ammissibile sc in trazione	MPa	4.02
Tensione ammissibile sc acciaio	MPa	260.00
Tensione tangenziale ammissibile tc0	MPa	0.80
Tensione tangenziale massima tc1	MPa	2.26
Coefficiente di omogeneizzazione n		15
Coefficiente di omogeneizzazione n in trazione		0.5
Sezione interamente reagente		No
Fessurazioni		
Verifica a decompressione		No
Verifica formazione fessure		No
Verifica aperture fessure		Si
Classe di esposizione		XC4
Tipo armatura		Poco sensibile
Combinazione Rara		No
Combinazione QP		Si
W ammissibile Combinazione QP	mm	0.200
Combinazione Freq.		Si
W ammissibile Combinazione Freq.	mm	0.300
Valore caratteristico apertura fessure wk(*wm)		1
Resistenza media a trazione fctm	MPa	3.4
Coefficiente di breve o lunga durata kt		0.40
Coefficiente di aderenza kl		0.80
Tensioni ammissibili di esercizio		
Verifica Combinazione Rara		Si
Tensione ammissibile sCls	MPa	22.41
Tensione ammissibile sAcciaio	MPa	360.00
Verifica Combinazione QP		Si
Tensione ammissibile sCls	MPa	16.81
Tensione ammissibile sAcciaio	MPa	360.00
Verifica Combinazione Freq.		No
Coefficienti di omogeneizzazione		
Acciaio - Cls compresso		15
Cls teso - Cls compresso		0.5
Armatura muri		
Minima percentuale armatura rispetto al Cls in direzione X	%	0.1
Minima percentuale armatura rispetto al Cls in direzione Y	%	0.1
Massima percentuale armatura rispetto al Cls in direzione X	%	2
Massima percentuale armatura rispetto al Cls in direzione Y	%	2
Verifica muri		
Step incremento armatura	cmq	0.01
Verifica muri come pareti		No



### 3. BASAMENTO PER BIOFILTRO BTK 1



#### Validazione del calcolo

Di seguito si riportano alcuni dati significativi del calcolo in base ai quali si ritiene che il codice di calcolo è affidabile ed i risultati accettati dal progettista.

**Risultati Analisi Dinamica - Statistiche matrice di rigidezza**  
Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

Minimo della diagonale	1.809725e+06
Massimo della diagonale	1.224345e+10
Rapporto Max/Min	6.765368e+03
Media della diagonale	1.131539e+09
Densità	4.179977e-01

#### Taglianti di piano

Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

I taglianti sono dati per combinazioni di calcolo C-S-Pm con C=Combinazione(1,2,...) S=Sisma(I,II) Pm=posizione masse(1,2,...). Le azioni, complessive, sono riferite al sistema di riferimento globale.

$\Theta = F_z \cdot dr / (F_h \cdot H)$  con:

Fz Forza verticale

dr Spostamento medio del piano rispetto al piano inferiore

Fh Tagliante

H Altezza del piano

dx spostamento medio di piano in direzione X

dy spostamento medio di piano in direzione Y

dr  $((dx_s - dx_i)^2 + (dy_s - dy_i)^2)^{0.5}$  s=impalcato superiore i=impalcato inferiore

Nel caso di combinazioni sismiche l'aliquota dovuta al sisma di dx e dy è valutata secondo le indicazioni in 7.3.3, moltiplicando lo spostamento per  $\mu_d$

**Combinazione:** 11-I-1 (SISMAxSLV)

Piano	Fx daN	Fy daN	Fz daN	dx mm	dy mm	$\Theta$
0	22901.45	-22252.56	77980.84	0.00	0.00	--
1	-23001.58	22271.23	-57182.73	-0.00	-0.00	0.000004

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Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	22901.45	-22252.56	22901.45	-22252.56
1	0.00	0.00	0.00	0.00	-23001.58	22271.23	-23001.58	22271.23

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 11-I-2 (SISMAxSLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	23103.29	-22372.44	77959.82	0.00	0.00	--
1	-23066.92	22344.33	-57188.33	-0.00	-0.00	0.000004

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	23103.29	-22372.44	23103.29	-22372.44
1	0.00	0.00	0.00	0.00	-23066.92	22344.33	-23066.92	22344.33

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 11-I-3 (SISMAxSLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	23092.50	-22366.94	78014.43	0.00	0.00	--
1	-23042.32	22377.32	-57206.67	-0.00	-0.00	0.000004

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	23092.50	-22366.94	23092.50	-22366.94
1	0.00	0.00	0.00	0.00	-23042.32	22377.32	-23042.32	22377.32

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 11-I-4 (SISMAxSLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	23113.00	-22377.73	78037.05	0.00	0.00	--
1	-23118.98	22393.10	-57203.45	-0.00	-0.00	0.000004

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	23113.00	-22377.73	23113.00	-22377.73

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Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
1	0.00	0.00	0.00	0.00	-23118.98	22393.10	-23118.98	22393.10

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 12-I-1 (SISMAYSLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	22901.45	-22252.56	77980.84	0.00	0.00	--
1	-23001.58	22271.23	-57182.73	-0.00	-0.00	0.000004

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	22901.45	-22252.56	22901.45	-22252.56
1	0.00	0.00	0.00	0.00	-23001.58	22271.23	-23001.58	22271.23

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 12-I-2 (SISMAYSLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	23103.29	-22372.44	77959.82	0.00	0.00	--
1	-23066.92	22344.33	-57188.33	-0.00	-0.00	0.000004

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	23103.29	-22372.44	23103.29	-22372.44
1	0.00	0.00	0.00	0.00	-23066.92	22344.33	-23066.92	22344.33

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 12-I-3 (SISMAYSLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	23092.50	-22366.94	78014.43	0.00	0.00	--
1	-23042.32	22377.32	-57206.67	-0.00	-0.00	0.000004

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	23092.50	-22366.94	23092.50	-22366.94
1	0.00	0.00	0.00	0.00	-23042.32	22377.32	-23042.32	22377.32

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Combinazione: 12-I-4 (SISMAYSLV)

Piano	Fx daN	Fy daN	Fz daN	dx mm	dy mm	Θ
0	23113.00	-22377.73	78037.05	0.00	0.00	--
1	-23118.98	22393.10	-57203.45	-0.00	-0.00	0.000004

Piano	FxPil/Isol. daN	FyPil/Isol. daN	FxPar daN	FyPar daN	FxShell daN	FyShell daN	FxTot daN	FyTot daN
0	0.00	0.00	0.00	0.00	23113.00	-22377.73	23113.00	-22377.73
1	0.00	0.00	0.00	0.00	-23118.98	22393.10	-23118.98	22393.10

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Nodi - Geometria e vincoli

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
	Coordinate [m]			Vincoli						
1	-16.000	0.000	0.000	1	1	0	0	0	1	0
2	-14.950	0.000	0.000	1	1	0	0	0	1	0
3	-13.950	0.000	0.000	1	1	0	0	0	1	0
4	-12.950	0.000	0.000	1	1	0	0	0	1	0
5	-11.950	0.000	0.000	1	1	0	0	0	1	0
6	-10.950	0.000	0.000	1	1	0	0	0	1	0
7	-9.950	0.000	0.000	1	1	0	0	0	1	0
8	-8.950	0.000	0.000	1	1	0	0	0	1	0
9	-7.950	0.000	0.000	1	1	0	0	0	1	0
10	-6.950	0.000	0.000	1	1	0	0	0	1	0
11	-5.950	0.000	0.000	1	1	0	0	0	1	0
12	-4.950	0.000	0.000	1	1	0	0	0	1	0
13	-3.950	0.000	0.000	1	1	0	0	0	1	0
14	-2.950	0.000	0.000	1	1	0	0	0	1	0
15	-1.950	0.000	0.000	1	1	0	0	0	1	0
16	0.000	0.000	0.000	1	1	0	0	0	1	0
17	-16.000	2.340	0.000	1	1	0	0	0	1	0
18	-14.950	2.340	0.000	1	1	0	0	0	1	0
19	-13.950	2.340	0.000	1	1	0	0	0	1	0
20	-12.950	2.340	0.000	1	1	0	0	0	1	0
21	-11.950	2.340	0.000	1	1	0	0	0	1	0
22	-10.950	2.340	0.000	1	1	0	0	0	1	0
23	-9.950	2.340	0.000	1	1	0	0	0	1	0
24	-8.950	2.340	0.000	1	1	0	0	0	1	0
25	-7.950	2.340	0.000	1	1	0	0	0	1	0
26	-6.950	2.340	0.000	1	1	0	0	0	1	0
27	-5.950	2.340	0.000	1	1	0	0	0	1	0
28	-4.950	2.340	0.000	1	1	0	0	0	1	0
29	-3.950	2.340	0.000	1	1	0	0	0	1	0
30	-2.950	2.340	0.000	1	1	0	0	0	1	0
31	-1.950	2.340	0.000	1	1	0	0	0	1	0
32	0.000	2.340	0.000	1	1	0	0	0	1	0
33	-16.000	3.000	0.000	1	1	0	0	0	1	0
34	-14.950	3.000	0.000	1	1	0	0	0	1	0
35	-13.950	3.000	0.000	1	1	0	0	0	1	0
36	-12.950	3.000	0.000	1	1	0	0	0	1	0

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
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BTK3**

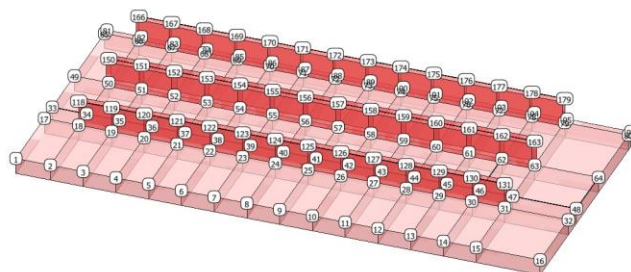
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Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
37	-11.950	3.000	0.000	1	1	0	0	0	1	0
38	-10.950	3.000	0.000	1	1	0	0	0	1	0
39	-9.950	3.000	0.000	1	1	0	0	0	1	0
40	-8.950	3.000	0.000	1	1	0	0	0	1	0
41	-7.950	3.000	0.000	1	1	0	0	0	1	0
42	-6.950	3.000	0.000	1	1	0	0	0	1	0
43	-5.950	3.000	0.000	1	1	0	0	0	1	0
44	-4.950	3.000	0.000	1	1	0	0	0	1	0
45	-3.950	3.000	0.000	1	1	0	0	0	1	0
46	-2.950	3.000	0.000	1	1	0	0	0	1	0
47	-1.950	3.000	0.000	1	1	0	0	0	1	0
48	0.000	3.000	0.000	1	1	0	0	0	1	0
49	-16.000	4.820	0.000	1	1	0	0	0	1	0
50	-14.950	4.820	0.000	1	1	0	0	0	1	0
51	-13.950	4.820	0.000	1	1	0	0	0	1	0
52	-12.950	4.820	0.000	1	1	0	0	0	1	0
53	-11.950	4.820	0.000	1	1	0	0	0	1	0
54	-10.950	4.820	0.000	1	1	0	0	0	1	0
55	-9.950	4.820	0.000	1	1	0	0	0	1	0
56	-8.950	4.820	0.000	1	1	0	0	0	1	0
57	-7.950	4.820	0.000	1	1	0	0	0	1	0
58	-6.950	4.820	0.000	1	1	0	0	0	1	0
59	-5.950	4.820	0.000	1	1	0	0	0	1	0
60	-4.950	4.820	0.000	1	1	0	0	0	1	0
61	-3.950	4.820	0.000	1	1	0	0	0	1	0
62	-2.950	4.820	0.000	1	1	0	0	0	1	0
63	-1.950	4.820	0.000	1	1	0	0	0	1	0
64	0.000	4.820	0.000	1	1	0	0	0	1	0
65	-16.000	7.300	0.000	1	1	0	0	0	1	0
66	-14.950	7.300	0.000	1	1	0	0	0	1	0
67	-13.950	7.300	0.000	1	1	0	0	0	1	0
68	-12.950	7.300	0.000	1	1	0	0	0	1	0
69	-11.950	7.300	0.000	1	1	0	0	0	1	0
70	-10.950	7.300	0.000	1	1	0	0	0	1	0
71	-9.950	7.300	0.000	1	1	0	0	0	1	0
72	-8.950	7.300	0.000	1	1	0	0	0	1	0
73	-7.950	7.300	0.000	1	1	0	0	0	1	0
74	-6.950	7.300	0.000	1	1	0	0	0	1	0
75	-5.950	7.300	0.000	1	1	0	0	0	1	0
76	-4.950	7.300	0.000	1	1	0	0	0	1	0
77	-3.950	7.300	0.000	1	1	0	0	0	1	0
78	-2.950	7.300	0.000	1	1	0	0	0	1	0
79	-1.950	7.300	0.000	1	1	0	0	0	1	0
80	0.000	7.300	0.000	1	1	0	0	0	1	0
81	-16.000	7.500	0.000	1	1	0	0	0	1	0
82	-14.950	7.500	0.000	1	1	0	0	0	1	0
83	-13.950	7.500	0.000	1	1	0	0	0	1	0
84	-12.950	7.500	0.000	1	1	0	0	0	1	0
85	-11.950	7.500	0.000	1	1	0	0	0	1	0
86	-10.950	7.500	0.000	1	1	0	0	0	1	0
87	-9.950	7.500	0.000	1	1	0	0	0	1	0
88	-8.950	7.500	0.000	1	1	0	0	0	1	0
89	-7.950	7.500	0.000	1	1	0	0	0	1	0
90	-6.950	7.500	0.000	1	1	0	0	0	1	0
91	-5.950	7.500	0.000	1	1	0	0	0	1	0
92	-4.950	7.500	0.000	1	1	0	0	0	1	0
93	-3.950	7.500	0.000	1	1	0	0	0	1	0
94	-2.950	7.500	0.000	1	1	0	0	0	1	0
95	-1.950	7.500	0.000	1	1	0	0	0	1	0
96	0.000	7.500	0.000	1	1	0	0	0	1	0
118	-14.950	2.340	0.800	0	0	0	0	0	0	1
119	-13.950	2.340	0.800	0	0	0	0	0	0	1
120	-12.950	2.340	0.800	0	0	0	0	0	0	1
121	-11.950	2.340	0.800	0	0	0	0	0	0	1
122	-10.950	2.340	0.800	0	0	0	0	0	0	1
123	-9.950	2.340	0.800	0	0	0	0	0	0	1
124	-8.950	2.340	0.800	0	0	0	0	0	0	1
125	-7.950	2.340	0.800	0	0	0	0	0	0	1
126	-6.950	2.340	0.800	0	0	0	0	0	0	1
127	-5.950	2.340	0.800	0	0	0	0	0	0	1
128	-4.950	2.340	0.800	0	0	0	0	0	0	1
129	-3.950	2.340	0.800	0	0	0	0	0	0	1
130	-2.950	2.340	0.800	0	0	0	0	0	0	1
131	-1.950	2.340	0.800	0	0	0	0	0	0	1
150	-14.950	4.820	0.800	0	0	0	0	0	0	1

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
151	-13.950	4.820	0.800	0	0	0	0	0	0	1
152	-12.950	4.820	0.800	0	0	0	0	0	0	1
153	-11.950	4.820	0.800	0	0	0	0	0	0	1
154	-10.950	4.820	0.800	0	0	0	0	0	0	1
155	-9.950	4.820	0.800	0	0	0	0	0	0	1
156	-8.950	4.820	0.800	0	0	0	0	0	0	1
157	-7.950	4.820	0.800	0	0	0	0	0	0	1
158	-6.950	4.820	0.800	0	0	0	0	0	0	1
159	-5.950	4.820	0.800	0	0	0	0	0	0	1
160	-4.950	4.820	0.800	0	0	0	0	0	0	1
161	-3.950	4.820	0.800	0	0	0	0	0	0	1
162	-2.950	4.820	0.800	0	0	0	0	0	0	1
163	-1.950	4.820	0.800	0	0	0	0	0	0	1
166	-14.950	7.300	0.800	0	0	0	0	0	0	1
167	-13.950	7.300	0.800	0	0	0	0	0	0	1
168	-12.950	7.300	0.800	0	0	0	0	0	0	1
169	-11.950	7.300	0.800	0	0	0	0	0	0	1
170	-10.950	7.300	0.800	0	0	0	0	0	0	1
171	-9.950	7.300	0.800	0	0	0	0	0	0	1
172	-8.950	7.300	0.800	0	0	0	0	0	0	1
173	-7.950	7.300	0.800	0	0	0	0	0	0	1
174	-6.950	7.300	0.800	0	0	0	0	0	0	1
175	-5.950	7.300	0.800	0	0	0	0	0	0	1
176	-4.950	7.300	0.800	0	0	0	0	0	0	1
177	-3.950	7.300	0.800	0	0	0	0	0	0	1
178	-2.950	7.300	0.800	0	0	0	0	0	0	1
179	-1.950	7.300	0.800	0	0	0	0	0	0	1



**Nodi - Carichi**

N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
		daN			daN*m			cm			°			°C
95	biofiltro	0.00	0.00	550.00	0.00	0.00	0.00							
118	biofiltro	0.00	0.00	550.00	0.00	0.00	0.00							
118	vento y	0.00	-90.00	0.00	150.00	0.00	0.00							
118	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
118	azione sismica SLV y	0.00	215.00	0.00	355.00	0.00	0.00							
118	azione sismica SLV x	220.00	0.00	0.00	0.00	355.00	0.00							
118	azione sismica SLD y	0.00	-85.00	0.00	140.00	0.00	0.00							
118	azione sismica SLD x	85.00	0.00	0.00	0.00	140.00	0.00							

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
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BTK3**

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N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
119	biofiltro	0.00	0.00	1100.0 0	0.00	0.00	0.00							
119	vento y	0.00	- 180.00	0.00	295.00	0.00	0.00							
119	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
119	azione sismica SLV y	0.00	- 430.00	0.00	710.00	0.00	0.00							
119	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
119	azione sismica SLD y	0.00	- 170.00	0.00	280.00	0.00	0.00							
119	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
120	biofiltro	0.00	0.00	1100.0 0	0.00	0.00	0.00							
120	vento y	0.00	- 180.00	0.00	295.00	0.00	0.00							
120	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
120	azione sismica SLV y	0.00	- 430.00	0.00	710.00	0.00	0.00							
120	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
120	azione sismica SLD y	0.00	- 170.00	0.00	280.00	0.00	0.00							
120	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
121	biofiltro	0.00	0.00	1100.0 0	0.00	0.00	0.00							
121	vento y	0.00	- 180.00	0.00	295.00	0.00	0.00							
121	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
121	azione sismica SLV y	0.00	- 430.00	0.00	710.00	0.00	0.00							
121	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
121	azione sismica SLD y	0.00	- 170.00	0.00	280.00	0.00	0.00							
121	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
122	biofiltro	0.00	0.00	1100.0 0	0.00	0.00	0.00							
122	vento y	0.00	- 180.00	0.00	295.00	0.00	0.00							
122	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
122	azione sismica SLV y	0.00	- 430.00	0.00	710.00	0.00	0.00							
122	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
122	azione sismica SLD y	0.00	- 170.00	0.00	280.00	0.00	0.00							
122	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
123	biofiltro	0.00	0.00	1100.0 0	0.00	0.00	0.00							
123	vento y	0.00	- 180.00	0.00	295.00	0.00	0.00							
123	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
123	azione sismica SLV y	0.00	- 430.00	0.00	710.00	0.00	0.00							
123	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
123	azione sismica SLD y	0.00	- 170.00	0.00	280.00	0.00	0.00							
123	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
124	biofiltro	0.00	0.00	1100.0 0	0.00	0.00	0.00							
124	vento y	0.00	- 180.00	0.00	295.00	0.00	0.00							
124	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
124	azione sismica SLV y	0.00	- 430.00	0.00	710.00	0.00	0.00							
124	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
124	azione sismica SLD y	0.00	- 170.00	0.00	280.00	0.00	0.00							

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
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BTK3**

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N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
124	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
125	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
125	vento y	0.00	-180.00	0.00	295.00	0.00	0.00							
125	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
125	azione sismica SLV y	0.00	-430.00	0.00	710.00	0.00	0.00							
125	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
125	azione sismica SLD y	0.00	-170.00	0.00	280.00	0.00	0.00							
125	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
126	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
126	vento y	0.00	-180.00	0.00	295.00	0.00	0.00							
126	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
126	azione sismica SLV y	0.00	-430.00	0.00	710.00	0.00	0.00							
126	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
126	azione sismica SLD y	0.00	-170.00	0.00	280.00	0.00	0.00							
126	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
127	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
127	vento y	0.00	-180.00	0.00	295.00	0.00	0.00							
127	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
127	azione sismica SLV y	0.00	-430.00	0.00	710.00	0.00	0.00							
127	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
127	azione sismica SLD y	0.00	-170.00	0.00	280.00	0.00	0.00							
127	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
128	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
128	vento y	0.00	-180.00	0.00	295.00	0.00	0.00							
128	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
128	azione sismica SLV y	0.00	-430.00	0.00	710.00	0.00	0.00							
128	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
128	azione sismica SLD y	0.00	-170.00	0.00	280.00	0.00	0.00							
128	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
129	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
129	vento y	0.00	-180.00	0.00	295.00	0.00	0.00							
129	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
129	azione sismica SLV y	0.00	-430.00	0.00	710.00	0.00	0.00							
129	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
129	azione sismica SLD y	0.00	-170.00	0.00	280.00	0.00	0.00							
129	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
130	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
130	vento y	0.00	-180.00	0.00	295.00	0.00	0.00							
130	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
130	azione sismica SLV y	0.00	-430.00	0.00	710.00	0.00	0.00							
130	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							



N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
130	azione sismica SLD y	0.00	-	0.00	-	0.00	0.00							
130	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
131	biofiltro	0.00	0.00	550.00	0.00	0.00	0.00							
131	vento y	0.00	-90.00	0.00	150.00	0.00	0.00							
131	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
131	azione sismica SLV y	0.00	-	0.00	-	0.00	0.00							
131	azione sismica SLV x	220.00	0.00	0.00	0.00	355.00	0.00							
131	azione sismica SLD y	0.00	-85.00	0.00	-	0.00	0.00							
131	azione sismica SLD x	85.00	0.00	0.00	0.00	140.00	0.00							
150	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
150	vento y	0.00	-90.00	0.00	150.00	0.00	0.00							
150	vento x	70.00	0.00	0.00	0.00	-	0.00							
150	azione sismica SLV y	0.00	-	0.00	-	0.00	0.00							
150	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
150	azione sismica SLD y	0.00	-	0.00	-	0.00	0.00							
150	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
151	biofiltro	0.00	0.00	2200.00	0.00	0.00	0.00							
151	vento y	0.00	-	0.00	295.00	0.00	0.00							
151	vento x	70.00	0.00	0.00	0.00	-	0.00							
151	azione sismica SLV y	0.00	-	0.00	-	0.00	0.00							
151	azione sismica SLV x	880.00	0.00	0.00	0.00	1420.00	0.00							
151	azione sismica SLD y	0.00	-	0.00	-	0.00	0.00							
151	azione sismica SLD x	340.00	0.00	0.00	0.00	560.00	0.00							
152	biofiltro	0.00	0.00	2200.00	0.00	0.00	0.00							
152	vento y	0.00	-	0.00	295.00	0.00	0.00							
152	vento x	70.00	0.00	0.00	0.00	-	0.00							
152	azione sismica SLV y	0.00	-	0.00	-	0.00	0.00							
152	azione sismica SLV x	880.00	0.00	0.00	0.00	1420.00	0.00							
152	azione sismica SLD y	0.00	-	0.00	-	0.00	0.00							
152	azione sismica SLD x	340.00	0.00	0.00	0.00	560.00	0.00							
153	biofiltro	0.00	0.00	2200.00	0.00	0.00	0.00							
153	vento y	0.00	-	0.00	295.00	0.00	0.00							
153	vento x	70.00	0.00	0.00	0.00	-	0.00							
153	azione sismica SLV y	0.00	-	0.00	-	0.00	0.00							
153	azione sismica SLV x	880.00	0.00	0.00	0.00	1420.00	0.00							
153	azione sismica SLD y	0.00	-	0.00	-	0.00	0.00							
153	azione sismica SLD x	340.00	0.00	0.00	0.00	560.00	0.00							
154	biofiltro	0.00	0.00	2200.00	0.00	0.00	0.00							
154	vento y	0.00	-	0.00	295.00	0.00	0.00							

N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
154	vento x	70.00	0.00	0.00	0.00	110.00	0.00							
154	azione sismica SLV y	0.00	860.00	0.00	1420.00	0.00	0.00							
154	azione sismica SLV x	880.00	0.00	0.00	0.00	1420.00	0.00							
154	azione sismica SLD y	0.00	340.00	0.00	560.00	0.00	0.00							
154	azione sismica SLD x	340.00	0.00	0.00	0.00	560.00	0.00							
155	biofiltro	0.00	0.00	2200.00	0.00	0.00	0.00							
155	vento y	0.00	180.00	0.00	295.00	0.00	0.00							
155	vento x	70.00	0.00	0.00	0.00	110.00	0.00							
155	azione sismica SLV y	0.00	860.00	0.00	1420.00	0.00	0.00							
155	azione sismica SLV x	880.00	0.00	0.00	0.00	1420.00	0.00							
155	azione sismica SLD y	0.00	340.00	0.00	560.00	0.00	0.00							
155	azione sismica SLD x	340.00	0.00	0.00	0.00	560.00	0.00							
156	biofiltro	0.00	0.00	2200.00	0.00	0.00	0.00							
156	vento y	0.00	180.00	0.00	295.00	0.00	0.00							
156	vento x	70.00	0.00	0.00	0.00	110.00	0.00							
156	azione sismica SLV y	0.00	860.00	0.00	1420.00	0.00	0.00							
156	azione sismica SLV x	880.00	0.00	0.00	0.00	1420.00	0.00							
156	azione sismica SLD y	0.00	340.00	0.00	560.00	0.00	0.00							
156	azione sismica SLD x	340.00	0.00	0.00	0.00	560.00	0.00							
157	biofiltro	0.00	0.00	2200.00	0.00	0.00	0.00							
157	vento y	0.00	180.00	0.00	295.00	0.00	0.00							
157	vento x	70.00	0.00	0.00	0.00	110.00	0.00							
157	azione sismica SLV y	0.00	860.00	0.00	1420.00	0.00	0.00							
157	azione sismica SLV x	880.00	0.00	0.00	0.00	1420.00	0.00							
157	azione sismica SLD y	0.00	340.00	0.00	560.00	0.00	0.00							
157	azione sismica SLD x	340.00	0.00	0.00	0.00	560.00	0.00							
158	biofiltro	0.00	0.00	2200.00	0.00	0.00	0.00							
158	vento y	0.00	180.00	0.00	295.00	0.00	0.00							
158	vento x	70.00	0.00	0.00	0.00	110.00	0.00							
158	azione sismica SLV y	0.00	860.00	0.00	1420.00	0.00	0.00							
158	azione sismica SLV x	880.00	0.00	0.00	0.00	1420.00	0.00							
158	azione sismica SLD y	0.00	340.00	0.00	560.00	0.00	0.00							
158	azione sismica SLD x	340.00	0.00	0.00	0.00	560.00	0.00							
159	biofiltro	0.00	0.00	2200.00	0.00	0.00	0.00							
159	vento y	0.00	180.00	0.00	295.00	0.00	0.00							
159	vento x	70.00	0.00	0.00	0.00	110.00	0.00							

N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
159	azione sismica SLV y	0.00	- 860.00	0.00	1420.0 0	0.00	0.00							
159	azione sismica SLV x	880.00	0.00	0.00	0.00	1420.0 0	0.00							
159	azione sismica SLD y	0.00	- 340.00	0.00	560.00	0.00	0.00							
159	azione sismica SLD x	340.00	0.00	0.00	0.00	560.00	0.00							
160	biofiltro	0.00	0.00	2200.0 0	0.00	0.00	0.00							
160	vento y	0.00	- 180.00	0.00	295.00	0.00	0.00							
160	vento x	70.00	0.00	0.00	0.00	110.00	0.00							
160	azione sismica SLV y	0.00	- 860.00	0.00	1420.0 0	0.00	0.00							
160	azione sismica SLV x	880.00	0.00	0.00	0.00	1420.0 0	0.00							
160	azione sismica SLD y	0.00	- 340.00	0.00	560.00	0.00	0.00							
160	azione sismica SLD x	340.00	0.00	0.00	0.00	560.00	0.00							
161	biofiltro	0.00	0.00	2200.0 0	0.00	0.00	0.00							
161	vento y	0.00	- 180.00	0.00	295.00	0.00	0.00							
161	vento x	70.00	0.00	0.00	0.00	110.00	0.00							
161	azione sismica SLV y	0.00	- 860.00	0.00	1420.0 0	0.00	0.00							
161	azione sismica SLV x	880.00	0.00	0.00	0.00	1420.0 0	0.00							
161	azione sismica SLD y	0.00	- 340.00	0.00	560.00	0.00	0.00							
161	azione sismica SLD x	340.00	0.00	0.00	0.00	560.00	0.00							
162	biofiltro	0.00	0.00	2200.0 0	0.00	0.00	0.00							
162	vento y	0.00	- 180.00	0.00	295.00	0.00	0.00							
162	vento x	70.00	0.00	0.00	0.00	110.00	0.00							
162	azione sismica SLV y	0.00	- 860.00	0.00	1420.0 0	0.00	0.00							
162	azione sismica SLV x	880.00	0.00	0.00	0.00	1420.0 0	0.00							
162	azione sismica SLD y	0.00	- 340.00	0.00	560.00	0.00	0.00							
162	azione sismica SLD x	340.00	0.00	0.00	0.00	560.00	0.00							
163	biofiltro	0.00	0.00	1100.0 0	0.00	0.00	0.00							
163	vento y	0.00	-90.00	0.00	150.00	0.00	0.00							
163	vento x	70.00	0.00	0.00	0.00	110.00	0.00							
163	azione sismica SLV y	0.00	- 430.00	0.00	710.00	0.00	0.00							
163	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
163	azione sismica SLD y	0.00	- 170.00	0.00	280.00	0.00	0.00							
163	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
166	biofiltro	0.00	0.00	550.00	0.00	0.00	0.00							
166	vento y	0.00	-90.00	0.00	150.00	0.00	0.00							
166	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
166	azione sismica SLV y	0.00	- 215.00	0.00	355.00	0.00	0.00							
166	azione sismica SLV x	220.00	0.00	0.00	0.00	355.00	0.00							
166	azione sismica SLD y	0.00	-85.00	0.00	140.00	0.00	0.00							

N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
166	azione sismica SLD x	85.00	0.00	0.00	0.00	140.00	0.00							
167	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
167	vento y	0.00	180.00	0.00	295.00	0.00	0.00							
167	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
167	azione sismica SLV y	0.00	430.00	0.00	710.00	0.00	0.00							
167	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
167	azione sismica SLD y	0.00	170.00	0.00	280.00	0.00	0.00							
167	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
168	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
168	vento y	0.00	180.00	0.00	295.00	0.00	0.00							
168	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
168	azione sismica SLV y	0.00	430.00	0.00	710.00	0.00	0.00							
168	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
168	azione sismica SLD y	0.00	170.00	0.00	280.00	0.00	0.00							
168	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
169	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
169	vento y	0.00	180.00	0.00	295.00	0.00	0.00							
169	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
169	azione sismica SLV y	0.00	430.00	0.00	710.00	0.00	0.00							
169	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
169	azione sismica SLD y	0.00	170.00	0.00	280.00	0.00	0.00							
169	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
170	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
170	vento y	0.00	180.00	0.00	295.00	0.00	0.00							
170	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
170	azione sismica SLV y	0.00	430.00	0.00	710.00	0.00	0.00							
170	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
170	azione sismica SLD y	0.00	170.00	0.00	280.00	0.00	0.00							
170	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
171	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
171	vento y	0.00	180.00	0.00	295.00	0.00	0.00							
171	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
171	azione sismica SLV y	0.00	430.00	0.00	710.00	0.00	0.00							
171	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
171	azione sismica SLD y	0.00	170.00	0.00	280.00	0.00	0.00							
171	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
172	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
172	vento y	0.00	180.00	0.00	295.00	0.00	0.00							
172	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
172	azione sismica SLV y	0.00	430.00	0.00	710.00	0.00	0.00							
172	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							

N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
172	azione sismica SLD y	0.00	-	0.00	-	0.00	0.00							
172	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
173	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
173	vento y	0.00	-	0.00	-	0.00	0.00							
173	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
173	azione sismica SLV y	0.00	-	0.00	-	0.00	0.00							
173	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
173	azione sismica SLD y	0.00	-	0.00	-	0.00	0.00							
173	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
174	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
174	vento y	0.00	-	0.00	-	0.00	0.00							
174	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
174	azione sismica SLV y	0.00	-	0.00	-	0.00	0.00							
174	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
174	azione sismica SLD y	0.00	-	0.00	-	0.00	0.00							
174	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
175	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
175	vento y	0.00	-	0.00	-	0.00	0.00							
175	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
175	azione sismica SLV y	0.00	-	0.00	-	0.00	0.00							
175	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
175	azione sismica SLD y	0.00	-	0.00	-	0.00	0.00							
175	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
176	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
176	vento y	0.00	-	0.00	-	0.00	0.00							
176	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
176	azione sismica SLV y	0.00	-	0.00	-	0.00	0.00							
176	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
176	azione sismica SLD y	0.00	-	0.00	-	0.00	0.00							
176	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
177	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
177	vento y	0.00	-	0.00	-	0.00	0.00							
177	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
177	azione sismica SLV y	0.00	-	0.00	-	0.00	0.00							
177	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
177	azione sismica SLD y	0.00	-	0.00	-	0.00	0.00							
177	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
178	biofiltro	0.00	0.00	1100.00	0.00	0.00	0.00							
178	vento y	0.00	-	0.00	-	0.00	0.00							
178	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
178	azione sismica SLV y	0.00	-	0.00	-	0.00	0.00							

N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
178	azione sismica SLV x	440.00	0.00	0.00	0.00	710.00	0.00							
178	azione sismica SLD y	0.00	170.00	0.00	280.00	0.00	0.00							
178	azione sismica SLD x	170.00	0.00	0.00	0.00	280.00	0.00							
179	biofiltro	0.00	0.00	550.00	0.00	0.00	0.00							
179	vento y	0.00	-90.00	0.00	150.00	0.00	0.00							
179	vento x	35.00	0.00	0.00	0.00	-55.00	0.00							
179	azione sismica SLV y	0.00	215.00	0.00	355.00	0.00	0.00							
179	azione sismica SLV x	220.00	0.00	0.00	0.00	355.00	0.00							
179	azione sismica SLD y	0.00	-85.00	0.00	140.00	0.00	0.00							
179	azione sismica SLD x	85.00	0.00	0.00	0.00	140.00	0.00							

#### Aste - Carichi

Descrizione carichi aste

UnifG	Uniforme globale
UnifL	Uniforme locale
VarG	Variabile lineare globale
VarL	Variabile lineare locale
PolG	Poligonale globale
Termico	Distorsione termica
Torcente	Carico torcente
Precomp.	Carico da precompressione
PolL	Poligonale locale

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					m	car. dist. daN/m coppie torc. daN*m/m			m	car. dist. daN/m coppie torc. daN*m/m		
<b>Trave 0</b>												
Sezione Nulla	130	131	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	130	129	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	130	129	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	161	162	vento x	UnifG	0.00	170.0 0	0.00	0.00	1.00	170.0 0	0.00	0.00
Sezione Nulla	161	162	serbatoio	UnifG	0.00	180.0 0	0.00	0.00	1.00	180.0 0	0.00	0.00
Sezione Nulla	162	163	vento x	UnifG	0.00	170.0 0	0.00	0.00	1.00	170.0 0	0.00	0.00
Sezione Nulla	178	177	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	178	179	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	178	177	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
<b>Trave 10</b>												
Sezione Nulla	127	126	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	127	126	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	129	128	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	129	128	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	158	159	vento x	UnifG	0.00	170.0 0	0.00	0.00	1.00	170.0 0	0.00	0.00
Sezione Nulla	158	159	serbatoio	UnifG	0.00	180.0 0	0.00	0.00	1.00	180.0 0	0.00	0.00
Sezione Nulla	160	161	vento x	UnifG	0.00	170.0 0	0.00	0.00	1.00	170.0 0	0.00	0.00
Sezione Nulla	160	161	serbatoio	UnifG	0.00	180.0 0	0.00	0.00	1.00	180.0 0	0.00	0.00
Sezione Nulla	175	174	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	175	174	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	177	176	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00

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Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
Sezione Nulla	177	176	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
<b>Trave 20</b>												
Sezione Nulla	124	123	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	124	123	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	126	125	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	126	125	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	128	127	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	128	127	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	155	156	vento x	UnifG	0.00	170.00	0.00	0.00	1.00	170.00	0.00	0.00
Sezione Nulla	155	156	serbatoio	UnifG	0.00	180.00	0.00	0.00	1.00	180.00	0.00	0.00
Sezione Nulla	157	158	vento x	UnifG	0.00	170.00	0.00	0.00	1.00	170.00	0.00	0.00
Sezione Nulla	157	158	serbatoio	UnifG	0.00	180.00	0.00	0.00	1.00	180.00	0.00	0.00
Sezione Nulla	159	160	vento x	UnifG	0.00	170.00	0.00	0.00	1.00	170.00	0.00	0.00
Sezione Nulla	159	160	serbatoio	UnifG	0.00	180.00	0.00	0.00	1.00	180.00	0.00	0.00
Sezione Nulla	172	171	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	172	171	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	174	173	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	174	173	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	176	175	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	176	175	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
<b>Trave 30</b>												
Sezione Nulla	121	120	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	121	120	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	123	122	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	123	122	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	125	124	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	125	124	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	152	153	vento x	UnifG	0.00	170.00	0.00	0.00	1.00	170.00	0.00	0.00
Sezione Nulla	152	153	serbatoio	UnifG	0.00	180.00	0.00	0.00	1.00	180.00	0.00	0.00
Sezione Nulla	154	155	vento x	UnifG	0.00	170.00	0.00	0.00	1.00	170.00	0.00	0.00
Sezione Nulla	154	155	serbatoio	UnifG	0.00	180.00	0.00	0.00	1.00	180.00	0.00	0.00
Sezione Nulla	156	157	vento x	UnifG	0.00	170.00	0.00	0.00	1.00	170.00	0.00	0.00
Sezione Nulla	156	157	serbatoio	UnifG	0.00	180.00	0.00	0.00	1.00	180.00	0.00	0.00
Sezione Nulla	169	168	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	169	168	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	171	170	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	171	170	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	173	172	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	173	172	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
<b>Trave 40</b>												

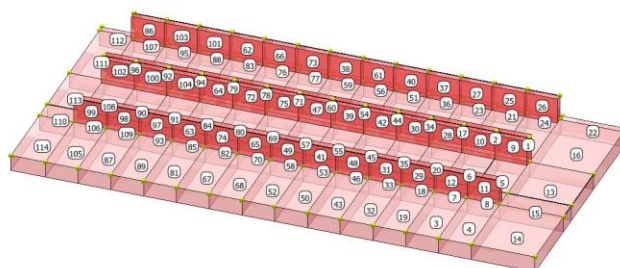
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Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
Sezione Nulla	120	119	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	120	119	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	122	121	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	122	121	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	151	152	vento x	UnifG	0.00	170.00	0.00	0.00	1.00	170.00	0.00	0.00
Sezione Nulla	151	152	serbatoio	UnifG	0.00	180.00	0.00	0.00	1.00	180.00	0.00	0.00
Sezione Nulla	153	154	vento x	UnifG	0.00	170.00	0.00	0.00	1.00	170.00	0.00	0.00
Sezione Nulla	153	154	serbatoio	UnifG	0.00	180.00	0.00	0.00	1.00	180.00	0.00	0.00
Sezione Nulla	168	167	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	168	167	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	170	169	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	170	169	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
<b>Trave 50</b>												
Sezione Nulla	119	118	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	119	118	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00
Sezione Nulla	150	151	vento x	UnifG	0.00	170.00	0.00	0.00	1.00	170.00	0.00	0.00
Sezione Nulla	150	151	serbatoio	UnifG	0.00	180.00	0.00	0.00	1.00	180.00	0.00	0.00
Sezione Nulla	167	166	vento x	UnifG	0.00	85.00	0.00	0.00	1.00	85.00	0.00	0.00
Sezione Nulla	167	166	serbatoio	UnifG	0.00	90.00	0.00	0.00	1.00	90.00	0.00	0.00



**Pareti - geometria e vincoli**

Parete	Nodi	Tipo	Materiale	Criterio	N.P.	N.P.X	N.P.Y	Spess.
								m
1	79-78-62-63	Platea	C35/45	CLS Platee ND	16			0.50
2	78-77-61-62	Platea	C35/45	CLS Platee ND	16			0.50
3	30-29-13-14	Platea	C35/45	CLS Platee ND	16			0.50



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Parete	Nodi	Tipo	Materiale	Criterio	N.P.	N.P.X	N.P.Y	Spess.
4	31-30-14-15	Platea	C35/45	CLS Platee ND	16			0.50
5	63-62-46-47	Platea	C35/45	CLS Platee ND	16			0.50
6	62-61-45-46	Platea	C35/45	CLS Platee ND	16			0.50
7	46-45-29-30	Platea	C35/45	CLS Platee ND	8			0.50
8	47-46-30-31	Platea	C35/45	CLS Platee ND	8			0.50
9	63-62-162-163	Discreto	C35/45	CLS Muri ND	16	4	4	0.40
10	62-61-161-162	Discreto	C35/45	CLS Muri ND	16	4	4	0.40
11	31-131-130-30	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
12	30-130-129-29	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
13	64-63-47-48	Platea	C35/45	CLS Platee ND	16			0.50
14	32-31-15-16	Platea	C35/45	CLS Platee ND	16			0.50
15	48-47-31-32	Platea	C35/45	CLS Platee ND	8			0.50
16	80-79-63-64	Platea	C35/45	CLS Platee ND	16			0.50
17	77-76-60-61	Platea	C35/45	CLS Platee ND	16			0.50
18	45-44-28-29	Platea	C35/45	CLS Platee ND	8			0.50
19	29-28-12-13	Platea	C35/45	CLS Platee ND	16			0.50
20	61-60-44-45	Platea	C35/45	CLS Platee ND	16			0.50
21	94-93-77-78	Platea	C35/45	CLS Platee ND	8			0.50
22	96-95-79-80	Platea	C35/45	CLS Platee ND	8			0.50
23	93-92-76-77	Platea	C35/45	CLS Platee ND	8			0.50
24	95-94-78-79	Platea	C35/45	CLS Platee ND	8			0.50
25	78-77-177-178	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
26	79-78-178-179	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
27	77-76-176-177	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
28	61-60-160-161	Discreto	C35/45	CLS Muri ND	16	4	4	0.40
29	29-129-128-28	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
30	60-59-159-160	Discreto	C35/45	CLS Muri ND	16	4	4	0.40
31	28-128-127-27	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
32	28-27-11-12	Platea	C35/45	CLS Platee ND	16			0.50
33	44-43-27-28	Platea	C35/45	CLS Platee ND	8			0.50
34	76-75-59-60	Platea	C35/45	CLS Platee ND	16			0.50
35	60-59-43-44	Platea	C35/45	CLS Platee ND	16			0.50
36	92-91-75-76	Platea	C35/45	CLS Platee ND	8			0.50
37	76-75-175-176	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
38	73-72-172-173	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
39	58-57-157-158	Discreto	C35/45	CLS Muri ND	16	4	4	0.40
40	75-74-174-175	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
41	26-126-125-25	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
42	59-58-158-159	Discreto	C35/45	CLS Muri ND	16	4	4	0.40
43	27-26-10-11	Platea	C35/45	CLS Platee ND	16			0.50
44	75-74-58-59	Platea	C35/45	CLS Platee ND	16			0.50
45	59-58-42-43	Platea	C35/45	CLS Platee ND	16			0.50
46	43-42-26-27	Platea	C35/45	CLS Platee ND	8			0.50
47	57-56-156-157	Discreto	C35/45	CLS Muri ND	16	4	4	0.40
48	27-127-126-26	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
49	25-125-124-24	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
50	26-25-9-10	Platea	C35/45	CLS Platee ND	16			0.50
51	91-90-74-75	Platea	C35/45	CLS Platee ND	8			0.50
52	25-24-8-9	Platea	C35/45	CLS Platee ND	16			0.50
53	42-41-25-26	Platea	C35/45	CLS Platee ND	8			0.50
54	74-73-57-58	Platea	C35/45	CLS Platee ND	16			0.50
55	58-57-41-42	Platea	C35/45	CLS Platee ND	16			0.50
56	90-89-73-74	Platea	C35/45	CLS Platee ND	8			0.50
57	57-56-40-41	Platea	C35/45	CLS Platee ND	16			0.50
58	41-40-24-25	Platea	C35/45	CLS Platee ND	8			0.50
59	89-88-72-73	Platea	C35/45	CLS Platee ND	8			0.50
60	73-72-56-57	Platea	C35/45	CLS Platee ND	16			0.50
61	74-73-173-174	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
62	70-69-169-170	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
63	22-122-121-21	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
64	54-53-153-154	Discreto	C35/45	CLS Muri ND	16	4	4	0.40
65	24-124-123-23	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
66	71-70-170-171	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
67	23-22-6-7	Platea	C35/45	CLS Platee ND	16			0.50
68	24-23-7-8	Platea	C35/45	CLS Platee ND	16			0.50
69	56-55-39-40	Platea	C35/45	CLS Platee ND	16			0.50
70	40-39-23-24	Platea	C35/45	CLS Platee ND	8			0.50
71	72-71-55-56	Platea	C35/45	CLS Platee ND	16			0.50
72	55-54-154-155	Discreto	C35/45	CLS Muri ND	16	4	4	0.40
73	72-71-171-172	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
74	23-123-122-22	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
75	56-55-155-156	Discreto	C35/45	CLS Muri ND	16	4	4	0.40
76	87-86-70-71	Platea	C35/45	CLS Platee ND	8			0.50
77	88-87-71-72	Platea	C35/45	CLS Platee ND	8			0.50
78	71-70-54-55	Platea	C35/45	CLS Platee ND	16			0.50

Parete	Nodi	Tipo	Materiale	Criterio	N.P.	N.P.X	N.P.Y	Spess.
79	70-69-53-54	Platea	C35/45	CLS Platee ND	16			0.50
80	55-54-38-39	Platea	C35/45	CLS Platee ND	16			0.50
81	22-21-5-6	Platea	C35/45	CLS Platee ND	16			0.50
82	39-38-22-23	Platea	C35/45	CLS Platee ND	8			0.50
83	86-85-69-70	Platea	C35/45	CLS Platee ND	8			0.50
84	54-53-37-38	Platea	C35/45	CLS Platee ND	16			0.50
85	38-37-21-22	Platea	C35/45	CLS Platee ND	8			0.50
86	67-66-166-167	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
87	20-19-3-4	Platea	C35/45	CLS Platee ND	16			0.50
88	85-84-68-69	Platea	C35/45	CLS Platee ND	8			0.50
89	21-20-4-5	Platea	C35/45	CLS Platee ND	16			0.50
90	52-51-35-36	Platea	C35/45	CLS Platee ND	16			0.50
91	53-52-36-37	Platea	C35/45	CLS Platee ND	16			0.50
92	68-67-51-52	Platea	C35/45	CLS Platee ND	16			0.50
93	37-36-20-21	Platea	C35/45	CLS Platee ND	8			0.50
94	69-68-52-53	Platea	C35/45	CLS Platee ND	16			0.50
95	84-83-67-68	Platea	C35/45	CLS Platee ND	8			0.50
96	67-66-50-51	Platea	C35/45	CLS Platee ND	16			0.50
97	21-121-120-20	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
98	20-120-119-19	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
99	19-119-118-18	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
100	52-51-151-152	Discreto	C35/45	CLS Muri ND	16	4	4	0.40
101	69-68-168-169	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
102	51-50-150-151	Discreto	C35/45	CLS Muri ND	16	4	4	0.40
103	68-67-167-168	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
104	53-52-152-153	Discreto	C35/45	CLS Muri ND	16	4	4	0.40
105	19-18-2-3	Platea	C35/45	CLS Platee ND	16			0.50
106	35-34-18-19	Platea	C35/45	CLS Platee ND	8			0.50
107	83-82-66-67	Platea	C35/45	CLS Platee ND	8			0.50
108	51-50-34-35	Platea	C35/45	CLS Platee ND	16			0.50
109	36-35-19-20	Platea	C35/45	CLS Platee ND	8			0.50
110	34-33-17-18	Platea	C35/45	CLS Platee ND	4			0.50
111	66-65-49-50	Platea	C35/45	CLS Platee ND	8			0.50
112	82-81-65-66	Platea	C35/45	CLS Platee ND	4			0.50
113	50-49-33-34	Platea	C35/45	CLS Platee ND	8			0.50
114	18-17-1-2	Platea	C35/45	CLS Platee ND	8			0.50

#### Muri - Carichi

Shell Indice dello shell  
Cond. Condizione di carico  
Tipo Tipologia di spinta  
 $\gamma$  Peso specifico: terreno o acqua  
Q Valore del carico uniforme  
Vert.1 Valore del carico nel primo vertice<sup>(1)</sup>  
Vert.2 Valore del carico nel secondo vertice<sup>(1)</sup>  
Vert.3 Valore del carico nel terzo vertice<sup>(1)</sup>  
Vert.4 Valore del carico nel quarto vertice<sup>(1)</sup>  
Hw Altezza del pelo libero dell'acqua

<sup>(1)</sup>: Per shell con numero di vertici maggiori 4, per carichi trapezoidali, il valore del carico nei vertici e' stampato a gruppi di 4 secondo l'ordine con cui i vertici sono stati definiti

Shell	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	$\gamma$
			daN/m <sup>2</sup>	daN/m <sup>2</sup>	daN/m <sup>2</sup>	daN/m <sup>2</sup>	daN/m <sup>2</sup>	m	daN/m <sup>3</sup>
1	Peso Proprio	Peso Proprio daN	3100.00						
1	NEVE	Uniforme GLOBZ	60.00						
1	4100	Uniforme_GLOBZ	4100.00						
2	Peso Proprio	Peso Proprio daN	3100.00						
2	NEVE	Uniforme GLOBZ	60.00						
2	4100	Uniforme_GLOBZ	4100.00						
3	Peso Proprio	Peso Proprio daN	2925.00						
3	NEVE	Uniforme GLOBZ	60.00						
3	accidentali	Uniforme GLOBZ	600.00						
3	ventilatore	Uniforme_GLOBZ	1000.00						
3	4100	Uniforme_GLOBZ	4100.00						

She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
4	Peso Proprio	Peso Proprio daN	2925.0 0						
4	NEVE	Uniforme GLOBZ	60.00						
4	accidentali	Uniforme GLOBZ	600.00						
4	4100	Uniforme GLOBZ	4100.0 0						
5	Peso Proprio	Peso Proprio daN	2275.0 0						
5	NEVE	Uniforme GLOBZ	60.00						
5	4100	Uniforme GLOBZ	4100.0 0						
6	Peso Proprio	Peso Proprio daN	2275.0 0						
6	NEVE	Uniforme GLOBZ	60.00						
6	4100	Uniforme GLOBZ	4100.0 0						
7	Peso Proprio	Peso Proprio daN	825.00						
7	NEVE	Uniforme GLOBZ	60.00						
7	4100	Uniforme GLOBZ	4100.0 0						
8	Peso Proprio	Peso Proprio daN	825.00						
8	NEVE	Uniforme GLOBZ	60.00						
8	4100	Uniforme GLOBZ	4100.0 0						
9	Peso Proprio	Peso Proprio daN	800.00						
10	Peso Proprio	Peso Proprio daN	800.00						
11	Peso Proprio	Peso Proprio daN	400.00						
11	vento y	Uniforme GLOBY	- 100.00						
12	Peso Proprio	Peso Proprio daN	400.00						
12	vento y	Uniforme GLOBY	- 100.00						
13	Peso Proprio	Peso Proprio daN	4436.2 5						
13	NEVE	Uniforme GLOBZ	60.00						
13	accidentali	Uniforme GLOBZ	600.00						
13	4100	Uniforme GLOBZ	4100.0 0						
14	Peso Proprio	Peso Proprio daN	5703.7 5						
14	NEVE	Uniforme GLOBZ	60.00						
14	accidentali	Uniforme GLOBZ	600.00						
14	4100	Uniforme GLOBZ	4100.0 0						
15	Peso Proprio	Peso Proprio daN	1608.7 5						
15	NEVE	Uniforme GLOBZ	60.00						
15	accidentali	Uniforme GLOBZ	600.00						
15	4100	Uniforme GLOBZ	4100.0 0						
16	Peso Proprio	Peso Proprio daN	6045.0 0						
16	NEVE	Uniforme GLOBZ	60.00						
16	accidentali	Uniforme GLOBZ	600.00						
16	4100	Uniforme GLOBZ	4100.0 0						
17	Peso Proprio	Peso Proprio daN	3100.0 0						
17	NEVE	Uniforme GLOBZ	60.00						
17	4100	Uniforme GLOBZ	4100.0 0						
18	Peso Proprio	Peso Proprio daN	825.00						
18	NEVE	Uniforme GLOBZ	60.00						
18	4100	Uniforme GLOBZ	4100.0 0						
19	Peso Proprio	Peso Proprio daN	2925.0 0						
19	NEVE	Uniforme GLOBZ	60.00						
19	accidentali	Uniforme GLOBZ	600.00						
19	4100	Uniforme GLOBZ	4100.0 0						
20	Peso Proprio	Peso Proprio daN	2275.0 0						
20	NEVE	Uniforme GLOBZ	60.00						

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
20	4100	Uniforme_GLOBZ	4100.0 0						
21	Peso Proprio	Peso Proprio daN	250.00						
21	NEVE	Uniforme_GLOBZ	60.00						
21	accidentali	Uniforme_GLOBZ	600.00						
21	4100	Uniforme_GLOBZ	4100.0 0						
22	Peso Proprio	Peso Proprio daN	487.50						
22	NEVE	Uniforme_GLOBZ	60.00						
22	accidentali	Uniforme_GLOBZ	600.00						
22	4100	Uniforme_GLOBZ	4100.0 0						
23	Peso Proprio	Peso Proprio daN	250.00						
23	NEVE	Uniforme_GLOBZ	60.00						
23	accidentali	Uniforme_GLOBZ	600.00						
23	4100	Uniforme_GLOBZ	4100.0 0						
24	Peso Proprio	Peso Proprio daN	250.00						
24	NEVE	Uniforme_GLOBZ	60.00						
24	accidentali	Uniforme_GLOBZ	600.00						
24	4100	Uniforme_GLOBZ	4100.0 0						
25	Peso Proprio	Peso Proprio daN	400.00						
26	Peso Proprio	Peso Proprio daN	400.00						
27	Peso Proprio	Peso Proprio daN	400.00						
28	Peso Proprio	Peso Proprio daN	800.00						
29	Peso Proprio	Peso Proprio daN	400.00						
29	vento y	Uniforme_GLOBY	- 100.00						
30	Peso Proprio	Peso Proprio daN	800.00						
31	Peso Proprio	Peso Proprio daN	400.00						
31	vento y	Uniforme_GLOBY	- 100.00						
32	Peso Proprio	Peso Proprio daN	2925.0 0						
32	NEVE	Uniforme_GLOBZ	60.00						
32	accidentali	Uniforme_GLOBZ	600.00						
32	4100	Uniforme_GLOBZ	4100.0 0						
33	Peso Proprio	Peso Proprio daN	825.00						
33	NEVE	Uniforme_GLOBZ	60.00						
33	4100	Uniforme_GLOBZ	4100.0 0						
34	Peso Proprio	Peso Proprio daN	3100.0 0						
34	NEVE	Uniforme_GLOBZ	60.00						
34	4100	Uniforme_GLOBZ	4100.0 0						
35	Peso Proprio	Peso Proprio daN	2275.0 0						
35	NEVE	Uniforme_GLOBZ	60.00						
35	4100	Uniforme_GLOBZ	4100.0 0						
36	Peso Proprio	Peso Proprio daN	250.00						
36	NEVE	Uniforme_GLOBZ	60.00						
36	accidentali	Uniforme_GLOBZ	600.00						
36	4100	Uniforme_GLOBZ	4100.0 0						
37	Peso Proprio	Peso Proprio daN	400.00						
38	Peso Proprio	Peso Proprio daN	400.00						
39	Peso Proprio	Peso Proprio daN	800.00						
40	Peso Proprio	Peso Proprio daN	400.00						
41	Peso Proprio	Peso Proprio daN	400.00						
41	vento y	Uniforme_GLOBY	- 100.00						
42	Peso Proprio	Peso Proprio daN	800.00						
43	Peso Proprio	Peso Proprio daN	2925.0 0						
43	NEVE	Uniforme_GLOBZ	60.00						
43	accidentali	Uniforme_GLOBZ	600.00						
43	4100	Uniforme_GLOBZ	4100.0 0						
44	Peso Proprio	Peso Proprio daN	3100.0 0						
44	NEVE	Uniforme_GLOBZ	60.00						

She ll	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
44	4100	Uniforme_GLOBZ	4100.0 0						
45	Peso Proprio	Peso Proprio daN	2275.0 0						
45	NEVE	Uniforme_GLOBZ	60.00						
45	4100	Uniforme_GLOBZ	4100.0 0						
46	Peso Proprio	Peso Proprio daN	825.00						
46	NEVE	Uniforme_GLOBZ	60.00						
46	4100	Uniforme_GLOBZ	4100.0 0						
47	Peso Proprio	Peso Proprio daN	800.00						
48	Peso Proprio	Peso Proprio daN	400.00						
48	vento y	Uniforme_GLOBY	- 100.00						
49	Peso Proprio	Peso Proprio daN	400.00						
49	vento y	Uniforme_GLOBY	- 100.00						
50	Peso Proprio	Peso Proprio daN	2925.0 0						
50	NEVE	Uniforme_GLOBZ	60.00						
50	accidentali	Uniforme_GLOBZ	600.00						
50	4100	Uniforme_GLOBZ	4100.0 0						
51	Peso Proprio	Peso Proprio daN	250.00						
51	NEVE	Uniforme_GLOBZ	60.00						
51	accidentali	Uniforme_GLOBZ	600.00						
51	4100	Uniforme_GLOBZ	4100.0 0						
52	Peso Proprio	Peso Proprio daN	2925.0 0						
52	NEVE	Uniforme_GLOBZ	60.00						
52	accidentali	Uniforme_GLOBZ	600.00						
52	4100	Uniforme_GLOBZ	4100.0 0						
53	Peso Proprio	Peso Proprio daN	825.00						
53	NEVE	Uniforme_GLOBZ	60.00						
53	4100	Uniforme_GLOBZ	4100.0 0						
54	Peso Proprio	Peso Proprio daN	3100.0 0						
54	NEVE	Uniforme_GLOBZ	60.00						
54	4100	Uniforme_GLOBZ	4100.0 0						
55	Peso Proprio	Peso Proprio daN	2275.0 0						
55	NEVE	Uniforme_GLOBZ	60.00						
55	4100	Uniforme_GLOBZ	4100.0 0						
56	Peso Proprio	Peso Proprio daN	250.00						
56	NEVE	Uniforme_GLOBZ	60.00						
56	accidentali	Uniforme_GLOBZ	600.00						
56	4100	Uniforme_GLOBZ	4100.0 0						
57	Peso Proprio	Peso Proprio daN	2275.0 0						
57	NEVE	Uniforme_GLOBZ	60.00						
57	4100	Uniforme_GLOBZ	4100.0 0						
58	Peso Proprio	Peso Proprio daN	825.00						
58	NEVE	Uniforme_GLOBZ	60.00						
58	4100	Uniforme_GLOBZ	4100.0 0						
59	Peso Proprio	Peso Proprio daN	250.00						
59	NEVE	Uniforme_GLOBZ	60.00						
59	accidentali	Uniforme_GLOBZ	600.00						
59	4100	Uniforme_GLOBZ	4100.0 0						
60	Peso Proprio	Peso Proprio daN	3100.0 0						
60	NEVE	Uniforme_GLOBZ	60.00						
60	4100	Uniforme_GLOBZ	4100.0 0						
61	Peso Proprio	Peso Proprio daN	400.00						
62	Peso Proprio	Peso Proprio daN	400.00						

She ll	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
63	Peso Proprio	Peso Proprio daN	400.00						
63	vento y	Uniforme_GLOBY	100.00						
64	Peso Proprio	Peso Proprio daN	800.00						
65	Peso Proprio	Peso Proprio daN	400.00						
65	vento y	Uniforme_GLOBY	100.00						
66	Peso Proprio	Peso Proprio daN	400.00						
67	Peso Proprio	Peso Proprio daN	2925.00						
67	NEVE	Uniforme_GLOBZ	60.00						
67	accidentali	Uniforme_GLOBZ	600.00						
67	4100	Uniforme_GLOBZ	4100.00						
68	Peso Proprio	Peso Proprio daN	2925.00						
68	NEVE	Uniforme_GLOBZ	60.00						
68	accidentali	Uniforme_GLOBZ	600.00						
68	4100	Uniforme_GLOBZ	4100.00						
69	Peso Proprio	Peso Proprio daN	2275.00						
69	NEVE	Uniforme_GLOBZ	60.00						
69	4100	Uniforme_GLOBZ	4100.00						
70	Peso Proprio	Peso Proprio daN	825.00						
70	NEVE	Uniforme_GLOBZ	60.00						
70	4100	Uniforme_GLOBZ	4100.00						
71	Peso Proprio	Peso Proprio daN	3100.00						
71	NEVE	Uniforme_GLOBZ	60.00						
71	4100	Uniforme_GLOBZ	4100.00						
72	Peso Proprio	Peso Proprio daN	800.00						
73	Peso Proprio	Peso Proprio daN	400.00						
74	Peso Proprio	Peso Proprio daN	400.00						
74	vento y	Uniforme_GLOBY	100.00						
75	Peso Proprio	Peso Proprio daN	800.00						
76	Peso Proprio	Peso Proprio daN	250.00						
76	NEVE	Uniforme_GLOBZ	60.00						
76	accidentali	Uniforme_GLOBZ	600.00						
76	4100	Uniforme_GLOBZ	4100.00						
77	Peso Proprio	Peso Proprio daN	250.00						
77	NEVE	Uniforme_GLOBZ	60.00						
77	accidentali	Uniforme_GLOBZ	600.00						
77	4100	Uniforme_GLOBZ	4100.00						
78	Peso Proprio	Peso Proprio daN	3100.00						
78	NEVE	Uniforme_GLOBZ	60.00						
78	4100	Uniforme_GLOBZ	4100.00						
79	Peso Proprio	Peso Proprio daN	3100.00						
79	NEVE	Uniforme_GLOBZ	60.00						
79	4100	Uniforme_GLOBZ	4100.00						
80	Peso Proprio	Peso Proprio daN	2275.00						
80	NEVE	Uniforme_GLOBZ	60.00						
80	4100	Uniforme_GLOBZ	4100.00						
81	Peso Proprio	Peso Proprio daN	2925.00						
81	NEVE	Uniforme_GLOBZ	60.00						
81	accidentali	Uniforme_GLOBZ	600.00						
81	4100	Uniforme_GLOBZ	4100.00						
82	Peso Proprio	Peso Proprio daN	825.00						
82	NEVE	Uniforme_GLOBZ	60.00						
82	4100	Uniforme_GLOBZ	4100.00						

She ll	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
83	Peso Proprio	Peso Proprio daN	250.00						
83	NEVE	Uniforme GLOBZ	60.00						
83	accidentali	Uniforme GLOBZ	600.00						
83	4100	Uniforme GLOBZ	4100.0 0						
84	Peso Proprio	Peso Proprio daN	2275.0 0						
84	NEVE	Uniforme GLOBZ	60.00						
84	4100	Uniforme GLOBZ	4100.0 0						
85	Peso Proprio	Peso Proprio daN	825.00						
85	NEVE	Uniforme GLOBZ	60.00						
85	4100	Uniforme GLOBZ	4100.0 0						
86	Peso Proprio	Peso Proprio daN	400.00						
87	Peso Proprio	Peso Proprio daN	2925.0 0						
87	NEVE	Uniforme GLOBZ	60.00						
87	accidentali	Uniforme GLOBZ	600.00						
87	4100	Uniforme GLOBZ	4100.0 0						
88	Peso Proprio	Peso Proprio daN	250.00						
88	NEVE	Uniforme GLOBZ	60.00						
88	accidentali	Uniforme GLOBZ	600.00						
88	4100	Uniforme GLOBZ	4100.0 0						
89	Peso Proprio	Peso Proprio daN	2925.0 0						
89	NEVE	Uniforme GLOBZ	60.00						
89	accidentali	Uniforme GLOBZ	600.00						
89	4100	Uniforme GLOBZ	4100.0 0						
90	Peso Proprio	Peso Proprio daN	2275.0 0						
90	NEVE	Uniforme GLOBZ	60.00						
90	serbatoio	Uniforme GLOBZ	1000.0 0						
90	4100	Uniforme GLOBZ	4100.0 0						
91	Peso Proprio	Peso Proprio daN	2275.0 0						
91	NEVE	Uniforme GLOBZ	60.00						
91	4100	Uniforme GLOBZ	4100.0 0						
92	Peso Proprio	Peso Proprio daN	3100.0 0						
92	NEVE	Uniforme GLOBZ	60.00						
92	serbatoio	Uniforme GLOBZ	1000.0 0						
92	4100	Uniforme GLOBZ	4100.0 0						
93	Peso Proprio	Peso Proprio daN	825.00						
93	NEVE	Uniforme GLOBZ	60.00						
93	4100	Uniforme GLOBZ	4100.0 0						
94	Peso Proprio	Peso Proprio daN	3100.0 0						
94	NEVE	Uniforme GLOBZ	60.00						
94	4100	Uniforme GLOBZ	4100.0 0						
95	Peso Proprio	Peso Proprio daN	250.00						
95	NEVE	Uniforme GLOBZ	60.00						
95	accidentali	Uniforme GLOBZ	600.00						
95	4100	Uniforme GLOBZ	4100.0 0						
96	Peso Proprio	Peso Proprio daN	3100.0 0						
96	NEVE	Uniforme GLOBZ	60.00						
96	serbatoio	Uniforme GLOBZ	1000.0 0						
96	4100	Uniforme GLOBZ	4100.0 0						
97	Peso Proprio	Peso Proprio daN	400.00						
97	vento y	Uniforme GLOBY	- 100.00						

She ll	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
98	Peso Proprio	Peso Proprio daN	400.00						
98	vento y	Uniforme_GLOBY	100.00						
99	Peso Proprio	Peso Proprio daN	400.00						
99	vento y	Uniforme_GLOBY	100.00						
100	Peso Proprio	Peso Proprio daN	800.00						
101	Peso Proprio	Peso Proprio daN	400.00						
102	Peso Proprio	Peso Proprio daN	800.00						
103	Peso Proprio	Peso Proprio daN	400.00						
104	Peso Proprio	Peso Proprio daN	800.00						
105	Peso Proprio	Peso Proprio daN	2925.00						
105	NEVE	Uniforme_GLOBZ	60.00						
105	accidentali	Uniforme_GLOBZ	600.00						
105	4100	Uniforme_GLOBZ	4100.00						
106	Peso Proprio	Peso Proprio daN	825.00						
106	NEVE	Uniforme_GLOBZ	60.00						
106	4100	Uniforme_GLOBZ	4100.00						
107	Peso Proprio	Peso Proprio daN	250.00						
107	NEVE	Uniforme_GLOBZ	60.00						
107	accidentali	Uniforme_GLOBZ	600.00						
107	4100	Uniforme_GLOBZ	4100.00						
108	Peso Proprio	Peso Proprio daN	2275.00						
108	NEVE	Uniforme_GLOBZ	60.00						
108	serbatoio	Uniforme_GLOBZ	1000.00						
108	4100	Uniforme_GLOBZ	4100.00						
109	Peso Proprio	Peso Proprio daN	825.00						
109	NEVE	Uniforme_GLOBZ	60.00						
109	4100	Uniforme_GLOBZ	4100.00						
110	Peso Proprio	Peso Proprio daN	866.25						
110	NEVE	Uniforme_GLOBZ	60.00						
110	accidentali	Uniforme_GLOBZ	600.00						
110	4100	Uniforme_GLOBZ	4100.00						
111	Peso Proprio	Peso Proprio daN	3255.00						
111	NEVE	Uniforme_GLOBZ	60.00						
111	accidentali	Uniforme_GLOBZ	600.00						
111	4100	Uniforme_GLOBZ	4100.00						
112	Peso Proprio	Peso Proprio daN	262.50						
112	NEVE	Uniforme_GLOBZ	60.00						
112	accidentali	Uniforme_GLOBZ	600.00						
112	4100	Uniforme_GLOBZ	4100.00						
113	Peso Proprio	Peso Proprio daN	2388.75						
113	NEVE	Uniforme_GLOBZ	60.00						
113	accidentali	Uniforme_GLOBZ	600.00						
113	4100	Uniforme_GLOBZ	4100.00						
114	Peso Proprio	Peso Proprio daN	3071.25						
114	NEVE	Uniforme_GLOBZ	60.00						
114	accidentali	Uniforme_GLOBZ	600.00						
114	4100	Uniforme_GLOBZ	4100.00						

Verifica Degli Spostamenti Relativi

Scenario di calcolo: ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO



Interp.	Comb.	$\eta_{Xv}$	$\eta_{Xh}$	$\eta_{Yv}$	$\eta_{Yh}$	Nodo1	Nodo2	$\eta$	$\eta_{Amm}$	Cs
		mm	mm	mm	mm			mm	mm	
0-1	24-IV-4	0.02	0.00	0.01	0.00	18	118	0.02	4.00	>100
0-1	24-IV-4	0.01	0.00	0.00	0.00	19	119	0.01	4.00	>100
0-1	24-IV-4	0.01	0.00	0.00	0.00	20	120	0.01	4.00	>100
0-1	24-IV-4	0.01	0.00	0.00	0.00	21	121	0.01	4.00	>100
0-1	24-IV-4	0.01	0.00	0.00	0.00	22	122	0.01	4.00	>100
0-1	24-IV-4	0.01	0.00	0.01	0.00	23	123	0.01	4.00	>100
0-1	24-IV-4	0.01	0.00	0.01	0.00	24	124	0.01	4.00	>100
0-1	24-IV-4	0.01	0.00	0.01	0.00	25	125	0.01	4.00	>100
0-1	24-IV-4	0.01	0.00	0.01	0.00	26	126	0.02	4.00	>100
0-1	24-X-4	0.02	0.00	0.02	0.00	27	127	0.02	4.00	>100
0-1	24-X-4	0.02	0.00	0.02	0.00	28	128	0.02	4.00	>100
0-1	24-X-4	0.02	0.00	0.02	0.00	29	129	0.02	4.00	>100
0-1	24-IV-4	0.03	0.00	0.03	0.00	30	130	0.03	4.00	>100
0-1	24-IV-4	0.03	0.00	0.02	0.00	31	131	0.03	4.00	>100
0-1	24-X-4	0.02	0.00	0.04	0.00	50	150	0.04	4.00	96
0-1	24-X-4	0.01	0.00	0.04	0.00	51	151	0.04	4.00	>100
0-1	24-X-4	0.02	0.00	0.04	0.00	52	152	0.04	4.00	>100
0-1	24-X-4	0.02	0.00	0.04	0.00	53	153	0.04	4.00	>100
0-1	24-X-4	0.02	0.00	0.03	0.00	54	154	0.03	4.00	>100
0-1	24-X-4	0.02	0.00	0.03	0.00	55	155	0.03	4.00	>100
0-1	24-IV-4	0.02	0.00	0.03	0.00	56	156	0.03	4.00	>100
0-1	24-X-4	0.02	0.00	0.03	0.00	57	157	0.03	4.00	>100
0-1	24-X-4	0.02	0.00	0.02	0.00	58	158	0.02	4.00	>100
0-1	24-X-4	0.02	0.00	0.02	0.00	59	159	0.02	4.00	>100
0-1	24-IV-4	0.02	0.00	0.02	0.00	60	160	0.02	4.00	>100
0-1	24-IV-4	0.03	0.00	0.02	0.00	61	161	0.03	4.00	>100
0-1	24-IV-4	0.03	0.00	0.02	0.00	62	162	0.03	4.00	>100
0-1	24-IV-4	0.03	0.00	0.02	0.00	63	163	0.03	4.00	>100
0-1	24-X-4	0.02	0.00	0.03	0.00	66	166	0.03	4.00	>100
0-1	24-X-4	0.02	0.00	0.03	0.00	67	167	0.03	4.00	>100
0-1	24-X-4	0.02	0.00	0.03	0.00	68	168	0.03	4.00	>100
0-1	24-X-4	0.02	0.00	0.03	0.00	69	169	0.03	4.00	>100
0-1	24-X-4	0.02	0.00	0.03	0.00	70	170	0.03	4.00	>100
0-1	24-X-4	0.02	0.00	0.03	0.00	71	171	0.03	4.00	>100
0-1	24-X-4	0.02	0.00	0.03	0.00	72	172	0.03	4.00	>100
0-1	24-X-4	0.02	0.00	0.02	0.00	73	173	0.02	4.00	>100
0-1	24-X-4	0.02	0.00	0.02	0.00	74	174	0.02	4.00	>100
0-1	24-X-4	0.03	0.00	0.02	0.00	75	175	0.03	4.00	>100
0-1	24-X-4	0.03	0.00	0.02	0.00	76	176	0.03	4.00	>100
0-1	24-X-4	0.03	0.00	0.02	0.00	77	177	0.03	4.00	>100
0-1	24-X-4	0.03	0.00	0.02	0.00	78	178	0.03	4.00	>100
0-1	24-X-4	0.04	0.00	0.02	0.00	79	179	0.04	4.00	>100
<b>Minimo</b>										
0-1	24-X-4	0.02	0.00	0.04	0.00	50	150	0.04	4.00	96

**Risultati Analisi Dinamica - Baricentri masse e masse**  
Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

Piano	Rigido	Massa daN	X m	Y m	Z m
0	No	0.00	0.00	0.00	0.00
1	Si	65612.50	-8.45	4.55	0.78

Piano	Rigido	Massa daN	X m	Y m	Z m
0	No	0.00	0.00	0.00	0.00
1	Si	65612.50	-7.80	4.80	0.78

Piano	Rigido	Massa daN	X m	Y m	Z m
0	No	0.00	0.00	0.00	0.00
1	Si	65612.50	-8.45	5.04	0.78

Piano	Rigido	Massa daN	X m	Y m	Z m
0	No	0.00	0.00	0.00	0.00

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
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PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
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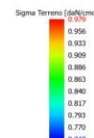
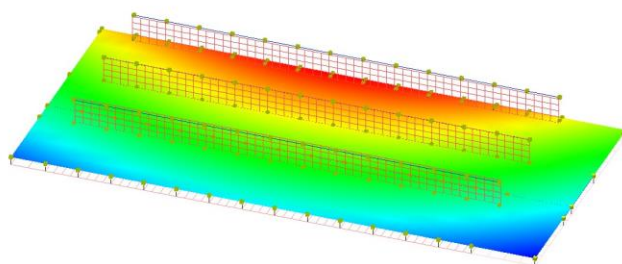
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Piano	Rigido	Massa	X	Y	Z
1	Si	65612.50	-9.10	4.80	0.78

**Risultati Analisi Dinamica - Sollecitazioni massime per combinazione - Sigma terreno platea**  
Scenario di calcolo: ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO

Combinazione	Muro	Nodi	SigmaMax daN/cm <sup>2</sup>	SigmaMin daN/cm <sup>2</sup>
1	59	89-88-72-73	0.21	0.16
2	88	85-84-68-69	0.39	0.14
3	59	89-88-72-73	0.98	0.75
4	112	82-81-65-66	0.40	0.25
5	112	82-81-65-66	0.41	0.24
6	112	82-81-65-66	0.40	0.25
7	112	82-81-65-66	0.42	0.25
8	112	82-81-65-66	0.41	0.26
9	112	82-81-65-66	0.40	0.25
10	107	83-82-66-67	0.42	0.24
11-I-1	107	83-82-66-67	0.25	0.16
11-II-1	107	83-82-66-67	0.25	0.16
11-I-2	88	85-84-68-69	0.25	0.16
11-II-2	107	83-82-66-67	0.25	0.16
11-I-3	95	84-83-67-68	0.25	0.16
11-II-3	107	83-82-66-67	0.25	0.16
11-I-4	95	84-83-67-68	0.25	0.16
11-II-4	107	83-82-66-67	0.25	0.16
12-I-1	107	83-82-66-67	0.25	0.16
12-II-1	107	83-82-66-67	0.25	0.16
12-I-2	88	85-84-68-69	0.25	0.16
12-II-2	107	83-82-66-67	0.25	0.16
12-I-3	95	84-83-67-68	0.25	0.16
12-II-3	107	83-82-66-67	0.25	0.16
12-I-4	95	84-83-67-68	0.25	0.16
12-II-4	107	83-82-66-67	0.25	0.16
Assoluti				
3	59	89-88-72-73	0.98	
2	88	85-84-68-69		0.14

Tipo diagramma: Tensioni medie terreno  
Combinazione corrente : Scenario ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO - C 3  
Tensioni medie terreno aste  
Tensioni medie terreno platee



**Risultati Analisi Dinamica - Spostamenti massimi - Nodi**  
Scenario di calcolo: ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
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la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Nodo	Trasl. X mm	Trasl. Y mm	Trasl. Z mm	Rotaz. X °	Rotaz. Y °	Rotaz. Z °
1	0.00(1)	0.00(1)	-3.84(3)	-0.01(2)	0.00(3)	0.00(1)
2	0.00(1)	0.00(1)	-3.88(3)	-0.01(2)	0.00(3)	0.00(1)
3	0.00(1)	0.00(1)	-3.92(3)	-0.01(2)	0.00(3)	0.00(1)
4	0.00(1)	0.00(1)	-3.95(3)	-0.01(2)	0.00(3)	0.00(1)
5	0.00(1)	0.00(1)	-3.98(3)	-0.01(2)	0.00(3)	0.00(1)
6	0.00(1)	0.00(1)	-4.00(3)	-0.01(2)	0.00(3)	0.00(1)
7	0.00(1)	0.00(1)	-4.01(3)	-0.01(2)	0.00(3)	0.00(1)
8	0.00(1)	0.00(1)	-4.02(3)	-0.01(2)	-0.00(11-II-1)	0.00(1)
9	0.00(1)	0.00(1)	-4.02(3)	-0.01(2)	-0.00(11-II-1)	0.00(1)
10	0.00(1)	0.00(1)	-4.01(3)	-0.01(2)	-0.00(3)	0.00(1)
11	0.00(1)	0.00(1)	-3.99(3)	-0.01(3)	-0.00(3)	0.00(1)
12	0.00(1)	0.00(1)	-3.97(3)	-0.01(3)	-0.00(3)	0.00(1)
13	0.00(1)	0.00(1)	-3.94(3)	-0.01(3)	-0.00(3)	0.00(1)
14	0.00(1)	0.00(1)	-3.89(3)	-0.01(3)	-0.00(3)	0.00(1)
15	0.00(1)	0.00(1)	-3.85(3)	-0.01(3)	-0.00(2)	0.00(1)
16	0.00(1)	0.00(1)	-3.73(3)	-0.01(3)	-0.00(2)	0.00(1)
17	0.00(1)	0.00(1)	-4.11(3)	-0.01(2)	0.00(3)	0.00(1)
18	0.00(1)	0.00(1)	-4.15(3)	-0.01(2)	0.00(3)	0.00(1)
19	0.00(1)	0.00(1)	-4.19(3)	-0.01(2)	0.00(3)	0.00(1)
20	0.00(1)	0.00(1)	-4.23(3)	-0.01(2)	0.00(3)	0.00(1)
21	0.00(1)	0.00(1)	-4.26(3)	-0.01(2)	0.00(3)	0.00(1)
22	0.00(1)	0.00(1)	-4.28(3)	-0.01(2)	0.00(3)	0.00(1)
23	0.00(1)	0.00(1)	-4.30(3)	-0.01(2)	0.00(3)	0.00(1)
24	0.00(1)	0.00(1)	-4.31(3)	-0.01(2)	-0.00(9)	0.00(1)
25	0.00(1)	0.00(1)	-4.30(3)	-0.01(2)	-0.00(2)	0.00(1)
26	0.00(1)	0.00(1)	-4.29(3)	-0.01(2)	-0.00(2)	0.00(1)
27	0.00(1)	0.00(1)	-4.27(3)	-0.01(3)	-0.00(3)	0.00(1)
28	0.00(1)	0.00(1)	-4.24(3)	-0.01(3)	-0.00(3)	0.00(1)
29	0.00(1)	0.00(1)	-4.20(3)	-0.01(3)	-0.00(3)	0.00(1)
30	0.00(1)	0.00(1)	-4.15(3)	-0.01(3)	-0.00(2)	0.00(1)
31	0.00(1)	0.00(1)	-4.09(3)	-0.01(3)	-0.00(2)	0.00(1)
32	0.00(1)	0.00(1)	-3.96(3)	-0.01(3)	-0.00(2)	0.00(1)
33	0.00(1)	0.00(1)	-4.18(3)	-0.01(2)	0.00(3)	0.00(1)
34	0.00(1)	0.00(1)	-4.22(3)	-0.01(2)	0.00(3)	0.00(1)
35	0.00(1)	0.00(1)	-4.27(3)	-0.01(2)	0.00(3)	0.00(1)
36	0.00(1)	0.00(1)	-4.31(3)	-0.01(2)	0.00(3)	0.00(1)
37	0.00(1)	0.00(1)	-4.34(3)	-0.01(2)	0.00(3)	0.00(1)
38	0.00(1)	0.00(1)	-4.36(3)	-0.01(2)	0.00(3)	0.00(1)
39	0.00(1)	0.00(1)	-4.38(3)	-0.01(2)	-0.00(9)	0.00(1)
40	0.00(1)	0.00(1)	-4.38(3)	-0.01(2)	-0.00(9)	0.00(1)
41	0.00(1)	0.00(1)	-4.38(3)	-0.01(2)	-0.00(2)	0.00(1)
42	0.00(1)	0.00(1)	-4.37(3)	-0.01(2)	-0.00(2)	0.00(1)
43	0.00(1)	0.00(1)	-4.35(3)	-0.01(3)	-0.00(2)	0.00(1)
44	0.00(1)	0.00(1)	-4.32(3)	-0.01(3)	-0.00(3)	0.00(1)
45	0.00(1)	0.00(1)	-4.27(3)	-0.01(3)	-0.00(3)	0.00(1)
46	0.00(1)	0.00(1)	-4.22(3)	-0.01(3)	-0.00(2)	0.00(1)
47	0.00(1)	0.00(1)	-4.16(3)	-0.01(3)	-0.00(2)	0.00(1)
48	0.00(1)	0.00(1)	-4.03(3)	-0.01(3)	-0.00(2)	0.00(1)
49	0.00(1)	0.00(1)	-4.37(3)	-0.01(2)	0.00(3)	0.00(1)
50	0.00(1)	0.00(1)	-4.42(3)	-0.01(2)	0.00(3)	0.00(1)
51	0.00(1)	0.00(1)	-4.47(3)	-0.01(2)	0.00(3)	0.00(1)
52	0.00(1)	0.00(1)	-4.51(3)	-0.01(2)	0.00(3)	0.00(1)
53	0.00(1)	0.00(1)	-4.55(3)	-0.01(2)	0.00(3)	0.00(1)
54	0.00(1)	0.00(1)	-4.57(3)	-0.01(2)	0.00(3)	0.00(1)
55	0.00(1)	0.00(1)	-4.59(3)	-0.01(2)	-0.00(9)	0.00(1)
56	0.00(1)	0.00(1)	-4.60(3)	-0.01(2)	-0.00(9)	0.00(1)
57	0.00(1)	0.00(1)	-4.59(3)	-0.01(2)	-0.00(2)	0.00(1)
58	0.00(1)	0.00(1)	-4.58(3)	-0.01(2)	-0.00(2)	0.00(1)
59	0.00(1)	0.00(1)	-4.56(3)	-0.01(3)	-0.00(2)	0.00(1)
60	0.00(1)	0.00(1)	-4.52(3)	-0.01(3)	-0.00(2)	0.00(1)
61	0.00(1)	0.00(1)	-4.47(3)	-0.01(3)	-0.00(2)	0.00(1)
62	0.00(1)	0.00(1)	-4.41(3)	-0.01(3)	-0.00(2)	0.00(1)
63	0.00(1)	0.00(1)	-4.35(3)	-0.01(3)	-0.00(2)	0.00(1)
64	0.00(1)	0.00(1)	-4.19(3)	-0.01(3)	-0.00(2)	0.00(1)
65	0.00(1)	0.00(1)	-4.62(3)	-0.01(2)	0.00(3)	0.00(1)
66	0.00(1)	0.00(1)	-4.68(3)	-0.01(2)	0.00(3)	0.00(1)
67	0.00(1)	0.00(1)	-4.73(3)	-0.01(2)	0.00(3)	0.00(1)
68	0.00(1)	0.00(1)	-4.78(3)	-0.01(2)	0.00(3)	0.00(1)
69	0.00(1)	0.00(1)	-4.82(3)	-0.01(2)	0.00(3)	0.00(1)
70	0.00(1)	0.00(1)	-4.85(3)	-0.01(2)	-0.00(9)	0.00(1)
71	0.00(1)	0.00(1)	-4.86(3)	-0.01(2)	-0.00(9)	0.00(1)
72	0.00(1)	0.00(1)	-4.87(3)	-0.01(2)	-0.00(9)	0.00(1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
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BTK3**

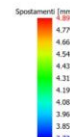
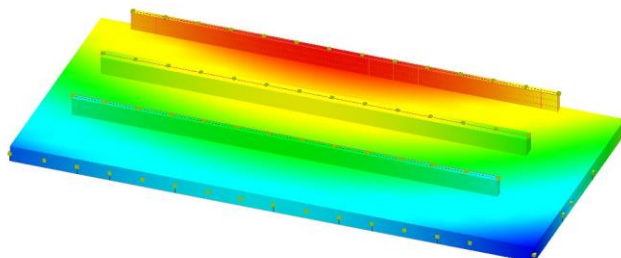
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Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
73	0.00(1)	0.00(1)	-4.87(3)	-0.01(2)	-0.00(2)	0.00(1)
74	0.00(1)	0.00(1)	-4.85(3)	-0.01(2)	-0.00(2)	0.00(1)
75	0.00(1)	0.00(1)	-4.82(3)	-0.01(3)	-0.00(2)	0.00(1)
76	0.00(1)	0.00(1)	-4.78(3)	-0.01(3)	-0.00(2)	0.00(1)
77	0.00(1)	0.00(1)	-4.73(3)	-0.01(3)	-0.00(2)	0.00(1)
78	0.00(1)	0.00(1)	-4.67(3)	-0.01(3)	-0.00(2)	0.00(1)
79	0.00(1)	0.00(1)	-4.59(3)	-0.01(3)	-0.00(2)	0.00(1)
80	0.00(1)	0.00(1)	-4.43(3)	-0.01(3)	-0.00(2)	0.00(1)
81	0.00(1)	0.00(1)	-4.64(3)	-0.01(2)	0.00(3)	0.00(1)
82	0.00(1)	0.00(1)	-4.70(3)	-0.01(2)	0.00(3)	0.00(1)
83	0.00(1)	0.00(1)	-4.75(3)	-0.01(2)	0.00(3)	0.00(1)
84	0.00(1)	0.00(1)	-4.80(3)	-0.01(2)	0.00(3)	0.00(1)
85	0.00(1)	0.00(1)	-4.84(3)	-0.01(2)	0.00(3)	0.00(1)
86	0.00(1)	0.00(1)	-4.87(3)	-0.01(2)	-0.00(9)	0.00(1)
87	0.00(1)	0.00(1)	-4.89(3)	-0.01(2)	-0.00(9)	0.00(1)
88	0.00(1)	0.00(1)	-4.89(3)	-0.01(2)	-0.00(9)	0.00(1)
89	0.00(1)	0.00(1)	-4.89(3)	-0.01(2)	-0.00(2)	0.00(1)
90	0.00(1)	0.00(1)	-4.88(3)	-0.01(2)	-0.00(2)	0.00(1)
91	0.00(1)	0.00(1)	-4.85(3)	-0.01(3)	-0.00(2)	0.00(1)
92	0.00(1)	0.00(1)	-4.81(3)	-0.01(3)	-0.00(2)	0.00(1)
93	0.00(1)	0.00(1)	-4.75(3)	-0.01(3)	-0.00(2)	0.00(1)
94	0.00(1)	0.00(1)	-4.69(3)	-0.01(3)	-0.00(2)	0.00(1)
95	0.00(1)	0.00(1)	-4.62(3)	-0.01(3)	-0.00(2)	0.00(1)
96	0.00(1)	0.00(1)	-4.45(3)	-0.01(3)	-0.00(2)	0.00(1)
118	-0.04(11-II-4)	0.16(10)	-4.17(3)	0.02(11-II-4)	-0.02(11-II-4)	-0.01(11-II-1)
119	0.03(3)	0.16(10)	-4.21(3)	0.02(11-II-1)	-0.01(11-II-4)	-0.00(11-II-1)
120	0.03(3)	0.15(10)	-4.25(3)	0.02(11-I-2)	-0.01(11-II-4)	-0.00(11-II-1)
121	0.02(3)	0.15(10)	-4.28(3)	0.02(11-II-2)	-0.01(11-II-4)	-0.00(11-II-1)
122	0.02(3)	0.15(10)	-4.30(3)	0.02(11-I-2)	-0.01(11-I-4)	-0.00(11-II-4)
123	-0.02(11-I-4)	0.15(10)	-4.31(3)	0.02(11-I-2)	-0.01(11-I-4)	-0.00(11-II-1)
124	-0.02(11-II-1)	0.14(10)	-4.32(3)	0.02(11-I-4)	-0.01(11-II-1)	-0.00(11-II-1)
125	-0.02(11-II-1)	0.14(10)	-4.32(3)	0.02(11-II-4)	-0.01(11-II-1)	-0.00(11-II-1)
126	-0.02(11-I-2)	0.13(10)	-4.31(3)	0.02(11-II-4)	-0.01(11-I-2)	-0.00(11-I-2)
127	-0.03(11-I-2)	0.13(10)	-4.29(3)	0.02(11-I-4)	-0.01(11-I-2)	-0.00(11-II-2)
128	-0.03(11-II-2)	0.13(10)	-4.26(3)	0.02(11-II-4)	-0.01(11-II-2)	-0.00(11-II-1)
129	-0.04(3)	0.12(10)	-4.22(3)	0.02(11-II-4)	-0.01(11-II-2)	-0.00(11-II-1)
130	-0.04(2)	0.12(10)	-4.17(3)	0.02(11-I-4)	-0.01(11-II-2)	-0.00(11-II-2)
131	-0.04(11-II-2)	0.12(10)	-4.11(3)	0.02(11-II-1)	-0.02(11-II-1)	0.00(11-I-1)
150	0.03(3)	0.11(2)	-4.43(3)	-0.01(10)	-0.02(11-II-4)	-0.00(11-II-3)
151	0.03(3)	0.11(2)	-4.47(3)	-0.01(10)	-0.01(11-II-4)	-0.00(9)
152	0.03(3)	0.11(2)	-4.52(3)	-0.01(10)	-0.01(11-II-4)	-0.00(9)
153	0.02(3)	0.10(2)	-4.55(3)	-0.01(10)	-0.01(11-II-4)	-0.00(9)
154	0.02(3)	0.10(2)	-4.58(3)	-0.01(10)	-0.01(11-I-4)	-0.00(9)
155	-0.02(11-I-4)	0.10(2)	-4.59(3)	-0.01(10)	-0.01(11-I-4)	-0.00(9)
156	-0.02(11-II-1)	0.10(2)	-4.60(3)	-0.01(10)	-0.01(11-II-1)	-0.00(2)
157	-0.02(11-II-1)	0.09(2)	-4.60(3)	-0.01(10)	-0.01(11-I-2)	-0.00(2)
158	-0.02(2)	0.09(2)	-4.58(3)	-0.01(10)	-0.01(11-I-2)	-0.00(2)
159	-0.03(2)	0.09(3)	-4.56(3)	-0.01(10)	-0.01(11-I-2)	-0.00(2)
160	-0.04(2)	0.09(3)	-4.52(3)	-0.01(10)	-0.01(11-II-2)	-0.00(2)
161	-0.05(2)	0.08(3)	-4.48(3)	-0.01(10)	-0.01(11-II-2)	-0.00(2)
162	-0.05(2)	0.08(3)	-4.42(3)	-0.01(10)	-0.01(11-II-2)	-0.00(2)
163	-0.05(11-II-2)	0.08(3)	-4.36(3)	-0.01(10)	-0.02(11-II-2)	0.00(11-I-3)
166	0.03(3)	0.21(10)	-4.70(3)	-0.03(10)	-0.02(11-II-4)	-0.00(11-I-3)
167	0.04(3)	0.21(10)	-4.75(3)	-0.03(10)	-0.01(11-II-4)	0.00(11-II-4)
168	0.03(3)	0.21(10)	-4.79(3)	-0.03(10)	-0.01(11-II-4)	0.00(11-II-3)
169	0.03(3)	0.21(10)	-4.83(3)	-0.03(10)	-0.01(11-II-4)	0.00(11-II-3)
170	-0.02(9)	0.21(10)	-4.86(3)	-0.03(10)	-0.01(11-I-4)	0.00(11-II-4)
171	-0.02(9)	0.21(10)	-4.88(3)	-0.03(10)	-0.01(11-I-4)	0.00(11-II-3)
172	-0.02(11-I-3)	0.21(10)	-4.88(3)	-0.03(10)	-0.01(11-I-3)	0.00(11-I-3)
173	-0.03(2)	0.20(10)	-4.88(3)	-0.03(10)	-0.01(11-I-3)	0.00(11-I-3)
174	-0.03(2)	0.20(10)	-4.87(3)	-0.03(10)	-0.01(11-I-2)	0.00(11-I-2)
175	-0.04(2)	0.20(10)	-4.84(3)	-0.03(10)	-0.01(11-I-2)	0.00(11-II-2)
176	-0.05(2)	0.20(10)	-4.80(3)	-0.03(10)	-0.01(11-II-2)	0.00(11-II-3)
177	-0.05(2)	0.19(10)	-4.75(3)	-0.03(10)	-0.01(11-II-2)	0.00(11-II-3)
178	-0.06(2)	0.19(10)	-4.68(3)	-0.03(10)	-0.01(11-II-2)	0.00(11-II-2)
179	-0.06(11-II-2)	0.19(10)	-4.62(3)	-0.03(10)	-0.02(11-II-2)	0.00(11-II-2)

Tipo diagramma: Deformata  
Combinazione corrente : Scenario ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO - C 3



Risultati Analisi Dinamica - Reazioni massime - Nodi  
Scenario di calcolo: ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO

Nodo	Rx daN	Ry daN	Rz daN	Mx daN*m	My daN*m	Mz daN*m
1	-30.32 (2)	-22.16 (11-II-4)	0	0	0	2.48 (2)
2	-111.57 (9)	-42.45 (11-I-3)	0	0	0	14.73 (3)
3	-155.64 (9)	-47.33 (11-I-3)	0	0	0	8.96 (2)
4	-199.75 (9)	-49.44 (3)	0	0	0	6.89 (2)
5	-239.24 (9)	-50.51 (3)	0	0	0	6.72 (2)
6	-278.57 (9)	-51.26 (3)	0	0	0	8.72 (2)
7	-320.89 (2)	-51.61 (3)	0	0	0	12.13 (2)
8	-388.61 (2)	-51.65 (3)	0	0	0	16.21 (2)
9	-458.24 (2)	-51.44 (3)	0	0	0	20.48 (2)
10	-526.63 (2)	-50.90 (3)	0	0	0	24.71 (2)
11	-591.36 (2)	-49.83 (3)	0	0	0	29.08 (2)
12	-652.29 (2)	-49.16 (2)	0	0	0	34.73 (2)
13	-607.14 (2)	-45.20 (3)	0	0	0	32.48 (2)
14	-150.32 (3)	-41.38 (3)	0	0	0	-15.85 (4)
15	126.20 (4)	-38.00 (3)	0	0	0	-27.87 (2)
16	61.29 (2)	20.63 (10)	0	0	0	-6.86 (2)
17	-116.91 (2)	252.39 (3)	0	0	0	-14.40 (2)
18	-532.28 (2)	-535.21 (2)	0	0	0	-31.25 (3)
19	243.00 (11-II-1)	-578.25 (10)	0	0	0	-30.37 (3)
20	148.39 (11-II-1)	-532.38 (10)	0	0	0	-17.96 (3)
21	100.82 (9)	-459.92 (10)	0	0	0	-10.31 (11-I-2)
22	86.65 (9)	-420.36 (10)	0	0	0	-11.30 (11-II-4)
23	77.88 (11-II-1)	-401.80 (10)	0	0	0	-12.50 (11-I-1)
24	77.17 (11-II-1)	-393.29 (10)	0	0	0	-13.29 (11-I-1)
25	78.00 (11-II-1)	-388.04 (10)	0	0	0	-15.60 (9)
26	82.11 (11-II-1)	-379.67 (10)	0	0	0	-19.36 (9)
27	94.75 (11-I-2)	-358.19 (10)	0	0	0	-22.73 (9)
28	122.89 (11-II-1)	-301.27 (10)	0	0	0	-25.72 (9)
29	172.35 (11-II-1)	275.96 (9)	0	0	0	-18.74 (9)
30	186.77 (11-II-1)	300.55 (9)	0	0	0	47.48 (2)
31	707.37 (2)	-300.86 (3)	0	0	0	62.02 (2)
32	133.60 (2)	445.56 (2)	0	0	0	31.22 (2)
33	-157.24 (2)	326.20 (3)	0	0	0	12.37 (3)
34	-468.07 (2)	244.86 (3)	0	0	0	16.68 (2)
35	-140.96 (3)	-190.62 (2)	0	0	0	4.60 (3)
36	214.22 (10)	204.54 (10)	0	0	0	-9.34 (10)
37	137.17 (10)	351.31 (10)	0	0	0	-6.02 (10)
38	67.08 (10)	401.72 (10)	0	0	0	-2.79 (10)
39	-49.05 (11-I-1)	422.08 (10)	0	0	0	1.67 (11-I-1)

Nodo	Rx	Ry	Rz	Mx	My	Mz
40	-55.03 (11-I-1)	430.77 (10)	0	0	0	1.87 (11-I-1)
41	-61.36 (2)	435.65 (10)	0	0	0	1.95 (2)
42	-75.59 (2)	442.39 (10)	0	0	0	2.34 (2)
43	-78.31 (10)	456.32 (10)	0	0	0	2.31 (10)
44	-74.20 (10)	481.76 (10)	0	0	0	1.89 (10)
45	103.22 (11-I-1)	513.72 (10)	0	0	0	-3.56 (11-I-1)
46	158.67 (11-I-1)	500.85 (10)	0	0	0	-5.06 (3)
47	449.70 (2)	499.91 (10)	0	0	0	15.13 (10)
48	55.02 (2)	477.73 (2)	0	0	0	13.18 (3)
49	-304.80 (2)	528.12 (3)	0	0	0	24.36 (2)
50	-1337.96 (2)	501.66 (3)	0	0	0	24.10 (2)
51	553.55 (9)	348.02 (3)	0	0	0	6.57 (2)
52	507.79 (9)	364.86 (3)	0	0	0	-11.74 (10)
53	334.05 (9)	383.23 (2)	0	0	0	4.14 (11-I-3)
54	261.12 (9)	402.35 (2)	0	0	0	7.34 (2)
55	226.17 (9)	407.12 (2)	0	0	0	12.90 (2)
56	203.56 (9)	404.82 (2)	0	0	0	17.07 (2)
57	197.16 (11-II-1)	399.67 (2)	0	0	0	19.96 (2)
58	205.83 (11-I-2)	394.07 (2)	0	0	0	21.34 (2)
59	222.50 (11-I-2)	388.69 (2)	0	0	0	20.81 (2)
60	260.26 (11-II-1)	381.22 (2)	0	0	0	18.10 (2)
61	327.54 (11-II-2)	362.77 (2)	0	0	0	16.09 (10)
62	-416.28 (3)	263.49 (11-II-3)	0	0	0	12.43 (10)
63	1169.73 (3)	424.55 (2)	0	0	0	-18.27 (3)
64	135.76 (3)	654.89 (2)	0	0	0	8.86 (10)
65	-222.79 (2)	-70.78 (10)	0	0	0	-23.41 (10)
66	-707.12 (2)	-438.39 (10)	0	0	0	-39.15 (2)
67	350.34 (9)	-706.95 (10)	0	0	0	32.09 (9)
68	377.79 (9)	-770.84 (10)	0	0	0	36.41 (9)
69	292.76 (9)	-862.31 (10)	0	0	0	24.34 (9)
70	258.57 (9)	-895.62 (10)	0	0	0	17.64 (9)
71	246.90 (9)	-907.75 (10)	0	0	0	14.82 (9)
72	238.10 (9)	-912.59 (10)	0	0	0	13.13 (9)
73	230.16 (9)	-914.19 (10)	0	0	0	12.04 (9)
74	223.38 (9)	-914.01 (10)	0	0	0	11.43 (9)
75	217.15 (9)	-912.22 (10)	0	0	0	11.18 (9)
76	215.79 (2)	-907.33 (10)	0	0	0	11.57 (11-II-3)
77	208.97 (11-II-3)	-897.80 (10)	0	0	0	15.21 (11-II-3)
78	208.42 (11-II-3)	-902.29 (10)	0	0	0	-17.56 (3)
79	830.38 (2)	-796.72 (10)	0	0	0	24.79 (3)
80	125.77 (3)	64.81 (3)	0	0	0	15.92 (3)
81	-46.88 (10)	8.09 (2)	0	0	0	0
82	-183.04 (10)	5.81 (2)	0	0	0	2.35 (10)
83	-53.92 (3)	7.01 (2)	0	0	0	0
84	-48.59 (3)	7.25 (2)	0	0	0	0
85	54.31 (9)	7.41 (2)	0	0	0	0
86	56.04 (9)	7.18 (2)	0	0	0	0
87	54.57 (9)	7.00 (2)	0	0	0	0
88	52.94 (10)	6.81 (2)	0	0	0	0
89	54.26 (2)	6.60 (2)	0	0	0	0
90	57.25 (2)	6.35 (2)	0	0	0	0
91	61.69 (2)	6.05 (3)	0	0	0	0
92	67.50 (2)	5.78 (3)	0	0	0	0
93	72.16 (2)	5.33 (3)	0	0	0	0
94	73.56 (10)	4.81 (3)	0	0	0	0
95	306.59 (10)	-138.98 (10)	0	0	0	-4.96 (10)
96	15.45 (3)	6.21 (10)	0	0	0	0

**Risultati Analisi Dinamica - Spostamenti massimi - Impalcati**  
Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Piano	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	mm	mm	mm	°	°	°
1	-0.02 (2-1)	0.11 (10-1)	-4.50 (3-1)	0.00 (1-1)	0.00 (1-1)	-0.00 (2-1)

**Risultati Analisi Dinamica - Spostamenti massimi - Impalcati (SLD)**  
Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

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la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Piano	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	mm	mm	mm	°	°	°
1	-0.01(23-II-1)	0.07(15-1)	-1.23(18-1)	0.00(13-1)	0.00(13-1)	-0.00(23-II-1)

**Risultati Analisi Dinamica - Sollecitazioni Massime - Muri discretizzati**  
Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
		MPa	MPa	MPa	daN*m/m	daN*m/m	daN*m/m
1	1	0.1(3)	-0.1(10)	0.0(10)	-286.33(3)	165.48(10)	-195.46(10)
1	2	0.1(3)	-0.1(10)	0.0(10)	-126.97(3)	342.75(10)	-151.22(10)
1	3	0.1(3)	-0.1(10)	0.0(10)	-112.40(3)	299.78(10)	45.65(3)
1	4	0.1(3)	-0.0(10)	0.0(10)	-265.84(3)	-175.80(3)	18.92(4)
1	5	0.1(3)	-0.1(10)	0.0(10)	-347.93(3)	152.63(10)	-126.78(10)
1	6	0.1(3)	-0.1(10)	0.0(10)	-246.56(3)	433.65(10)	-130.80(10)
1	7	0.1(3)	-0.0(10)	0.0(10)	-246.59(3)	371.03(10)	-73.41(2)
1	8	0.1(3)	-0.0(10)	0.0(2)	-360.85(3)	-294.20(3)	-125.66(2)
1	9	0.1(3)	-0.1(10)	0.0(10)	-369.49(3)	167.46(10)	-106.73(10)
1	10	0.1(3)	-0.1(10)	0.0(10)	-332.73(3)	456.22(10)	-116.74(10)
1	11	0.1(3)	-0.0(10)	0.0(10)	-340.08(3)	377.94(10)	-121.61(2)
1	12	0.1(3)	-0.0(10)	0.0(2)	-391.01(3)	-306.43(3)	-154.14(2)
1	13	0.1(3)	-0.1(10)	0.0(10)	-385.97(3)	210.71(10)	-77.69(10)
1	14	0.1(3)	-0.1(10)	0.0(10)	-405.05(3)	402.48(10)	-117.15(10)
1	15	0.1(3)	-0.1(10)	0.0(2)	-415.72(3)	321.04(10)	-209.03(2)
1	16	0.1(3)	0.0(3)	0.0(2)	-405.37(3)	-220.36(3)	-213.45(2)
2	1	0.1(3)	-0.1(10)	0.0(10)	-316.00(3)	218.94(10)	-127.90(10)
2	2	0.1(3)	-0.1(10)	0.0(10)	-270.06(3)	413.27(10)	-105.44(10)
2	3	0.1(3)	-0.1(10)	0.0(10)	-276.86(3)	321.36(10)	36.42(3)
2	4	0.1(3)	0.0(3)	0.0(2)	-333.15(3)	-213.43(3)	-42.96(2)
2	5	0.1(3)	-0.1(10)	0.0(10)	-353.29(3)	190.05(10)	-98.85(10)
2	6	0.1(3)	-0.1(10)	0.0(10)	-314.79(3)	490.69(10)	-117.60(10)
2	7	0.1(3)	-0.1(10)	0.0(2)	-322.59(3)	386.69(10)	-89.38(2)
2	8	0.1(3)	-0.0(10)	0.0(2)	-378.86(3)	-314.83(3)	-117.19(2)
2	9	0.1(3)	-0.1(10)	0.0(10)	-384.63(3)	190.13(10)	-92.36(10)
2	10	0.1(3)	-0.1(10)	0.0(10)	-361.47(3)	496.44(10)	-120.68(10)
2	11	0.1(3)	-0.1(10)	0.0(2)	-368.24(3)	395.15(10)	-122.14(2)
2	12	0.1(3)	-0.0(10)	0.0(2)	-416.69(3)	-330.81(3)	-139.54(2)
2	13	0.1(3)	-0.1(10)	0.0(10)	-414.48(3)	219.36(10)	-70.52(2)
2	14	0.1(3)	-0.1(10)	0.0(2)	-410.50(3)	427.20(10)	-127.43(10)
2	15	0.1(3)	-0.1(10)	0.0(2)	-418.72(3)	338.97(10)	-228.43(10)
2	16	0.1(3)	0.0(3)	0.0(2)	-434.84(3)	-250.94(3)	-206.08(2)
3	1	0.1(2)	0.0(2)	0.0(2)	-379.06(2)	-175.49(3)	-171.35(2)
3	2	0.1(2)	0.0(2)	0.0(2)	-374.73(2)	-90.91(2)	-187.32(2)
3	3	0.1(2)	0.0(2)	0.0(2)	-437.93(2)	-45.80(2)	-177.92(2)
3	4	0.1(2)	0.0(2)	0.0(2)	-462.09(2)	-18.37(10)	-100.20(2)
3	5	0.1(2)	0.0(2)	0.0(2)	-432.75(2)	-224.70(3)	-166.13(2)
3	6	0.1(2)	0.0(2)	0.0(2)	-460.80(2)	-100.54(2)	-176.25(2)
3	7	0.1(2)	0.0(2)	0.0(2)	-498.28(2)	-54.79(9)	-176.92(2)
3	8	0.1(2)	0.0(2)	0.0(2)	-494.59(2)	26.36(3)	-89.78(2)
3	9	0.1(2)	0.0(2)	0.0(2)	-447.85(2)	-231.08(3)	-180.14(2)
3	10	0.1(2)	0.0(2)	0.0(2)	-472.30(2)	-99.05(2)	-178.18(2)
3	11	0.1(2)	0.0(2)	0.0(2)	-478.70(2)	-52.32(9)	-180.88(2)
3	12	0.1(2)	0.0(2)	0.0(2)	-473.98(2)	28.57(3)	-88.64(2)
3	13	0.1(2)	0.0(2)	0.0(2)	-419.35(2)	-189.08(3)	-177.48(2)
3	14	0.1(2)	0.0(2)	0.0(2)	-419.97(2)	-91.01(2)	-162.86(10)
3	15	0.1(2)	0.0(2)	0.0(2)	-371.02(2)	-37.50(9)	-155.01(2)
3	16	0.1(2)	0.0(2)	0.0(2)	-390.63(2)	16.18(3)	-100.26(2)
4	1	0.1(2)	0.0(2)	0.0(2)	-223.67(2)	-141.08(3)	-172.93(3)
4	2	0.1(2)	0.0(2)	0.0(2)	-133.44(3)	-42.93(2)	-189.96(3)
4	3	0.1(2)	0.0(2)	0.0(2)	-167.96(3)	-18.25(2)	-147.30(2)
4	4	0.1(2)	0.0(2)	0.0(2)	-222.27(2)	7.34(2)	-83.39(2)
4	5	0.1(2)	0.0(2)	0.0(2)	-314.65(2)	-201.44(3)	-116.69(3)
4	6	0.1(2)	0.0(2)	0.0(2)	-256.64(2)	-48.17(2)	-152.02(2)
4	7	0.1(2)	0.0(2)	0.0(2)	-260.00(2)	-24.41(10)	-145.42(2)
4	8	0.1(2)	0.0(2)	0.0(2)	-288.58(2)	19.97(3)	-94.09(2)
4	9	0.1(2)	0.0(2)	0.0(2)	-378.95(2)	-217.43(3)	-104.87(3)
4	10	0.1(2)	0.0(2)	0.0(2)	-384.21(2)	-68.92(2)	-134.32(2)
4	11	0.1(2)	0.0(2)	0.0(2)	-376.98(2)	-36.10(10)	-146.43(2)
4	12	0.1(2)	0.0(2)	0.0(2)	-362.12(2)	21.45(3)	-98.60(2)
4	13	0.1(2)	0.0(2)	0.0(2)	-445.15(2)	-179.90(2)	-113.91(2)
4	14	0.1(2)	0.0(2)	0.0(2)	-522.31(2)	-100.94(2)	-112.43(2)
4	15	0.1(2)	0.0(2)	0.0(2)	-502.19(2)	-54.09(2)	-123.87(2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
4	16	0.1 (2)	0.0 (2)	0.0 (2)	-443.78 (2)	-19.58 (10)	-88.48 (2)
5	1	0.1 (3)	-0.0 (10)	0.0 (2)	-281.92 (3)	-224.02 (3)	-187.25 (2)
5	2	0.1 (3)	-0.0 (10)	0.0 (2)	-137.34 (2)	217.88 (10)	-229.28 (2)
5	3	0.1 (2)	-0.0 (10)	0.0 (2)	-127.91 (2)	200.11 (10)	-162.14 (3)
5	4	0.1 (2)	-0.0 (10)	0.0 (2)	-199.11 (2)	96.16 (9)	-135.17 (2)
5	5	0.1 (3)	-0.0 (10)	0.0 (2)	-368.16 (3)	-329.24 (3)	-118.21 (10)
5	6	0.1 (3)	-0.0 (10)	0.0 (2)	-271.17 (2)	266.19 (10)	-167.50 (2)
5	7	0.1 (2)	-0.0 (10)	0.0 (2)	-241.39 (2)	247.54 (10)	-159.57 (2)
5	8	0.1 (2)	-0.0 (10)	0.0 (2)	-270.05 (2)	94.47 (9)	-162.25 (2)
5	9	0.1 (3)	-0.0 (10)	0.0 (2)	-386.68 (3)	-340.12 (3)	-106.69 (10)
5	10	0.1 (3)	-0.0 (10)	0.0 (2)	-349.45 (3)	271.59 (10)	-136.11 (2)
5	11	0.1 (2)	-0.0 (10)	0.0 (2)	-333.35 (2)	261.05 (10)	-152.69 (2)
5	12	0.1 (2)	-0.0 (10)	0.0 (2)	-333.05 (2)	103.78 (9)	-166.01 (2)
5	13	0.1 (3)	0.0 (3)	0.0 (2)	-402.52 (3)	-273.00 (3)	-87.92 (10)
5	14	0.1 (2)	-0.0 (10)	0.0 (2)	-417.55 (3)	234.49 (10)	-91.02 (10)
5	15	0.1 (2)	-0.0 (10)	0.0 (2)	-405.77 (2)	232.28 (10)	-133.72 (2)
5	16	0.1 (2)	-0.0 (10)	0.0 (2)	-377.36 (2)	120.93 (9)	-161.86 (2)
6	1	0.1 (3)	0.0 (3)	0.0 (2)	-332.21 (3)	-269.84 (3)	-172.10 (2)
6	2	0.1 (3)	-0.0 (10)	0.0 (2)	-282.11 (2)	235.86 (10)	-210.89 (2)
6	3	0.1 (2)	-0.0 (10)	0.0 (2)	-286.30 (2)	238.77 (10)	-177.30 (2)
6	4	0.1 (2)	-0.0 (10)	0.0 (2)	-327.43 (2)	127.12 (9)	-159.29 (2)
6	5	0.1 (3)	0.0 (3)	0.0 (2)	-375.42 (3)	-355.65 (3)	-137.14 (2)
6	6	0.1 (3)	-0.0 (10)	0.0 (2)	-327.72 (3)	274.26 (10)	-165.55 (2)
6	7	0.1 (2)	-0.0 (10)	0.0 (2)	-329.13 (2)	281.00 (10)	-165.96 (2)
6	8	0.1 (2)	-0.0 (10)	0.0 (2)	-354.52 (2)	120.68 (9)	-173.26 (2)
6	9	0.1 (3)	0.0 (3)	0.0 (2)	-412.59 (3)	-372.14 (3)	-131.97 (2)
6	10	0.1 (3)	-0.0 (10)	0.0 (2)	-376.47 (3)	275.45 (10)	-156.31 (2)
6	11	0.1 (2)	-0.0 (10)	0.0 (2)	-362.72 (2)	283.20 (10)	-163.33 (2)
6	12	0.1 (2)	-0.0 (10)	0.0 (2)	-374.91 (2)	122.27 (9)	-175.81 (2)
6	13	0.1 (3)	0.0 (3)	0.0 (2)	-436.39 (3)	-309.72 (3)	-106.89 (2)
6	14	0.1 (3)	-0.0 (10)	0.0 (2)	-431.20 (3)	235.30 (10)	-101.06 (10)
6	15	0.1 (2)	-0.0 (10)	0.0 (2)	-403.46 (3)	243.93 (10)	-152.43 (10)
6	16	0.1 (2)	-0.0 (10)	0.0 (2)	-385.85 (2)	130.33 (9)	-176.28 (2)
7	1	0.1 (2)	0.0 (3)	0.0 (2)	-342.30 (2)	141.04 (9)	-124.64 (2)
7	2	0.1 (2)	0.0 (3)	0.0 (2)	-371.78 (2)	-186.05 (3)	-136.59 (2)
7	3	0.1 (2)	0.0 (3)	0.0 (2)	-363.60 (2)	227.01 (10)	-154.03 (2)
7	4	0.1 (2)	0.0 (3)	0.0 (2)	-409.58 (2)	-275.24 (10)	-174.40 (2)
7	5	0.1 (2)	0.0 (3)	0.0 (2)	-378.47 (2)	228.76 (10)	-166.33 (2)
7	6	0.1 (2)	0.0 (3)	0.0 (2)	-425.06 (2)	-279.39 (10)	-185.54 (2)
7	7	0.1 (2)	0.0 (3)	0.0 (2)	-389.66 (2)	141.47 (9)	-204.71 (2)
7	8	0.1 (2)	0.0 (3)	0.0 (2)	-419.30 (2)	-202.61 (3)	-213.43 (2)
8	1	0.1 (2)	0.0 (3)	0.0 (2)	-221.96 (2)	119.36 (10)	-80.36 (2)
8	2	0.1 (2)	0.0 (3)	0.0 (2)	-275.87 (2)	-212.08 (2)	-108.55 (2)
8	3	0.1 (2)	0.0 (3)	0.0 (2)	-290.50 (2)	201.75 (10)	-113.12 (2)
8	4	0.1 (2)	0.0 (3)	0.0 (2)	-349.23 (2)	-270.46 (10)	-164.01 (2)
8	5	0.1 (2)	0.0 (3)	0.0 (2)	-329.87 (2)	206.91 (10)	-129.65 (2)
8	6	0.1 (2)	0.0 (3)	0.0 (2)	-370.67 (2)	-268.65 (10)	-168.24 (2)
8	7	0.1 (2)	0.0 (3)	0.0 (2)	-371.39 (2)	131.31 (9)	-168.92 (2)
8	8	0.1 (2)	0.0 (3)	0.0 (2)	-397.49 (2)	-192.66 (3)	-182.19 (2)
9	1	-0.1 (3)	-0.3 (3)	-0.1 (3)	-64.18 (10)	756.53 (11-II-3)	86.12 (11-II-2)
9	2	-0.0 (3)	-0.2 (3)	-0.0 (11-II-2)	64.94 (11-II-3)	1055.23 (11-II-3)	-23.75 (2)
9	3	0.1 (11-II-2)	-0.2 (9)	-0.1 (11-II-2)	175.06 (11-II-3)	1691.99 (11-II-3)	-380.73 (11-II-3)
9	4	0.2 (11-I-2)	-0.7 (11-I-2)	0.1 (11-I-2)	-389.98 (11-I-3)	2709.22 (11-II-3)	-900.58 (11-II-3)
9	5	-0.0 (3)	-0.1 (3)	-0.1 (3)	-83.58 (10)	762.95 (11-II-3)	51.40 (11-II-2)
9	6	-0.1 (3)	-0.1 (3)	-0.1 (3)	-86.80 (10)	889.98 (11-II-3)	-39.50 (2)
9	7	-0.1 (3)	-0.1 (11-I-2)	0.1 (11-II-2)	-128.31 (10)	639.70 (11-II-3)	-100.30 (11-II-3)
9	8	-0.2 (11-II-2)	0.0 (11-I-2)	0.1 (11-II-2)	-322.08 (11-I-3)	-33.19 (11-I-3)	93.82 (11-I-3)
9	9	-0.0 (3)	-0.1 (9)	-0.1 (3)	-84.06 (10)	808.30 (11-II-3)	-52.09 (2)
9	10	-0.1 (3)	-0.1 (9)	-0.1 (3)	-82.82 (10)	892.22 (11-II-3)	-61.36 (10)
9	11	-0.1 (3)	-0.0 (9)	0.1 (11-II-2)	140.32 (11-II-3)	710.04 (11-II-3)	222.93 (11-II-2)
9	12	-0.0 (11-II-2)	-0.0 (11-I-2)	0.0 (11-II-2)	-129.26 (11-I-3)	-47.22 (10)	52.28 (11-II-2)
9	13	-0.0 (3)	-0.1 (9)	-0.1 (3)	102.40 (11-II-3)	844.73 (11-II-3)	-56.56 (2)
9	14	-0.1 (3)	-0.1 (9)	-0.1 (3)	106.80 (11-I-2)	1071.99 (11-II-3)	-64.47 (10)
9	15	-0.2 (11-II-2)	-0.1 (9)	-0.1 (11-I-2)	-15.67 (10)	1590.96 (11-II-3)	340.05 (11-II-2)
9	16	-0.1 (3)	0.9 (11-II-2)	0.1 (11-II-2)	303.68 (11-II-2)	2615.73 (11-II-3)	1333.09 (11-I-2)
10	1	-0.0 (3)	-0.1 (11-II-2)	-0.0 (3)	108.17 (11-II-3)	846.28 (11-II-3)	-60.27 (2)
10	2	-0.1 (3)	-0.2 (11-I-2)	-0.0 (3)	123.55 (11-I-2)	1077.14 (11-II-3)	-57.10 (2)



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
10	3	-0.1 (3)	-0.3 (11-I-2)	-0.1 (11-II-4)	39.26 (11-II-2)	1597.04 (11-II-3)	-355.01 (11-II-3)
10	4	-0.2 (3)	-1.2 (11-II-2)	0.2 (11-II-2)	332.22 (11-I-3)	2617.46 (11-II-3)	-1342.27 (11-II-3)
10	5	-0.0 (3)	-0.1 (11-II-2)	-0.0 (3)	95.95 (11-II-3)	826.02 (11-II-3)	-64.20 (2)
10	6	-0.1 (3)	-0.1 (11-II-2)	0.1 (11-I-4)	110.92 (11-II-4)	916.83 (11-II-3)	-61.21 (2)
10	7	-0.2 (3)	-0.1 (11-II-2)	0.1 (11-II-2)	228.18 (11-I-2)	729.66 (11-II-3)	-212.18 (11-II-3)
10	8	-0.2 (3)	0.0 (11-I-2)	0.0 (11-II-2)	-50.58 (10)	50.71 (11-II-3)	-49.97 (11-II-3)
10	9	-0.0 (3)	-0.1 (9)	-0.0 (3)	96.47 (11-II-3)	822.92 (11-II-3)	-66.48 (2)
10	10	-0.1 (3)	-0.1 (9)	-0.0 (3)	113.78 (11-II-3)	917.23 (11-II-3)	-72.24 (10)
10	11	-0.2 (3)	-0.1 (9)	0.1 (11-II-1)	233.28 (11-II-3)	730.63 (11-II-3)	172.81 (11-I-3)
10	12	-0.2 (3)	-0.0 (11-I-2)	0.0 (11-II-2)	-49.18 (10)	51.18 (11-II-3)	-60.49 (10)
10	13	-0.0 (11-II-2)	-0.1 (9)	-0.0 (3)	111.30 (11-II-4)	839.35 (11-II-4)	-69.44 (2)
10	14	-0.1 (3)	-0.1 (9)	-0.0 (3)	135.45 (11-I-2)	1078.00 (11-II-4)	-75.95 (10)
10	15	-0.2 (11-II-2)	-0.2 (9)	-0.1 (11-I-1)	58.45 (11-II-2)	1600.16 (11-II-4)	320.86 (11-I-3)
10	16	-0.3 (3)	0.9 (11-I-2)	0.1 (11-II-2)	354.15 (11-II-2)	2618.55 (11-I-2)	1322.40 (11-II-2)
11	1	-0.3 (2)	-0.1 (2)	-0.1 (2)	511.88 (10)	42.61 (10)	-59.71 (11-I-1)
11	2	-0.1 (2)	-0.0 (2)	-0.1 (2)	-545.75 (11-II-1)	60.71 (10)	-23.23 (11-I-1)
11	3	-0.1 (9)	-0.0 (2)	-0.1 (2)	-561.50 (11-II-1)	62.48 (10)	13.85 (11-II-1)
11	4	-0.1 (9)	-0.0 (2)	-0.1 (2)	-540.89 (11-II-1)	-74.90 (11-I-1)	16.58 (11-II-2)
11	5	-0.2 (2)	-0.0 (9)	-0.0 (11-II-2)	-625.62 (11-I-1)	21.02 (10)	-49.08 (11-I-1)
11	6	-0.1 (2)	-0.1 (2)	-0.1 (2)	-600.99 (11-I-1)	47.18 (10)	-35.65 (11-I-1)
11	7	-0.1 (9)	-0.1 (2)	-0.1 (2)	-604.67 (11-I-1)	49.58 (10)	14.85 (11-II-1)
11	8	-0.1 (9)	-0.1 (2)	-0.1 (2)	-635.41 (11-I-1)	-105.67 (11-I-1)	29.19 (11-I-2)
11	9	-0.2 (9)	0.1 (11-II-1)	-0.1 (11-II-1)	-861.86 (11-I-1)	-76.49 (11-I-1)	95.37 (11-II-1)
11	10	-0.1 (11-I-1)	-0.1 (2)	0.1 (11-II-1)	-536.48 (11-I-1)	63.63 (10)	35.54 (11-II-1)
11	11	-0.0 (9)	-0.1 (2)	0.1 (11-II-1)	-538.89 (11-I-1)	65.67 (10)	-57.49 (11-I-1)
11	12	-0.1 (9)	-0.2 (11-II-2)	-0.1 (11-I-1)	-852.62 (11-I-1)	-79.58 (11-I-1)	-59.73 (11-I-1)
11	13	-0.7 (11-I-1)	0.2 (11-I-2)	0.1 (11-II-2)	-1480.38 (11-I-1)	38.97 (11-I-2)	596.62 (11-I-1)
11	14	0.0 (11-I-2)	-0.2 (11-II-2)	0.1 (11-II-1)	-84.96 (11-I-1)	81.96 (10)	84.52 (11-II-1)
11	15	-0.0 (11-I-1)	-0.0 (11-II-2)	0.0 (11-II-1)	-94.39 (11-I-1)	81.92 (10)	-101.52 (11-I-1)
11	16	0.9 (11-II-1)	-0.2 (2)	0.1 (11-II-1)	-1453.90 (11-I-1)	-21.79 (11-I-1)	-654.91 (11-I-1)
12	1	-0.1 (11-II-2)	-0.0 (2)	-0.0 (2)	-532.72 (11-II-1)	-76.45 (11-I-1)	8.47 (2)
12	2	-0.1 (11-II-2)	-0.0 (2)	-0.0 (3)	-544.33 (11-II-1)	61.97 (10)	9.64 (10)
12	3	-0.1 (3)	-0.0 (2)	-0.0 (3)	-541.42 (11-II-1)	61.81 (10)	15.93 (11-II-2)
12	4	-0.1 (3)	-0.0 (11-I-1)	-0.0 (3)	-520.17 (11-II-1)	-73.33 (11-I-1)	17.51 (11-II-2)
12	5	-0.2 (11-II-2)	-0.1 (2)	-0.0 (2)	-631.54 (11-I-1)	-115.88 (11-I-1)	7.28 (2)
12	6	-0.1 (11-II-2)	-0.1 (2)	0.1 (11-II-1)	-599.89 (11-I-1)	49.32 (10)	-9.85 (11-I-2)
12	7	-0.1 (9)	-0.1 (2)	0.0 (11-II-1)	-600.15 (11-I-1)	48.73 (10)	19.52 (11-II-2)
12	8	-0.1 (9)	-0.1 (2)	-0.0 (3)	-628.07 (11-I-1)	-108.27 (11-I-1)	26.91 (11-II-2)
12	9	-0.3 (11-II-2)	-0.1 (2)	-0.1 (11-I-2)	-852.01 (11-I-1)	-107.75 (11-I-1)	89.96 (11-II-2)
12	10	-0.1 (11-II-2)	-0.2 (2)	0.1 (11-II-2)	-539.08 (11-I-1)	-90.85 (11-I-1)	56.02 (11-II-2)
12	11	-0.1 (9)	-0.2 (2)	0.1 (11-II-1)	-540.68 (11-I-1)	-73.06 (11-I-1)	-51.40 (11-I-2)
12	12	-0.2 (9)	-0.2 (11-I-1)	-0.1 (11-I-1)	-852.09 (11-I-1)	-86.28 (11-I-1)	-61.00 (11-I-2)
12	13	-1.1 (11-II-2)	-0.2 (2)	0.2 (11-II-2)	-1470.12 (11-I-2)	-158.85 (11-I-1)	725.06 (11-II-2)
12	14	0.0 (11-I-1)	-0.2 (2)	0.0 (11-II-1)	-97.34 (11-I-1)	-120.17 (11-I-1)	98.54 (11-II-2)
12	15	-0.0 (11-I-1)	-0.2 (2)	0.0 (11-II-1)	-94.83 (11-I-1)	-95.21 (11-I-1)	-97.43 (11-I-2)
12	16	0.9 (11-II-1)	-0.3 (2)	0.1 (11-II-1)	-1454.43 (11-II-2)	-30.63 (11-I-1)	-655.03 (11-I-2)
13	1	0.0 (3)	-0.0 (10)	0.0 (2)	72.36 (3)	224.20 (10)	-61.37 (2)
13	2	0.0 (3)	-0.0 (10)	0.0 (2)	117.35 (3)	171.38 (10)	-48.60 (3)
13	3	0.0 (2)	-0.0 (10)	0.0 (2)	97.98 (3)	107.66 (10)	-47.60 (3)
13	4	0.0 (2)	-0.0 (10)	0.0 (2)	32.37 (3)	-124.73 (3)	-61.81 (3)
13	5	0.0 (3)	-0.0 (10)	0.0 (2)	57.58 (2)	258.88 (10)	-96.12 (2)
13	6	0.0 (2)	-0.0 (10)	0.0 (2)	72.42 (3)	182.22 (10)	-168.56 (2)
13	7	0.0 (2)	-0.0 (10)	0.0 (2)	35.40 (3)	103.57 (10)	-168.76 (2)
13	8	0.0 (2)	-0.0 (10)	0.0 (2)	-37.28 (10)	-164.67 (2)	-177.18 (2)
13	9	0.0 (3)	-0.0 (10)	0.0 (2)	-53.00 (3)	187.53 (10)	-90.25 (10)
13	10	0.0 (2)	-0.0 (10)	0.0 (2)	-67.63 (2)	187.42 (10)	-208.81 (2)
13	11	0.0 (2)	-0.0 (10)	0.0 (2)	-110.12 (2)	130.46 (10)	-189.45 (2)
13	12	0.0 (2)	-0.0 (10)	0.0 (2)	-125.38 (2)	-109.19 (2)	-184.87 (2)
13	13	0.0 (3)	-0.0 (10)	0.0 (2)	-323.20 (3)	-129.06 (3)	-173.53 (2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
13	14	0.0 (2)	-0.0 (10)	0.0 (2)	-403.69 (3)	175.45 (10)	-204.49 (2)
13	15	0.0 (2)	-0.0 (10)	0.0 (2)	-349.20 (2)	152.57 (10)	-177.61 (2)
13	16	0.0 (2)	-0.0 (10)	0.0 (2)	-269.99 (2)	-73.01 (3)	-165.86 (2)
14	1	0.0 (2)	0.0 (3)	0.0 (2)	49.72 (2)	-53.03 (3)	-46.56 (3)
14	2	0.0 (2)	0.0 (3)	0.0 (2)	102.92 (2)	-57.09 (3)	-63.83 (3)
14	3	0.0 (2)	0.0 (3)	0.0 (2)	92.15 (2)	-35.12 (3)	-48.02 (3)
14	4	0.0 (2)	0.0 (3)	0.0 (3)	33.15 (2)	-16.58 (10)	-29.38 (2)
14	5	0.0 (2)	0.0 (3)	0.0 (2)	13.26 (9)	68.19 (10)	-104.63 (3)
14	6	0.0 (2)	0.0 (3)	0.0 (2)	20.01 (4)	-71.22 (3)	-126.75 (3)
14	7	0.0 (2)	0.0 (3)	0.0 (2)	-33.31 (3)	-52.10 (3)	-111.06 (2)
14	8	0.0 (2)	0.0 (3)	0.0 (3)	-49.27 (3)	-32.55 (10)	-81.60 (2)
14	9	0.0 (2)	0.0 (2)	0.0 (2)	-108.26 (2)	-104.25 (3)	-112.06 (3)
14	10	0.0 (2)	0.0 (2)	0.0 (2)	-131.44 (2)	-74.61 (2)	-154.50 (3)
14	11	0.0 (2)	0.0 (2)	0.0 (2)	-159.27 (2)	-48.03 (2)	-131.90 (2)
14	12	0.0 (2)	0.0 (3)	0.0 (3)	-151.73 (2)	-28.34 (10)	-99.03 (2)
14	13	0.0 (2)	0.0 (2)	0.0 (2)	-300.62 (2)	-127.41 (3)	-165.17 (2)
14	14	0.0 (2)	0.0 (2)	0.0 (2)	-375.93 (2)	-92.37 (2)	-150.17 (2)
14	15	0.0 (2)	0.0 (2)	0.0 (2)	-336.40 (2)	-55.63 (2)	-120.67 (2)
14	16	0.0 (2)	0.0 (2)	0.0 (3)	-269.56 (2)	-19.26 (10)	-84.71 (2)
15	1	0.0 (2)	0.0 (3)	0.0 (2)	19.37 (2)	83.67 (10)	-49.84 (3)
15	2	0.0 (2)	0.0 (3)	0.0 (2)	8.14 (2)	-133.53 (3)	-92.74 (2)
15	3	0.0 (2)	0.0 (3)	0.0 (2)	-7.46 (2)	110.60 (10)	-96.36 (3)
15	4	0.0 (2)	0.0 (3)	0.0 (3)	-17.26 (2)	-133.49 (3)	-156.45 (2)
15	5	0.0 (2)	0.0 (3)	0.0 (2)	-89.16 (2)	116.40 (10)	-65.84 (3)
15	6	0.0 (2)	0.0 (3)	0.0 (3)	-96.44 (2)	-119.24 (2)	-170.23 (2)
15	7	0.0 (2)	0.0 (3)	0.0 (2)	-260.34 (2)	84.05 (10)	-88.65 (2)
15	8	0.0 (2)	0.0 (3)	0.0 (2)	-273.04 (2)	-155.16 (2)	-142.59 (2)
16	1	0.0 (3)	-0.0 (10)	0.0 (2)	81.10 (3)	80.99 (3)	-48.88 (10)
16	2	0.0 (3)	-0.0 (10)	0.0 (2)	149.44 (3)	194.10 (2)	-63.11 (10)
16	3	0.0 (3)	-0.0 (10)	0.0 (2)	144.36 (3)	217.27 (10)	-37.97 (10)
16	4	0.0 (3)	-0.0 (10)	0.0 (2)	63.69 (3)	134.83 (10)	-41.22 (2)
16	5	0.0 (3)	-0.0 (10)	0.0 (2)	65.59 (2)	75.37 (3)	-88.49 (10)
16	6	0.0 (3)	-0.0 (10)	0.0 (2)	102.98 (3)	231.05 (10)	-112.70 (10)
16	7	0.0 (3)	-0.0 (10)	0.0 (2)	88.47 (3)	240.22 (10)	-87.32 (2)
16	8	0.0 (3)	-0.0 (10)	0.0 (10)	28.62 (3)	100.23 (10)	-137.31 (2)
16	9	0.0 (3)	-0.0 (10)	0.0 (2)	-66.14 (3)	36.34 (3)	-140.71 (10)
16	10	0.0 (3)	-0.0 (10)	0.0 (10)	-75.93 (3)	273.88 (10)	-137.17 (10)
16	11	0.0 (3)	-0.0 (10)	0.0 (10)	-81.23 (3)	263.43 (10)	-68.90 (2)
16	12	0.0 (3)	-0.0 (10)	0.0 (10)	-86.54 (3)	-139.14 (3)	-130.05 (2)
16	13	0.0 (3)	-0.0 (10)	0.0 (10)	-354.45 (3)	92.91 (10)	-203.76 (10)
16	14	0.0 (3)	-0.1 (10)	0.0 (10)	-414.63 (3)	283.33 (10)	-133.96 (10)
16	15	0.0 (3)	-0.1 (10)	0.0 (10)	-420.58 (3)	253.80 (10)	-104.50 (2)
16	16	0.0 (3)	-0.0 (10)	0.0 (10)	-340.24 (3)	-148.26 (3)	-71.51 (2)
17	1	0.1 (3)	-0.1 (10)	0.0 (2)	-364.01 (3)	222.08 (10)	-122.32 (10)
17	2	0.1 (3)	-0.1 (10)	0.0 (2)	-323.75 (3)	434.68 (10)	-101.75 (10)
17	3	0.1 (3)	-0.1 (10)	0.0 (10)	-335.42 (3)	340.90 (10)	60.07 (3)
17	4	0.1 (3)	0.0 (3)	0.0 (2)	-387.75 (3)	-255.93 (3)	-45.00 (2)
17	5	0.1 (3)	-0.1 (10)	0.0 (2)	-396.77 (3)	190.14 (10)	-94.71 (10)
17	6	0.1 (3)	-0.1 (10)	0.0 (2)	-354.22 (3)	514.26 (10)	-119.10 (2)
17	7	0.1 (3)	-0.1 (10)	0.0 (2)	-362.90 (3)	406.57 (10)	-96.44 (2)
17	8	0.1 (3)	-0.0 (10)	0.0 (2)	-434.39 (3)	-365.07 (3)	-120.58 (2)
17	9	0.1 (3)	-0.1 (10)	0.0 (2)	-419.10 (3)	189.25 (10)	-89.40 (2)
17	10	0.1 (3)	-0.1 (10)	0.0 (2)	-385.86 (3)	517.19 (10)	-124.83 (2)
17	11	0.1 (3)	-0.1 (10)	0.0 (2)	-392.43 (3)	409.03 (10)	-133.08 (2)
17	12	0.1 (3)	-0.0 (10)	0.0 (2)	-454.86 (3)	-375.67 (3)	-145.56 (2)
17	13	0.1 (3)	-0.1 (10)	0.0 (2)	-435.76 (3)	219.92 (10)	-73.85 (2)
17	14	0.1 (3)	-0.1 (10)	0.0 (2)	-418.63 (3)	440.60 (10)	-136.58 (2)
17	15	0.1 (3)	-0.1 (10)	0.0 (2)	-424.39 (3)	346.83 (10)	-244.14 (10)
17	16	0.1 (3)	0.0 (3)	0.0 (2)	-453.32 (3)	-282.96 (3)	-221.51 (2)
18	1	0.1 (2)	0.0 (3)	0.0 (2)	-382.99 (2)	134.07 (9)	-161.72 (2)
18	2	0.1 (2)	0.0 (3)	0.0 (2)	-412.49 (2)	-204.39 (3)	-168.40 (2)
18	3	0.1 (2)	0.0 (3)	0.0 (2)	-365.52 (2)	214.44 (10)	-196.34 (2)
18	4	0.1 (2)	0.0 (3)	0.0 (2)	-404.37 (2)	-285.16 (10)	-193.97 (2)
18	5	0.1 (3)	0.0 (3)	0.0 (2)	-363.52 (3)	209.49 (10)	-199.60 (2)
18	6	0.1 (2)	0.0 (3)	0.0 (2)	-386.51 (2)	-286.78 (10)	-197.84 (2)
18	7	0.1 (3)	0.0 (3)	0.0 (2)	-380.13 (3)	123.19 (9)	-219.99 (2)
18	8	0.1 (3)	0.0 (3)	0.0 (2)	-387.82 (3)	-217.54 (3)	-217.23 (2)
19	1	0.1 (2)	0.0 (2)	0.0 (2)	-461.41 (2)	-190.57 (3)	-234.64 (2)
19	2	0.1 (2)	0.0 (2)	0.0 (2)	-522.19 (2)	-95.03 (2)	-241.02 (2)
19	3	0.1 (2)	0.0 (2)	0.0 (2)	-607.84 (2)	-58.73 (9)	-215.53 (2)
19	4	0.1 (2)	0.0 (2)	0.0 (2)	-559.28 (2)	-29.84 (10)	-113.40 (2)
19	5	0.1 (2)	0.0 (2)	0.0 (2)	-411.87 (2)	-244.38 (3)	-230.61 (2)
19	6	0.1 (2)	0.0 (2)	0.0 (2)	-416.12 (2)	-67.66 (2)	-219.07 (2)
19	7	0.1 (2)	0.0 (2)	0.0 (2)	-442.46 (2)	-33.89 (9)	-212.58 (2)
19	8	0.1 (2)	0.0 (2)	0.0 (2)	-429.36 (2)	29.11 (3)	-78.73 (2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
19	9	0.1 (2)	0.0 (2)	0.0 (2)	-374.38 (3)	-248.23 (3)	-222.66 (2)
19	10	0.1 (2)	0.0 (2)	0.0 (2)	-333.01 (3)	-48.22 (2)	-207.24 (2)
19	11	0.1 (2)	0.0 (2)	0.0 (2)	-307.51 (3)	30.91 (3)	-208.12 (2)
19	12	0.1 (2)	0.0 (2)	0.0 (2)	-320.66 (2)	32.26 (3)	-79.55 (2)
19	13	0.1 (2)	0.0 (2)	0.1 (2)	-373.08 (3)	-199.34 (3)	-179.70 (2)
19	14	0.1 (2)	0.0 (2)	0.1 (2)	-342.84 (3)	-53.67 (11-II-4)	-172.80 (10)
19	15	0.1 (2)	0.0 (2)	0.0 (2)	-290.84 (3)	16.16 (10)	-166.99 (2)
19	16	0.1 (2)	0.0 (2)	0.0 (2)	-285.53 (3)	28.19 (2)	-104.45 (2)
20	1	0.1 (3)	0.1 (3)	0.0 (2)	-389.44 (3)	-315.91 (3)	-194.42 (2)
20	2	0.1 (3)	-0.0 (10)	0.0 (2)	-340.12 (3)	233.20 (10)	-238.64 (2)
20	3	0.1 (3)	-0.0 (10)	0.0 (2)	-342.75 (2)	242.19 (10)	-204.23 (2)
20	4	0.1 (2)	-0.0 (10)	0.0 (2)	-365.28 (2)	130.25 (9)	-182.16 (2)
20	5	0.1 (3)	0.0 (3)	0.0 (2)	-431.89 (3)	-410.13 (3)	-156.43 (2)
20	6	0.1 (3)	-0.0 (10)	0.0 (2)	-373.46 (3)	271.38 (10)	-181.08 (2)
20	7	0.1 (3)	-0.0 (10)	0.0 (2)	-357.45 (3)	284.37 (10)	-185.40 (2)
20	8	0.1 (3)	-0.0 (10)	0.0 (2)	-362.68 (2)	124.04 (9)	-186.67 (2)
20	9	0.1 (3)	0.0 (3)	0.0 (2)	-451.87 (3)	-422.48 (3)	-144.61 (2)
20	10	0.1 (3)	-0.0 (10)	0.0 (2)	-403.08 (3)	269.62 (10)	-164.75 (2)
20	11	0.1 (3)	-0.0 (10)	0.0 (2)	-383.89 (3)	284.31 (10)	-176.25 (2)
20	12	0.1 (3)	-0.0 (10)	0.0 (2)	-373.16 (3)	123.33 (9)	-184.37 (2)
20	13	0.1 (3)	0.1 (3)	0.0 (2)	-454.94 (3)	-346.85 (3)	-106.31 (2)
20	14	0.1 (3)	-0.0 (10)	0.0 (2)	-434.62 (3)	227.73 (10)	-102.05 (10)
20	15	0.1 (3)	-0.0 (10)	0.0 (2)	-405.50 (3)	241.27 (10)	-161.05 (10)
20	16	0.1 (3)	-0.0 (10)	0.0 (2)	-386.94 (3)	124.89 (9)	-179.72 (2)
21	1	0.1 (3)	0.0 (2)	0.0 (10)	-340.41 (3)	5.20 (2)	6.62 (11-II-3)
21	2	0.1 (3)	0.0 (3)	0.0 (10)	-341.20 (3)	-6.98 (3)	-66.95 (10)
21	3	0.1 (3)	0.0 (3)	0.0 (10)	-361.07 (3)	4.95 (3)	22.68 (2)
21	4	0.1 (3)	0.0 (3)	0.0 (10)	-364.66 (3)	-9.72 (3)	-84.50 (10)
21	5	0.1 (3)	0.0 (3)	0.0 (10)	-373.81 (3)	5.76 (3)	24.89 (2)
21	6	0.1 (3)	0.0 (3)	0.0 (10)	-377.16 (3)	-10.09 (3)	-86.20 (10)
21	7	0.1 (3)	0.0 (3)	0.0 (2)	-404.26 (3)	1.71 (3)	6.54 (11-II-3)
21	8	0.1 (3)	0.0 (3)	0.0 (10)	-405.63 (3)	-11.71 (3)	-66.19 (2)
22	1	-0.0 (2)	0.0 (10)	0.0 (3)	19.36 (2)	1.97 (10)	10.00 (3)
22	2	-0.0 (2)	-0.0 (10)	0.0 (2)	24.22 (2)	7.59 (2)	-27.98 (3)
22	3	-0.0 (2)	-0.0 (2)	0.0 (2)	20.12 (2)	-2.64 (10)	25.67 (3)
22	4	-0.0 (2)	-0.0 (10)	0.0 (10)	30.32 (2)	16.27 (10)	-81.55 (2)
22	5	0.0 (3)	-0.0 (10)	0.0 (2)	-53.92 (3)	-7.67 (10)	90.54 (3)
22	6	0.0 (3)	-0.0 (10)	0.0 (10)	-39.96 (3)	24.37 (10)	-171.92 (2)
22	7	0.1 (3)	-0.0 (10)	0.0 (10)	-286.97 (3)	3.82 (11-II-3)	32.20 (3)
22	8	0.1 (3)	-0.0 (10)	0.0 (10)	-287.13 (3)	46.33 (10)	-188.63 (10)
23	1	0.1 (3)	0.0 (2)	0.0 (2)	-386.46 (3)	6.20 (2)	3.93 (11-II-3)
23	2	0.1 (3)	0.0 (3)	0.0 (2)	-386.95 (3)	-9.69 (3)	-65.30 (2)
23	3	0.1 (3)	0.0 (3)	0.0 (2)	-405.64 (3)	6.31 (3)	20.92 (2)
23	4	0.1 (3)	0.0 (3)	0.0 (10)	-409.27 (3)	-13.11 (3)	-82.95 (2)
23	5	0.1 (3)	0.0 (3)	0.0 (2)	-412.70 (3)	6.55 (3)	21.69 (2)
23	6	0.1 (3)	0.0 (3)	0.0 (2)	-416.74 (3)	-12.80 (3)	-86.13 (2)
23	7	0.1 (3)	0.0 (3)	0.0 (2)	-433.97 (3)	2.53 (3)	4.26 (11-II-3)
23	8	0.1 (3)	0.0 (3)	0.0 (2)	-435.61 (3)	-13.12 (3)	-65.92 (2)
24	1	0.1 (3)	-0.0 (4)	0.0 (10)	-395.08 (3)	9.93 (3)	14.90 (11-II-2)
24	2	0.1 (3)	-0.0 (9)	0.0 (10)	-405.76 (3)	34.05 (11-II-2)	-91.61 (10)
24	3	0.1 (3)	0.0 (10)	0.0 (10)	-380.58 (3)	-7.63 (11-II-3)	-8.12 (4)
24	4	0.1 (3)	-0.0 (11-II-2)	0.0 (10)	-376.69 (3)	21.40 (11-II-2)	-98.92 (10)
24	5	0.1 (3)	0.0 (3)	0.0 (10)	-354.16 (3)	4.48 (3)	20.02 (11-II-3)
24	6	0.1 (3)	-0.0 (11-II-2)	0.0 (10)	-357.62 (3)	-10.89 (10)	-100.02 (10)
24	7	0.1 (3)	0.0 (3)	0.0 (10)	-360.44 (3)	-2.55 (11-II-3)	10.02 (11-II-2)
24	8	0.1 (3)	0.0 (10)	0.0 (10)	-361.05 (3)	-7.64 (10)	-69.01 (10)
25	1	-0.0 (3)	-0.1 (10)	-0.1 (3)	-104.73 (10)	-800.25 (10)	-12.99 (10)
25	2	-0.1 (3)	-0.2 (11-I-3)	-0.0 (3)	-110.61 (10)	-762.17 (10)	17.23 (11-II-2)
25	3	-0.1 (3)	-0.3 (11-I-3)	-0.1 (11-I-2)	-63.25 (10)	-818.19 (10)	73.26 (10)
25	4	-0.2 (3)	-1.1 (11-I-3)	0.2 (11-II-2)	-17.07 (10)	-1158.15 (10)	554.77 (10)
25	5	-0.0 (3)	-0.1 (11-II-3)	-0.0 (3)	-95.70 (10)	-805.38 (10)	-12.78 (10)
25	6	-0.1 (3)	-0.1 (11-I-3)	0.1 (11-II-3)	-75.01 (10)	-729.08 (10)	-8.70 (10)
25	7	-0.2 (3)	-0.1 (11-I-3)	0.1 (11-II-3)	-107.53 (10)	-559.17 (10)	52.90 (10)
25	8	-0.2 (3)	0.0 (11-I-3)	0.0 (11-II-3)	-136.51 (10)	-106.54 (10)	94.69 (10)
25	9	-0.0 (3)	-0.1 (9)	-0.0 (3)	-95.48 (10)	-802.66 (10)	-12.97 (11-I-2)
25	10	-0.1 (3)	-0.1 (9)	-0.0 (3)	-75.26 (10)	-727.22 (10)	-18.88 (11-I-2)
25	11	-0.2 (3)	-0.1 (9)	0.1 (11-II-3)	-108.18 (10)	-557.99 (10)	-61.63 (10)
25	12	-0.2 (3)	-0.0 (11-I-3)	0.0 (11-II-3)	-137.68 (10)	-106.64 (10)	-96.22 (10)
25	13	-0.0 (3)	-0.1 (9)	-0.0 (3)	-104.06 (10)	-792.22 (10)	-10.57 (11-I-2)
25	14	-0.1 (3)	-0.1 (9)	-0.0 (3)	-111.07 (10)	-756.99 (10)	-14.91 (11-I-2)
25	15	-0.2 (11-II-2)	-0.2 (9)	-0.1 (11-II-3)	82.96 (11-II-3)	-814.81 (10)	-83.29 (10)
25	16	-0.3 (3)	0.9 (11-II-3)	0.1 (11-II-3)	142.92 (11-II-3)	-1155.15 (10)	-554.39 (10)
26	1	-0.1 (3)	-0.3 (3)	-0.1 (3)	-63.71 (10)	-802.73 (10)	58.43 (11-II-4)
26	2	-0.0 (3)	-0.2 (3)	-0.0 (11-II-2)	-32.98 (10)	-771.06 (10)	67.32 (11-I-2)
26	3	0.1 (11-II-3)	-0.2 (9)	-0.1 (11-II-2)	-82.96 (10)	-834.80 (10)	121.35 (10)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
26	4	0.2 (11-I-2)	-0.7 (11-I-3)	0.1 (11-II-3)	-188.11 (11-II-2)	-1185.33 (10)	499.95 (10)
26	5	-0.0 (3)	-0.1 (3)	-0.1 (3)	-91.69 (10)	-814.20 (10)	29.87 (11-I-2)
26	6	-0.1 (3)	-0.1 (3)	-0.1 (3)	-65.90 (10)	-737.57 (10)	46.72 (11-I-2)
26	7	-0.1 (3)	-0.1 (11-I-3)	0.1 (11-II-3)	-94.20 (10)	-562.96 (10)	48.92 (10)
26	8	-0.2 (11-II-2)	0.0 (11-I-2)	0.1 (11-II-3)	-122.95 (10)	-99.40 (10)	90.56 (10)
26	9	-0.0 (3)	-0.1 (9)	-0.1 (3)	-96.05 (10)	-814.95 (10)	-4.88 (2)
26	10	-0.1 (3)	-0.1 (9)	-0.1 (3)	-72.51 (10)	-733.34 (10)	-4.57 (2)
26	11	-0.1 (3)	-0.0 (9)	0.1 (11-II-3)	-103.32 (10)	-561.31 (10)	-63.56 (10)
26	12	-0.0 (3)	-0.0 (11-I-2)	0.0 (11-II-3)	-131.74 (10)	-108.33 (10)	-99.77 (10)
26	13	-0.0 (3)	-0.1 (9)	-0.1 (3)	-105.12 (10)	-803.45 (10)	-8.09 (11-II-2)
26	14	-0.1 (3)	-0.1 (9)	-0.1 (3)	-110.66 (10)	-763.82 (10)	-8.87 (11-II-2)
26	15	-0.2 (11-II-2)	-0.1 (9)	-0.1 (11-I-3)	68.97 (11-I-3)	-818.71 (10)	-83.77 (10)
26	16	-0.2 (3)	0.9 (11-II-3)	0.1 (11-II-3)	126.49 (11-I-3)	-1158.33 (10)	-559.36 (10)
27	1	-0.0 (3)	-0.1 (11-II-3)	-0.0 (3)	-103.85 (10)	-790.70 (10)	-13.04 (10)
27	2	-0.1 (3)	-0.2 (11-II-3)	0.0 (9)	-110.82 (10)	-755.98 (10)	15.56 (11-I-2)
27	3	-0.2 (3)	-0.3 (11-II-3)	0.1 (9)	-65.04 (10)	-814.36 (10)	71.65 (10)
27	4	-0.3 (3)	-1.2 (11-II-3)	0.2 (11-II-3)	-22.63 (10)	-1154.99 (10)	553.24 (10)
27	5	-0.1 (3)	-0.1 (11-II-3)	0.0 (11-I-4)	-94.88 (10)	-797.97 (10)	-13.20 (10)
27	6	-0.1 (3)	-0.1 (11-II-3)	0.1 (11-I-4)	-74.74 (10)	-724.04 (10)	-10.24 (10)
27	7	-0.2 (3)	-0.1 (11-II-3)	0.1 (11-II-2)	-107.71 (10)	-556.44 (10)	50.37 (10)
27	8	-0.2 (3)	0.0 (11-I-3)	0.0 (11-II-3)	-136.97 (10)	-106.21 (10)	92.24 (10)
27	9	-0.1 (3)	-0.1 (9)	0.0 (11-I-4)	-94.77 (10)	-797.31 (10)	-12.58 (11-II-2)
27	10	-0.1 (3)	-0.1 (9)	0.0 (11-I-4)	-74.61 (10)	-723.51 (10)	-18.46 (11-II-2)
27	11	-0.2 (3)	-0.1 (9)	0.1 (11-I-4)	-107.38 (10)	-556.05 (10)	-63.85 (10)
27	12	-0.3 (3)	-0.0 (11-I-3)	0.0 (11-II-3)	-136.71 (10)	-106.20 (10)	-98.22 (10)
27	13	-0.0 (3)	-0.1 (9)	-0.0 (3)	-103.51 (10)	-788.63 (10)	-10.18 (11-II-2)
27	14	-0.1 (3)	-0.1 (9)	-0.0 (11-II-4)	-110.37 (10)	-754.38 (10)	-14.28 (11-II-2)
27	15	-0.2 (11-II-3)	-0.2 (9)	-0.1 (11-II-4)	82.69 (11-I-3)	-813.38 (10)	-84.95 (10)
27	16	-0.3 (3)	0.9 (11-I-3)	0.1 (11-II-3)	141.29 (11-I-3)	-1154.83 (10)	-555.69 (10)
28	1	-0.0 (3)	-0.1 (11-II-2)	0.0 (9)	111.04 (11-I-2)	836.76 (11-I-2)	-69.92 (2)
28	2	-0.1 (3)	-0.2 (11-II-2)	0.0 (9)	135.56 (11-I-2)	1077.04 (11-I-2)	-68.95 (2)
28	3	-0.2 (3)	-0.3 (11-II-2)	0.1 (9)	58.77 (11-II-2)	1600.01 (11-I-2)	-362.89 (11-II-3)
28	4	-0.3 (3)	-1.1 (11-II-2)	0.2 (11-II-2)	354.62 (11-II-2)	2618.56 (11-I-2)	-1346.30 (11-II-3)
28	5	-0.1 (3)	-0.1 (11-II-2)	0.0 (11-I-4)	95.98 (11-I-2)	816.32 (11-I-2)	-71.96 (2)
28	6	-0.1 (3)	-0.1 (11-II-2)	0.1 (11-I-4)	114.64 (11-I-2)	914.86 (11-I-2)	-70.17 (2)
28	7	-0.2 (3)	-0.1 (11-II-2)	0.1 (11-II-2)	235.30 (11-I-2)	730.59 (11-I-2)	-213.98 (11-II-3)
28	8	-0.2 (3)	0.0 (11-I-1)	0.0 (11-II-2)	-46.02 (10)	51.37 (11-I-2)	-51.15 (11-II-3)
28	9	-0.1 (3)	-0.1 (9)	0.0 (11-I-4)	95.88 (11-I-2)	816.33 (11-I-2)	-72.16 (2)
28	10	-0.1 (3)	-0.1 (9)	0.1 (11-I-4)	114.39 (11-I-2)	914.77 (11-I-2)	-78.87 (10)
28	11	-0.2 (3)	-0.1 (9)	0.1 (11-I-4)	235.15 (11-I-2)	730.61 (11-I-2)	174.06 (11-I-3)
28	12	-0.2 (3)	-0.0 (11-I-2)	0.0 (11-II-4)	-45.20 (10)	51.40 (11-I-2)	-64.69 (10)
28	13	-0.0 (3)	-0.1 (9)	-0.0 (3)	110.68 (11-I-2)	835.56 (11-I-2)	-73.76 (2)
28	14	-0.1 (3)	-0.1 (9)	-0.0 (11-II-4)	135.08 (11-I-2)	1076.37 (11-I-2)	-81.26 (10)
28	15	-0.2 (11-I-1)	-0.2 (9)	-0.1 (11-II-4)	58.67 (11-I-2)	1600.00 (11-I-2)	322.74 (11-I-3)
28	16	-0.3 (3)	0.9 (11-I-2)	0.1 (11-I-2)	354.67 (11-I-2)	2618.81 (11-I-2)	1323.71 (11-I-3)
29	1	-0.1 (11-II-2)	-0.0 (2)	0.0 (9)	-516.23 (11-II-1)	-74.51 (11-I-1)	11.79 (10)
29	2	-0.1 (11-I-1)	-0.0 (2)	0.0 (11-I-4)	-532.95 (11-I-4)	61.52 (10)	12.25 (10)
29	3	-0.1 (9)	-0.0 (2)	0.0 (11-I-4)	-534.38 (11-I-4)	61.36 (10)	14.94 (2)
29	4	-0.1 (9)	-0.0 (11-I-1)	0.0 (9)	-516.18 (11-I-4)	-72.65 (11-I-4)	16.45 (11-II-2)
29	5	-0.2 (11-II-2)	-0.1 (2)	0.0 (9)	-624.01 (11-I-1)	-115.24 (11-I-1)	10.26 (10)
29	6	-0.1 (11-II-2)	-0.1 (2)	0.1 (11-II-2)	-593.32 (11-I-4)	48.01 (10)	-13.21 (11-I-2)
29	7	-0.1 (9)	-0.1 (2)	0.0 (11-I-4)	-595.53 (11-I-4)	47.77 (10)	16.66 (11-II-2)
29	8	-0.1 (9)	-0.1 (3)	-0.0 (11-II-4)	-625.21 (11-I-4)	-107.12 (11-I-1)	24.78 (11-II-2)
29	9	-0.3 (11-II-2)	-0.2 (2)	0.1 (9)	-849.77 (11-I-1)	-108.07 (11-I-1)	86.00 (11-II-2)
29	10	-0.1 (11-I-1)	-0.2 (2)	0.1 (11-I-1)	-536.60 (11-II-4)	-88.89 (11-I-1)	51.78 (11-II-2)
29	11	-0.1 (9)	-0.2 (2)	0.1 (11-II-1)	-538.58 (11-II-4)	-70.82 (11-I-1)	-54.57 (11-I-2)
29	12	-0.2 (9)	-0.2 (11-I-1)	-0.1 (11-I-1)	-850.65 (11-II-4)	-84.51 (11-I-1)	-63.30 (11-I-2)
29	13	-1.1 (11-II-2)	-0.3 (2)	0.2 (11-I-1)	-1470.01 (11-II-2)	-160.28 (11-I-1)	722.62 (11-I-1)
29	14	0.0 (11-I-1)	-0.2 (2)	0.0 (11-II-1)	-96.94 (11-II-4)	-118.30 (11-I-1)	95.08 (11-II-2)
29	15	-0.0 (11-II-1)	-0.2 (2)	0.0 (11-II-1)	-94.39 (11-I-4)	-92.57 (11-I-1)	-100.05 (11-I-2)
29	16	0.9 (11-II-1)	-0.3 (3)	0.1 (11-II-1)	-1454.18 (11-I-1)	-27.57 (11-I-1)	-656.71 (11-II-2)
30	1	-0.0 (3)	-0.1 (4)	0.0 (9)	110.66 (11-I-3)	835.38 (11-I-3)	-72.94 (2)
30	2	-0.1 (3)	-0.2 (11-II-2)	0.0 (9)	135.02 (11-I-2)	1076.45 (11-I-3)	-72.38 (2)
30	3	-0.2 (3)	-0.3 (11-II-2)	0.1 (9)	58.45 (11-I-2)	1600.05 (11-I-3)	-360.93 (11-II-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
30	4	-0.3(3)	-1.2(11-II-2)	0.2(11-II-2)	354.43(11-I-2)	2618.78(11-I-3)	-1345.09(11-I-2)
30	5	-0.1(3)	-0.1(10)	0.0(11-I-4)	95.86(11-I-3)	816.61(11-I-3)	-74.02(2)
30	6	-0.1(3)	-0.1(11-I-1)	0.1(11-II-2)	114.23(11-I-3)	915.11(11-I-3)	-72.43(2)
30	7	-0.2(3)	-0.1(11-I-1)	0.1(11-II-2)	234.72(11-I-3)	730.78(11-I-3)	-212.16(11-I-2)
30	8	-0.3(3)	0.0(11-I-4)	0.0(11-II-2)	-43.70(10)	51.41(11-I-3)	-49.96(11-I-2)
30	9	-0.1(3)	-0.1(9)	0.0(11-I-4)	95.95(11-I-3)	817.82(11-I-3)	-73.32(2)
30	10	-0.1(3)	-0.1(9)	0.1(11-I-4)	114.14(11-I-3)	915.75(11-I-3)	-81.31(10)
30	11	-0.2(3)	-0.1(9)	0.1(11-I-4)	234.71(11-I-2)	731.14(11-I-3)	174.81(11-I-3)
30	12	-0.3(3)	-0.0(11-II-1)	0.0(11-I-4)	-43.15(10)	51.51(11-I-3)	-66.13(10)
30	13	-0.0(3)	-0.1(9)	0.0(9)	110.85(11-I-3)	837.81(11-I-3)	-74.10(2)
30	14	-0.1(3)	-0.1(9)	-0.0(11-II-4)	134.84(11-I-2)	1077.92(11-I-3)	-82.95(10)
30	15	-0.2(11-II-4)	-0.2(9)	-0.1(11-II-4)	58.60(11-II-3)	1601.04(11-I-3)	323.44(11-II-2)
30	16	-0.3(3)	0.9(11-II-1)	0.1(11-II-1)	354.78(11-II-3)	2619.31(11-I-3)	1324.18(11-I-3)
31	1	-0.1(10)	-0.0(3)	0.0(9)	-514.27(11-I-4)	-74.17(11-I-4)	12.43(10)
31	2	-0.1(11-I-1)	-0.1(3)	0.0(11-II-2)	-532.39(11-I-4)	61.24(10)	12.52(10)
31	3	-0.1(9)	-0.1(3)	0.0(11-II-2)	-534.45(11-I-4)	61.18(10)	14.43(2)
31	4	-0.1(9)	-0.0(3)	0.0(9)	-516.60(11-I-4)	-72.66(11-I-4)	15.96(11-I-2)
31	5	-0.2(11-I-1)	-0.1(3)	0.0(9)	-622.49(11-I-4)	-114.49(11-I-1)	11.01(10)
31	6	-0.1(11-I-1)	-0.1(3)	0.1(11-II-2)	-592.65(11-I-4)	47.52(10)	-13.84(11-II-2)
31	7	-0.1(9)	-0.1(3)	0.1(11-I-4)	-595.33(11-I-4)	47.44(10)	15.68(11-I-2)
31	8	-0.1(9)	-0.1(3)	-0.0(11-II-4)	-625.29(11-I-4)	-106.95(11-II-4)	24.02(11-I-2)
31	9	-0.3(11-I-1)	-0.2(3)	0.1(9)	-848.97(11-II-4)	-106.98(11-I-1)	83.65(11-II-1)
31	10	-0.1(11-I-1)	-0.2(3)	0.1(11-I-1)	-536.13(11-I-4)	-88.11(11-II-4)	50.12(11-II-1)
31	11	-0.1(9)	-0.2(3)	0.1(11-I-1)	-538.37(11-I-4)	-70.39(11-II-4)	-55.21(11-II-2)
31	12	-0.2(9)	-0.2(11-I-1)	-0.1(11-I-1)	-850.63(11-I-4)	-84.06(11-I-1)	-63.81(11-II-2)
31	13	-1.2(11-I-1)	-0.3(3)	0.2(11-I-1)	-1469.94(11-I-1)	-158.72(11-I-1)	721.02(11-I-1)
31	14	0.0(11-I-1)	-0.2(3)	0.0(11-II-1)	-96.79(11-I-4)	-117.20(11-II-4)	93.64(11-I-1)
31	15	-0.0(11-II-1)	-0.2(3)	0.0(11-II-1)	-94.32(11-I-4)	-91.97(11-II-4)	-100.65(11-II-2)
31	16	0.9(11-II-1)	-0.3(3)	0.1(11-II-1)	-1454.78(11-I-1)	-27.02(11-I-1)	-657.43(11-II-2)
32	1	0.1(3)	0.0(2)	0.0(2)	-389.50(2)	-202.08(3)	-242.05(2)
32	2	0.1(3)	0.0(2)	0.0(2)	-410.37(2)	-59.99(2)	-263.73(2)
32	3	0.1(3)	0.0(11-I-4)	0.0(2)	-473.69(2)	-26.53(9)	-236.30(2)
32	4	0.1(3)	0.0(11-I-4)	0.0(2)	-430.71(2)	-17.60(10)	-129.16(2)
32	5	0.1(3)	0.0(2)	0.0(2)	-379.60(3)	-257.83(3)	-218.07(2)
32	6	0.1(3)	0.0(2)	0.0(2)	-338.03(3)	-46.60(11-I-4)	-215.31(2)
32	7	0.1(3)	0.0(11-I-4)	0.0(2)	-343.81(2)	33.30(3)	-220.66(2)
32	8	0.1(3)	0.0(11-II-4)	0.0(2)	-326.48(2)	31.39(3)	-92.63(2)
32	9	0.1(3)	0.0(2)	0.0(2)	-378.50(3)	-259.56(3)	-205.49(2)
32	10	0.1(3)	0.0(2)	0.0(2)	-331.99(3)	-44.84(11-I-4)	-194.37(2)
32	11	0.1(3)	0.0(11-I-4)	0.0(2)	-306.39(3)	36.75(3)	-207.97(2)
32	12	0.1(3)	0.0(11-I-4)	0.0(2)	-300.59(3)	35.35(2)	-88.31(2)
32	13	0.1(3)	0.0(2)	0.1(2)	-366.50(3)	-205.84(3)	-161.10(10)
32	14	0.1(3)	0.0(2)	0.1(2)	-328.41(3)	-52.37(11-I-4)	-160.46(10)
32	15	0.1(3)	0.0(11-I-4)	0.0(2)	-281.44(3)	26.94(2)	-165.26(10)
32	16	0.1(3)	0.0(11-I-4)	0.0(2)	-281.32(3)	30.62(2)	-104.62(2)
33	1	0.1(3)	0.0(3)	0.0(2)	-370.27(3)	114.55(9)	-171.60(2)
33	2	0.1(3)	0.0(3)	0.0(2)	-378.81(3)	-220.93(2)	-170.78(2)
33	3	0.1(3)	0.0(3)	0.0(2)	-367.00(3)	194.84(10)	-199.15(2)
33	4	0.1(3)	0.0(3)	0.0(2)	-388.96(3)	-286.10(10)	-185.20(2)
33	5	0.1(3)	0.0(3)	0.0(2)	-368.64(3)	192.94(10)	-197.71(2)
33	6	0.1(3)	0.0(3)	0.0(2)	-389.92(3)	-285.83(10)	-187.16(2)
33	7	0.1(3)	0.0(3)	0.0(2)	-376.41(3)	110.42(9)	-212.57(2)
33	8	0.1(3)	0.0(3)	0.0(2)	-383.38(3)	-225.75(3)	-205.17(2)
34	1	0.1(3)	-0.1(10)	0.0(2)	-402.90(3)	221.85(10)	-120.98(10)
34	2	0.1(3)	-0.1(10)	0.0(2)	-368.03(3)	443.56(10)	-107.25(9)
34	3	0.1(3)	-0.1(10)	0.0(2)	-380.93(3)	344.07(10)	74.79(3)
34	4	0.1(3)	0.0(3)	0.0(2)	-426.96(3)	-286.94(3)	-44.89(2)
34	5	0.1(3)	-0.1(10)	0.0(2)	-421.79(3)	189.17(10)	-96.37(2)
34	6	0.1(3)	-0.1(10)	0.0(2)	-379.35(3)	525.27(10)	-122.04(2)
34	7	0.1(3)	-0.1(10)	0.0(2)	-387.25(3)	411.20(10)	-103.92(2)
34	8	0.1(3)	-0.0(10)	0.0(2)	-458.58(3)	-397.83(3)	-121.90(2)
34	9	0.1(3)	-0.1(10)	0.0(2)	-431.34(3)	188.90(10)	-92.78(2)
34	10	0.1(3)	-0.1(10)	0.0(2)	-392.23(3)	526.95(10)	-127.68(2)
34	11	0.1(3)	-0.1(10)	0.0(2)	-397.19(3)	412.80(10)	-141.50(2)
34	12	0.1(3)	-0.0(10)	0.0(2)	-464.88(3)	-403.69(3)	-147.10(2)
34	13	0.1(3)	-0.1(10)	0.0(2)	-434.60(3)	220.83(10)	-73.77(2)
34	14	0.1(3)	-0.1(10)	0.0(2)	-407.20(3)	447.20(10)	-140.48(2)
34	15	0.1(3)	-0.1(10)	0.0(2)	-410.76(3)	348.49(10)	-252.89(2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
34	16	0.1 (3)	0.0 (3)	0.0 (2)	-448.07 (3)	-302.08 (3)	-228.08 (2)
35	1	0.1 (3)	0.1 (3)	0.0 (2)	-429.03 (3)	-352.01 (3)	-205.47 (2)
35	2	0.1 (3)	-0.0 (10)	0.0 (2)	-387.19 (3)	220.15 (10)	-253.49 (2)
35	3	0.1 (3)	-0.0 (10)	0.0 (2)	-367.88 (3)	234.11 (10)	-220.33 (2)
35	4	0.1 (3)	-0.0 (10)	0.0 (2)	-371.04 (3)	122.51 (9)	-191.51 (2)
35	5	0.1 (3)	0.0 (3)	0.0 (2)	-455.67 (3)	-448.28 (3)	-164.18 (2)
35	6	0.1 (3)	0.0 (3)	0.0 (2)	-396.76 (3)	258.24 (10)	-180.81 (2)
35	7	0.1 (3)	-0.0 (10)	0.0 (2)	-378.53 (3)	277.82 (10)	-187.30 (2)
35	8	0.1 (3)	-0.0 (10)	0.0 (2)	-373.82 (3)	122.82 (9)	-183.48 (2)
35	9	0.1 (3)	0.0 (3)	0.0 (2)	-461.58 (3)	-455.24 (3)	-148.82 (2)
35	10	0.1 (3)	0.0 (3)	0.0 (2)	-405.97 (3)	256.85 (10)	-159.16 (2)
35	11	0.1 (3)	-0.0 (10)	0.0 (2)	-386.09 (3)	278.11 (10)	-171.40 (2)
35	12	0.1 (3)	-0.0 (10)	0.0 (2)	-377.55 (3)	123.08 (9)	-176.04 (2)
35	13	0.1 (3)	0.1 (3)	0.0 (2)	-449.46 (3)	-369.73 (3)	-100.76 (2)
35	14	0.1 (3)	-0.0 (10)	0.1 (2)	-417.82 (3)	216.61 (10)	-95.88 (10)
35	15	0.1 (3)	-0.0 (10)	0.0 (2)	-390.33 (3)	234.63 (10)	-155.73 (10)
35	16	0.1 (3)	-0.0 (10)	0.0 (2)	-381.38 (3)	119.99 (9)	-168.54 (10)
36	1	0.1 (3)	0.0 (2)	0.0 (2)	-417.23 (3)	6.31 (2)	2.13 (11-I-2)
36	2	0.1 (3)	0.0 (3)	0.0 (2)	-418.66 (3)	-11.18 (3)	-63.47 (2)
36	3	0.1 (3)	0.0 (3)	0.0 (2)	-427.14 (3)	6.77 (3)	16.82 (2)
36	4	0.1 (3)	0.0 (3)	0.0 (2)	-431.33 (3)	-13.98 (3)	-79.27 (2)
36	5	0.1 (3)	0.0 (3)	0.0 (2)	-428.47 (3)	6.84 (3)	17.70 (2)
36	6	0.1 (3)	0.0 (3)	0.0 (2)	-432.96 (3)	-13.73 (3)	-82.07 (2)
36	7	0.1 (3)	0.0 (3)	0.0 (2)	-440.86 (3)	3.14 (3)	2.61 (11-I-2)
36	8	0.1 (3)	0.0 (3)	0.0 (2)	-442.55 (3)	-13.60 (2)	-62.83 (2)
37	1	-0.0 (3)	-0.1 (4)	0.0 (9)	-103.47 (10)	-788.39 (10)	-13.26 (10)
37	2	-0.1 (3)	-0.2 (11-II-3)	0.0 (9)	-110.26 (10)	-754.19 (10)	15.82 (11-II-2)
37	3	-0.2 (3)	-0.3 (11-II-3)	0.1 (9)	-64.20 (10)	-813.34 (10)	70.52 (10)
37	4	-0.3 (3)	-1.2 (11-II-3)	0.2 (11-II-3)	-21.56 (10)	-1154.73 (10)	552.34 (10)
37	5	-0.1 (3)	-0.1 (11-II-3)	0.0 (11-II-2)	-94.63 (10)	-796.51 (10)	-13.28 (10)
37	6	-0.1 (3)	-0.1 (11-II-3)	0.1 (11-II-2)	-74.33 (10)	-722.84 (10)	-10.69 (10)
37	7	-0.2 (3)	-0.1 (11-II-3)	0.1 (11-II-2)	-107.08 (10)	-555.71 (10)	49.67 (10)
37	8	-0.3 (3)	0.0 (11-I-4)	0.0 (11-II-3)	-136.16 (10)	-106.02 (10)	91.58 (10)
37	9	-0.1 (3)	-0.1 (9)	0.0 (11-II-2)	-94.61 (10)	-796.39 (10)	-12.41 (11-I-2)
37	10	-0.1 (3)	-0.1 (9)	0.1 (11-I-4)	-74.33 (10)	-722.71 (10)	-18.14 (11-I-2)
37	11	-0.2 (3)	-0.1 (9)	0.1 (11-I-4)	-106.93 (10)	-555.55 (10)	-64.25 (10)
37	12	-0.3 (3)	-0.0 (11-I-3)	0.0 (11-II-4)	-136.13 (10)	-106.07 (10)	-98.60 (10)
37	13	-0.0 (3)	-0.1 (9)	0.0 (9)	-103.41 (10)	-788.04 (10)	-10.05 (11-I-2)
37	14	-0.1 (3)	-0.1 (9)	-0.0 (11-II-4)	-110.19 (10)	-753.86 (10)	-14.05 (11-I-2)
37	15	-0.2 (11-II-3)	-0.2 (9)	-0.1 (11-II-4)	82.32 (11-II-3)	-813.05 (10)	-85.13 (10)
37	16	-0.3 (3)	0.9 (11-I-3)	0.1 (11-I-3)	141.02 (11-II-3)	-1154.74 (10)	-555.85 (10)
38	1	-0.0 (3)	-0.1 (10)	0.0 (9)	-103.34 (10)	-787.69 (10)	-12.53 (10)
38	2	-0.1 (3)	-0.2 (11-II-4)	0.0 (9)	-110.03 (10)	-753.61 (10)	16.43 (11-I-3)
38	3	-0.2 (3)	-0.3 (11-II-4)	0.1 (9)	-63.84 (10)	-812.98 (10)	71.08 (10)
38	4	-0.3 (3)	-1.1 (11-II-4)	0.2 (11-II-4)	-21.11 (10)	-1154.63 (10)	552.72 (10)
38	5	-0.1 (3)	-0.1 (4)	0.0 (11-II-3)	-94.52 (10)	-795.94 (10)	-12.45 (10)
38	6	-0.1 (3)	-0.1 (11-II-4)	0.1 (11-II-3)	-74.14 (10)	-722.37 (10)	-9.93 (10)
38	7	-0.2 (3)	-0.1 (11-II-4)	0.1 (11-I-4)	-106.79 (10)	-555.42 (10)	50.39 (10)
38	8	-0.3 (3)	0.0 (11-II-4)	0.0 (11-I-1)	-135.78 (10)	-105.94 (10)	92.16 (10)
38	9	-0.1 (3)	-0.1 (9)	0.0 (11-II-3)	-94.51 (10)	-795.88 (10)	-12.32 (11-II-3)
38	10	-0.1 (3)	-0.1 (9)	0.1 (11-II-3)	-74.16 (10)	-722.30 (10)	-18.18 (11-II-3)
38	11	-0.2 (3)	-0.1 (9)	0.1 (11-II-2)	-106.66 (10)	-555.30 (10)	-63.38 (10)
38	12	-0.3 (3)	-0.0 (11-II-2)	0.0 (11-II-2)	-135.80 (10)	-106.00 (10)	-97.89 (10)
38	13	-0.0 (3)	-0.1 (9)	0.0 (9)	-103.30 (10)	-787.50 (10)	-9.92 (11-II-3)
38	14	-0.1 (3)	-0.1 (9)	-0.0 (11-I-3)	-110.00 (10)	-753.45 (10)	-14.08 (11-II-3)
38	15	-0.2 (11-II-4)	-0.2 (9)	-0.1 (11-I-2)	82.41 (11-II-3)	-812.82 (10)	-84.13 (10)
38	16	-0.3 (3)	0.9 (11-I-4)	0.1 (11-I-4)	141.59 (11-II-3)	-1154.68 (10)	-555.13 (10)
39	1	-0.0 (3)	-0.1 (4)	0.0 (9)	110.79 (11-I-4)	836.69 (11-I-3)	-69.32 (2)
39	2	-0.1 (3)	-0.2 (11-II-4)	0.0 (9)	135.06 (11-II-2)	1077.29 (11-I-3)	-69.04 (2)
39	3	-0.2 (3)	-0.3 (11-II-4)	0.1 (9)	58.55 (11-II-3)	1600.64 (11-I-3)	-360.06 (11-I-3)
39	4	-0.3 (3)	-1.1 (11-II-4)	0.2 (11-II-4)	354.68 (11-II-3)	2619.11 (11-I-3)	-1344.94 (11-I-3)
39	5	-0.1 (3)	-0.1 (10)	0.0 (11-II-2)	95.95 (11-I-4)	817.05 (11-I-4)	-69.22 (2)
39	6	-0.1 (3)	-0.1 (11-II-4)	0.1 (11-II-2)	114.35 (11-I-4)	915.36 (11-I-4)	-67.90 (2)
39	7	-0.2 (3)	-0.1 (11-II-4)	0.1 (11-I-1)	234.86 (11-I-4)	730.91 (11-I-4)	-211.43 (11-I-3)
39	8	-0.2 (3)	0.0 (11-II-4)	0.0 (11-II-4)	-41.17 (10)	51.43 (11-I-4)	-49.58 (11-I-3)
39	9	-0.1 (3)	-0.1 (9)	0.0 (11-II-2)	95.99 (11-I-4)	817.60 (11-I-4)	-67.47 (2)
39	10	-0.1 (3)	-0.1 (9)	0.1 (11-II-2)	114.30 (11-I-4)	915.53 (11-I-4)	-79.21 (10)
39	11	-0.2 (3)	-0.1 (9)	0.1 (11-II-2)	234.90 (11-I-4)	730.97 (11-I-4)	177.22 (11-II-3)
39	12	-0.2 (3)	-0.0 (11-I-4)	0.0 (11-I-4)	-40.91 (10)	51.47 (11-I-4)	-65.04 (10)
39	13	-0.0 (3)	-0.1 (9)	0.0 (9)	110.84 (11-I-4)	836.93 (11-I-4)	-67.35 (2)
39	14	-0.1 (3)	-0.1 (9)	-0.0 (11-I-2)	134.97 (11-II-2)	1077.22 (11-I-4)	-80.04 (10)
39	15	-0.2 (11-II-4)	-0.2 (9)	-0.1 (11-I-2)	58.33 (11-II-4)	1600.47 (11-I-4)	326.02 (11-II-3)
39	16	-0.3 (3)	0.9 (11-I-4)	0.1 (11-I-4)	354.36 (11-II-4)	2618.98 (11-I-4)	1325.41 (11-II-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
40	1	-0.0(3)	-0.1(4)	0.0(9)	-103.40(10)	-788.01(10)	-13.12(10)
40	2	-0.1(3)	-0.2(11-II-3)	0.0(9)	-110.13(10)	-753.84(10)	15.93(11-II-2)
40	3	-0.2(3)	-0.3(11-II-3)	0.1(9)	-64.00(10)	-813.11(10)	70.49(10)
40	4	-0.3(3)	-1.2(11-II-3)	0.2(11-II-3)	-21.30(10)	-1154.67(10)	552.29(10)
40	5	-0.1(3)	-0.1(11-II-3)	0.0(11-II-2)	-94.59(10)	-796.26(10)	-13.10(10)
40	6	-0.1(3)	-0.1(11-II-3)	0.1(11-II-2)	-74.25(10)	-722.61(10)	-10.58(10)
40	7	-0.2(3)	-0.1(11-II-3)	0.1(11-II-3)	-106.95(10)	-555.56(10)	49.74(10)
40	8	-0.3(3)	0.0(11-II-4)	0.0(11-II-3)	-135.97(10)	-105.97(10)	91.62(10)
40	9	-0.1(3)	-0.1(9)	0.0(11-II-2)	-94.58(10)	-796.20(10)	-12.29(11-II-2)
40	10	-0.1(3)	-0.1(9)	0.1(11-II-2)	-74.27(10)	-722.55(10)	-17.93(11-II-2)
40	11	-0.2(3)	-0.1(9)	0.1(11-II-4)	-106.83(10)	-555.44(10)	-64.11(10)
40	12	-0.3(3)	-0.0(11-I-3)	0.0(11-I-4)	-136.00(10)	-106.04(10)	-98.49(10)
40	13	-0.0(3)	-0.1(9)	0.0(9)	-103.37(10)	-787.87(10)	-9.96(11-I-3)
40	14	-0.1(3)	-0.1(9)	-0.0(11-I-2)	-110.13(10)	-753.72(10)	-13.89(11-I-3)
40	15	-0.2(11-II-4)	-0.2(9)	-0.1(11-II-4)	82.25(11-II-3)	-812.97(10)	-84.94(10)
40	16	-0.3(3)	0.9(11-I-3)	0.1(11-I-3)	141.53(11-II-3)	-1154.72(10)	-555.72(10)
41	1	-0.1(10)	-0.0(3)	0.0(9)	-515.12(11-I-2)	-74.24(11-I-4)	11.84(10)
41	2	-0.1(2)	-0.1(3)	0.0(11-II-2)	-533.09(11-I-2)	61.12(10)	11.78(10)
41	3	-0.1(9)	-0.0(3)	0.0(11-II-2)	-534.98(11-I-4)	61.11(10)	13.25(11-I-2)
41	4	-0.1(9)	-0.0(3)	0.0(9)	-516.96(11-I-4)	-72.70(11-I-4)	15.31(11-I-2)
41	5	-0.2(11-I-1)	-0.1(3)	0.0(9)	-622.93(11-II-4)	-114.38(11-I-4)	-11.11(11-II-2)
41	6	-0.1(11-I-1)	-0.1(3)	0.1(11-II-2)	-593.06(11-II-4)	47.33(10)	-14.63(11-II-2)
41	7	-0.1(9)	-0.1(3)	0.1(11-II-2)	-595.67(11-II-4)	47.31(10)	14.92(11-I-2)
41	8	-0.1(9)	-0.1(3)	-0.0(11-I-2)	-625.58(11-II-4)	-106.92(11-II-4)	23.35(11-I-2)
41	9	-0.3(11-I-1)	-0.2(3)	0.1(9)	-849.22(11-II-4)	-106.28(11-II-2)	82.70(11-I-2)
41	10	-0.1(11-I-1)	-0.2(3)	0.1(11-I-1)	-536.33(11-II-4)	-88.04(11-I-4)	49.29(11-I-2)
41	11	-0.1(9)	-0.2(3)	0.1(11-I-2)	-538.53(11-II-4)	-70.37(11-II-2)	-55.87(11-II-2)
41	12	-0.2(9)	-0.2(11-II-4)	-0.1(11-I-2)	-850.81(11-II-4)	-84.02(11-I-1)	-64.46(11-II-2)
41	13	-1.1(11-I-1)	-0.3(3)	0.2(11-I-1)	-1469.50(11-I-1)	-157.47(11-II-2)	719.67(11-II-4)
41	14	0.0(11-I-1)	-0.2(3)	0.0(11-II-4)	-96.82(11-II-4)	-117.08(11-I-4)	92.95(11-I-2)
41	15	-0.0(11-I-4)	-0.2(3)	0.0(11-II-1)	-94.36(11-II-4)	-91.96(11-II-2)	-101.15(11-II-2)
41	16	0.9(11-II-1)	-0.3(3)	0.1(11-II-1)	-1453.57(11-II-4)	-27.60(11-I-1)	-657.62(11-II-4)
42	1	-0.0(3)	-0.1(4)	0.0(9)	110.86(11-I-3)	837.59(11-I-3)	-72.40(2)
42	2	-0.1(3)	-0.2(11-I-1)	0.0(9)	134.92(11-I-4)	1077.96(11-I-3)	-71.97(2)
42	3	-0.2(3)	-0.3(11-I-1)	0.1(9)	58.52(11-II-3)	1601.07(11-I-3)	-360.30(11-I-2)
42	4	-0.3(3)	-1.2(11-I-1)	0.2(11-I-1)	354.70(11-II-3)	2619.29(11-I-3)	-1344.91(11-I-3)
42	5	-0.1(3)	-0.1(10)	0.0(11-II-2)	96.04(11-I-3)	818.23(11-I-3)	-72.75(2)
42	6	-0.1(3)	-0.1(11-I-1)	0.1(11-II-2)	114.29(11-I-3)	916.18(11-I-3)	-71.29(2)
42	7	-0.2(3)	-0.1(11-I-1)	0.1(11-II-2)	234.78(11-I-4)	731.35(11-I-3)	-211.65(11-I-2)
42	8	-0.3(3)	0.0(11-II-4)	0.0(11-I-1)	-42.15(10)	51.52(11-I-3)	-49.65(11-I-2)
42	9	-0.1(3)	-0.1(9)	0.0(11-II-2)	96.08(11-I-3)	818.64(11-I-3)	-71.40(2)
42	10	-0.1(3)	-0.1(9)	0.1(11-II-2)	114.29(11-I-3)	916.23(11-I-3)	-81.12(10)
42	11	-0.2(3)	-0.1(9)	0.1(11-I-4)	234.85(11-I-3)	731.34(11-I-3)	175.87(11-II-2)
42	12	-0.3(3)	-0.0(11-II-1)	0.0(11-I-4)	-41.75(10)	51.54(11-I-3)	-66.07(10)
42	13	-0.0(3)	-0.1(9)	0.0(9)	110.89(11-I-3)	837.77(11-I-3)	-71.60(2)
42	14	-0.1(3)	-0.1(9)	-0.0(11-I-2)	135.00(11-II-2)	1077.82(11-I-3)	-82.25(10)
42	15	-0.2(11-II-4)	-0.2(9)	-0.1(11-II-4)	58.49(11-II-3)	1600.88(11-I-3)	324.62(11-II-2)
42	16	-0.3(3)	0.9(11-I-4)	0.1(11-I-4)	354.61(11-II-3)	2619.18(11-I-3)	1324.56(11-II-2)
43	1	0.1(3)	0.0(3)	0.0(2)	-374.17(3)	-209.04(3)	-233.37(2)
43	2	0.1(3)	0.0(11-I-4)	0.0(10)	-347.64(3)	-56.60(11-I-4)	-259.95(2)
43	3	0.1(3)	0.0(11-I-4)	0.0(2)	-379.03(2)	-12.72(9)	-233.01(2)
43	4	0.1(3)	-0.0(10)	0.0(2)	-341.71(2)	13.80(3)	-127.73(2)
43	5	0.1(3)	0.0(2)	0.0(2)	-376.42(3)	-265.59(3)	-201.14(2)
43	6	0.1(3)	0.0(11-I-4)	0.0(2)	-334.13(3)	-47.19(11-I-4)	-200.17(2)
43	7	0.1(3)	0.0(11-I-4)	0.0(2)	-321.29(3)	36.79(3)	-209.31(2)
43	8	0.1(3)	0.0(11-I-4)	0.0(2)	-311.12(3)	32.92(3)	-91.86(2)
43	9	0.1(3)	0.0(2)	0.0(2)	-369.53(3)	-266.01(3)	-186.74(2)
43	10	0.1(3)	0.0(2)	0.0(2)	-320.67(3)	-44.40(11-I-4)	-176.25(2)
43	11	0.1(3)	0.0(11-I-4)	0.0(2)	-296.21(3)	40.25(2)	-193.48(2)
43	12	0.1(3)	0.0(11-I-4)	0.0(2)	-291.22(3)	37.81(2)	-85.61(2)
43	13	0.1(3)	0.0(3)	0.0(2)	-352.36(3)	-209.64(3)	-150.74(10)
43	14	0.1(3)	0.0(11-I-4)	0.1(2)	-310.74(3)	-51.22(11-I-4)	-149.33(10)



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
43	15	0.1(3)	0.0(11-I-4)	0.0(2)	-270.03(3)	30.62(2)	-157.78(10)
43	16	0.1(3)	0.0(11-I-4)	0.0(2)	-272.31(3)	30.62(2)	-96.96(2)
44	1	0.1(3)	-0.1(10)	0.0(2)	-419.31(3)	221.80(10)	-119.07(10)
44	2	0.1(3)	-0.1(10)	0.0(2)	-389.62(3)	446.95(10)	-111.81(9)
44	3	0.1(3)	-0.1(10)	0.0(2)	-401.43(3)	342.71(10)	88.58(3)
44	4	0.1(3)	0.0(3)	0.0(2)	-440.56(3)	-305.54(3)	47.20(3)
44	5	0.1(3)	-0.1(10)	0.0(2)	-426.89(3)	188.93(10)	-96.47(2)
44	6	0.1(3)	-0.1(10)	0.0(2)	-385.26(3)	530.04(10)	-120.94(2)
44	7	0.1(3)	-0.1(10)	0.0(2)	-391.80(3)	410.89(10)	-105.41(2)
44	8	0.1(3)	-0.0(10)	0.0(2)	-461.30(3)	-416.41(3)	-118.51(2)
44	9	0.1(3)	-0.1(10)	0.0(2)	-427.12(3)	188.93(10)	-92.46(2)
44	10	0.1(3)	-0.1(10)	0.0(2)	-384.32(3)	531.33(10)	-126.34(2)
44	11	0.1(3)	-0.1(10)	0.0(2)	-388.22(3)	412.34(10)	-142.80(2)
44	12	0.1(3)	-0.0(10)	0.0(2)	-458.49(3)	-419.15(3)	-143.27(2)
44	13	0.1(3)	-0.1(10)	0.0(2)	-421.32(3)	221.28(10)	-71.39(2)
44	14	0.1(3)	-0.1(10)	0.0(9)	-387.10(3)	449.94(10)	-139.73(2)
44	15	0.1(3)	-0.1(10)	0.0(2)	-390.21(3)	347.08(10)	-255.97(2)
44	16	0.1(3)	0.0(3)	0.0(2)	-432.73(3)	-312.48(3)	-226.89(2)
45	1	0.1(3)	0.1(3)	0.0(2)	-441.54(3)	-373.86(3)	-206.65(2)
45	2	0.1(3)	-0.0(10)	0.0(10)	-405.75(3)	207.51(10)	-254.95(2)
45	3	0.1(3)	-0.0(10)	0.0(10)	-383.16(3)	226.15(10)	-220.67(2)
45	4	0.1(3)	-0.0(10)	0.0(2)	-377.99(3)	116.48(9)	-186.58(2)
45	5	0.1(3)	0.0(3)	0.0(2)	-457.40(3)	-470.13(3)	-162.49(2)
45	6	0.1(3)	0.0(3)	0.0(2)	-398.81(3)	245.99(10)	-172.18(2)
45	7	0.1(3)	-0.0(10)	0.0(2)	-379.67(3)	271.32(10)	-178.01(2)
45	8	0.1(3)	-0.0(10)	0.0(2)	-372.19(3)	121.67(9)	-171.47(2)
45	9	0.1(3)	0.1(3)	0.0(2)	-454.71(3)	-473.52(3)	-144.73(2)
45	10	0.1(3)	0.0(3)	0.0(2)	-395.12(3)	245.43(10)	-147.64(2)
45	11	0.1(3)	-0.0(10)	0.0(2)	-375.15(3)	272.04(10)	-158.52(2)
45	12	0.1(3)	-0.0(10)	0.0(2)	-368.24(3)	122.18(9)	-161.78(2)
45	13	0.1(3)	0.1(3)	0.0(2)	-434.06(3)	-382.45(3)	-95.55(10)
45	14	0.1(3)	0.0(3)	0.0(2)	-395.48(3)	206.47(10)	-87.03(10)
45	15	0.1(3)	-0.0(10)	0.0(2)	-369.22(3)	228.12(10)	-146.25(10)
45	16	0.1(3)	-0.0(10)	0.0(2)	-366.44(3)	115.67(9)	-161.24(10)
46	1	0.1(3)	0.0(3)	0.0(2)	-374.99(3)	104.03(9)	-164.09(2)
46	2	0.1(3)	0.0(3)	0.0(2)	-383.13(3)	-229.29(2)	-160.89(2)
46	3	0.1(3)	0.0(3)	0.0(2)	-363.96(3)	184.71(10)	-188.22(2)
46	4	0.1(3)	0.0(3)	0.0(2)	-385.47(3)	-285.50(10)	-171.11(2)
46	5	0.1(3)	0.0(3)	0.0(2)	-359.94(3)	183.85(10)	-185.02(2)
46	6	0.1(3)	0.0(3)	0.0(2)	-381.32(3)	-285.31(10)	-172.47(2)
46	7	0.1(3)	0.0(3)	0.0(2)	-363.12(3)	102.28(9)	-198.29(2)
46	8	0.1(3)	0.0(3)	0.0(2)	-369.76(3)	-230.38(2)	-189.61(2)
47	1	-0.0(3)	-0.1(4)	0.0(9)	110.76(11-I-4)	836.13(11-I-4)	-64.75(2)
47	2	-0.1(3)	-0.2(11-II-4)	0.0(9)	135.00(11-II-2)	1076.88(11-I-4)	-64.61(2)
47	3	-0.2(3)	-0.3(11-II-4)	0.1(9)	58.34(11-II-4)	1600.32(11-I-4)	-359.51(11-I-3)
47	4	-0.3(3)	-1.1(11-II-4)	0.2(11-II-4)	354.37(11-II-4)	2618.92(11-I-4)	-1344.37(11-I-3)
47	5	-0.1(3)	-0.1(10)	0.0(11-I-1)	95.85(11-I-4)	816.25(11-I-4)	-64.43(2)
47	6	-0.1(3)	-0.1(11-II-4)	0.1(11-I-1)	114.29(11-II-2)	914.81(11-I-4)	-63.23(2)
47	7	-0.2(3)	-0.1(11-II-4)	0.1(11-II-4)	234.86(11-II-2)	730.63(11-I-4)	-210.82(11-I-3)
47	8	-0.2(3)	0.0(11-II-4)	0.0(11-I-4)	-40.64(10)	51.38(11-I-4)	-49.20(11-I-3)
47	9	-0.1(3)	-0.1(9)	0.0(11-I-1)	95.84(11-I-4)	816.17(11-I-4)	-62.47(2)
47	10	-0.1(3)	-0.1(9)	0.1(11-I-1)	114.24(11-I-4)	914.52(11-I-4)	-76.34(10)
47	11	-0.2(3)	-0.1(9)	0.1(11-II-2)	234.86(11-II-2)	730.42(11-II-2)	178.92(11-II-3)
47	12	-0.2(3)	-0.0(11-II-2)	0.0(11-II-2)	-40.45(10)	51.36(11-II-2)	-63.45(10)
47	13	-0.0(3)	-0.1(9)	0.0(9)	110.71(11-II-2)	835.79(11-II-2)	-62.19(2)
47	14	-0.1(3)	-0.1(9)	-0.0(11-II-1)	134.96(11-II-2)	1076.41(11-II-2)	-77.00(10)
47	15	-0.2(11-II-4)	-0.2(9)	-0.1(11-I-2)	58.33(11-I-2)	1599.97(11-II-2)	327.59(11-II-3)
47	16	-0.3(3)	0.9(11-I-4)	0.1(11-I-4)	354.28(11-I-2)	2618.77(11-II-2)	1326.21(11-II-3)
48	1	-0.1(10)	-0.0(3)	0.0(9)	-514.82(11-I-4)	-74.21(11-I-4)	12.26(10)
48	2	-0.1(11-I-1)	-0.1(3)	0.0(11-II-2)	-532.93(11-I-4)	61.14(10)	12.24(10)
48	3	-0.1(9)	-0.1(3)	0.0(11-II-2)	-534.93(11-I-4)	61.11(10)	13.52(2)
48	4	-0.1(9)	-0.0(3)	0.0(9)	-517.01(11-I-2)	-72.70(11-I-4)	15.57(11-II-2)
48	5	-0.2(11-I-1)	-0.1(3)	0.0(9)	-622.73(11-I-4)	-114.39(11-II-4)	10.89(10)
48	6	-0.1(11-I-1)	-0.1(3)	0.1(11-II-2)	-592.92(11-I-4)	47.37(10)	-14.18(11-I-1)
48	7	-0.1(9)	-0.1(3)	0.1(11-II-2)	-595.59(11-I-4)	47.33(10)	15.11(11-II-1)
48	8	-0.1(9)	-0.1(3)	-0.0(11-I-2)	-625.54(11-I-4)	-106.96(11-I-4)	23.51(11-II-2)
48	9	-0.3(11-I-1)	-0.2(3)	0.1(9)	-849.05(11-I-4)	-106.46(11-I-1)	82.99(11-II-1)
48	10	-0.1(11-I-1)	-0.2(3)	0.1(11-I-1)	-536.23(11-I-4)	-88.05(11-II-4)	49.54(11-II-1)
48	11	-0.1(9)	-0.2(3)	0.1(11-I-4)	-538.48(11-II-4)	-70.38(11-I-4)	-55.37(11-I-2)



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
48	12	-0.2 (9)	-0.2 (11-II-4)	-0.1 (11-II-4)	-850.80 (11-II-4)	-84.02 (11-I-1)	-63.96 (11-I-2)
48	13	-1.2 (11-I-1)	-0.3 (3)	0.2 (11-I-1)	-1470.41 (11-I-1)	-157.44 (11-II-4)	720.52 (11-I-1)
48	14	0.0 (11-I-1)	-0.2 (3)	0.0 (11-II-1)	-96.80 (11-I-4)	-117.10 (11-II-4)	93.15 (11-I-1)
48	15	-0.0 (11-II-1)	-0.2 (3)	0.0 (11-II-1)	-94.34 (11-II-4)	-91.96 (11-I-4)	-100.75 (11-I-2)
48	16	0.9 (11-II-1)	-0.3 (3)	0.1 (11-II-1)	-1454.07 (11-I-1)	-27.39 (11-I-1)	-657.52 (11-I-1)
49	1	-0.1 (10)	-0.0 (3)	0.0 (9)	-515.04 (11-I-4)	-74.23 (11-I-4)	11.39 (10)
49	2	-0.1 (2)	-0.0 (3)	0.0 (11-I-1)	-533.05 (11-I-4)	61.13 (10)	11.33 (10)
49	3	-0.1 (9)	-0.0 (3)	0.0 (11-I-1)	-534.99 (11-II-2)	61.13 (10)	12.97 (11-II-1)
49	4	-0.1 (9)	-0.0 (3)	0.0 (9)	-517.07 (11-II-2)	-72.71 (11-II-2)	15.04 (11-I-2)
49	5	-0.2 (11-II-4)	-0.1 (3)	0.0 (9)	-622.95 (11-I-4)	-114.34 (11-I-4)	-11.55 (11-I-1)
49	6	-0.1 (11-II-4)	-0.1 (3)	0.1 (11-I-1)	-593.07 (11-I-4)	47.35 (10)	-15.05 (11-I-1)
49	7	-0.1 (9)	-0.1 (3)	0.1 (11-I-1)	-595.70 (11-I-4)	47.34 (10)	14.72 (11-II-1)
49	8	-0.1 (9)	-0.1 (3)	-0.0 (11-II-1)	-625.63 (11-II-2)	-106.92 (11-II-4)	23.11 (11-I-2)
49	9	-0.3 (11-II-4)	-0.2 (3)	0.1 (9)	-849.22 (11-II-4)	-106.36 (11-II-1)	82.59 (11-II-1)
49	10	-0.1 (11-II-4)	-0.2 (3)	0.1 (11-II-4)	-536.33 (11-II-4)	-88.02 (11-I-4)	49.16 (11-II-1)
49	11	-0.1 (9)	-0.2 (3)	0.1 (11-II-2)	-538.53 (11-I-4)	-70.38 (11-II-4)	-56.25 (11-I-1)
49	12	-0.2 (9)	-0.2 (11-II-4)	-0.1 (11-I-2)	-850.78 (11-I-4)	-83.92 (11-I-1)	-64.79 (11-II-2)
49	13	-1.1 (11-II-4)	-0.3 (3)	0.2 (11-I-2)	-1469.08 (11-II-4)	-157.68 (11-II-1)	719.45 (11-I-2)
49	14	0.0 (11-I-1)	-0.2 (3)	0.0 (11-II-1)	-96.82 (11-I-4)	-117.07 (11-I-4)	92.83 (11-II-1)
49	15	-0.0 (11-I-1)	-0.2 (3)	0.0 (11-II-1)	-94.36 (11-II-4)	-91.96 (11-II-4)	-101.44 (11-II-1)
49	16	0.9 (11-I-4)	-0.2 (3)	0.1 (11-I-4)	-1453.16 (11-II-2)	-27.33 (11-I-1)	-657.47 (11-II-4)
50	1	0.1 (3)	0.0 (3)	0.0 (10)	-364.61 (3)	-212.78 (3)	-218.54 (2)
50	2	0.1 (3)	0.0 (11-I-4)	0.0 (10)	-338.34 (3)	-57.49 (11-I-4)	-246.78 (2)
50	3	0.1 (3)	0.0 (11-I-4)	0.0 (10)	-332.58 (3)	13.15 (3)	-219.32 (2)
50	4	0.1 (3)	-0.0 (10)	0.0 (2)	-319.21 (3)	15.12 (3)	-119.78 (2)
50	5	0.1 (3)	0.0 (2)	0.0 (2)	-364.04 (3)	-269.73 (3)	-182.47 (2)
50	6	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-321.09 (3)	-47.18 (11-I-4)	-182.79 (2)
50	7	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-306.06 (3)	38.78 (3)	-191.92 (2)
50	8	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-295.75 (3)	33.90 (3)	-86.28 (2)
50	9	0.1 (3)	0.0 (2)	0.0 (2)	-355.28 (3)	-269.53 (3)	-167.66 (2)
50	10	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-305.93 (3)	-43.90 (11-I-4)	-158.10 (2)
50	11	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-283.17 (3)	43.10 (2)	-175.19 (2)
50	12	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-278.29 (3)	38.08 (2)	-79.45 (2)
50	13	0.1 (3)	0.0 (2)	0.0 (2)	-336.85 (3)	-211.95 (3)	-141.67 (10)
50	14	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-294.86 (3)	-50.48 (11-I-4)	-140.07 (10)
50	15	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-260.91 (3)	30.15 (2)	-149.04 (10)
50	16	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-263.27 (3)	29.27 (2)	-90.84 (10)
51	1	0.1 (3)	0.0 (2)	0.0 (2)	-427.18 (3)	6.26 (2)	-2.54 (9)
51	2	0.1 (3)	0.0 (3)	0.0 (2)	-429.09 (3)	-11.91 (3)	-60.20 (2)
51	3	0.1 (3)	0.0 (3)	0.0 (2)	-429.37 (3)	6.98 (3)	13.84 (2)
51	4	0.1 (3)	0.0 (3)	0.0 (2)	-433.76 (3)	-14.19 (3)	-74.70 (2)
51	5	0.1 (3)	0.0 (2)	0.0 (2)	-427.11 (3)	6.98 (3)	15.02 (2)
51	6	0.1 (3)	0.0 (3)	0.0 (2)	-431.74 (3)	-14.14 (3)	-77.67 (2)
51	7	0.1 (3)	0.0 (3)	0.0 (2)	-433.02 (3)	3.63 (3)	1.75 (11-I-2)
51	8	0.1 (3)	0.0 (3)	0.0 (2)	-434.72 (3)	-13.90 (2)	-59.54 (2)
52	1	0.1 (3)	0.0 (2)	0.0 (10)	-349.35 (3)	-215.28 (2)	-202.48 (2)
52	2	0.1 (3)	0.0 (11-I-4)	0.0 (10)	-322.13 (3)	-57.62 (11-I-4)	-231.20 (2)
52	3	0.1 (3)	0.0 (11-I-4)	0.0 (10)	-309.51 (3)	14.67 (3)	-202.66 (2)
52	4	0.1 (3)	-0.0 (10)	0.0 (2)	-297.16 (3)	16.36 (3)	-109.89 (2)
52	5	0.1 (3)	0.0 (2)	0.0 (2)	-348.80 (3)	-271.72 (3)	-164.21 (2)
52	6	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-305.25 (3)	-46.87 (11-I-4)	-165.92 (2)
52	7	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-288.42 (3)	39.56 (3)	-173.35 (2)
52	8	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-278.60 (3)	34.53 (3)	-79.57 (2)
52	9	0.1 (3)	0.0 (2)	0.0 (2)	-340.38 (3)	-271.27 (3)	-149.60 (2)
52	10	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-291.67 (3)	-43.48 (11-I-4)	-141.25 (2)
52	11	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-270.93 (3)	43.32 (2)	-156.53 (2)
52	12	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-265.74 (3)	37.48 (2)	-72.65 (2)
52	13	0.1 (3)	0.0 (2)	0.0 (2)	-322.67 (3)	-213.33 (3)	-134.15 (10)
52	14	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-282.09 (3)	-50.12 (11-I-4)	-132.33 (10)
52	15	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-255.12 (3)	28.06 (2)	-140.49 (10)
52	16	0.1 (3)	0.0 (11-I-4)	0.0 (2)	-256.33 (3)	27.38 (2)	-85.96 (10)
53	1	0.1 (3)	0.0 (3)	0.0 (2)	-366.22 (3)	97.54 (4)	-150.04 (2)
53	2	0.1 (3)	0.0 (3)	0.0 (2)	-374.12 (3)	-234.70 (2)	-146.89 (2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
53	3	0.1(3)	0.0(3)	0.0(2)	-351.59(3)	178.61(10)	-172.16(2)
53	4	0.1(3)	0.0(3)	0.0(2)	-372.94(3)	-286.49(10)	-156.35(2)
53	5	0.1(3)	0.0(3)	0.0(2)	-345.29(3)	177.98(10)	-168.52(2)
53	6	0.1(3)	0.0(3)	0.0(2)	-366.85(3)	-286.72(10)	-157.88(2)
53	7	0.1(3)	0.0(3)	0.0(2)	-346.95(3)	96.14(9)	-189.62(10)
53	8	0.1(3)	0.0(3)	0.0(2)	-353.68(3)	-235.24(2)	-181.05(10)
54	1	0.1(3)	-0.1(10)	0.0(2)	-419.02(3)	221.94(10)	-118.06(9)
54	2	0.1(3)	-0.1(10)	0.0(2)	-392.09(3)	448.69(10)	-114.19(9)
54	3	0.1(3)	-0.1(10)	0.0(2)	-401.82(3)	340.55(10)	103.20(3)
54	4	0.1(3)	0.0(3)	0.0(2)	-436.83(3)	-315.66(3)	62.88(3)
54	5	0.1(3)	-0.1(10)	0.0(2)	-419.54(3)	188.94(10)	-92.89(2)
54	6	0.1(3)	-0.1(10)	0.0(2)	-378.27(3)	532.54(10)	-116.11(2)
54	7	0.1(3)	-0.1(10)	0.0(2)	-383.54(3)	409.09(10)	-101.34(2)
54	8	0.1(3)	0.0(3)	0.0(2)	-451.84(3)	-426.22(3)	-111.99(2)
54	9	0.1(3)	-0.1(10)	0.0(2)	-414.32(3)	188.84(10)	-88.51(2)
54	10	0.1(3)	-0.1(10)	0.0(2)	-369.49(3)	533.34(10)	-121.24(2)
54	11	0.1(3)	-0.1(10)	0.0(2)	-373.07(3)	410.07(10)	-138.49(2)
54	12	0.1(3)	0.0(3)	0.0(2)	-444.62(3)	-427.12(3)	-136.51(2)
54	13	0.1(3)	-0.1(10)	0.0(9)	-403.31(3)	221.04(10)	-66.70(2)
54	14	0.1(3)	-0.1(10)	0.0(9)	-365.63(3)	450.32(10)	-135.13(2)
54	15	0.1(3)	-0.1(10)	-0.0(3)	-369.72(3)	343.60(10)	-253.10(2)
54	16	0.1(3)	0.0(3)	0.0(2)	-414.79(3)	-317.73(3)	-221.19(2)
55	1	0.1(3)	0.1(3)	0.0(2)	-436.89(3)	-385.83(3)	-200.79(2)
55	2	0.1(3)	0.0(3)	0.0(10)	-404.21(3)	197.99(10)	-248.66(2)
55	3	0.1(3)	-0.0(10)	0.0(10)	-379.85(3)	220.22(10)	-212.58(2)
55	4	0.1(3)	-0.0(10)	0.0(2)	-370.48(3)	111.81(9)	-175.59(2)
55	5	0.1(3)	0.1(3)	0.0(2)	-447.25(3)	-481.63(3)	-154.20(2)
55	6	0.1(3)	0.0(3)	0.0(2)	-388.78(3)	236.37(10)	-160.29(2)
55	7	0.1(3)	-0.0(10)	0.0(2)	-369.22(3)	265.88(10)	-164.89(2)
55	8	0.1(3)	-0.0(10)	0.0(2)	-360.49(3)	119.51(9)	-157.79(2)
55	9	0.1(3)	0.1(3)	0.0(2)	-440.55(3)	-482.87(3)	-135.15(2)
55	10	0.1(3)	0.0(3)	0.0(2)	-379.00(3)	235.85(10)	-134.55(2)
55	11	0.1(3)	-0.0(10)	0.0(2)	-359.12(3)	266.32(10)	-143.87(2)
55	12	0.1(3)	-0.0(10)	0.0(2)	-353.16(3)	119.69(9)	-147.38(2)
55	13	0.1(3)	0.1(3)	0.0(2)	-416.18(3)	-388.85(3)	-88.86(10)
55	14	0.1(3)	0.0(3)	0.0(2)	-374.37(3)	196.91(10)	78.80(3)
55	15	0.1(3)	-0.0(10)	0.0(2)	-349.01(3)	221.35(10)	-136.93(10)
55	16	0.1(3)	-0.0(10)	0.0(2)	-349.25(3)	110.88(9)	-153.68(10)
56	1	0.1(3)	0.0(2)	0.0(2)	-423.35(3)	6.23(2)	-2.52(9)
56	2	0.1(3)	0.0(2)	0.0(2)	-425.50(3)	-12.40(3)	-56.94(2)
56	3	0.1(3)	0.0(3)	0.0(2)	-420.17(3)	7.10(2)	12.41(10)
56	4	0.1(3)	0.0(3)	0.0(2)	-424.65(3)	-14.25(3)	-70.46(2)
56	5	0.1(3)	0.0(2)	0.0(2)	-416.26(3)	7.06(3)	14.25(10)
56	6	0.1(3)	0.0(3)	0.0(2)	-420.92(3)	-14.35(3)	-73.61(2)
56	7	0.1(3)	0.0(3)	0.0(2)	-417.77(3)	4.04(3)	1.28(11-I-2)
56	8	0.1(3)	0.0(3)	0.0(2)	-419.51(3)	-14.14(2)	-56.38(2)
57	1	0.1(3)	0.1(3)	0.0(10)	-424.27(3)	-391.42(3)	-191.28(2)
57	2	0.1(3)	0.0(3)	0.0(10)	-392.80(3)	190.24(10)	-239.33(2)
57	3	0.1(3)	-0.0(10)	0.0(10)	-367.49(3)	215.24(10)	-201.56(2)
57	4	0.1(3)	-0.0(10)	0.0(10)	-356.63(3)	107.67(4)	-163.28(2)
57	5	0.1(3)	0.1(3)	0.0(2)	-432.52(3)	-486.44(3)	-142.29(2)
57	6	0.1(3)	0.0(3)	0.0(2)	-374.15(3)	227.60(10)	-148.22(2)
57	7	0.1(3)	0.0(3)	0.0(2)	-354.46(3)	260.44(10)	-151.71(2)
57	8	0.1(3)	-0.0(10)	0.0(2)	-345.42(3)	116.49(4)	-145.59(2)
57	9	0.1(3)	0.1(3)	0.0(2)	-424.46(3)	-486.28(3)	-122.63(2)
57	10	0.1(3)	0.0(3)	0.0(2)	-362.30(3)	226.09(10)	-122.17(2)
57	11	0.1(3)	0.0(3)	0.0(2)	-342.67(3)	259.81(10)	-130.88(10)
57	12	0.1(3)	-0.0(10)	0.0(2)	-337.25(3)	115.99(4)	-135.22(2)
57	13	0.1(3)	0.1(2)	0.0(2)	-398.81(3)	-390.84(3)	-81.37(10)
57	14	0.1(3)	0.0(3)	0.0(2)	-356.00(3)	185.90(10)	97.83(3)
57	15	0.1(3)	-0.0(10)	0.0(2)	-331.50(3)	213.07(10)	-128.99(10)
57	16	0.1(3)	-0.0(10)	0.0(2)	-333.00(3)	105.18(4)	-147.55(10)
58	1	0.1(3)	0.0(3)	0.0(2)	-351.86(3)	-95.60(3)	-134.29(2)
58	2	0.1(3)	0.0(3)	0.0(2)	-359.68(3)	-238.91(2)	-132.74(2)
58	3	0.1(3)	0.0(2)	0.0(2)	-336.30(3)	173.66(10)	-155.11(2)
58	4	0.1(3)	0.0(3)	0.0(2)	-357.73(3)	-288.94(10)	-143.30(2)
58	5	0.1(3)	0.0(2)	0.0(2)	-329.67(3)	172.75(10)	-151.63(2)
58	6	0.1(3)	0.0(2)	0.0(2)	-351.47(3)	-289.56(10)	-145.33(2)
58	7	0.1(3)	0.0(2)	0.0(2)	-331.29(3)	-95.50(3)	-181.77(10)
58	8	0.1(3)	0.0(2)	0.0(2)	-338.33(3)	-239.77(2)	-175.91(10)
59	1	0.1(3)	0.0(2)	0.0(2)	-412.67(3)	6.23(2)	-2.07(3)
59	2	0.1(3)	0.0(2)	0.0(2)	-414.91(3)	-12.78(3)	-53.77(2)
59	3	0.1(3)	0.0(3)	0.0(2)	-405.76(3)	7.26(2)	12.93(10)
59	4	0.1(3)	0.0(3)	0.0(2)	-410.31(3)	-14.25(3)	-66.47(2)
59	5	0.1(3)	0.0(2)	0.0(2)	-401.40(3)	7.18(2)	14.95(10)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
59	6	0.1(3)	0.0(3)	0.0(2)	-406.05(3)	-14.45(3)	-69.67(2)
59	7	0.1(3)	0.0(3)	0.0(2)	-399.63(3)	4.40(3)	1.54(10)
59	8	0.1(3)	0.0(3)	0.0(2)	-401.40(3)	-14.38(2)	-53.17(2)
60	1	0.1(3)	-0.1(10)	0.0(2)	-409.85(3)	222.40(10)	-118.40(9)
60	2	0.1(3)	-0.1(10)	0.0(2)	-383.99(3)	450.00(10)	-113.99(9)
60	3	0.1(3)	-0.1(10)	0.0(2)	-391.42(3)	338.29(10)	118.35(3)
60	4	0.1(3)	0.0(3)	0.0(2)	-424.71(3)	-320.47(3)	78.93(3)
60	5	0.1(3)	-0.1(10)	0.0(2)	-406.39(3)	189.15(10)	-85.92(2)
60	6	0.1(3)	-0.1(10)	0.0(2)	-365.28(3)	533.84(10)	-108.11(2)
60	7	0.1(3)	-0.1(10)	0.0(2)	-369.62(3)	406.18(10)	-93.31(2)
60	8	0.1(3)	0.0(3)	0.0(2)	-437.42(3)	-432.78(2)	-104.16(2)
60	9	0.1(3)	-0.1(10)	0.0(2)	-398.13(3)	188.56(10)	-81.17(2)
60	10	0.1(3)	-0.1(10)	0.0(2)	-352.48(3)	533.53(10)	-113.01(2)
60	11	0.1(3)	-0.0(10)	0.0(2)	-356.38(3)	405.84(10)	-130.37(2)
60	12	0.1(3)	0.0(3)	0.0(2)	-428.58(3)	-435.28(2)	-128.68(2)
60	13	0.1(3)	-0.1(10)	0.0(9)	-384.00(3)	219.99(10)	-59.86(2)
60	14	0.1(3)	-0.1(10)	0.0(9)	-345.03(3)	448.27(10)	-127.59(2)
60	15	0.1(3)	-0.1(10)	-0.0(3)	-351.00(3)	337.33(10)	-246.43(2)
60	16	0.1(3)	0.0(3)	0.0(9)	-397.22(3)	-323.05(2)	-213.18(2)
61	1	-0.0(3)	-0.1(10)	0.0(9)	-103.37(10)	-787.87(10)	-12.87(10)
61	2	-0.1(3)	-0.2(11-II-4)	0.0(9)	-110.08(10)	-753.73(10)	16.16(11-II-3)
61	3	-0.2(3)	-0.3(11-II-4)	0.1(9)	-63.92(10)	-813.05(10)	70.72(10)
61	4	-0.3(3)	-1.2(11-II-4)	0.2(11-II-4)	-21.21(10)	-1154.65(10)	552.46(10)
61	5	-0.1(3)	-0.1(11-II-4)	0.0(11-II-2)	-94.56(10)	-796.13(10)	-12.83(10)
61	6	-0.1(3)	-0.1(11-II-4)	0.1(11-II-2)	-74.20(10)	-722.50(10)	-10.31(10)
61	7	-0.2(3)	-0.1(11-II-4)	0.1(11-II-3)	-106.88(10)	-555.50(10)	50.00(10)
61	8	-0.3(3)	0.0(11-II-4)	0.0(11-II-4)	-135.89(10)	-105.96(10)	91.84(10)
61	9	-0.1(3)	-0.1(9)	0.0(11-II-2)	-94.55(10)	-796.06(10)	-12.30(11-I-3)
61	10	-0.1(3)	-0.1(9)	0.1(11-II-2)	-74.22(10)	-722.44(10)	-17.98(11-I-3)
61	11	-0.2(3)	-0.1(9)	0.1(11-II-2)	-106.76(10)	-555.38(10)	-63.81(10)
61	12	-0.3(3)	-0.0(11-I-4)	0.0(11-I-4)	-135.92(10)	-106.02(10)	-98.25(10)
61	13	-0.0(3)	-0.1(9)	0.0(9)	-103.34(10)	-787.72(10)	-9.94(11-I-3)
61	14	-0.1(3)	-0.1(9)	-0.0(11-I-2)	-110.08(10)	-753.62(10)	-13.98(11-I-3)
61	15	-0.2(11-II-4)	-0.2(9)	-0.1(11-I-2)	82.40(11-I-3)	-812.91(10)	-84.61(10)
61	16	-0.3(3)	0.9(11-I-4)	0.1(11-I-4)	141.78(11-I-3)	-1154.70(10)	-555.48(10)
62	1	-0.0(3)	-0.1(4)	0.0(11-II-4)	-103.01(10)	-786.18(10)	-10.08(10)
62	2	-0.1(3)	-0.2(11-I-3)	0.0(9)	-109.51(10)	-752.62(10)	16.55(11-II-4)
62	3	-0.2(3)	-0.3(11-I-3)	0.1(9)	-63.13(10)	-812.43(10)	73.69(10)
62	4	-0.3(3)	-1.2(11-I-3)	0.2(11-I-3)	-20.29(10)	-1154.51(10)	554.63(10)
62	5	-0.1(3)	-0.1(4)	0.0(11-II-4)	-94.17(10)	-794.29(10)	-9.66(10)
62	6	-0.1(3)	-0.1(11-I-3)	0.1(11-II-4)	-73.58(10)	-721.29(10)	9.10(11-II-4)
62	7	-0.2(3)	-0.1(11-I-3)	0.1(11-I-2)	-106.01(10)	-554.83(10)	53.28(10)
62	8	-0.2(3)	0.0(11-I-3)	0.0(11-II-2)	-134.88(10)	-105.80(10)	94.52(10)
62	9	-0.0(3)	-0.1(9)	0.0(11-II-4)	-94.16(10)	-794.23(10)	-11.86(11-I-4)
62	10	-0.1(3)	-0.1(9)	0.1(11-II-4)	-73.57(10)	-721.15(10)	-17.68(11-I-4)
62	11	-0.2(3)	-0.1(9)	0.1(11-II-4)	-105.86(10)	-554.69(10)	-60.19(10)
62	12	-0.2(3)	-0.0(11-I-2)	0.0(11-II-3)	-134.83(10)	-105.85(10)	-95.29(10)
62	13	-0.0(3)	-0.1(9)	-0.0(4)	-102.91(10)	-785.70(10)	-9.46(11-I-4)
62	14	-0.1(3)	-0.1(9)	-0.0(4)	-109.36(10)	-752.26(10)	-13.53(11-I-4)
62	15	-0.2(11-I-3)	-0.2(9)	-0.1(11-I-4)	83.23(11-II-3)	-812.19(10)	-80.62(10)
62	16	-0.3(3)	0.9(11-II-3)	0.1(11-II-3)	143.38(11-II-3)	-1154.53(10)	-552.57(10)
63	1	-0.1(10)	-0.0(3)	0.0(11-II-4)	-515.29(11-II-2)	-74.24(11-II-2)	10.42(10)
63	2	-0.1(11-II-1)	-0.0(3)	0.0(11-II-4)	-533.16(11-II-2)	61.13(10)	10.37(10)
63	3	-0.1(9)	-0.0(3)	0.0(11-II-4)	-534.92(11-II-2)	61.10(10)	12.28(11-I-4)
63	4	-0.1(9)	-0.0(3)	0.0(11-II-4)	-516.81(11-II-2)	-72.68(11-II-2)	14.39(11-I-4)
63	5	-0.2(11-II-1)	-0.1(3)	0.0(9)	-623.11(11-II-2)	-114.32(11-I-2)	-12.10(11-I-4)
63	6	-0.1(11-II-1)	-0.1(3)	0.1(11-II-4)	-593.15(11-II-2)	47.35(10)	-15.56(11-I-1)
63	7	-0.1(9)	-0.1(3)	0.1(11-II-4)	-595.69(11-II-2)	47.29(10)	13.95(11-II-1)
63	8	-0.1(9)	-0.1(3)	-0.0(11-I-4)	-625.54(11-II-2)	-106.97(11-II-1)	22.34(11-I-4)
63	9	-0.3(11-II-1)	-0.1(3)	0.1(9)	-849.36(11-I-2)	-106.37(11-II-1)	81.87(11-II-4)
63	10	-0.1(11-II-1)	-0.2(3)	0.1(11-II-1)	-536.41(11-II-2)	-87.98(11-I-2)	48.36(11-I-4)
63	11	-0.1(9)	-0.2(3)	0.1(11-I-1)	-538.57(11-II-2)	-70.37(11-I-2)	-56.85(11-II-1)
63	12	-0.2(9)	-0.2(11-II-1)	-0.1(11-II-1)	-850.84(11-II-2)	-84.30(11-II-1)	-65.34(11-II-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
63	13	-1.2 (11-II-1)	-0.2 (3)	0.2 (11-II-1)	-1470.62 (11-II-1)	-157.38 (11-II-1)	719.86 (11-II-1)
63	14	0.0 (11-II-1)	-0.2 (3)	0.0 (11-II-1)	-96.83 (11-II-2)	-117.01 (11-II-2)	92.22 (11-I-4)
63	15	-0.0 (11-I-1)	-0.2 (3)	0.0 (11-II-1)	-94.37 (11-II-2)	-91.97 (11-I-2)	-101.98 (11-II-1)
63	16	0.9 (11-I-1)	-0.2 (3)	0.1 (11-I-1)	-1454.96 (11-II-1)	-27.84 (11-I-1)	-658.75 (11-II-1)
64	1	-0.0 (3)	-0.1 (4)	0.0 (11-II-4)	110.72 (11-II-3)	836.24 (11-II-3)	-53.59 (9)
64	2	-0.1 (3)	-0.2 (11-II-1)	0.0 (9)	134.99 (11-I-2)	1077.03 (11-II-3)	-53.40 (9)
64	3	-0.2 (3)	-0.3 (11-II-1)	0.1 (9)	58.56 (11-I-3)	1600.48 (11-II-3)	-355.47 (11-II-3)
64	4	-0.3 (3)	-1.2 (11-II-1)	0.2 (11-II-1)	354.66 (11-I-3)	2619.03 (11-II-3)	-1341.98 (11-II-3)
64	5	-0.0 (3)	-0.1 (10)	0.0 (11-II-4)	95.88 (11-II-3)	816.70 (11-II-3)	-53.54 (9)
64	6	-0.1 (3)	-0.1 (11-II-1)	0.1 (11-I-2)	114.27 (11-II-3)	915.20 (11-II-3)	-52.36 (9)
64	7	-0.2 (3)	-0.1 (11-II-1)	0.1 (11-I-2)	234.89 (11-I-2)	730.87 (11-II-3)	-206.68 (11-II-3)
64	8	-0.2 (3)	0.0 (11-II-1)	0.0 (11-I-2)	-38.50 (10)	51.43 (11-II-3)	-46.62 (11-II-3)
64	9	-0.0 (3)	-0.1 (9)	0.0 (11-II-4)	95.95 (11-II-3)	817.07 (11-II-3)	-52.12 (9)
64	10	-0.1 (3)	-0.1 (9)	0.1 (11-II-4)	114.38 (11-II-3)	915.23 (11-II-3)	-62.89 (10)
64	11	-0.2 (3)	-0.1 (9)	0.1 (11-II-4)	235.11 (11-I-2)	730.83 (11-II-3)	180.80 (11-I-3)
64	12	-0.2 (3)	-0.0 (11-I-1)	0.0 (11-II-4)	-37.98 (10)	51.45 (11-II-3)	-55.73 (10)
64	13	-0.0 (3)	-0.1 (9)	-0.0 (10)	110.85 (11-II-3)	836.34 (11-II-3)	-51.53 (9)
64	14	-0.1 (3)	-0.1 (9)	-0.0 (11-I-4)	135.31 (11-I-2)	1076.92 (11-II-3)	-62.46 (10)
64	15	-0.2 (11-II-1)	-0.2 (9)	-0.1 (11-I-4)	58.97 (11-I-4)	1600.25 (11-II-3)	329.74 (11-I-3)
64	16	-0.2 (3)	0.9 (11-I-1)	0.1 (11-I-1)	354.96 (11-I-4)	2618.82 (11-II-3)	1327.55 (11-II-3)
65	1	-0.1 (10)	-0.0 (3)	0.0 (9)	-515.25 (11-II-2)	-74.25 (11-II-2)	11.00 (10)
65	2	-0.1 (2)	-0.0 (3)	0.0 (11-I-1)	-533.35 (11-II-2)	61.15 (10)	10.96 (10)
65	3	-0.1 (9)	-0.0 (3)	0.0 (11-I-1)	-535.37 (11-I-2)	61.15 (10)	12.66 (11-I-4)
65	4	-0.1 (9)	-0.0 (3)	0.0 (9)	-517.45 (11-I-2)	-72.74 (11-II-2)	14.74 (11-I-3)
65	5	-0.2 (11-I-2)	-0.1 (3)	0.0 (9)	-623.06 (11-II-2)	-114.34 (11-II-4)	-11.75 (11-I-2)
65	6	-0.1 (11-I-2)	-0.1 (3)	0.1 (11-II-4)	-593.23 (11-II-2)	47.39 (10)	-15.11 (11-II-4)
65	7	-0.1 (9)	-0.1 (3)	0.1 (11-I-1)	-595.91 (11-I-2)	47.38 (10)	14.28 (11-II-2)
65	8	-0.1 (9)	-0.1 (3)	-0.0 (11-II-1)	-625.87 (11-I-2)	-106.90 (11-II-2)	22.70 (11-II-1)
65	9	-0.3 (11-I-2)	-0.1 (3)	0.1 (9)	-849.20 (11-II-2)	-106.40 (11-II-1)	82.20 (11-II-2)
65	10	-0.1 (11-I-2)	-0.2 (3)	0.1 (11-II-4)	-536.39 (11-I-2)	-88.00 (11-II-4)	48.66 (11-I-4)
65	11	-0.1 (9)	-0.2 (3)	0.1 (11-I-1)	-538.64 (11-I-2)	-70.34 (11-II-2)	-56.26 (11-I-2)
65	12	-0.2 (9)	-0.2 (11-I-2)	-0.1 (11-II-1)	-850.98 (11-I-2)	-83.73 (11-I-4)	-64.77 (11-I-2)
65	13	-1.1 (11-I-2)	-0.2 (3)	0.2 (11-II-1)	-1468.93 (11-I-2)	-158.01 (11-II-1)	719.53 (11-II-2)
65	14	0.0 (11-II-2)	-0.2 (3)	0.0 (11-II-1)	-96.83 (11-I-2)	-117.04 (11-II-4)	92.44 (11-I-4)
65	15	-0.0 (11-I-1)	-0.2 (3)	0.0 (11-II-3)	-94.38 (11-I-2)	-91.91 (11-II-2)	-101.47 (11-I-2)
65	16	0.9 (11-II-2)	-0.2 (3)	0.1 (11-II-2)	-1453.76 (11-I-2)	-26.94 (11-I-4)	-657.65 (11-I-2)
66	1	-0.0 (3)	-0.1 (10)	0.0 (11-II-4)	-103.18 (10)	-786.95 (10)	-11.28 (10)
66	2	-0.1 (3)	-0.2 (11-I-2)	0.0 (9)	-109.77 (10)	-753.11 (10)	16.51 (11-II-3)
66	3	-0.2 (3)	-0.3 (11-I-2)	0.1 (9)	-63.48 (10)	-812.70 (10)	72.42 (10)
66	4	-0.3 (3)	-1.2 (11-I-2)	0.2 (11-I-3)	-20.70 (10)	-1154.57 (10)	553.71 (10)
66	5	-0.1 (3)	-0.1 (4)	0.0 (11-II-4)	-94.34 (10)	-795.11 (10)	-11.04 (10)
66	6	-0.1 (3)	-0.1 (11-I-3)	0.1 (11-II-4)	-73.85 (10)	-721.80 (10)	9.01 (11-I-3)
66	7	-0.2 (3)	-0.1 (11-I-3)	0.1 (11-I-2)	-106.39 (10)	-555.10 (10)	51.89 (10)
66	8	-0.2 (3)	0.0 (11-I-2)	0.0 (11-I-2)	-135.31 (10)	-105.86 (10)	93.38 (10)
66	9	-0.1 (3)	-0.1 (9)	0.0 (11-II-4)	-94.33 (10)	-795.00 (10)	-12.04 (11-II-3)
66	10	-0.1 (3)	-0.1 (9)	0.1 (11-II-4)	-73.84 (10)	-721.67 (10)	-17.90 (11-II-3)
66	11	-0.2 (3)	-0.1 (9)	0.1 (11-II-3)	-106.23 (10)	-554.95 (10)	-61.71 (10)
66	12	-0.2 (3)	-0.0 (11-II-3)	0.0 (11-II-3)	-135.26 (10)	-105.91 (10)	-96.52 (10)
66	13	-0.0 (3)	-0.1 (9)	0.0 (11-II-4)	-103.08 (10)	-786.49 (10)	-9.63 (11-II-3)
66	14	-0.1 (3)	-0.1 (9)	-0.0 (11-I-4)	-109.64 (10)	-752.74 (10)	-13.76 (11-II-3)
66	15	-0.2 (11-I-2)	-0.2 (9)	-0.1 (11-I-3)	82.35 (11-I-3)	-812.42 (10)	-82.26 (10)
66	16	-0.3 (3)	0.9 (11-II-3)	0.1 (11-II-3)	141.27 (11-II-2)	-1154.58 (10)	-553.76 (10)
67	1	0.1 (3)	0.0 (2)	0.0 (10)	-319.16 (3)	-218.03 (2)	-173.97 (2)
67	2	0.1 (3)	0.0 (11-II-2)	0.0 (10)	-290.91 (3)	-57.03 (11-II-2)	-201.82 (2)
67	3	0.1 (3)	0.0 (11-II-2)	0.0 (10)	-266.07 (3)	14.90 (3)	-169.16 (2)
67	4	0.1 (3)	-0.0 (10)	0.0 (10)	-256.21 (3)	17.87 (3)	-89.33 (2)
67	5	0.1 (3)	0.0 (2)	0.0 (9)	-319.54 (3)	-274.95 (2)	-139.71 (9)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
67	6	0.1(3)	0.0(3)	0.0(10)	-276.30(3)	-46.53(11-II-2)	-141.12(9)
67	7	0.1(3)	0.0(11-II-2)	0.0(10)	-256.92(3)	39.76(2)	-143.67(9)
67	8	0.1(3)	0.0(11-I-2)	0.0(9)	-248.10(3)	34.65(3)	-69.75(9)
67	9	0.1(3)	0.0(2)	0.0(9)	-311.39(3)	-274.62(2)	-133.65(9)
67	10	0.1(3)	0.0(3)	0.0(9)	-265.17(3)	-43.57(11-II-2)	-129.67(9)
67	11	0.1(3)	0.0(11-II-2)	0.0(9)	-249.16(3)	43.88(2)	-135.47(9)
67	12	0.1(3)	0.0(11-II-2)	0.0(9)	-243.62(3)	36.20(2)	-66.40(9)
67	13	0.1(3)	0.0(2)	0.0(9)	-293.34(3)	-216.60(2)	-121.81(10)
67	14	0.1(3)	0.0(11-II-2)	0.0(2)	-255.70(3)	-50.68(11-II-2)	-117.24(10)
67	15	0.1(3)	0.0(11-II-2)	0.0(9)	-242.90(3)	26.03(10)	-122.09(10)
67	16	0.1(3)	0.0(11-II-2)	0.0(9)	-242.98(3)	24.03(2)	-74.92(10)
68	1	0.1(3)	0.0(2)	0.0(10)	-333.54(3)	-217.02(2)	-187.40(2)
68	2	0.1(3)	0.0(11-I-4)	0.0(10)	-305.24(3)	-57.34(11-II-2)	-215.97(2)
68	3	0.1(3)	0.0(11-II-2)	0.0(10)	-286.23(3)	15.37(3)	-185.78(2)
68	4	0.1(3)	-0.0(10)	0.0(10)	-275.47(3)	17.35(3)	-99.68(2)
68	5	0.1(3)	0.0(2)	0.0(10)	-333.93(3)	-273.01(2)	-147.44(2)
68	6	0.1(3)	0.0(11-II-2)	0.0(10)	-290.14(3)	-46.59(11-II-2)	-150.38(2)
68	7	0.1(3)	0.0(11-II-2)	0.0(10)	-271.85(3)	39.19(3)	-155.13(2)
68	8	0.1(3)	0.0(11-II-2)	0.0(2)	-262.67(3)	34.81(3)	-72.75(2)
68	9	0.1(3)	0.0(2)	0.0(2)	-326.29(3)	-272.42(2)	-136.65(9)
68	10	0.1(3)	0.0(2)	0.0(2)	-278.77(3)	-43.37(11-II-2)	-134.81(10)
68	11	0.1(3)	0.0(11-II-2)	0.0(2)	-260.28(3)	43.03(2)	-142.53(10)
68	12	0.1(3)	0.0(11-II-2)	0.0(2)	-254.73(3)	36.69(2)	-68.30(10)
68	13	0.1(3)	0.0(2)	0.0(2)	-309.32(3)	-215.19(2)	-127.92(10)
68	14	0.1(3)	0.0(11-II-2)	0.0(2)	-270.58(3)	-50.22(11-II-2)	-125.34(10)
68	15	0.1(3)	0.0(11-II-2)	0.0(2)	-250.69(3)	25.94(2)	-132.00(10)
68	16	0.1(3)	0.0(11-II-4)	0.0(2)	-250.73(3)	25.46(2)	-80.90(10)
69	1	0.1(3)	0.1(2)	0.0(10)	-409.64(3)	-396.22(2)	-180.44(2)
69	2	0.1(3)	0.0(2)	0.0(10)	-379.02(3)	181.94(10)	-230.02(2)
69	3	0.1(3)	-0.0(10)	0.0(10)	-353.20(3)	209.73(10)	-190.94(2)
69	4	0.1(3)	-0.0(10)	0.0(10)	-341.79(3)	103.58(4)	-152.18(2)
69	5	0.1(3)	0.1(2)	0.0(10)	-416.92(3)	-494.04(2)	-128.56(2)
69	6	0.1(3)	0.0(2)	0.0(10)	-359.09(3)	217.09(10)	-137.39(2)
69	7	0.1(3)	0.0(2)	0.0(10)	-339.49(3)	253.63(10)	-140.17(2)
69	8	0.1(3)	-0.0(10)	0.0(10)	-330.47(3)	113.19(4)	-136.06(2)
69	9	0.1(3)	0.1(2)	0.0(9)	-408.06(3)	-497.93(2)	-108.49(2)
69	10	0.1(3)	0.0(2)	0.0(9)	-346.05(3)	213.47(10)	-117.14(10)
69	11	0.1(3)	0.0(2)	0.0(2)	-326.85(3)	251.14(10)	-125.89(10)
69	12	0.1(3)	-0.0(10)	0.0(2)	-322.02(3)	111.73(4)	-130.34(10)
69	13	0.1(3)	0.1(2)	0.0(9)	-381.28(3)	-406.80(2)	-72.98(10)
69	14	0.1(3)	0.0(2)	0.0(9)	-338.06(3)	170.89(10)	115.52(3)
69	15	0.1(3)	-0.0(10)	0.0(2)	-314.66(3)	201.72(10)	-121.86(10)
69	16	0.1(3)	-0.0(10)	0.0(2)	-317.35(3)	98.29(4)	-142.95(10)
70	1	0.1(3)	0.0(2)	0.0(10)	-336.81(3)	-96.67(3)	-119.29(2)
70	2	0.1(3)	0.0(2)	0.0(10)	-344.66(3)	-242.19(2)	-120.26(2)
70	3	0.1(3)	0.0(2)	0.0(9)	-321.34(3)	167.84(10)	-138.98(2)
70	4	0.1(3)	0.0(2)	0.0(2)	-342.94(3)	-291.94(10)	-133.07(9)
70	5	0.1(3)	0.0(2)	0.0(9)	-314.78(3)	166.24(10)	-136.21(9)
70	6	0.1(3)	0.0(2)	0.0(2)	-336.88(3)	-292.72(10)	-137.93(9)
70	7	0.1(3)	0.0(2)	0.0(2)	-316.22(3)	-98.80(2)	-175.07(10)
70	8	0.1(3)	0.0(2)	0.0(2)	-323.69(3)	-243.42(2)	-172.54(10)
71	1	0.1(3)	-0.1(10)	0.0(2)	-397.39(3)	223.09(10)	-116.27(9)
71	2	0.1(3)	-0.1(10)	0.0(2)	-372.34(3)	450.51(10)	-110.73(9)
71	3	0.1(3)	-0.1(10)	0.0(2)	-377.70(3)	334.84(10)	133.31(3)
71	4	0.1(3)	0.0(2)	0.0(2)	-410.24(3)	-328.35(2)	94.81(3)
71	5	0.1(3)	-0.1(10)	0.0(2)	-391.06(3)	189.52(10)	-76.16(9)
71	6	0.1(3)	-0.1(10)	0.0(2)	-350.43(3)	533.33(10)	-100.85(9)
71	7	0.1(3)	-0.0(10)	0.0(2)	-354.28(3)	400.75(10)	-85.26(9)
71	8	0.1(3)	0.0(2)	0.0(2)	-421.82(3)	-446.87(2)	-97.29(9)
71	9	0.1(3)	-0.1(10)	0.0(9)	-380.29(3)	188.00(10)	-70.39(2)
71	10	0.1(3)	-0.1(10)	0.0(9)	-334.45(3)	530.95(10)	-101.80(2)
71	11	0.1(3)	-0.0(10)	0.0(9)	-339.18(3)	397.86(10)	-119.48(2)
71	12	0.1(3)	0.0(2)	0.0(9)	-411.96(3)	-450.43(2)	-120.69(2)
71	13	0.1(3)	-0.1(10)	0.0(9)	-363.06(3)	217.83(10)	-50.60(2)
71	14	0.1(3)	-0.1(10)	0.0(9)	-323.42(3)	442.48(10)	-117.35(2)
71	15	0.1(3)	-0.1(10)	-0.0(3)	-331.78(3)	326.16(10)	-237.76(10)
71	16	0.1(3)	0.0(2)	-0.0(3)	-379.23(3)	-338.13(2)	-206.86(10)
72	1	-0.0(3)	-0.1(4)	0.0(9)	110.66(11-II-2)	835.30(11-II-2)	-56.08(9)
72	2	-0.1(3)	-0.2(11-I-2)	0.0(9)	134.90(11-I-4)	1076.32(11-II-2)	-55.96(9)
72	3	-0.2(3)	-0.3(11-I-2)	0.1(9)	58.19(11-I-3)	1599.95(11-II-2)	-356.69(11-I-4)
72	4	-0.3(3)	-1.2(11-I-2)	0.2(11-I-2)	354.14(11-I-3)	2618.76(11-II-2)	-1342.61(11-I-4)
72	5	-0.1(3)	-0.1(10)	0.0(11-II-4)	95.80(11-II-3)	816.13(11-II-3)	-56.42(9)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
72	6	-0.1 (3)	-0.1 (11-I-2)	0.1 (11-II-4)	114.20 (11-II-2)	914.72 (11-II-3)	-55.36 (9)
72	7	-0.2 (3)	-0.1 (11-I-2)	0.1 (11-I-2)	234.72 (11-II-2)	730.55 (11-II-3)	-207.93 (11-I-4)
72	8	-0.2 (3)	0.0 (11-I-2)	0.0 (11-I-2)	-39.68 (10)	51.36 (11-II-3)	-47.40 (11-I-4)
72	9	-0.1 (3)	-0.1 (9)	0.0 (11-II-4)	95.88 (11-II-3)	817.08 (11-II-3)	-55.51 (9)
72	10	-0.1 (3)	-0.1 (9)	0.1 (11-II-4)	114.20 (11-II-2)	915.18 (11-II-3)	-68.64 (10)
72	11	-0.2 (3)	-0.1 (9)	0.1 (11-II-4)	234.82 (11-II-2)	730.81 (11-II-3)	180.05 (11-II-3)
72	12	-0.2 (3)	-0.0 (11-II-2)	0.0 (11-II-1)	-39.37 (10)	51.43 (11-II-3)	-59.06 (10)
72	13	-0.0 (3)	-0.1 (9)	0.0 (11-II-4)	110.75 (11-II-3)	836.75 (11-II-3)	-55.69 (9)
72	14	-0.1 (3)	-0.1 (9)	-0.0 (11-I-4)	134.95 (11-II-2)	1077.14 (11-II-3)	-68.83 (10)
72	15	-0.2 (11-I-2)	-0.2 (9)	-0.1 (11-I-4)	58.54 (11-I-3)	1600.50 (11-II-3)	328.70 (11-II-3)
72	16	-0.3 (3)	0.9 (11-II-2)	0.1 (11-II-2)	354.63 (11-I-3)	2619.05 (11-II-3)	1327.15 (11-II-3)
73	1	-0.0 (3)	-0.1 (10)	0.0 (9)	-103.28 (10)	-787.42 (10)	-12.03 (10)
73	2	-0.1 (3)	-0.2 (11-I-2)	0.0 (9)	-109.93 (10)	-753.43 (10)	16.49 (11-II-3)
73	3	-0.2 (3)	-0.3 (11-I-2)	0.1 (9)	-63.71 (10)	-812.87 (10)	71.61 (10)
73	4	-0.3 (3)	-1.2 (11-I-2)	0.2 (11-I-2)	-20.96 (10)	-1154.61 (10)	553.11 (10)
73	5	-0.1 (3)	-0.1 (4)	0.0 (11-II-4)	-94.46 (10)	-795.64 (10)	-11.89 (10)
73	6	-0.1 (3)	-0.1 (11-I-2)	0.1 (11-II-4)	-74.03 (10)	-722.16 (10)	-9.36 (10)
73	7	-0.2 (3)	-0.1 (11-I-2)	0.1 (11-II-4)	-106.64 (10)	-555.30 (10)	50.98 (10)
73	8	-0.2 (3)	0.0 (11-I-2)	0.0 (11-I-3)	-135.61 (10)	-105.91 (10)	92.64 (10)
73	9	-0.1 (3)	-0.1 (9)	0.0 (11-II-4)	-94.44 (10)	-795.56 (10)	-12.21 (11-I-3)
73	10	-0.1 (3)	-0.1 (9)	0.1 (11-I-3)	-74.04 (10)	-722.07 (10)	-18.08 (11-I-3)
73	11	-0.2 (3)	-0.1 (9)	0.1 (11-II-3)	-106.50 (10)	-555.17 (10)	-62.73 (10)
73	12	-0.2 (3)	-0.0 (11-II-3)	0.0 (11-II-2)	-135.60 (10)	-105.97 (10)	-97.36 (10)
73	13	-0.0 (3)	-0.1 (9)	0.0 (11-II-4)	-103.22 (10)	-787.12 (10)	-9.82 (11-I-3)
73	14	-0.1 (3)	-0.1 (9)	-0.0 (11-I-4)	-109.87 (10)	-753.18 (10)	-13.99 (11-I-3)
73	15	-0.2 (11-I-2)	-0.2 (9)	-0.1 (11-I-3)	82.21 (11-I-3)	-812.66 (10)	-83.40 (10)
73	16	-0.3 (3)	0.9 (11-II-2)	0.1 (11-II-2)	140.79 (11-I-3)	-1154.64 (10)	-554.59 (10)
74	1	-0.1 (10)	-0.0 (3)	0.0 (9)	-515.57 (11-I-2)	-74.27 (11-II-2)	10.70 (10)
74	2	-0.1 (4)	-0.0 (3)	0.0 (11-II-4)	-533.53 (11-I-2)	61.17 (10)	10.67 (10)
74	3	-0.1 (9)	-0.0 (3)	0.0 (11-II-4)	-535.38 (11-II-2)	61.16 (10)	12.45 (11-I-3)
74	4	-0.1 (9)	-0.0 (3)	0.0 (11-II-4)	-517.30 (11-II-2)	-72.73 (11-II-2)	14.54 (11-II-4)
74	5	-0.2 (11-II-1)	-0.1 (3)	0.0 (9)	-623.25 (11-I-2)	-114.34 (11-II-2)	-11.85 (11-I-1)
74	6	-0.1 (11-II-1)	-0.1 (3)	0.1 (11-II-4)	-593.35 (11-I-2)	47.41 (10)	-15.30 (11-I-1)
74	7	-0.1 (9)	-0.1 (3)	0.1 (11-II-4)	-595.92 (11-II-2)	47.39 (10)	14.06 (11-II-1)
74	8	-0.1 (9)	-0.1 (3)	-0.0 (11-I-4)	-625.79 (11-II-2)	-106.91 (11-I-2)	22.48 (11-II-1)
74	9	-0.3 (11-II-1)	-0.1 (3)	0.1 (9)	-849.39 (11-I-2)	-106.36 (11-II-1)	81.89 (11-I-4)
74	10	-0.1 (11-II-1)	-0.2 (3)	0.1 (11-II-1)	-536.47 (11-I-2)	-87.99 (11-II-2)	48.41 (11-II-1)
74	11	-0.1 (9)	-0.2 (3)	0.1 (11-I-1)	-538.66 (11-I-2)	-70.33 (11-II-2)	-56.46 (11-II-1)
74	12	-0.2 (9)	-0.2 (11-II-1)	-0.1 (11-II-1)	-850.96 (11-I-2)	-83.87 (11-II-1)	-64.90 (11-I-1)
74	13	-1.2 (11-II-1)	-0.2 (3)	0.2 (11-II-1)	-1469.53 (11-II-1)	-157.84 (11-II-1)	719.74 (11-II-1)
74	14	0.0 (11-I-1)	-0.2 (3)	0.0 (11-II-1)	-96.85 (11-I-2)	-117.01 (11-II-2)	92.19 (11-II-1)
74	15	-0.0 (11-I-1)	-0.2 (3)	0.0 (11-II-1)	-94.38 (11-I-2)	-91.90 (11-II-2)	-101.64 (11-II-1)
74	16	0.9 (11-I-1)	-0.2 (3)	0.1 (11-I-1)	-1454.89 (11-II-1)	-26.74 (11-I-1)	-658.20 (11-II-1)
75	1	-0.0 (3)	-0.1 (4)	0.0 (9)	110.69 (11-II-2)	835.46 (11-II-2)	-59.44 (2)
75	2	-0.1 (3)	-0.2 (11-I-2)	0.0 (9)	134.98 (11-II-2)	1076.40 (11-II-2)	-59.39 (2)
75	3	-0.2 (3)	-0.3 (11-I-2)	0.1 (9)	58.24 (11-I-2)	1599.98 (11-II-2)	-358.23 (11-I-3)
75	4	-0.3 (3)	-1.1 (11-I-2)	0.2 (11-I-2)	354.18 (11-I-2)	2618.76 (11-II-2)	-1343.42 (11-I-4)
75	5	-0.1 (3)	-0.1 (10)	0.0 (11-II-4)	95.84 (11-II-2)	816.12 (11-II-2)	-59.02 (2)
75	6	-0.1 (3)	-0.1 (11-I-2)	0.1 (11-II-4)	114.27 (11-II-2)	914.72 (11-II-2)	-57.89 (2)
75	7	-0.2 (3)	-0.1 (11-I-2)	0.1 (11-II-4)	234.81 (11-II-2)	730.57 (11-II-2)	-209.44 (11-I-3)
75	8	-0.2 (3)	0.0 (11-I-2)	0.0 (11-I-2)	-40.26 (10)	51.37 (11-II-2)	-48.29 (11-I-3)
75	9	-0.1 (3)	-0.1 (9)	0.0 (11-II-4)	95.87 (11-II-2)	816.63 (11-II-2)	-57.24 (9)
75	10	-0.1 (3)	-0.1 (9)	0.1 (11-II-4)	114.23 (11-II-2)	914.87 (11-II-2)	-72.88 (10)
75	11	-0.2 (3)	-0.1 (9)	0.1 (11-I-1)	234.82 (11-II-2)	730.62 (11-II-2)	179.81 (11-II-3)
75	12	-0.2 (3)	-0.0 (11-II-2)	0.0 (11-II-2)	-40.06 (10)	51.40 (11-II-2)	-61.49 (10)
75	13	-0.0 (3)	-0.1 (9)	0.0 (11-II-4)	110.73 (11-II-2)	835.98 (11-II-2)	-57.78 (9)
75	14	-0.1 (3)	-0.1 (9)	-0.0 (11-I-4)	134.90 (11-I-4)	1076.56 (11-II-2)	-73.37 (10)
75	15	-0.2 (11-I-2)	-0.2 (9)	-0.1 (11-II-1)	58.37 (11-I-3)	1600.05 (11-II-2)	328.40 (11-II-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
75	16	-0.3 (3)	0.9 (11-II-2)	0.1 (11-II-2)	354.32 (11-I-3)	2618.79 (11-II-2)	1326.97 (11-II-3)
76	1	0.1 (3)	0.0 (2)	0.0 (9)	-384.10 (3)	6.27 (2)	-2.87 (3)
76	2	0.1 (3)	0.0 (2)	0.0 (9)	-386.29 (3)	-13.29 (3)	-50.16 (9)
76	3	0.1 (3)	0.0 (2)	0.0 (9)	-370.38 (3)	7.54 (2)	18.12 (9)
76	4	0.1 (3)	0.0 (2)	0.0 (2)	-374.94 (3)	-15.21 (2)	-61.26 (9)
76	5	0.1 (3)	0.0 (3)	0.0 (9)	-364.95 (3)	7.65 (2)	19.88 (9)
76	6	0.1 (3)	0.0 (2)	0.0 (9)	-369.45 (3)	-14.65 (2)	-67.78 (9)
76	7	0.1 (3)	0.0 (3)	0.0 (9)	-355.57 (3)	5.07 (3)	4.64 (4)
76	8	0.1 (3)	0.0 (3)	0.0 (9)	-357.19 (3)	-15.07 (2)	-50.90 (9)
77	1	0.1 (3)	0.0 (2)	0.0 (10)	-399.33 (3)	6.25 (2)	-2.41 (3)
77	2	0.1 (3)	0.0 (2)	0.0 (2)	-401.56 (3)	-13.07 (3)	-50.87 (10)
77	3	0.1 (3)	0.0 (3)	0.0 (10)	-389.27 (3)	7.40 (2)	15.07 (9)
77	4	0.1 (3)	0.0 (3)	0.0 (2)	-393.85 (3)	-14.47 (2)	-62.34 (10)
77	5	0.1 (3)	0.0 (2)	0.0 (9)	-384.72 (3)	7.39 (2)	16.79 (9)
77	6	0.1 (3)	0.0 (3)	0.0 (9)	-389.31 (3)	-14.49 (3)	-68.74 (9)
77	7	0.1 (3)	0.0 (3)	0.0 (9)	-379.67 (3)	4.73 (3)	2.82 (10)
77	8	0.1 (3)	0.0 (3)	0.0 (9)	-381.42 (3)	-14.67 (2)	-52.28 (9)
78	1	0.1 (3)	-0.1 (10)	0.0 (2)	-383.83 (3)	223.76 (10)	-110.35 (9)
78	2	0.1 (3)	-0.1 (10)	0.0 (2)	-360.88 (3)	448.61 (10)	-103.22 (9)
78	3	0.1 (3)	-0.1 (10)	0.0 (10)	-364.73 (3)	327.92 (10)	147.10 (3)
78	4	0.1 (3)	0.0 (2)	0.0 (10)	-395.97 (3)	-340.93 (2)	109.86 (3)
78	5	0.1 (3)	-0.1 (10)	0.0 (9)	-373.66 (3)	190.01 (10)	-66.71 (9)
78	6	0.1 (3)	-0.1 (10)	0.0 (2)	-334.40 (3)	528.74 (10)	-93.45 (9)
78	7	0.1 (3)	-0.0 (10)	0.0 (2)	-338.27 (3)	389.88 (10)	-78.92 (9)
78	8	0.1 (3)	0.0 (2)	0.0 (9)	-405.28 (3)	-462.41 (2)	-97.78 (9)
78	9	0.1 (3)	-0.1 (10)	0.0 (9)	-359.02 (3)	187.03 (10)	-56.73 (9)
78	10	0.1 (3)	-0.1 (10)	0.0 (9)	-313.09 (3)	522.68 (10)	-88.48 (9)
78	11	0.1 (3)	-0.0 (10)	0.0 (9)	-319.07 (3)	382.67 (10)	-107.15 (9)
78	12	0.1 (3)	0.0 (2)	0.0 (9)	-392.90 (3)	-467.82 (2)	-119.87 (9)
78	13	0.1 (3)	-0.1 (10)	0.0 (9)	-336.73 (3)	213.85 (10)	45.27 (3)
78	14	0.1 (3)	-0.1 (10)	0.0 (9)	-295.57 (3)	429.58 (10)	-103.74 (2)
78	15	0.1 (3)	-0.1 (10)	-0.0 (3)	-306.48 (3)	306.29 (10)	-227.68 (10)
78	16	0.1 (3)	0.0 (2)	-0.0 (3)	-356.75 (3)	-356.73 (2)	-199.37 (10)
79	1	0.1 (3)	-0.1 (10)	0.0 (2)	-367.71 (3)	224.12 (10)	-97.45 (9)
79	2	0.1 (3)	-0.1 (10)	0.0 (2)	-349.36 (3)	440.41 (10)	-88.94 (9)
79	3	0.1 (3)	-0.1 (10)	0.0 (10)	-352.67 (3)	313.51 (10)	158.43 (3)
79	4	0.1 (3)	0.0 (2)	0.0 (10)	-380.85 (3)	-355.44 (2)	123.13 (3)
79	5	0.1 (3)	-0.1 (10)	0.0 (9)	-350.90 (3)	191.01 (10)	-48.66 (9)
79	6	0.1 (3)	-0.1 (10)	0.0 (9)	-314.32 (3)	513.98 (10)	-79.08 (9)
79	7	0.1 (3)	-0.0 (10)	0.0 (9)	-318.87 (3)	367.71 (10)	-70.30 (9)
79	8	0.1 (3)	0.0 (2)	0.0 (9)	-384.61 (3)	-478.68 (2)	-98.81 (9)
79	9	0.1 (3)	-0.1 (10)	0.0 (9)	-329.44 (3)	186.02 (10)	-36.97 (9)
79	10	0.1 (3)	-0.1 (10)	0.0 (9)	-283.20 (3)	500.64 (10)	-73.15 (9)
79	11	0.1 (3)	-0.0 (10)	0.0 (9)	-290.75 (3)	352.78 (10)	-98.57 (9)
79	12	0.1 (3)	0.0 (2)	0.0 (9)	-366.40 (3)	-485.39 (2)	-120.89 (9)
79	13	0.1 (3)	-0.1 (10)	0.0 (9)	-298.67 (3)	206.90 (10)	55.87 (3)
79	14	0.1 (3)	-0.1 (10)	0.0 (9)	-268.03 (2)	400.65 (10)	-85.35 (2)
79	15	0.1 (3)	-0.0 (10)	-0.0 (3)	-267.49 (3)	269.78 (10)	-214.47 (10)
79	16	0.1 (3)	0.1 (2)	-0.0 (3)	-323.07 (3)	-377.05 (2)	-189.77 (10)
80	1	0.1 (3)	0.1 (2)	0.0 (10)	-395.40 (3)	-410.83 (2)	-176.64 (9)
80	2	0.1 (3)	0.0 (2)	0.0 (10)	-366.85 (3)	170.47 (10)	-229.19 (9)
80	3	0.1 (3)	-0.0 (10)	0.0 (10)	-340.67 (3)	202.06 (10)	-182.41 (2)
80	4	0.1 (3)	0.0 (2)	0.0 (10)	-327.98 (3)	99.24 (4)	-143.60 (9)
80	5	0.1 (3)	0.1 (2)	0.0 (9)	-400.62 (3)	-512.26 (2)	-119.29 (9)
80	6	0.1 (3)	0.0 (2)	0.0 (10)	-344.30 (3)	201.87 (10)	-137.61 (9)
80	7	0.1 (3)	0.0 (2)	0.0 (10)	-324.95 (3)	243.69 (10)	-139.24 (9)
80	8	0.1 (3)	0.0 (2)	0.0 (9)	-315.80 (3)	110.31 (4)	-140.84 (9)
80	9	0.1 (3)	0.1 (2)	0.0 (9)	-389.57 (3)	-518.07 (2)	-101.20 (9)
80	10	0.1 (3)	0.0 (2)	0.0 (9)	-327.95 (3)	194.84 (10)	-113.12 (9)
80	11	0.1 (3)	0.0 (2)	0.0 (9)	-309.41 (3)	238.23 (10)	-121.99 (10)
80	12	0.1 (3)	0.0 (2)	0.0 (9)	-305.68 (3)	107.49 (4)	-134.38 (9)
80	13	0.1 (3)	0.1 (2)	0.0 (9)	-359.67 (3)	-426.91 (2)	85.21 (3)
80	14	0.1 (3)	0.0 (2)	0.0 (9)	-315.12 (3)	-160.70 (2)	131.62 (3)
80	15	0.1 (3)	0.0 (2)	0.0 (9)	-293.32 (3)	184.86 (10)	-113.46 (10)
80	16	0.1 (3)	0.0 (2)	0.0 (9)	-298.76 (3)	89.46 (4)	-138.83 (10)
81	1	0.1 (3)	0.0 (2)	0.0 (10)	-305.09 (3)	-217.42 (2)	-161.61 (2)
81	2	0.1 (3)	0.0 (11-II-2)	0.0 (10)	-279.20 (3)	-56.42 (11-II-2)	-187.76 (2)
81	3	0.1 (3)	0.0 (11-II-2)	0.0 (10)	-249.25 (3)	18.59 (10)	-151.61 (2)
81	4	0.1 (3)	-0.0 (10)	0.0 (10)	-238.56 (3)	17.64 (3)	-82.52 (9)
81	5	0.1 (3)	0.0 (3)	0.0 (9)	-302.70 (3)	-275.20 (2)	-136.98 (9)
81	6	0.1 (3)	0.0 (3)	0.0 (9)	-261.35 (3)	-46.28 (11-II-2)	-137.54 (9)
81	7	0.1 (3)	0.0 (11-I-2)	0.0 (9)	-241.36 (3)	43.67 (2)	-135.53 (9)
81	8	0.1 (3)	0.0 (11-I-2)	0.0 (9)	-232.35 (3)	33.88 (3)	-66.56 (9)
81	9	0.1 (3)	0.0 (3)	0.0 (9)	-291.22 (3)	-274.12 (2)	-129.89 (9)



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
81	10	0.1(3)	0.0(3)	0.0(9)	-246.21(3)	-43.68(11-II-2)	-124.16(9)
81	11	0.1(3)	0.0(11-I-2)	0.0(9)	-232.98(3)	47.49(2)	-125.82(9)
81	12	0.1(3)	0.0(11-I-2)	0.0(9)	-228.27(3)	36.42(2)	-62.37(9)
81	13	0.1(3)	0.0(3)	0.0(9)	-268.75(3)	-213.23(2)	-112.69(10)
81	14	0.1(3)	0.0(11-I-2)	0.0(9)	-230.61(3)	-51.12(11-I-2)	116.61(3)
81	15	0.1(3)	0.0(11-II-2)	0.0(9)	-224.93(3)	29.55(10)	-107.52(10)
81	16	0.1(3)	0.0(11-II-2)	0.0(9)	-227.34(3)	23.58(2)	-66.24(10)
82	1	0.1(3)	0.0(2)	0.0(10)	-322.63(3)	-101.07(2)	-106.10(2)
82	2	0.1(3)	0.0(2)	0.0(10)	-330.67(3)	-243.93(2)	-109.98(2)
82	3	0.1(3)	0.0(2)	0.0(9)	-306.64(3)	159.18(10)	-132.11(9)
82	4	0.1(3)	0.0(2)	0.0(9)	-328.47(3)	-293.80(10)	-137.03(9)
82	5	0.1(3)	0.0(2)	0.0(9)	-299.07(3)	156.36(10)	-133.29(9)
82	6	0.1(3)	0.0(2)	0.0(9)	-321.60(3)	-294.20(10)	-142.29(9)
82	7	0.1(3)	0.0(2)	0.0(9)	-298.63(3)	-105.89(2)	-168.89(10)
82	8	0.1(3)	0.0(2)	0.0(9)	-306.62(3)	-244.62(2)	-170.29(10)
83	1	0.1(3)	0.0(2)	0.0(9)	-364.31(3)	6.26(2)	-3.68(3)
83	2	0.1(3)	0.0(2)	0.0(9)	-366.48(3)	-13.44(3)	-47.76(9)
83	3	0.1(3)	0.0(2)	0.0(9)	-345.41(3)	7.70(2)	21.56(9)
83	4	0.1(3)	0.0(2)	0.0(9)	-349.90(3)	-16.37(2)	-57.42(9)
83	5	0.1(3)	0.0(3)	0.0(9)	-337.61(3)	7.98(2)	23.27(9)
83	6	0.1(3)	0.0(2)	0.0(9)	-341.97(3)	-15.34(2)	-62.15(9)
83	7	0.1(3)	0.0(3)	0.0(9)	-322.00(3)	5.41(3)	7.12(4)
83	8	0.1(3)	0.0(3)	0.0(9)	-323.32(3)	-15.56(2)	-45.62(9)
84	1	0.1(3)	0.1(2)	0.0(10)	-380.45(3)	-428.64(2)	-173.16(9)
84	2	0.1(3)	0.0(2)	-0.0(3)	-356.57(3)	-158.93(2)	-233.07(9)
84	3	0.1(3)	0.0(2)	0.0(10)	-329.91(3)	189.52(10)	-185.75(9)
84	4	0.1(3)	0.0(2)	0.0(10)	-313.80(3)	94.02(4)	-149.36(9)
84	5	0.1(3)	0.1(2)	0.0(9)	-380.43(3)	-534.15(2)	-108.13(9)
84	6	0.1(3)	0.1(2)	0.0(9)	-327.09(3)	178.05(10)	-136.26(9)
84	7	0.1(3)	0.0(2)	0.0(9)	-308.15(3)	226.56(10)	-140.54(9)
84	8	0.1(3)	0.0(2)	0.0(9)	-298.40(3)	108.03(4)	-148.65(9)
84	9	0.1(3)	0.1(2)	0.0(9)	-364.01(3)	-541.13(2)	-87.78(9)
84	10	0.1(3)	0.1(2)	0.0(9)	-302.71(3)	165.49(10)	-108.71(9)
84	11	0.1(3)	0.0(2)	0.0(9)	-285.14(3)	215.58(10)	-120.42(9)
84	12	0.1(3)	0.0(2)	0.0(9)	-283.57(3)	102.81(4)	-141.39(9)
84	13	0.1(3)	0.1(2)	0.0(9)	-327.22(3)	-449.38(2)	98.29(3)
84	14	0.1(3)	0.1(2)	0.0(9)	-279.28(3)	-186.61(2)	145.56(3)
84	15	0.1(3)	0.0(2)	0.0(9)	-260.05(3)	156.22(10)	101.82(3)
84	16	0.1(3)	0.0(2)	0.0(9)	-271.16(3)	-92.19(2)	-133.14(10)
85	1	0.1(3)	0.0(2)	0.0(9)	-307.63(3)	-108.42(2)	-99.31(9)
85	2	0.1(3)	0.0(2)	0.0(9)	-316.12(3)	-241.97(2)	-110.23(9)
85	3	0.1(3)	0.0(2)	0.0(9)	-289.04(3)	144.31(10)	-129.86(9)
85	4	0.1(3)	0.0(2)	0.0(9)	-311.14(3)	-290.39(10)	-142.73(9)
85	5	0.1(3)	0.0(2)	0.0(9)	-278.07(3)	139.18(10)	-131.12(9)
85	6	0.1(3)	0.0(2)	0.0(9)	-301.24(3)	-288.66(10)	-148.07(9)
85	7	0.1(3)	0.0(2)	0.0(9)	-272.75(3)	-116.01(2)	-162.79(9)
85	8	0.1(3)	0.0(2)	0.0(9)	-281.36(3)	-238.59(2)	-168.57(9)
86	1	-0.0(2)	-0.1(11-II-3)	0.1(2)	-102.87(10)	-788.76(10)	12.21(11-II-4)
86	2	-0.1(2)	-0.1(11-II-3)	0.1(2)	-108.07(10)	-752.91(10)	21.84(11-II-4)
86	3	0.2(11-II-4)	-0.3(11-II-3)	0.1(9)	-60.30(10)	-811.76(10)	79.98(10)
86	4	-0.2(2)	-1.2(11-II-3)	0.3(11-II-3)	-16.58(10)	-1153.98(10)	559.26(10)
86	5	-0.0(2)	-0.1(11-II-3)	0.1(2)	-93.21(10)	-796.76(10)	8.04(11-I-4)
86	6	-0.1(2)	-0.1(11-II-3)	0.1(2)	-69.06(10)	-720.42(10)	10.39(11-I-4)
86	7	-0.1(2)	-0.1(11-II-3)	0.2(11-II-3)	-98.86(10)	-554.02(10)	61.46(10)
86	8	0.1(11-II-4)	0.0(11-I-4)	0.1(11-II-3)	-126.37(10)	-106.69(10)	100.59(10)
86	9	-0.1(11-II-3)	-0.1(11-II-3)	0.1(2)	-88.39(10)	-791.98(10)	-21.15(11-II-4)
86	10	-0.1(11-II-3)	-0.1(2)	0.1(2)	-62.22(10)	-722.03(10)	-31.58(11-II-4)
86	11	-0.1(2)	0.1(11-I-3)	0.1(11-II-3)	-89.43(10)	-554.14(10)	-48.54(10)
86	12	0.2(11-II-4)	0.0(9)	0.1(11-II-3)	-117.21(10)	-97.60(10)	-87.03(10)
86	13	-0.1(2)	-0.3(2)	0.1(2)	-60.93(10)	-775.26(10)	48.09(10)
86	14	-0.0(11-II-3)	-0.3(11-II-3)	-0.0(11-II-4)	-31.51(10)	-753.25(10)	-43.07(11-II-4)
86	15	-0.2(11-II-3)	-0.3(11-II-3)	-0.2(11-II-4)	-80.76(10)	-823.72(10)	-119.04(10)
86	16	-0.2(11-I-4)	0.6(11-I-3)	-0.0(3)	36.23(9)	-1177.58(10)	-491.89(10)
87	1	0.1(3)	0.0(3)	0.0(9)	-257.63(3)	-207.49(3)	-139.81(9)
87	2	0.0(3)	0.0(11-II-3)	-0.0(3)	-246.88(3)	-54.19(11-I-3)	-147.81(9)
87	3	0.0(3)	-0.0(10)	-0.0(3)	-211.76(3)	33.73(10)	-116.06(9)
87	4	0.0(3)	-0.0(10)	0.0(9)	-192.10(3)	16.61(2)	-60.09(9)
87	5	0.1(3)	0.0(3)	0.0(9)	-237.27(3)	-256.16(2)	-105.53(9)
87	6	0.0(3)	0.0(3)	0.0(9)	-206.19(3)	61.84(10)	-99.46(9)
87	7	0.0(3)	0.0(3)	0.0(9)	-187.99(3)	55.69(2)	-91.99(9)
87	8	0.0(3)	0.0(3)	0.0(9)	-176.02(3)	34.67(2)	-43.57(9)
87	9	0.0(3)	0.0(3)	0.0(9)	-208.65(3)	-251.15(2)	-88.60(9)
87	10	0.0(3)	0.0(3)	0.0(9)	-166.82(3)	64.21(10)	80.99(3)
87	11	0.0(3)	0.0(3)	0.0(9)	-159.71(3)	59.32(2)	-76.07(9)
87	12	0.0(3)	0.0(3)	0.0(9)	-159.00(3)	37.43(2)	39.21(3)



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
87	13	0.0(3)	0.0(3)	0.0(9)	-175.13(2)	-197.36(3)	111.03(3)
87	14	0.0(3)	0.0(3)	0.0(9)	-123.22(3)	55.03(10)	136.07(3)
87	15	0.0(3)	-0.0(10)	0.0(9)	-127.80(3)	42.04(10)	101.56(3)
87	16	0.0(3)	-0.0(10)	0.0(9)	-142.05(3)	24.17(2)	48.11(3)
88	1	0.1(3)	0.0(2)	0.0(9)	-334.31(3)	6.12(2)	5.84(4)
88	2	0.1(3)	0.0(2)	0.0(9)	-336.47(3)	-13.95(2)	-40.75(9)
88	3	0.1(3)	0.0(2)	0.0(9)	-308.06(3)	7.69(2)	25.51(9)
88	4	0.1(3)	0.0(2)	-0.0(3)	-312.29(3)	-17.84(2)	-46.89(9)
88	5	0.1(2)	0.0(3)	0.0(9)	-296.50(2)	8.29(2)	27.68(9)
88	6	0.1(2)	0.0(2)	0.0(11-II-4)	-300.76(2)	-16.09(2)	-48.38(9)
88	7	0.1(2)	0.0(3)	-0.0(3)	-335.35(2)	5.69(3)	10.84(4)
88	8	0.1(2)	0.0(3)	-0.0(3)	-339.61(2)	-15.21(2)	36.93(3)
89	1	0.1(3)	0.0(3)	0.0(9)	-287.08(3)	-212.11(2)	-156.96(9)
89	2	0.1(3)	0.0(11-I-2)	0.0(10)	-266.85(3)	-55.58(11-I-2)	-169.71(2)
89	3	0.1(3)	0.0(11-I-2)	0.0(10)	-232.96(3)	25.80(10)	-137.87(9)
89	4	0.1(3)	-0.0(10)	0.0(9)	-219.05(3)	16.40(3)	-74.43(9)
89	5	0.1(3)	0.0(3)	0.0(9)	-277.79(3)	-269.93(2)	-130.10(9)
89	6	0.1(3)	0.0(3)	0.0(9)	-240.27(3)	48.79(10)	-126.77(9)
89	7	0.1(3)	0.0(11-I-2)	0.0(9)	-220.47(3)	50.05(2)	-120.07(9)
89	8	0.1(3)	0.0(11-I-2)	0.0(9)	-210.54(3)	34.21(2)	-58.65(9)
89	9	0.1(3)	0.0(3)	0.0(9)	-259.13(3)	-266.10(2)	-119.23(9)
89	10	0.1(3)	0.0(3)	0.0(9)	-215.42(3)	51.33(10)	-108.81(9)
89	11	0.1(3)	0.0(11-I-2)	0.0(9)	-205.40(3)	54.00(2)	-107.43(9)
89	12	0.0(3)	0.0(11-I-2)	0.0(9)	-202.58(3)	37.39(2)	-52.99(9)
89	13	0.1(3)	0.0(3)	0.0(9)	-228.21(3)	-204.92(3)	102.88(3)
89	14	0.1(3)	0.0(3)	0.0(9)	-187.79(3)	-51.60(11-II-3)	129.12(3)
89	15	0.1(3)	0.0(11-II-3)	0.0(9)	-188.99(3)	36.22(10)	94.39(3)
89	16	0.0(3)	-0.0(10)	0.0(9)	-196.48(3)	24.16(2)	-52.69(10)
90	1	0.1(2)	0.1(2)	-0.0(3)	-324.83(3)	-441.82(2)	-130.93(9)
90	2	0.1(2)	0.1(2)	-0.0(3)	-320.19(3)	-235.17(2)	-201.98(9)
90	3	0.1(2)	0.0(2)	-0.0(3)	-293.09(3)	-139.00(2)	-184.71(9)
90	4	0.1(2)	0.0(2)	0.0(9)	-262.87(3)	-97.13(2)	-154.59(9)
90	5	0.1(2)	0.1(2)	0.0(9)	-376.48(2)	-530.93(2)	-60.44(9)
90	6	0.1(2)	0.1(2)	-0.0(3)	-321.63(2)	-248.94(2)	-95.55(9)
90	7	0.1(2)	0.1(2)	0.0(9)	-292.27(2)	-129.75(2)	-114.25(9)
90	8	0.1(2)	0.0(2)	0.0(9)	-255.35(2)	102.21(4)	-135.65(9)
90	9	0.1(2)	0.1(2)	0.0(9)	-398.57(2)	-528.34(2)	60.26(3)
90	10	0.1(2)	0.1(2)	0.0(9)	-358.72(2)	-262.35(2)	86.37(3)
90	11	0.1(2)	0.1(2)	0.0(9)	-327.28(2)	-142.29(2)	83.15(3)
90	12	0.1(2)	0.0(2)	0.0(9)	-273.88(2)	95.04(4)	-109.37(9)
90	13	0.1(2)	0.1(2)	0.0(9)	-387.95(2)	-443.23(2)	111.49(3)
90	14	0.1(2)	0.1(2)	0.0(9)	-365.91(2)	-268.00(2)	159.88(3)
90	15	0.1(2)	0.1(2)	0.0(9)	-321.51(2)	-171.99(2)	121.26(3)
90	16	0.1(2)	0.0(2)	0.0(9)	-273.18(2)	-109.67(2)	89.99(3)
91	1	0.1(3)	0.1(2)	-0.0(3)	-360.02(3)	-443.19(2)	-159.33(9)
91	2	0.1(3)	0.1(2)	-0.0(3)	-344.25(3)	-180.77(2)	-227.91(9)
91	3	0.1(3)	0.0(2)	0.0(10)	-316.78(3)	164.91(10)	-190.78(9)
91	4	0.1(3)	0.0(2)	0.0(9)	-294.47(3)	86.91(4)	-159.00(9)
91	5	0.1(3)	0.1(2)	0.0(9)	-349.90(3)	-545.80(2)	-81.28(9)
91	6	0.1(3)	0.1(2)	0.0(9)	-301.63(3)	-178.91(2)	-121.65(9)
91	7	0.1(3)	0.0(2)	0.0(9)	-283.39(3)	187.72(10)	-138.42(9)
91	8	0.1(3)	0.0(2)	0.0(9)	-272.48(3)	107.15(4)	-162.28(9)
91	9	0.1(3)	0.1(2)	0.0(9)	-323.97(3)	-547.57(2)	-55.79(9)
91	10	0.1(3)	0.1(2)	0.0(9)	-265.82(2)	-199.71(2)	-88.39(9)
91	11	0.1(3)	0.0(2)	0.0(9)	-247.40(3)	162.55(10)	-113.37(9)
91	12	0.1(3)	0.0(2)	0.0(9)	-249.23(3)	98.17(4)	-153.77(9)
91	13	0.1(3)	0.1(2)	0.0(9)	-370.24(2)	-458.17(2)	107.91(3)
91	14	0.1(3)	0.1(2)	0.0(9)	-375.08(2)	-236.77(2)	155.85(3)
91	15	0.1(3)	0.0(2)	0.0(9)	-338.02(2)	-139.02(2)	113.05(3)
91	16	0.1(3)	0.0(2)	0.0(9)	-271.33(2)	-109.11(2)	-120.33(10)
92	1	0.1(2)	-0.1(10)	-0.0(3)	-302.88(3)	218.92(10)	-51.59(11-II-3)
92	2	0.1(2)	-0.1(10)	0.0(2)	-302.50(3)	344.16(10)	74.34(3)
92	3	0.1(2)	-0.0(10)	0.0(10)	-308.58(3)	209.59(10)	166.73(3)
92	4	0.1(2)	0.1(2)	0.0(9)	-324.19(3)	-367.97(2)	138.02(3)
92	5	0.1(2)	-0.1(10)	-0.0(3)	-353.05(2)	203.36(10)	36.02(3)
92	6	0.1(2)	-0.0(10)	0.0(9)	-330.64(2)	378.31(10)	59.42(3)
92	7	0.1(2)	-0.0(10)	0.0(9)	-336.27(2)	225.78(10)	61.46(3)
92	8	0.1(2)	0.0(2)	0.0(9)	-386.62(2)	-470.95(2)	-85.71(9)
92	9	0.1(2)	-0.1(10)	-0.0(3)	-382.02(2)	197.10(10)	39.57(3)
92	10	0.1(2)	-0.0(10)	-0.0(3)	-385.48(2)	351.57(10)	53.81(3)
92	11	0.1(2)	0.0(2)	-0.0(3)	-390.66(2)	200.38(10)	-71.31(9)
92	12	0.1(2)	0.0(2)	-0.0(3)	-416.22(2)	-471.14(2)	-94.98(9)
92	13	0.1(2)	-0.0(10)	-0.0(3)	-388.73(2)	192.65(10)	68.31(3)
92	14	0.1(2)	-0.0(10)	-0.0(3)	-400.51(2)	270.69(10)	-69.13(2)
92	15	0.1(2)	-0.0(10)	-0.0(3)	-406.90(2)	138.87(10)	-159.56(10)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
92	16	0.1 (2)	0.1 (2)	-0.0 (3)	-404.39 (2)	-376.38 (2)	-132.00 (9)
93	1	0.1 (3)	0.0 (2)	0.0 (9)	-287.11 (3)	-121.42 (2)	-101.43 (9)
93	2	0.1 (3)	0.0 (2)	0.0 (9)	-296.40 (3)	-232.03 (3)	-116.66 (9)
93	3	0.1 (3)	0.0 (2)	0.0 (9)	-262.77 (3)	114.90 (10)	-127.90 (9)
93	4	0.1 (3)	0.0 (2)	0.0 (9)	-285.03 (3)	-268.06 (10)	-148.24 (9)
93	5	0.1 (3)	0.0 (2)	0.0 (9)	-245.23 (3)	-106.81 (2)	-127.85 (9)
93	6	0.1 (3)	0.0 (2)	0.0 (9)	-268.99 (3)	-261.70 (3)	-151.04 (9)
93	7	0.1 (3)	0.0 (2)	0.0 (9)	-231.51 (3)	-131.35 (2)	-146.02 (9)
93	8	0.1 (3)	0.0 (2)	0.0 (9)	-240.56 (3)	-223.60 (3)	-155.65 (9)
94	1	0.1 (3)	-0.1 (10)	-0.0 (3)	-343.78 (3)	225.53 (10)	-69.56 (9)
94	2	0.1 (3)	-0.1 (10)	0.0 (2)	-333.06 (3)	416.04 (10)	65.73 (3)
94	3	0.1 (3)	-0.0 (10)	0.0 (10)	-337.13 (3)	283.21 (10)	165.43 (3)
94	4	0.1 (3)	0.1 (2)	0.0 (9)	-360.00 (3)	-365.77 (2)	133.08 (3)
94	5	0.1 (3)	-0.1 (10)	0.0 (9)	-316.46 (3)	197.19 (10)	30.83 (3)
94	6	0.1 (3)	-0.1 (10)	0.0 (9)	-284.41 (3)	471.42 (10)	-52.97 (9)
94	7	0.1 (3)	-0.0 (10)	0.0 (9)	-290.37 (3)	318.87 (10)	-64.04 (9)
94	8	0.1 (3)	0.0 (2)	0.0 (9)	-353.46 (3)	-482.98 (2)	-105.53 (9)
94	9	0.1 (3)	-0.1 (10)	0.0 (9)	-304.54 (2)	190.02 (10)	35.87 (3)
94	10	0.1 (3)	-0.1 (10)	-0.0 (3)	-279.13 (2)	441.45 (10)	47.70 (3)
94	11	0.1 (3)	-0.0 (10)	-0.0 (3)	-281.09 (2)	287.86 (10)	-91.56 (9)
94	12	0.1 (3)	0.0 (2)	0.0 (9)	-332.28 (2)	-486.85 (2)	-127.40 (9)
94	13	0.1 (3)	-0.1 (10)	0.0 (9)	-380.65 (2)	195.72 (10)	64.02 (3)
94	14	0.1 (3)	-0.1 (10)	-0.0 (3)	-415.57 (2)	332.78 (10)	-68.00 (2)
94	15	0.1 (3)	-0.0 (10)	-0.0 (3)	-418.25 (2)	197.23 (10)	-194.98 (10)
94	16	0.1 (3)	0.1 (2)	-0.0 (3)	-389.13 (2)	-387.01 (2)	-176.34 (10)
95	1	0.1 (2)	0.0 (2)	-0.0 (3)	-337.07 (2)	6.60 (2)	-6.68 (3)
95	2	0.1 (2)	0.0 (2)	-0.0 (3)	-338.59 (2)	-15.38 (2)	40.64 (3)
95	3	0.1 (2)	0.0 (2)	-0.0 (3)	-357.28 (2)	9.27 (2)	-22.47 (3)
95	4	0.1 (2)	0.0 (2)	-0.0 (3)	-362.48 (2)	-20.53 (2)	55.79 (3)
95	5	0.1 (2)	0.0 (2)	-0.0 (3)	-366.09 (2)	9.23 (2)	-21.29 (3)
95	6	0.1 (2)	0.0 (2)	0.0 (11-I-4)	-370.53 (2)	-18.81 (2)	53.89 (3)
95	7	0.1 (2)	0.0 (2)	-0.0 (3)	-372.21 (2)	5.42 (3)	6.39 (11-II-3)
95	8	0.1 (2)	0.0 (3)	-0.0 (3)	-375.16 (2)	-14.40 (2)	42.65 (3)
96	1	0.1 (2)	-0.0 (10)	-0.0 (3)	-410.08 (2)	186.47 (10)	-64.01 (11-II-3)
96	2	0.1 (2)	-0.0 (10)	-0.0 (3)	-455.55 (2)	267.27 (10)	71.45 (3)
96	3	0.1 (2)	-0.0 (10)	0.0 (9)	-471.07 (2)	143.96 (10)	165.78 (3)
96	4	0.1 (2)	0.1 (2)	0.0 (9)	-434.73 (2)	-386.33 (2)	146.30 (3)
96	5	0.1 (2)	-0.0 (10)	-0.0 (3)	-383.36 (2)	162.78 (10)	38.46 (3)
96	6	0.1 (2)	-0.0 (10)	-0.0 (3)	-380.21 (2)	317.90 (10)	59.39 (3)
96	7	0.1 (2)	0.0 (2)	0.0 (9)	-393.49 (2)	193.19 (10)	59.35 (3)
96	8	0.1 (2)	0.0 (2)	0.0 (9)	-428.17 (2)	-488.15 (2)	86.66 (3)
96	9	0.1 (2)	-0.0 (10)	-0.0 (3)	-329.15 (2)	136.32 (10)	50.53 (3)
96	10	0.1 (2)	-0.0 (10)	-0.0 (3)	-251.69 (2)	307.78 (10)	64.53 (3)
96	11	0.1 (2)	0.0 (2)	-0.0 (3)	-263.56 (2)	196.76 (10)	-66.30 (9)
96	12	0.1 (2)	0.0 (2)	-0.0 (3)	-377.94 (2)	-480.94 (2)	59.00 (3)
96	13	0.1 (2)	-0.0 (10)	-0.0 (3)	-206.25 (2)	113.59 (10)	97.27 (3)
96	14	0.1 (2)	-0.0 (10)	-0.0 (3)	-84.77 (10)	239.82 (10)	52.92 (3)
96	15	0.1 (2)	-0.0 (10)	-0.0 (3)	-86.88 (11-II-4)	151.18 (10)	-158.23 (2)
96	16	0.1 (2)	0.1 (2)	-0.0 (3)	-231.77 (2)	-354.18 (2)	-127.12 (11-II-4)
97	1	-0.1 (10)	-0.0 (3)	0.0 (11-I-2)	-514.85 (11-II-2)	-74.22 (11-II-2)	9.94 (10)
97	2	-0.1 (11-II-1)	-0.0 (3)	0.0 (11-I-2)	-532.87 (11-II-2)	60.96 (10)	-10.60 (11-II-4)
97	3	-0.1 (9)	-0.0 (3)	0.0 (11-I-2)	-534.95 (11-II-2)	60.86 (10)	12.11 (11-I-4)
97	4	-0.1 (9)	-0.0 (3)	0.0 (11-I-2)	-517.45 (11-II-1)	-72.84 (11-II-2)	14.10 (11-II-4)
97	5	-0.2 (11-II-1)	-0.1 (3)	0.0 (9)	-622.91 (11-II-2)	-114.47 (11-II-1)	-12.63 (11-II-4)
97	6	-0.1 (11-II-1)	-0.1 (3)	0.1 (11-I-2)	-593.07 (11-II-2)	47.06 (10)	-16.25 (11-II-4)
97	7	-0.1 (9)	-0.1 (3)	0.1 (11-II-4)	-595.78 (11-II-2)	46.91 (10)	13.75 (11-I-4)
97	8	-0.1 (9)	-0.1 (3)	-0.0 (11-I-4)	-626.06 (11-II-1)	-107.43 (11-II-1)	22.02 (11-II-4)
97	9	-0.3 (11-II-1)	0.1 (11-I-1)	0.1 (9)	-849.27 (11-II-2)	-106.70 (11-II-1)	81.81 (11-I-4)
97	10	-0.1 (11-II-1)	-0.1 (3)	0.1 (11-II-1)	-536.41 (11-II-2)	-88.22 (11-II-1)	48.31 (11-I-4)
97	11	-0.1 (9)	-0.1 (3)	0.1 (11-I-1)	-538.67 (11-II-1)	-70.75 (11-II-1)	-57.82 (11-II-4)
97	12	-0.2 (9)	-0.2 (11-II-1)	-0.1 (11-I-4)	-851.43 (11-II-1)	-84.80 (11-II-1)	-66.61 (11-I-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
97	13	-1.2 (11-II-1)	-0.2 (3)	0.2 (11-II-1)	-1470.56 (11-II-1)	-157.66 (11-II-1)	719.45 (11-I-4)
97	14	0.0 (11-II-1)	-0.1 (3)	0.0 (11-II-1)	-96.84 (11-II-2)	-117.34 (11-II-1)	92.17 (11-I-4)
97	15	-0.0 (11-I-1)	-0.1 (3)	0.0 (11-II-1)	-94.39 (11-II-2)	-92.48 (11-II-1)	-102.81 (11-II-1)
97	16	0.9 (11-I-1)	-0.2 (3)	0.1 (11-I-1)	-1454.98 (11-II-1)	-28.67 (11-I-1)	-659.74 (11-II-1)
98	1	-0.1 (11-II-1)	-0.0 (3)	0.0 (3)	-516.80 (11-II-1)	-74.58 (11-II-1)	-8.74 (11-I-4)
98	2	-0.1 (11-II-1)	-0.0 (3)	0.1 (11-II-1)	-536.49 (11-II-1)	60.72 (10)	-11.51 (11-I-4)
98	3	-0.1 (9)	-0.0 (3)	0.0 (11-II-1)	-540.52 (11-II-1)	60.77 (10)	11.31 (11-II-4)
98	4	-0.1 (9)	-0.0 (11-I-4)	0.0 (3)	-524.40 (11-II-1)	-73.18 (11-II-1)	13.64 (11-II-4)
98	5	-0.2 (11-II-1)	-0.1 (3)	0.0 (3)	-624.04 (11-II-1)	-115.03 (11-II-1)	-13.76 (11-I-4)
98	6	-0.1 (11-II-1)	-0.1 (3)	0.1 (11-II-1)	-594.68 (11-II-1)	46.74 (10)	-17.47 (11-I-4)
98	7	-0.1 (9)	-0.1 (3)	0.1 (11-II-1)	-597.41 (11-II-1)	46.83 (10)	13.22 (11-II-4)
98	8	-0.1 (9)	-0.0 (3)	0.0 (2)	-626.19 (11-II-1)	-105.25 (11-II-1)	22.84 (11-II-4)
98	9	-0.3 (11-II-1)	0.1 (11-I-1)	0.1 (9)	-849.99 (11-II-1)	-107.33 (11-II-1)	81.13 (11-II-4)
98	10	-0.1 (11-II-1)	-0.1 (3)	0.1 (11-II-1)	-536.79 (11-II-1)	-88.49 (11-II-1)	47.74 (11-II-4)
98	11	-0.1 (9)	-0.1 (3)	0.1 (11-II-4)	-538.32 (11-II-1)	-69.52 (11-II-1)	-58.18 (11-I-4)
98	12	-0.2 (9)	-0.1 (11-I-4)	-0.1 (11-I-4)	-849.12 (11-II-1)	-79.64 (11-II-1)	-64.51 (11-I-4)
98	13	-1.2 (11-II-1)	-0.2 (3)	0.2 (11-II-1)	-1470.57 (11-II-1)	-159.16 (11-II-1)	719.09 (11-II-1)
98	14	0.0 (11-II-1)	-0.1 (3)	0.0 (11-II-1)	-96.79 (11-II-1)	-117.41 (11-II-1)	91.84 (11-II-4)
98	15	-0.0 (11-I-1)	-0.1 (3)	0.0 (11-II-1)	-93.97 (11-II-1)	-90.32 (11-II-1)	-102.72 (11-I-4)
98	16	0.9 (11-I-1)	-0.1 (3)	0.1 (11-II-4)	-1454.31 (11-II-1)	-21.09 (11-I-1)	-657.45 (11-I-4)
99	1	-0.1 (11-II-1)	-0.0 (3)	0.1 (2)	-522.18 (11-II-1)	-73.23 (11-II-1)	-7.04 (11-I-4)
99	2	-0.1 (11-II-1)	-0.0 (2)	0.1 (2)	-532.25 (11-II-1)	61.85 (10)	6.53 (10)
99	3	-0.1 (11-II-1)	-0.0 (11-II-1)	0.0 (2)	511.91 (10)	60.73 (10)	37.67 (11-II-1)
99	4	-0.3 (11-II-1)	-0.0 (2)	0.0 (2)	511.98 (10)	42.67 (10)	76.51 (11-II-1)
99	5	-0.1 (11-II-1)	-0.0 (3)	0.1 (2)	-619.78 (11-II-1)	-107.56 (11-II-1)	-8.65 (11-I-1)
99	6	-0.1 (11-II-1)	-0.1 (2)	0.1 (11-II-1)	-582.45 (11-II-1)	48.17 (10)	7.74 (9)
99	7	-0.1 (9)	-0.1 (11-II-1)	0.0 (2)	-576.00 (11-II-1)	46.99 (10)	55.31 (11-II-1)
99	8	-0.3 (11-II-1)	-0.0 (11-II-1)	-0.0 (11-II-4)	-596.11 (11-II-1)	21.05 (10)	76.71 (11-II-1)
99	9	-0.3 (11-II-1)	0.2 (11-II-4)	0.1 (9)	-843.88 (11-II-1)	-93.23 (11-II-1)	89.32 (11-II-1)
99	10	-0.1 (11-II-1)	-0.1 (3)	0.2 (11-II-1)	-526.53 (11-II-1)	63.46 (10)	66.66 (11-II-1)
99	11	0.1 (11-I-1)	-0.1 (11-I-4)	0.1 (11-II-1)	-523.82 (11-II-1)	63.23 (10)	39.19 (10)
99	12	-0.3 (11-II-1)	-0.2 (11-II-1)	-0.2 (11-II-1)	-856.82 (11-II-1)	-57.52 (11-II-1)	80.25 (10)
99	13	-1.1 (11-II-1)	-0.1 (3)	0.3 (11-II-1)	-1468.80 (11-II-1)	-141.31 (11-II-1)	726.43 (11-II-1)
99	14	0.0 (11-I-1)	0.1 (11-II-4)	0.1 (11-II-1)	-94.50 (11-II-1)	79.19 (10)	106.85 (11-II-1)
99	15	0.0 (9)	0.2 (11-II-4)	0.1 (11-II-1)	-75.40 (11-II-1)	81.51 (10)	-70.84 (11-II-1)
99	16	0.6 (11-I-1)	-0.2 (11-I-4)	-0.0 (9)	-1488.85 (11-II-1)	201.93 (11-II-4)	-520.11 (11-II-1)
100	1	-0.0 (2)	-0.1 (11-I-4)	0.0 (3)	112.45 (11-I-2)	844.09 (11-I-2)	-39.37 (9)
100	2	-0.1 (2)	-0.2 (11-I-4)	0.0 (3)	137.55 (11-I-4)	1081.75 (11-I-2)	-45.10 (11-II-3)
100	3	0.1 (11-II-4)	-0.3 (11-I-4)	0.1 (9)	61.38 (11-I-4)	1602.23 (11-I-2)	-349.32 (11-II-3)
100	4	-0.2 (2)	-1.2 (11-I-4)	0.2 (11-II-4)	357.36 (11-I-4)	2619.01 (11-I-2)	-1338.40 (11-II-4)
100	5	-0.0 (2)	-0.1 (11-I-4)	0.1 (11-I-2)	98.08 (11-I-2)	829.72 (11-I-2)	-36.91 (9)
100	6	-0.1 (2)	-0.1 (11-I-4)	0.1 (11-I-2)	116.62 (11-I-2)	922.27 (11-I-2)	-40.21 (11-II-3)
100	7	-0.1 (2)	-0.1 (11-I-4)	0.1 (11-II-1)	237.11 (11-I-2)	733.44 (11-I-2)	-199.83 (11-II-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
100	8	-0.2 (2)	0.0 (11-I-4)	0.0 (11-II-4)	-32.97 (10)	51.78 (11-I-2)	-42.46 (11-II-4)
100	9	-0.0 (2)	-0.1 (3)	0.0 (11-I-2)	98.08 (11-I-2)	836.26 (11-I-2)	-33.16 (9)
100	10	-0.1 (2)	-0.1 (3)	0.1 (11-I-2)	114.44 (11-I-2)	924.25 (11-I-2)	-40.69 (10)
100	11	-0.1 (2)	0.1 (11-II-4)	0.1 (11-II-4)	233.13 (11-I-2)	733.31 (11-I-2)	187.13 (11-I-3)
100	12	-0.1 (2)	-0.0 (11-I-4)	0.0 (11-I-4)	-31.77 (10)	51.51 (11-I-2)	-43.14 (10)
100	13	-0.0 (11-I-4)	-0.1 (3)	0.0 (2)	111.27 (11-I-2)	861.03 (11-I-2)	-29.79 (9)
100	14	-0.1 (2)	-0.1 (9)	0.0 (2)	128.24 (11-I-4)	1085.80 (11-I-2)	-37.58 (10)
100	15	-0.1 (11-I-4)	-0.2 (9)	-0.1 (11-I-4)	45.61 (11-II-3)	1601.23 (11-I-2)	332.33 (11-I-3)
100	16	-0.2 (2)	0.9 (11-II-4)	0.1 (11-II-4)	339.03 (11-II-3)	2618.25 (11-I-2)	1329.50 (11-I-3)
101	1	-0.0 (3)	-0.1 (4)	0.0 (3)	-102.83 (10)	-785.40 (10)	9.03 (11-I-4)
101	2	-0.1 (3)	-0.2 (11-I-3)	0.0 (3)	-109.26 (10)	-752.22 (10)	16.89 (11-I-4)
101	3	-0.1 (3)	-0.3 (11-I-3)	0.1 (9)	-62.83 (10)	-812.26 (10)	75.42 (10)
101	4	-0.2 (3)	-1.2 (11-I-3)	0.2 (11-I-3)	-19.97 (10)	-1154.48 (10)	555.88 (10)
101	5	-0.0 (3)	-0.1 (11-I-3)	0.0 (11-I-2)	-94.05 (10)	-793.78 (10)	-7.58 (10)
101	6	-0.1 (3)	-0.1 (11-I-3)	0.1 (11-I-2)	-73.42 (10)	-721.08 (10)	9.59 (11-I-4)
101	7	-0.2 (3)	-0.1 (11-I-3)	0.1 (11-II-2)	-105.84 (10)	-554.75 (10)	55.04 (10)
101	8	-0.2 (3)	0.0 (11-I-3)	0.0 (11-II-3)	-134.72 (10)	-105.79 (10)	95.93 (10)
101	9	-0.0 (3)	-0.1 (9)	0.0 (11-I-2)	-94.17 (10)	-794.33 (10)	-11.52 (11-I-4)
101	10	-0.1 (3)	-0.1 (9)	0.1 (11-I-2)	-73.59 (10)	-721.24 (10)	-17.00 (11-II-4)
101	11	-0.2 (3)	-0.1 (9)	0.1 (11-II-4)	-105.90 (10)	-554.74 (10)	-58.44 (10)
101	12	-0.2 (3)	-0.0 (11-I-3)	0.0 (11-I-3)	-134.87 (10)	-105.86 (10)	-93.88 (10)
101	13	-0.0 (2)	-0.1 (9)	0.0 (3)	-103.06 (10)	-786.45 (10)	-8.96 (11-II-4)
101	14	-0.1 (2)	-0.1 (9)	-0.0 (4)	-109.57 (10)	-752.65 (10)	-12.45 (11-II-4)
101	15	-0.2 (11-I-3)	-0.2 (9)	-0.1 (11-I-4)	83.82 (11-I-3)	-812.37 (10)	-78.90 (10)
101	16	-0.2 (2)	0.9 (11-II-3)	0.1 (11-II-3)	144.11 (11-II-4)	-1154.56 (10)	-551.33 (10)
102	1	-0.0 (2)	-0.1 (11-II-4)	0.1 (2)	105.45 (11-I-2)	860.14 (11-I-2)	26.99 (3)
102	2	-0.0 (2)	-0.1 (11-II-4)	0.1 (2)	111.92 (11-I-4)	1082.40 (11-I-2)	-54.83 (11-II-4)
102	3	0.2 (11-II-4)	-0.3 (11-II-4)	0.1 (9)	20.80 (11-I-4)	1596.17 (11-I-2)	-360.35 (11-II-4)
102	4	-0.1 (2)	-1.1 (11-II-4)	0.3 (11-II-4)	311.35 (11-II-3)	2616.69 (11-I-3)	-1344.14 (11-II-4)
102	5	-0.0 (2)	-0.1 (11-II-4)	0.1 (2)	81.86 (11-I-3)	827.08 (11-I-3)	-35.26 (11-II-4)
102	6	-0.1 (2)	-0.1 (11-II-4)	0.1 (2)	-66.51 (10)	906.33 (11-I-3)	-75.48 (11-II-4)
102	7	-0.1 (2)	-0.1 (11-II-4)	0.2 (11-II-4)	147.30 (11-I-3)	717.28 (11-I-3)	-239.65 (11-II-4)
102	8	0.1 (11-II-4)	0.0 (11-I-4)	0.1 (11-II-4)	-121.02 (11-II-3)	44.66 (11-I-3)	-61.98 (11-II-4)
102	9	-0.1 (11-II-4)	-0.1 (11-II-4)	0.1 (2)	73.39 (11-I-3)	790.16 (11-I-3)	-72.05 (11-II-4)
102	10	-0.1 (11-II-4)	-0.1 (9)	0.1 (2)	-72.54 (10)	909.45 (11-I-3)	-39.07 (11-II-4)
102	11	-0.1 (2)	0.1 (11-I-4)	0.1 (11-II-4)	120.43 (11-I-3)	649.67 (11-I-3)	87.57 (11-I-4)
102	12	0.2 (11-II-4)	0.0 (9)	0.1 (11-II-4)	-315.49 (11-II-3)	-30.76 (11-II-3)	-100.58 (11-II-4)
102	13	-0.1 (2)	-0.3 (2)	0.1 (2)	58.73 (11-I-3)	803.12 (11-I-3)	-104.41 (11-II-4)
102	14	-0.0 (11-II-4)	-0.3 (11-II-4)	-0.0 (11-II-4)	67.23 (11-I-3)	1080.53 (11-I-3)	-35.42 (10)
102	15	-0.2 (11-II-4)	-0.3 (11-II-4)	-0.2 (11-II-4)	177.25 (11-I-3)	1703.20 (11-I-3)	373.82 (11-I-3)
102	16	-0.2 (11-I-4)	0.6 (11-I-4)	-0.0 (3)	-387.36 (11-II-3)	2711.44 (11-I-3)	897.83 (11-I-3)
103	1	-0.0 (2)	-0.1 (11-I-3)	0.0 (3)	-103.07 (10)	-786.60 (10)	9.75 (11-II-4)
103	2	-0.1 (2)	-0.2 (11-I-3)	0.0 (3)	-109.57 (10)	-752.85 (10)	18.69 (11-II-4)
103	3	0.1 (11-II-3)	-0.3 (11-I-3)	0.1 (9)	-63.18 (10)	-812.51 (10)	77.07 (10)
103	4	-0.2 (2)	-1.2 (11-I-3)	0.2 (11-I-3)	-20.34 (10)	-1154.52 (10)	557.08 (10)
103	5	-0.0 (2)	-0.1 (11-I-3)	0.1 (11-I-2)	-94.31 (10)	-795.24 (10)	8.29 (11-II-4)
103	6	-0.1 (2)	-0.1 (11-I-3)	0.1 (11-I-3)	-73.72 (10)	-721.84 (10)	12.19 (11-II-4)
103	7	-0.2 (2)	-0.1 (11-I-3)	0.1 (11-II-3)	-106.14 (10)	-555.02 (10)	56.63 (10)
103	8	-0.2 (2)	0.0 (11-I-3)	0.0 (11-II-3)	-135.02 (10)	-105.83 (10)	97.24 (10)
103	9	-0.0 (2)	-0.1 (3)	0.0 (11-I-3)	-94.40 (10)	-795.98 (10)	-9.54 (11-I-4)
103	10	-0.1 (2)	-0.1 (3)	0.1 (11-I-3)	-73.71 (10)	-721.99 (10)	-13.34 (11-I-4)
103	11	-0.1 (2)	0.1 (11-II-3)	0.1 (11-II-3)	-105.89 (10)	-554.89 (10)	-56.82 (10)
103	12	-0.2 (2)	-0.0 (11-I-3)	0.0 (11-II-3)	-134.74 (10)	-105.82 (10)	-92.51 (10)
103	13	-0.0 (2)	-0.1 (3)	0.0 (2)	-103.19 (10)	-788.41 (10)	6.74 (10)
103	14	-0.1 (2)	-0.1 (3)	0.0 (2)	-109.22 (10)	-753.20 (10)	-7.93 (11-I-4)
103	15	-0.1 (11-I-4)	-0.1 (9)	-0.1 (11-I-3)	85.22 (11-II-3)	-812.20 (10)	-76.97 (10)
103	16	-0.2 (2)	0.9 (11-I-3)	0.1 (11-II-4)	145.25 (11-II-3)	-1154.43 (10)	-549.85 (10)
104	1	-0.0 (3)	-0.1 (4)	0.0 (3)	110.88 (11-II-3)	835.83 (11-II-3)	-48.69 (9)
104	2	-0.1 (3)	-0.2 (11-I-4)	0.0 (3)	135.62 (11-I-2)	1076.87 (11-II-3)	-49.52 (11-II-3)
104	3	-0.1 (3)	-0.3 (11-I-4)	0.1 (9)	59.32 (11-I-4)	1600.28 (11-II-3)	-353.95 (11-II-3)
104	4	-0.2 (3)	-1.2 (11-I-4)	0.2 (11-I-4)	355.35 (11-I-4)	2618.81 (11-II-3)	-1341.12 (11-II-3)
104	5	-0.0 (3)	-0.1 (10)	0.0 (11-I-2)	96.19 (11-I-2)	816.85 (11-II-3)	-47.80 (9)
104	6	-0.1 (3)	-0.1 (11-I-4)	0.1 (11-I-2)	115.21 (11-I-2)	915.46 (11-II-3)	-46.45 (9)
104	7	-0.2 (3)	-0.1 (11-I-4)	0.1 (11-I-2)	236.22 (11-I-2)	731.04 (11-II-3)	-204.77 (11-II-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
104	8	-0.2 (3)	0.0 (11-I-4)	0.0 (11-II-1)	-36.28 (10)	51.49 (11-II-3)	-45.47 (11-II-3)
104	9	-0.0 (3)	-0.1 (9)	0.0 (11-I-2)	96.58 (11-I-2)	818.93 (11-I-2)	-45.43 (9)
104	10	-0.1 (3)	-0.1 (9)	0.1 (11-I-2)	115.67 (11-I-2)	916.60 (11-I-2)	-54.18 (10)
104	11	-0.2 (3)	-0.1 (9)	0.1 (11-II-4)	236.85 (11-I-2)	731.54 (11-I-2)	183.80 (11-I-3)
104	12	-0.2 (3)	-0.0 (11-I-1)	0.0 (11-II-4)	-35.47 (10)	51.61 (11-I-2)	-50.72 (10)
104	13	-0.0 (3)	-0.1 (9)	-0.0 (10)	111.93 (11-I-2)	840.93 (11-I-2)	-43.46 (9)
104	14	-0.1 (3)	-0.1 (9)	-0.0 (4)	137.02 (11-I-4)	1079.88 (11-I-2)	-52.67 (10)
104	15	-0.2 (11-I-4)	-0.2 (9)	-0.1 (11-I-4)	60.96 (11-I-4)	1601.54 (11-I-2)	333.46 (11-I-3)
104	16	-0.2 (3)	0.9 (11-II-4)	0.1 (11-II-4)	357.00 (11-I-4)	2618.95 (11-I-2)	1329.77 (11-I-3)
105	1	0.0 (3)	0.0 (3)	-0.0 (3)	-214.98 (3)	-201.65 (3)	-102.87 (9)
105	2	0.0 (3)	0.0 (3)	-0.0 (3)	-216.38 (3)	56.62 (10)	-109.51 (9)
105	3	0.0 (3)	-0.0 (10)	-0.0 (3)	-179.37 (3)	37.54 (10)	-78.62 (9)
105	4	0.0 (3)	-0.0 (10)	-0.0 (3)	-149.60 (3)	14.44 (2)	-38.85 (9)
105	5	0.0 (2)	0.0 (3)	-0.0 (3)	-195.88 (2)	-241.41 (2)	-70.11 (9)
105	6	0.0 (3)	0.0 (3)	-0.0 (3)	-158.29 (3)	70.84 (10)	75.38 (3)
105	7	0.0 (3)	0.0 (3)	-0.0 (3)	-136.09 (3)	50.94 (2)	67.52 (3)
105	8	0.0 (3)	0.0 (3)	-0.0 (3)	-120.61 (3)	29.22 (2)	39.61 (3)
105	9	0.0 (2)	0.0 (3)	-0.0 (3)	-166.21 (2)	-225.32 (2)	70.85 (3)
105	10	0.0 (3)	0.0 (3)	-0.0 (3)	-97.01 (3)	69.25 (10)	100.86 (3)
105	11	0.0 (3)	0.0 (3)	-0.0 (3)	-86.42 (3)	51.06 (9)	76.93 (3)
105	12	0.0 (3)	0.0 (3)	0.0 (9)	-90.45 (3)	30.39 (2)	42.27 (3)
105	13	0.0 (2)	0.0 (3)	-0.0 (3)	-100.03 (2)	-164.20 (3)	119.64 (3)
105	14	0.0 (3)	0.0 (3)	0.0 (9)	-18.49 (3)	53.67 (10)	137.60 (3)
105	15	0.0 (3)	0.0 (3)	0.0 (9)	-36.81 (3)	39.16 (9)	93.62 (3)
105	16	0.0 (3)	0.0 (3)	0.0 (9)	-60.99 (3)	19.27 (2)	43.60 (3)
106	1	0.1 (2)	0.0 (2)	0.0 (9)	-257.25 (2)	-143.40 (2)	88.41 (3)
106	2	0.0 (2)	0.0 (2)	0.0 (9)	-235.48 (2)	-220.39 (3)	101.44 (3)
106	3	0.1 (2)	0.0 (2)	-0.0 (3)	-229.49 (2)	-133.27 (2)	-62.59 (9)
106	4	0.0 (2)	0.0 (2)	-0.0 (3)	-217.15 (2)	-260.04 (3)	98.00 (3)
106	5	0.0 (2)	0.0 (2)	-0.0 (3)	-188.01 (2)	-122.47 (2)	-61.77 (9)
106	6	0.0 (2)	0.0 (2)	-0.0 (3)	-196.92 (2)	-268.03 (3)	93.42 (3)
106	7	0.0 (2)	0.0 (2)	-0.0 (3)	-113.11 (2)	-125.41 (2)	-66.81 (9)
106	8	0.0 (2)	0.0 (2)	-0.0 (3)	-125.92 (2)	-222.46 (3)	-71.28 (11-II-4)
107	1	0.1 (2)	0.0 (2)	-0.0 (3)	-366.66 (2)	4.92 (2)	11.62 (11-II-4)
107	2	0.1 (2)	0.0 (10)	-0.0 (3)	-371.15 (2)	-14.53 (2)	45.25 (3)
107	3	0.1 (2)	0.0 (2)	-0.0 (3)	-357.12 (2)	8.68 (2)	26.24 (11-II-3)
107	4	0.1 (2)	0.0 (10)	-0.0 (3)	-364.07 (2)	-24.07 (10)	64.70 (3)
107	5	0.1 (2)	0.0 (10)	-0.0 (3)	-364.44 (2)	16.16 (2)	-21.09 (3)
107	6	0.1 (2)	0.0 (10)	-0.0 (3)	-371.57 (2)	-43.66 (10)	78.85 (3)
107	7	0.1 (2)	0.0 (2)	-0.0 (10)	-312.11 (2)	12.65 (2)	-9.52 (2)
107	8	0.1 (2)	0.0 (10)	-0.0 (10)	-321.78 (2)	-35.87 (2)	74.69 (10)
108	1	0.1 (2)	0.1 (2)	-0.0 (3)	-415.30 (2)	-454.76 (2)	-122.69 (9)
108	2	0.1 (2)	0.1 (2)	-0.0 (3)	-429.54 (2)	-268.71 (2)	-175.89 (9)
108	3	0.1 (2)	0.0 (2)	-0.0 (3)	-392.68 (2)	-177.73 (2)	-143.20 (9)
108	4	0.1 (2)	0.0 (2)	-0.0 (3)	-303.69 (2)	-116.01 (2)	-97.55 (9)
108	5	0.1 (2)	0.1 (2)	-0.0 (3)	-414.83 (2)	-552.90 (2)	-75.73 (9)
108	6	0.1 (2)	0.1 (2)	-0.0 (3)	-373.22 (2)	-240.27 (2)	80.45 (3)
108	7	0.1 (2)	0.1 (2)	-0.0 (3)	-325.18 (2)	-136.73 (2)	88.16 (3)
108	8	0.1 (2)	0.0 (2)	-0.0 (3)	-256.94 (2)	85.32 (4)	96.01 (3)
108	9	0.1 (2)	0.1 (2)	-0.0 (3)	-382.79 (2)	-555.44 (2)	57.72 (3)
108	10	0.1 (2)	0.1 (2)	-0.0 (3)	-272.30 (2)	-208.93 (2)	117.58 (3)
108	11	0.1 (2)	0.1 (2)	-0.0 (3)	-208.33 (2)	-119.80 (2)	105.34 (3)
108	12	0.1 (2)	0.0 (2)	-0.0 (3)	-182.33 (2)	80.65 (4)	100.28 (3)
108	13	0.1 (2)	0.1 (2)	-0.0 (3)	-250.80 (2)	-437.07 (2)	133.39 (3)
108	14	0.1 (2)	0.1 (2)	0.0 (9)	-86.32 (10)	-195.21 (2)	179.72 (3)
108	15	0.1 (2)	0.0 (2)	0.0 (9)	-56.17 (10)	-125.95 (2)	120.33 (3)
108	16	0.0 (2)	0.0 (2)	-0.0 (3)	-89.09 (2)	-96.89 (2)	86.38 (3)
109	1	0.1 (2)	0.0 (2)	0.0 (9)	-253.72 (3)	-142.48 (2)	-99.14 (9)
109	2	0.1 (3)	0.0 (2)	0.0 (9)	-263.59 (3)	-224.89 (3)	-110.50 (9)
109	3	0.1 (2)	0.0 (2)	0.0 (9)	-240.74 (2)	-140.66 (2)	-107.82 (9)
109	4	0.1 (3)	0.0 (2)	0.0 (9)	-241.95 (3)	-254.37 (3)	-120.57 (9)
109	5	0.1 (2)	0.0 (2)	0.0 (9)	-245.47 (2)	-145.04 (2)	-96.92 (9)
109	6	0.1 (2)	0.0 (2)	0.0 (9)	-226.85 (2)	-250.66 (3)	-109.64 (9)
109	7	0.1 (2)	0.0 (2)	-0.0 (3)	-240.27 (2)	-144.52 (2)	-95.61 (9)
109	8	0.1 (2)	0.0 (3)	0.0 (9)	-215.09 (2)	-213.09 (3)	-99.76 (9)
110	1	0.0 (2)	0.0 (2)	-0.0 (3)	-117.82 (2)	-142.40 (2)	54.87 (3)
110	2	0.0 (2)	0.0 (2)	-0.0 (3)	-106.49 (2)	-189.62 (3)	73.78 (3)
110	3	0.0 (2)	0.0 (2)	-0.0 (3)	22.19 (2)	-130.76 (2)	-34.05 (11-II-4)
110	4	0.0 (2)	0.0 (2)	-0.0 (3)	25.41 (2)	-157.37 (3)	55.12 (3)
111	1	0.0 (2)	-0.0 (10)	-0.0 (3)	-213.78 (2)	61.28 (10)	96.47 (3)
111	2	0.0 (2)	-0.0 (10)	-0.0 (3)	-257.54 (2)	188.43 (10)	81.86 (3)
111	3	0.0 (2)	-0.0 (10)	0.0 (9)	-278.70 (2)	102.27 (10)	55.34 (3)
111	4	0.0 (2)	0.0 (2)	0.0 (9)	-238.49 (2)	-330.24 (2)	-89.80 (11-II-4)
111	5	0.0 (2)	-0.0 (10)	-0.0 (3)	60.80 (2)	55.21 (3)	34.85 (3)
111	6	0.0 (2)	-0.0 (10)	-0.0 (3)	126.22 (2)	189.03 (10)	29.38 (3)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
111	7	0.0(2)	-0.0(10)	-0.0(3)	134.36(2)	125.09(10)	-72.85(2)
111	8	0.0(2)	0.0(2)	-0.0(3)	61.01(2)	-277.29(2)	-38.88(9)
112	1	0.0(2)	-0.0(10)	-0.0(10)	-175.87(2)	-5.99(10)	-34.12(2)
112	2	0.0(2)	0.0(11-II-3)	-0.0(10)	-166.16(2)	7.65(10)	73.59(10)
112	3	0.0(10)	-0.0(2)	-0.0(2)	16.17(3)	1.36(2)	-35.53(10)
112	4	0.0(2)	-0.0(10)	-0.0(3)	17.27(3)	15.78(10)	50.72(2)
113	1	0.0(2)	0.1(2)	-0.0(3)	-226.20(2)	-349.71(2)	129.51(3)
113	2	0.0(2)	0.1(2)	-0.0(3)	-269.60(2)	-242.20(2)	138.69(3)
113	3	0.0(2)	0.0(2)	-0.0(3)	-209.08(2)	-163.80(2)	114.21(3)
113	4	0.0(2)	0.0(2)	-0.0(3)	-136.06(2)	-125.90(2)	92.76(3)
113	5	0.0(2)	0.1(2)	-0.0(3)	68.33(2)	-281.91(2)	47.69(3)
113	6	0.0(2)	0.1(2)	-0.0(3)	128.86(2)	-189.41(2)	84.72(3)
113	7	0.0(2)	0.0(2)	-0.0(3)	91.87(2)	-132.61(2)	63.19(3)
113	8	0.0(2)	0.0(2)	-0.0(3)	34.98(2)	-117.97(3)	57.31(3)
114	1	0.0(2)	0.0(3)	-0.0(3)	-93.07(2)	-135.93(3)	107.70(3)
114	2	0.0(3)	0.0(3)	-0.0(3)	-102.80(3)	-78.01(3)	88.72(3)
114	3	0.0(3)	0.0(3)	-0.0(3)	-84.02(3)	-34.79(3)	58.68(3)
114	4	0.0(3)	0.0(3)	-0.0(3)	-63.70(3)	12.36(11-II-4)	32.99(3)
114	5	0.0(2)	0.0(3)	-0.0(3)	22.56(3)	-123.04(2)	58.78(3)
114	6	0.0(3)	0.0(3)	-0.0(3)	39.51(2)	-67.93(3)	67.65(3)
114	7	0.0(3)	0.0(3)	-0.0(3)	23.18(2)	31.59(9)	46.61(3)
114	8	0.0(3)	0.0(3)	-0.0(3)	8.14(2)	12.96(11-II-4)	20.45(3)

**Risultati Analisi Dinamica - Sollecitazioni massime per combinazione - Sigma terreno platea - S.L.E**  
Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

Combinazione	Muro	Nodi	SigmaMax daN/cm <sup>2</sup>	SigmaMin daN/cm <sup>2</sup>
13	59	89-88-72-73	0.27	0.17
14	112	82-81-65-66	0.29	0.18
15	107	83-82-66-67	0.30	0.17
16	112	82-81-65-66	0.29	0.18
17	112	82-81-65-66	0.29	0.19
18	107	83-82-66-67	0.30	0.18
19	107	83-82-66-67	0.28	0.17
20	107	83-82-66-67	0.28	0.18
21	107	83-82-66-67	0.28	0.17
22	107	83-82-66-67	0.28	0.17
23-I-1	112	82-81-65-66	0.29	0.17
23-II-1	112	82-81-65-66	0.29	0.17
23-I-2	112	82-81-65-66	0.29	0.17
23-II-2	112	82-81-65-66	0.29	0.17
23-I-3	112	82-81-65-66	0.29	0.17
23-II-3	112	82-81-65-66	0.29	0.17
23-I-4	112	82-81-65-66	0.29	0.17
23-II-4	112	82-81-65-66	0.29	0.17
24-I-1	112	82-81-65-66	0.29	0.17
24-II-1	112	82-81-65-66	0.29	0.17
24-I-2	112	82-81-65-66	0.29	0.17
24-II-2	112	82-81-65-66	0.29	0.17
24-I-3	112	82-81-65-66	0.29	0.17
24-II-3	112	82-81-65-66	0.29	0.17
24-I-4	112	82-81-65-66	0.29	0.17
24-II-4	112	82-81-65-66	0.29	0.17
Assoluti				
15	107	83-82-66-67	0.30	
22	107	83-82-66-67		0.17

**Risultati Analisi Dinamica - Spostamenti massimi - Nodi - S.L.E.**  
Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	mm	mm	mm	°	°	°
1	0.00(13)	0.00(13)	-1.01(17)	-0.00(15)	0.00(13)	0.00(13)
2	0.00(13)	0.00(13)	-1.01(17)	-0.00(15)	0.00(13)	0.00(13)
3	0.00(13)	0.00(13)	-1.01(17)	-0.00(15)	0.00(13)	0.00(13)
4	0.00(13)	0.00(13)	-1.01(17)	-0.00(15)	0.00(13)	0.00(13)
5	0.00(13)	0.00(13)	-1.01(17)	-0.00(15)	0.00(13)	0.00(13)
6	0.00(13)	0.00(13)	-1.01(17)	-0.00(15)	0.00(13)	0.00(13)

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BTK3**

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Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
7	0.00 (13)	0.00 (13)	-1.01 (17)	-0.00 (15)	0.00 (13)	0.00 (13)
8	0.00 (13)	0.00 (13)	-1.01 (17)	-0.00 (15)	-0.00 (23-II-1)	0.00 (13)
9	0.00 (13)	0.00 (13)	-1.01 (17)	-0.00 (15)	-0.00 (23-II-1)	0.00 (13)
10	0.00 (13)	0.00 (13)	-1.01 (17)	-0.00 (15)	-0.00 (23-II-1)	0.00 (13)
11	0.00 (13)	0.00 (13)	-1.01 (17)	-0.00 (15)	-0.00 (13)	0.00 (13)
12	0.00 (13)	0.00 (13)	-1.01 (17)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
13	0.00 (13)	0.00 (13)	-1.01 (17)	-0.00 (13)	-0.00 (23-II-2)	0.00 (13)
14	0.00 (13)	0.00 (13)	-1.00 (17)	-0.00 (13)	-0.00 (23-II-2)	0.00 (13)
15	0.00 (13)	0.00 (13)	-0.98 (17)	-0.00 (13)	-0.00 (23-II-2)	0.00 (13)
16	0.00 (13)	0.00 (13)	-0.93 (17)	-0.00 (13)	-0.00 (23-II-2)	0.00 (13)
17	0.00 (13)	0.00 (13)	-1.15 (17)	-0.00 (15)	0.00 (13)	0.00 (13)
18	0.00 (13)	0.00 (13)	-1.15 (17)	-0.00 (15)	0.00 (13)	0.00 (13)
19	0.00 (13)	0.00 (13)	-1.15 (17)	-0.00 (15)	0.00 (13)	0.00 (13)
20	0.00 (13)	0.00 (13)	-1.14 (17)	-0.00 (15)	0.00 (13)	0.00 (13)
21	0.00 (13)	0.00 (13)	-1.14 (17)	-0.00 (15)	0.00 (13)	0.00 (13)
22	0.00 (13)	0.00 (13)	-1.13 (17)	-0.00 (15)	-0.00 (23-I-4)	0.00 (13)
23	0.00 (13)	0.00 (13)	-1.13 (17)	-0.00 (15)	-0.00 (23-I-4)	0.00 (13)
24	0.00 (13)	0.00 (13)	-1.12 (17)	-0.00 (15)	-0.00 (23-II-1)	0.00 (13)
25	0.00 (13)	0.00 (13)	-1.12 (17)	-0.00 (15)	-0.00 (23-II-1)	0.00 (13)
26	0.00 (13)	0.00 (13)	-1.11 (17)	-0.00 (15)	-0.00 (23-I-2)	0.00 (13)
27	0.00 (13)	0.00 (13)	-1.10 (17)	-0.00 (15)	-0.00 (23-I-2)	0.00 (13)
28	0.00 (13)	0.00 (13)	-1.09 (17)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
29	0.00 (13)	0.00 (13)	-1.08 (17)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
30	0.00 (13)	0.00 (13)	-1.06 (17)	-0.00 (13)	-0.00 (23-II-2)	0.00 (13)
31	0.00 (13)	0.00 (13)	-1.04 (17)	-0.00 (13)	-0.00 (23-II-2)	0.00 (13)
32	0.00 (13)	0.00 (13)	-1.00 (17)	-0.00 (13)	-0.00 (23-II-2)	0.00 (13)
33	0.00 (13)	0.00 (13)	-1.19 (17)	-0.00 (15)	0.00 (13)	0.00 (13)
34	0.00 (13)	0.00 (13)	-1.19 (17)	-0.00 (15)	0.00 (13)	0.00 (13)
35	0.00 (13)	0.00 (13)	-1.19 (17)	-0.00 (15)	0.00 (13)	0.00 (13)
36	0.00 (13)	0.00 (13)	-1.18 (17)	-0.00 (15)	0.00 (13)	0.00 (13)
37	0.00 (13)	0.00 (13)	-1.17 (17)	-0.00 (15)	-0.00 (23-II-4)	0.00 (13)
38	0.00 (13)	0.00 (13)	-1.17 (17)	-0.00 (15)	-0.00 (23-I-4)	0.00 (13)
39	0.00 (13)	0.00 (13)	-1.16 (17)	-0.00 (15)	-0.00 (23-I-4)	0.00 (13)
40	0.00 (13)	0.00 (13)	-1.15 (17)	-0.00 (15)	-0.00 (23-II-1)	0.00 (13)
41	0.00 (13)	0.00 (13)	-1.14 (17)	-0.00 (15)	-0.00 (23-II-1)	0.00 (13)
42	0.00 (13)	0.00 (13)	-1.14 (17)	-0.00 (15)	-0.00 (23-I-2)	0.00 (13)
43	0.00 (13)	0.00 (13)	-1.13 (17)	-0.00 (15)	-0.00 (23-I-2)	0.00 (13)
44	0.00 (13)	0.00 (13)	-1.12 (17)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
45	0.00 (13)	0.00 (13)	-1.10 (17)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
46	0.00 (13)	0.00 (13)	-1.08 (17)	-0.00 (13)	-0.00 (23-II-2)	0.00 (13)
47	0.00 (13)	0.00 (13)	-1.06 (17)	-0.00 (13)	-0.00 (23-II-2)	0.00 (13)
48	0.00 (13)	0.00 (13)	-1.01 (17)	-0.00 (13)	-0.00 (23-II-2)	0.00 (13)
49	0.00 (13)	0.00 (13)	-1.31 (18)	-0.00 (15)	0.00 (13)	0.00 (13)
50	0.00 (13)	0.00 (13)	-1.31 (18)	-0.00 (15)	0.00 (13)	0.00 (13)
51	0.00 (13)	0.00 (13)	-1.30 (18)	-0.00 (15)	0.00 (13)	0.00 (13)
52	0.00 (13)	0.00 (13)	-1.30 (18)	-0.00 (15)	-0.00 (23-II-4)	0.00 (13)
53	0.00 (13)	0.00 (13)	-1.28 (18)	-0.00 (15)	-0.00 (23-II-4)	0.00 (13)
54	0.00 (13)	0.00 (13)	-1.27 (18)	-0.00 (15)	-0.00 (23-I-4)	0.00 (13)
55	0.00 (13)	0.00 (13)	-1.26 (18)	-0.00 (15)	-0.00 (23-I-4)	0.00 (13)
56	0.00 (13)	0.00 (13)	-1.25 (18)	-0.00 (15)	-0.00 (23-II-1)	0.00 (13)
57	0.00 (13)	0.00 (13)	-1.24 (18)	-0.00 (15)	-0.00 (23-I-2)	0.00 (13)
58	0.00 (13)	0.00 (13)	-1.22 (18)	-0.00 (15)	-0.00 (23-I-2)	0.00 (13)
59	0.00 (13)	0.00 (13)	-1.21 (18)	-0.00 (15)	-0.00 (23-I-2)	0.00 (13)
60	0.00 (13)	0.00 (13)	-1.19 (18)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
61	0.00 (13)	0.00 (13)	-1.17 (18)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
62	0.00 (13)	0.00 (13)	-1.15 (18)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
63	0.00 (13)	0.00 (13)	-1.13 (18)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
64	0.00 (13)	0.00 (13)	-1.07 (18)	-0.00 (13)	-0.00 (23-II-2)	0.00 (13)
65	0.00 (13)	0.00 (13)	-1.48 (15)	-0.00 (15)	0.00 (13)	0.00 (13)
66	0.00 (13)	0.00 (13)	-1.48 (15)	-0.00 (15)	0.00 (13)	0.00 (13)
67	0.00 (13)	0.00 (13)	-1.48 (15)	-0.00 (15)	0.00 (13)	0.00 (13)
68	0.00 (13)	0.00 (13)	-1.47 (15)	-0.00 (15)	-0.00 (23-II-4)	0.00 (13)
69	0.00 (13)	0.00 (13)	-1.46 (15)	-0.00 (15)	-0.00 (23-II-4)	0.00 (13)
70	0.00 (13)	0.00 (13)	-1.44 (15)	-0.00 (15)	-0.00 (23-I-4)	0.00 (13)
71	0.00 (13)	0.00 (13)	-1.42 (15)	-0.00 (15)	-0.00 (23-I-4)	0.00 (13)
72	0.00 (13)	0.00 (13)	-1.41 (15)	-0.00 (15)	-0.00 (23-I-3)	0.00 (13)
73	0.00 (13)	0.00 (13)	-1.39 (15)	-0.00 (15)	-0.00 (23-I-2)	0.00 (13)
74	0.00 (13)	0.00 (13)	-1.37 (15)	-0.00 (15)	-0.00 (23-I-2)	0.00 (13)
75	0.00 (13)	0.00 (13)	-1.35 (15)	-0.00 (15)	-0.00 (23-I-2)	0.00 (13)
76	0.00 (13)	0.00 (13)	-1.33 (15)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
77	0.00 (13)	0.00 (13)	-1.30 (15)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
78	0.00 (13)	0.00 (13)	-1.27 (15)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
79	0.00 (13)	0.00 (13)	-1.24 (15)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
80	0.00 (13)	0.00 (13)	-1.18 (15)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
81	0.00 (13)	0.00 (13)	-1.50 (15)	-0.00 (15)	0.00 (13)	0.00 (13)



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
82	0.00 (13)	0.00 (13)	-1.50 (15)	-0.00 (15)	0.00 (13)	0.00 (13)
83	0.00 (13)	0.00 (13)	-1.50 (15)	-0.00 (15)	0.00 (13)	0.00 (13)
84	0.00 (13)	0.00 (13)	-1.49 (15)	-0.00 (15)	-0.00 (23-II-4)	0.00 (13)
85	0.00 (13)	0.00 (13)	-1.47 (15)	-0.00 (15)	-0.00 (23-II-4)	0.00 (13)
86	0.00 (13)	0.00 (13)	-1.46 (15)	-0.00 (15)	-0.00 (23-I-4)	0.00 (13)
87	0.00 (13)	0.00 (13)	-1.44 (15)	-0.00 (15)	-0.00 (23-I-4)	0.00 (13)
88	0.00 (13)	0.00 (13)	-1.42 (15)	-0.00 (15)	-0.00 (23-I-3)	0.00 (13)
89	0.00 (13)	0.00 (13)	-1.40 (15)	-0.00 (15)	-0.00 (23-I-3)	0.00 (13)
90	0.00 (13)	0.00 (13)	-1.39 (15)	-0.00 (15)	-0.00 (23-I-2)	0.00 (13)
91	0.00 (13)	0.00 (13)	-1.36 (15)	-0.00 (15)	-0.00 (23-I-2)	0.00 (13)
92	0.00 (13)	0.00 (13)	-1.34 (15)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
93	0.00 (13)	0.00 (13)	-1.32 (15)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
94	0.00 (13)	0.00 (13)	-1.29 (15)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
95	0.00 (13)	0.00 (13)	-1.25 (15)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
96	0.00 (13)	0.00 (13)	-1.19 (15)	-0.00 (15)	-0.00 (23-II-2)	0.00 (13)
118	-0.02 (23-II-4)	0.11 (15)	-1.16 (17)	-0.01 (15)	-0.01 (23-II-4)	-0.00 (23-II-1)
119	-0.01 (23-II-4)	0.11 (15)	-1.16 (17)	-0.01 (15)	-0.00 (23-II-4)	-0.00 (23-II-1)
120	-0.01 (23-II-4)	0.11 (15)	-1.15 (17)	-0.01 (15)	-0.01 (23-II-4)	-0.00 (23-II-1)
121	-0.01 (23-II-4)	0.10 (15)	-1.15 (17)	-0.01 (15)	-0.00 (23-II-4)	-0.00 (23-II-1)
122	-0.01 (23-I-4)	0.10 (15)	-1.14 (17)	-0.01 (15)	-0.00 (23-I-4)	-0.00 (23-II-4)
123	-0.01 (23-I-4)	0.10 (15)	-1.14 (17)	-0.01 (15)	-0.00 (23-I-4)	-0.00 (23-II-1)
124	-0.01 (23-II-1)	0.10 (15)	-1.13 (17)	-0.01 (15)	-0.00 (23-II-1)	-0.00 (23-II-1)
125	-0.01 (23-II-1)	0.09 (15)	-1.13 (17)	-0.01 (15)	-0.00 (23-II-1)	-0.00 (23-II-1)
126	-0.01 (23-I-2)	0.09 (15)	-1.12 (17)	-0.01 (15)	-0.00 (23-I-2)	-0.00 (23-I-2)
127	-0.02 (23-I-2)	0.09 (15)	-1.11 (17)	-0.01 (15)	-0.01 (23-I-2)	-0.00 (23-II-2)
128	-0.02 (23-II-2)	0.09 (15)	-1.10 (17)	-0.01 (15)	-0.01 (23-II-2)	-0.00 (23-II-1)
129	-0.02 (23-II-2)	0.08 (15)	-1.09 (17)	-0.01 (15)	-0.01 (23-II-2)	-0.00 (23-II-1)
130	-0.03 (23-II-2)	0.08 (15)	-1.07 (17)	-0.01 (15)	-0.01 (23-II-2)	-0.00 (23-II-2)
131	-0.03 (23-II-2)	0.08 (15)	-1.06 (17)	-0.01 (15)	-0.01 (23-II-2)	0.00 (23-I-1)
150	-0.02 (23-II-4)	0.07 (15)	-1.31 (18)	-0.01 (15)	-0.01 (23-II-4)	-0.00 (23-II-3)
151	-0.01 (23-II-4)	0.07 (15)	-1.31 (18)	-0.01 (15)	-0.00 (23-II-4)	-0.00 (23-II-4)
152	-0.02 (23-II-4)	0.07 (15)	-1.30 (18)	-0.01 (15)	-0.01 (23-II-4)	-0.00 (23-II-3)
153	-0.02 (23-II-4)	0.07 (15)	-1.29 (18)	-0.01 (15)	-0.01 (23-II-4)	-0.00 (23-II-3)
154	-0.02 (23-I-4)	0.06 (15)	-1.28 (18)	-0.01 (15)	-0.01 (23-I-4)	-0.00 (23-I-3)
155	-0.02 (23-I-4)	0.06 (15)	-1.26 (18)	-0.01 (15)	-0.01 (23-I-4)	-0.00 (23-I-3)
156	-0.02 (23-II-1)	0.06 (15)	-1.25 (18)	-0.01 (15)	-0.01 (23-II-1)	-0.00 (23-I-3)
157	-0.02 (23-II-1)	0.06 (15)	-1.24 (18)	-0.01 (15)	-0.01 (23-I-2)	-0.00 (23-I-3)
158	-0.02 (23-I-2)	0.06 (15)	-1.23 (18)	-0.01 (15)	-0.01 (23-I-2)	-0.00 (23-I-3)
159	-0.02 (23-I-2)	0.05 (15)	-1.21 (18)	-0.00 (15)	-0.01 (23-I-2)	-0.00 (23-I-2)
160	-0.02 (23-II-2)	0.05 (15)	-1.20 (18)	-0.00 (15)	-0.01 (23-II-2)	-0.00 (15)
161	-0.03 (23-II-2)	0.05 (15)	-1.18 (18)	-0.00 (15)	-0.01 (23-II-2)	-0.00 (15)
162	-0.03 (23-II-2)	0.05 (15)	-1.15 (18)	-0.00 (15)	-0.01 (23-II-2)	-0.00 (15)
163	-0.03 (23-II-2)	0.05 (15)	-1.13 (18)	-0.00 (15)	-0.01 (23-II-2)	0.00 (23-I-3)
166	-0.02 (23-II-4)	0.14 (15)	-1.52 (15)	-0.02 (15)	-0.01 (23-II-4)	0.00 (15)
167	-0.02 (23-II-4)	0.14 (15)	-1.51 (15)	-0.02 (15)	-0.01 (23-II-4)	0.00 (23-II-4)
168	-0.02 (23-II-4)	0.14 (15)	-1.50 (15)	-0.02 (15)	-0.01 (23-II-4)	0.00 (23-II-3)
169	-0.02 (23-II-4)	0.14 (15)	-1.49 (15)	-0.02 (15)	-0.01 (23-II-4)	0.00 (23-II-3)
170	-0.02 (23-I-4)	0.14 (15)	-1.47 (15)	-0.02 (15)	-0.01 (23-I-4)	0.00 (23-II-4)
171	-0.02 (23-I-4)	0.14 (15)	-1.46 (15)	-0.02 (15)	-0.01 (23-I-4)	0.00 (23-II-3)
172	-0.02 (23-I-3)	0.14 (15)	-1.44 (15)	-0.02 (15)	-0.01 (23-I-3)	0.00 (23-I-3)
173	-0.02 (23-I-3)	0.14 (15)	-1.42 (15)	-0.02 (15)	-0.01 (23-I-3)	0.00 (23-I-3)
174	-0.02 (23-I-2)	0.14 (15)	-1.40 (15)	-0.02 (15)	-0.01 (23-I-2)	0.00 (23-I-2)
175	-0.03 (23-I-2)	0.13 (15)	-1.38 (15)	-0.02 (15)	-0.01 (23-I-2)	0.00 (23-II-2)
176	-0.03 (23-II-2)	0.13 (15)	-1.36 (15)	-0.02 (15)	-0.01 (23-II-2)	0.00 (23-II-3)
177	-0.03 (23-II-2)	0.13 (15)	-1.33 (15)	-0.02 (15)	-0.01 (23-II-2)	0.00 (23-II-3)
178	-0.03 (23-II-2)	0.13 (15)	-1.31 (15)	-0.02 (15)	-0.01 (23-II-2)	0.00 (23-II-2)
179	-0.04 (23-II-2)	0.13 (15)	-1.28 (15)	-0.02 (15)	-0.01 (23-II-2)	0.00 (23-II-2)

**Risultati Analisi Dinamica - Reazioni massime - Nodi - S.L.E**  
Scenario di calcolo: ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO

Nodo	Rx	Ry	Rz	Mx	My	Mz
	daN	daN	daN	daN*m	daN*m	daN*m
1	-17.52 (23-II-1)	-11.95 (23-II-4)	0	0	0	1.64 (15)
2	-93.78 (23-I-4)	-17.11 (23-I-3)	0	0	0	4.60 (13)
3	-129.51 (23-I-4)	-26.92 (23-I-3)	0	0	0	4.95 (23-II-1)
4	-166.64 (23-II-3)	-30.10 (23-I-2)	0	0	0	4.98 (23-II-1)
5	-201.58 (23-II-3)	-31.09 (23-I-2)	0	0	0	6.04 (23-I-3)
6	-235.40 (23-II-3)	-31.80 (23-I-2)	0	0	0	7.99 (23-II-3)
7	-267.69 (23-II-3)	-32.28 (23-I-2)	0	0	0	10.31 (23-II-3)
8	-298.14 (23-II-3)	-32.56 (23-I-4)	0	0	0	12.64 (23-II-1)
9	-326.56 (23-II-3)	-32.77 (23-II-4)	0	0	0	14.79 (23-II-1)
10	-352.87 (23-II-3)	-32.89 (23-II-4)	0	0	0	16.77 (23-II-2)



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

Pagina 76 di 262

Nodo	Rx	Ry	Rz	Mx	My	Mz
11	-377.26 (23-II-3)	-32.81 (23-II-4)	0	0	0	18.88 (23-II-3)
12	-401.51 (23-I-2)	-32.60 (23-II-4)	0	0	0	21.98 (23-II-3)
13	-359.98 (23-I-2)	-21.27 (23-II-3)	0	0	0	21.49 (15)
14	-54.84 (13)	-16.44 (23-II-3)	0	0	0	-11.21 (23-I-1)
15	79.36 (14)	-13.05 (23-II-3)	0	0	0	-15.64 (23-I-1)
16	31.04 (22)	13.75 (15)	0	0	0	-3.64 (22)
17	-59.63 (23-II-1)	-154.37 (23-II-4)	0	0	0	-7.68 (23-II-4)
18	-334.73 (23-II-1)	-414.96 (23-II-1)	0	0	0	-19.11 (13)
19	153.05 (23-II-1)	-392.69 (15)	0	0	0	-12.17 (16)
20	105.76 (23-II-1)	-363.04 (15)	0	0	0	-6.12 (13)
21	74.44 (23-II-1)	-315.28 (15)	0	0	0	4.13 (15)
22	59.22 (23-I-4)	-289.25 (15)	0	0	0	2.14 (15)
23	47.90 (23-II-1)	-277.08 (15)	0	0	0	-5.62 (23-I-1)
24	36.77 (23-II-1)	-271.52 (15)	0	0	0	-9.05 (23-I-1)
25	26.03 (23-II-1)	-268.04 (15)	0	0	0	-11.76 (23-I-1)
26	-19.04 (15)	-262.39 (15)	0	0	0	-13.70 (23-II-2)
27	-34.10 (15)	-247.86 (15)	0	0	0	-15.17 (16)
28	-60.89 (15)	-209.49 (15)	0	0	0	-17.02 (16)
29	-94.21 (15)	176.11 (16)	0	0	0	-12.08 (16)
30	-73.94 (13)	194.41 (16)	0	0	0	26.33 (23-I-1)
31	372.55 (22)	-90.78 (13)	0	0	0	34.58 (15)
32	62.65 (22)	245.95 (15)	0	0	0	11.15 (22)
33	-93.38 (23-II-4)	188.69 (13)	0	0	0	10.23 (13)
34	-193.30 (23-II-1)	246.28 (13)	0	0	0	-11.14 (13)
35	35.93 (23-I-1)	224.49 (13)	0	0	0	-1.46 (23-I-1)
36	148.60 (23-II-1)	230.06 (13)	0	0	0	-6.48 (23-II-1)
37	89.78 (15)	236.84 (15)	0	0	0	-3.95 (15)
38	43.64 (15)	270.30 (15)	0	0	0	-1.82 (15)
39	11.98 (15)	283.77 (15)	0	0	0	0
40	-33.42 (23-I-1)	289.50 (15)	0	0	0	1.05 (23-I-1)
41	-50.50 (23-I-1)	292.71 (15)	0	0	0	1.63 (23-I-1)
42	-57.84 (23-II-2)	297.20 (15)	0	0	0	1.83 (23-II-2)
43	-53.93 (23-II-2)	306.54 (15)	0	0	0	1.57 (23-II-2)
44	-48.67 (15)	323.60 (15)	0	0	0	1.23 (15)
45	-23.65 (15)	345.02 (15)	0	0	0	0
46	83.86 (23-I-1)	336.97 (15)	0	0	0	-1.99 (23-I-1)
47	134.27 (22)	338.36 (15)	0	0	0	9.96 (15)
48	21.66 (22)	257.89 (15)	0	0	0	3.98 (15)
49	-181.00 (23-II-4)	242.01 (13)	0	0	0	11.89 (15)
50	-819.16 (23-II-4)	201.15 (22)	0	0	0	17.18 (23-I-4)
51	476.48 (23-II-4)	216.64 (23-I-3)	0	0	0	2.48 (22)
52	396.05 (23-II-4)	211.14 (23-I-2)	0	0	0	-7.79 (15)
53	244.84 (23-II-4)	236.69 (23-II-3)	0	0	0	-1.95 (15)
54	186.71 (23-I-4)	249.30 (23-II-3)	0	0	0	7.04 (23-II-3)
55	162.13 (23-I-4)	251.05 (23-II-2)	0	0	0	10.71 (23-II-3)
56	147.87 (23-II-1)	248.65 (23-II-2)	0	0	0	13.02 (23-II-3)
57	141.50 (23-II-1)	245.30 (23-I-4)	0	0	0	14.22 (23-II-3)
58	142.89 (23-I-2)	242.13 (23-I-3)	0	0	0	14.33 (23-II-3)
59	150.45 (23-I-2)	239.26 (23-I-3)	0	0	0	13.21 (23-II-3)
60	162.01 (23-II-1)	234.01 (23-I-3)	0	0	0	12.17 (15)
61	157.00 (23-II-2)	224.27 (23-II-3)	0	0	0	10.88 (15)
62	-202.72 (13)	185.74 (23-II-3)	0	0	0	8.44 (15)
63	492.33 (22)	189.54 (22)	0	0	0	-3.71 (22)
64	49.42 (22)	326.57 (15)	0	0	0	5.98 (15)
65	-127.44 (23-II-3)	-51.82 (13)	0	0	0	-15.99 (15)
66	-390.27 (23-II-3)	-310.92 (13)	0	0	0	-19.34 (23-I-4)
67	328.23 (23-II-3)	-476.26 (15)	0	0	0	26.63 (23-II-3)
68	312.74 (23-II-3)	-518.71 (15)	0	0	0	27.52 (23-II-3)
69	235.00 (23-II-3)	-579.81 (15)	0	0	0	17.53 (23-II-4)
70	205.09 (23-I-3)	-602.09 (15)	0	0	0	12.38 (23-I-4)
71	194.88 (23-I-3)	-610.21 (15)	0	0	0	10.26 (23-I-3)
72	187.97 (23-I-3)	-613.45 (15)	0	0	0	9.06 (23-I-3)
73	181.83 (23-I-3)	-614.50 (15)	0	0	0	8.31 (23-I-3)
74	176.78 (23-I-3)	-614.33 (15)	0	0	0	7.98 (23-I-2)
75	174.23 (23-I-2)	-613.05 (15)	0	0	0	8.10 (23-I-2)
76	173.04 (23-II-2)	-609.64 (15)	0	0	0	8.62 (23-II-3)
77	166.39 (23-II-3)	-603.02 (15)	0	0	0	8.64 (23-II-3)
78	108.22 (23-II-3)	-606.18 (15)	0	0	0	-10.62 (13)
79	432.37 (15)	-535.66 (15)	0	0	0	5.24 (23-II-3)
80	42.58 (13)	-12.36 (15)	0	0	0	8.35 (13)
81	-32.01 (15)	5.03 (15)	0	0	0	0
82	-125.34 (15)	3.52 (23-I-3)	0	0	0	1.79 (13)
83	-36.40 (13)	3.67 (23-II-3)	0	0	0	0
84	45.37 (23-II-4)	3.53 (23-I-3)	0	0	0	0
85	47.53 (23-II-4)	3.52 (23-I-2)	0	0	0	0

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
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Nodo	Rx	Ry	Rz	Mx	My	Mz
86	47.34 (23-I-3)	3.27 (23-II-2)	0	0	0	0
87	45.70 (23-I-3)	3.07 (23-I-2)	0	0	0	0
88	43.45 (23-I-3)	2.92 (22)	0	0	0	0
89	41.31 (23-I-3)	2.79 (22)	0	0	0	0
90	39.74 (23-I-3)	2.65 (22)	0	0	0	0
91	39.41 (15)	2.51 (22)	0	0	0	0
92	42.67 (15)	2.35 (22)	0	0	0	0
93	46.65 (15)	2.14 (15)	0	0	0	0
94	51.01 (15)	1.99 (22)	0	0	0	0
95	209.60 (15)	-92.58 (15)	0	0	0	-3.32 (15)
96	10.50 (15)	4.16 (15)	0	0	0	0

**Risultati Analisi Dinamica - Sollecitazioni Massime - Muri discretizzati - S.L.E**  
Scenario di calcolo: ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO

Muro	Pann.	Sxx MPa	Syy MPa	Sxy MPa	Mxx daN*m/m	Myy daN*m/m	Mxy daN*m/m
1	1	0.0 (13)	-0.0 (15)	0.0 (15)	-136.12 (13)	110.27 (15)	-133.59 (15)
1	2	0.0 (13)	-0.0 (15)	0.0 (15)	-76.84 (13)	232.78 (15)	-103.39 (15)
1	3	0.0 (22)	-0.0 (15)	0.0 (15)	-62.81 (13)	202.38 (15)	28.84 (13)
1	4	0.0 (22)	-0.0 (15)	0.0 (15)	-119.82 (22)	-40.56 (13)	17.68 (13)
1	5	0.0 (13)	-0.0 (15)	0.0 (15)	-138.95 (13)	100.84 (15)	-86.45 (15)
1	6	0.0 (13)	-0.0 (15)	0.0 (15)	-83.47 (13)	294.83 (15)	-89.98 (15)
1	7	0.0 (22)	-0.0 (15)	0.0 (15)	-83.72 (22)	250.97 (15)	-41.63 (15)
1	8	0.0 (22)	-0.0 (15)	0.0 (15)	-148.98 (22)	-114.10 (13)	-61.98 (15)
1	9	0.0 (13)	-0.0 (15)	0.0 (15)	-129.94 (13)	110.71 (15)	-72.77 (15)
1	10	0.0 (13)	-0.0 (15)	0.0 (15)	-92.88 (22)	309.75 (15)	-80.40 (15)
1	11	0.0 (22)	-0.0 (15)	0.0 (15)	-99.64 (22)	255.19 (15)	-72.24 (15)
1	12	0.0 (22)	-0.0 (15)	0.0 (15)	-147.63 (22)	-123.85 (13)	-80.81 (15)
1	13	0.0 (13)	-0.0 (15)	0.0 (15)	-121.28 (13)	140.24 (15)	-53.28 (15)
1	14	0.0 (13)	-0.0 (15)	0.0 (15)	-105.28 (22)	272.08 (15)	-80.90 (15)
1	15	0.0 (13)	-0.0 (15)	0.0 (15)	-112.91 (22)	215.54 (15)	-140.46 (15)
1	16	0.0 (22)	-0.0 (15)	0.0 (15)	-139.96 (22)	-67.22 (13)	-134.75 (15)
2	1	0.0 (13)	-0.0 (15)	0.0 (15)	-111.29 (13)	146.27 (15)	-87.82 (15)
2	2	0.0 (13)	-0.1 (15)	0.0 (15)	-88.53 (13)	279.87 (15)	-78.64 (23-I-2)
2	3	0.0 (13)	-0.0 (15)	0.0 (15)	-96.31 (22)	216.15 (15)	36.58 (13)
2	4	0.0 (22)	-0.0 (15)	0.0 (15)	-127.05 (22)	-69.85 (13)	23.00 (13)
2	5	0.0 (13)	-0.0 (15)	0.0 (15)	-122.26 (13)	126.34 (15)	-67.69 (15)
2	6	0.0 (13)	-0.0 (15)	0.0 (15)	-91.18 (13)	332.89 (15)	-80.88 (15)
2	7	0.0 (13)	-0.0 (15)	0.0 (15)	-95.94 (22)	260.77 (15)	-55.87 (15)
2	8	0.0 (22)	-0.0 (15)	0.0 (15)	-139.69 (22)	-137.55 (13)	-63.28 (15)
2	9	0.0 (13)	-0.0 (15)	0.0 (15)	-129.74 (13)	126.28 (15)	-63.27 (15)
2	10	0.0 (13)	-0.0 (15)	0.0 (15)	-100.61 (13)	336.58 (15)	-83.04 (15)
2	11	0.0 (13)	-0.0 (15)	0.0 (15)	-105.11 (23-II-2)	266.34 (15)	-81.97 (15)
2	12	0.0 (22)	-0.0 (15)	0.0 (15)	-146.95 (23-II-2)	-144.21 (13)	-81.26 (15)
2	13	0.0 (13)	-0.0 (15)	0.0 (15)	-135.00 (13)	146.21 (15)	-48.30 (15)
2	14	0.0 (13)	-0.1 (15)	0.0 (23-I-2)	-122.74 (23-II-2)	288.71 (15)	-87.81 (15)
2	15	0.0 (13)	-0.0 (15)	0.0 (23-I-2)	-129.46 (23-II-2)	227.51 (15)	-157.29 (15)
2	16	0.0 (22)	-0.0 (15)	0.0 (15)	-152.85 (23-II-2)	-82.66 (13)	-137.46 (15)
3	1	0.0 (23-I-1)	0.0 (23-II-3)	0.0 (23-II-2)	-179.64 (22)	-91.70 (23-II-3)	-80.19 (23-II-2)
3	2	0.1 (23-I-1)	0.0 (23-II-3)	0.0 (15)	-185.52 (22)	-60.94 (23-II-3)	-91.86 (23-II-2)
3	3	0.1 (23-I-1)	0.0 (23-II-3)	0.0 (15)	-219.63 (22)	-34.67 (23-II-3)	-90.95 (23-II-2)
3	4	0.1 (23-I-1)	0.0 (23-II-3)	0.0 (15)	-236.06 (23-II-2)	-12.01 (15)	-52.04 (23-II-2)
3	5	0.0 (23-I-1)	0.0 (23-II-3)	0.0 (23-II-2)	-214.87 (23-I-1)	-106.32 (23-II-3)	-81.61 (23-II-2)
3	6	0.1 (23-I-1)	0.0 (23-II-3)	0.0 (23-II-2)	-237.45 (23-I-1)	-71.21 (23-II-3)	-93.65 (23-II-2)
3	7	0.1 (23-I-1)	0.0 (23-II-3)	0.0 (23-II-2)	-262.98 (23-I-1)	-37.91 (23-I-2)	-94.83 (23-II-2)
3	8	0.1 (23-I-1)	0.0 (23-II-3)	0.0 (23-II-2)	-262.14 (23-I-1)	-15.39 (15)	-48.45 (23-II-2)
3	9	0.0 (23-I-1)	0.0 (23-II-3)	0.0 (23-II-2)	-223.47 (23-I-1)	-111.99 (23-II-3)	-94.04 (23-II-2)
3	10	0.1 (23-I-1)	0.0 (23-II-3)	0.0 (23-II-2)	-248.07 (23-I-1)	-71.51 (23-II-3)	-98.19 (23-II-2)
3	11	0.1 (23-I-1)	0.0 (23-II-3)	0.0 (23-II-2)	-256.07 (23-I-1)	-35.79 (23-I-2)	-99.63 (23-II-2)
3	12	0.1 (23-I-1)	0.0 (23-II-3)	0.0 (23-II-2)	-252.88 (23-I-1)	-12.36 (15)	-48.76 (23-II-2)
3	13	0.0 (23-I-1)	0.0 (23-II-3)	0.0 (23-II-2)	-206.07 (23-I-1)	-103.43 (23-II-3)	-108.58 (15)
3	14	0.1 (23-I-1)	0.0 (23-II-3)	0.0 (23-II-2)	-215.02 (23-I-1)	-64.78 (23-II-3)	-110.11 (15)
3	15	0.1 (23-I-1)	0.0 (23-I-3)	0.0 (23-II-2)	-190.89 (23-I-1)	-28.61 (23-I-3)	-99.01 (15)

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BTK3**

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Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
3	16	0.1 (23-I-1)	0.0 (23-II-3)	0.0 (23-II-2)	-202.69 (23-I-1)	-3.62 (15)	-57.24 (15)
4	1	0.0 (22)	0.0 (23-II-3)	0.0 (15)	-95.72 (22)	-52.83 (23-II-3)	-64.00 (15)
4	2	0.0 (22)	0.0 (23-II-3)	0.0 (15)	-49.78 (13)	-25.91 (23-II-3)	-71.11 (23-II-3)
4	3	0.0 (22)	0.0 (23-II-3)	0.0 (15)	-61.85 (13)	-13.36 (23-II-2)	-62.77 (23-II-3)
4	4	0.0 (22)	0.0 (23-II-3)	0.0 (15)	-93.44 (22)	3.79 (22)	-38.18 (23-II-2)
4	5	0.0 (22)	0.0 (23-II-3)	0.0 (15)	-143.82 (22)	-79.80 (23-II-3)	-41.26 (15)
4	6	0.0 (22)	0.0 (23-II-3)	0.0 (15)	-115.96 (22)	-36.86 (23-II-3)	-67.74 (23-II-2)
4	7	0.0 (22)	0.0 (23-II-3)	0.0 (15)	-117.81 (22)	-20.55 (23-II-2)	-67.83 (23-II-2)
4	8	0.0 (22)	0.0 (23-II-3)	0.0 (15)	-135.31 (22)	-6.66 (15)	-48.20 (23-II-2)
4	9	0.0 (22)	0.0 (23-II-3)	0.0 (23-II-2)	-179.20 (22)	-95.28 (23-II-3)	-41.39 (15)
4	10	0.0 (22)	0.0 (23-II-3)	0.0 (23-II-2)	-189.24 (22)	-51.47 (23-II-3)	-65.83 (23-II-2)
4	11	0.0 (22)	0.0 (23-II-3)	0.0 (23-II-2)	-189.69 (22)	-29.58 (23-II-2)	-71.66 (23-II-2)
4	12	0.0 (22)	0.0 (23-II-3)	0.0 (23-II-2)	-182.01 (22)	-10.74 (15)	-52.24 (23-II-2)
4	13	0.0 (22)	0.0 (23-II-3)	0.0 (23-II-2)	-222.45 (23-I-1)	-97.40 (23-II-3)	-64.31 (15)
4	14	0.0 (22)	0.0 (23-II-3)	0.0 (23-II-2)	-281.75 (23-I-1)	-68.94 (23-II-3)	-74.64 (15)
4	15	0.0 (22)	0.0 (23-II-3)	0.0 (23-II-2)	-275.06 (23-I-1)	-41.61 (23-II-3)	-73.21 (15)
4	16	0.0 (23-I-1)	0.0 (23-II-3)	0.0 (23-II-2)	-238.10 (23-I-1)	-12.77 (15)	-47.08 (15)
5	1	0.0 (22)	-0.0 (15)	0.0 (15)	-127.28 (22)	-54.02 (23-I-2)	-117.23 (15)
5	2	0.0 (22)	-0.0 (15)	0.0 (15)	-71.69 (15)	143.61 (15)	-121.29 (22)
5	3	0.0 (22)	-0.0 (15)	0.0 (15)	-71.65 (15)	132.50 (15)	-75.22 (23-II-3)
5	4	0.0 (22)	-0.0 (15)	0.0 (15)	-94.98 (22)	62.12 (16)	-50.68 (23-II-2)
5	5	0.0 (22)	-0.0 (15)	0.0 (15)	-157.56 (22)	-118.80 (23-I-2)	-81.24 (15)
5	6	0.0 (22)	-0.0 (15)	0.0 (15)	-109.33 (22)	176.01 (15)	-94.66 (23-II-2)
5	7	0.0 (22)	-0.0 (15)	0.0 (15)	-94.25 (22)	164.71 (15)	-78.40 (23-II-2)
5	8	0.0 (22)	-0.0 (15)	0.0 (15)	-111.91 (22)	61.02 (16)	-64.06 (23-II-2)
5	9	0.0 (22)	-0.0 (15)	0.0 (15)	-155.14 (22)	-142.81 (23-I-2)	-73.16 (15)
5	10	0.0 (22)	-0.0 (15)	0.0 (15)	-128.62 (22)	178.99 (15)	-82.93 (23-II-2)
5	11	0.0 (22)	-0.0 (15)	0.0 (15)	-119.73 (22)	173.52 (15)	-76.35 (23-II-2)
5	12	0.0 (22)	-0.0 (15)	0.0 (15)	-130.97 (22)	67.12 (16)	-68.82 (23-II-2)
5	13	0.0 (22)	-0.0 (15)	0.0 (23-II-2)	-156.33 (23-II-2)	-114.36 (23-I-2)	-60.09 (15)
5	14	0.0 (22)	-0.0 (15)	0.0 (23-I-2)	-162.88 (23-II-2)	153.07 (15)	-61.95 (15)
5	15	0.0 (22)	-0.0 (15)	0.0 (23-I-2)	-148.23 (23-II-2)	153.12 (15)	-89.76 (15)
5	16	0.0 (22)	-0.0 (15)	0.0 (23-II-2)	-145.12 (22)	78.17 (16)	-87.17 (15)
6	1	0.0 (23-II-2)	-0.0 (15)	0.0 (15)	-133.05 (22)	-127.05 (23-I-2)	-107.46 (23-I-2)
6	2	0.0 (23-II-2)	-0.0 (15)	0.0 (15)	-113.98 (22)	154.22 (15)	-139.39 (23-II-2)
6	3	0.0 (22)	-0.0 (15)	0.0 (15)	-115.95 (22)	157.82 (15)	-103.83 (23-II-2)
6	4	0.0 (22)	-0.0 (15)	0.0 (15)	-136.95 (22)	82.60 (16)	-79.06 (23-II-2)
6	5	0.0 (23-II-2)	-0.0 (15)	0.0 (15)	-153.73 (23-II-2)	-195.83 (23-I-2)	-82.77 (15)
6	6	0.0 (23-II-2)	-0.0 (15)	0.0 (15)	-122.42 (22)	179.99 (15)	-96.44 (23-II-2)
6	7	0.0 (23-II-2)	-0.0 (15)	0.0 (15)	-124.80 (22)	186.65 (15)	-91.55 (23-II-2)
6	8	0.0 (22)	-0.0 (15)	0.0 (15)	-144.10 (22)	78.60 (16)	-89.09 (23-II-2)
6	9	0.0 (23-II-2)	-0.0 (15)	0.0 (23-II-2)	-167.86 (23-II-2)	-207.89 (23-I-2)	-80.29 (15)
6	10	0.0 (23-II-2)	-0.0 (15)	0.0 (23-II-2)	-145.24 (23-II-2)	180.56 (15)	-86.96 (15)
6	11	0.0 (23-II-2)	-0.0 (15)	0.0 (23-II-2)	-142.86 (23-I-1)	187.92 (15)	-88.59 (15)
6	12	0.0 (23-I-1)	-0.0 (15)	0.0 (23-II-2)	-153.58 (23-I-1)	79.54 (16)	-92.19 (23-II-2)
6	13	0.0 (23-II-2)	-0.0 (15)	0.0 (23-II-2)	-175.11 (23-II-2)	-157.19 (23-I-2)	-66.47 (15)
6	14	0.0 (23-II-2)	-0.0 (15)	0.0 (23-II-2)	-172.79 (23-I-1)	153.04 (15)	-68.24 (15)
6	15	0.0 (23-I-1)	-0.0 (15)	0.0 (23-II-2)	-162.35 (23-I-1)	160.64 (15)	-103.43 (15)
6	16	0.0 (23-I-1)	-0.0 (15)	0.0 (23-II-2)	-163.46 (23-I-1)	84.38 (16)	-107.28 (15)
7	1	0.0 (22)	-0.0 (16)	0.0 (15)	-144.76 (22)	91.30 (16)	-44.18 (23-II-2)
7	2	0.0 (23-I-1)	0.0 (13)	0.0 (15)	-173.45 (22)	-125.40 (15)	-51.82 (23-II-2)
7	3	0.0 (22)	0.0 (13)	0.0 (23-II-2)	-149.41 (23-I-1)	149.33 (15)	-75.42 (15)
7	4	0.0 (23-I-1)	0.0 (13)	0.0 (15)	-193.93 (23-I-1)	-190.26 (15)	-86.77 (23-II-2)
7	5	0.0 (23-I-1)	0.0 (13)	0.0 (23-II-2)	-160.06 (23-I-1)	150.42 (15)	-85.97 (15)
7	6	0.0 (23-I-1)	0.0 (13)	0.0 (23-II-2)	-201.07 (23-I-1)	-193.15 (15)	-98.36 (23-II-2)
7	7	0.0 (23-I-1)	-0.0 (16)	0.0 (23-II-2)	-169.83 (23-I-1)	91.30 (16)	-126.18 (15)
7	8	0.0 (23-I-1)	0.0 (13)	0.0 (23-II-2)	-196.28 (23-I-1)	-130.88 (15)	-124.86 (15)
8	1	0.0 (22)	-0.0 (16)	0.0 (15)	-95.93 (22)	77.57 (15)	-17.62 (15)
8	2	0.0 (22)	0.0 (15)	0.0 (15)	-130.96 (22)	-114.46 (15)	-29.72 (15)
8	3	0.0 (22)	0.0 (15)	0.0 (15)	-120.09 (22)	133.29 (15)	-43.14 (15)
8	4	0.0 (22)	0.0 (13)	0.0 (15)	-163.73 (22)	-187.60 (15)	-61.23 (15)
8	5	0.0 (22)	0.0 (13)	0.0 (23-II-2)	-134.40 (22)	136.44 (15)	-53.64 (15)
8	6	0.0 (22)	0.0 (13)	0.0 (15)	-171.81 (22)	-186.11 (15)	-65.66 (23-II-2)
8	7	0.0 (22)	-0.0 (16)	0.0 (23-II-2)	-154.62 (22)	84.86 (16)	-94.36 (15)
8	8	0.0 (22)	0.0 (13)	0.0 (23-II-2)	-180.19 (22)	-124.59 (15)	-93.29 (15)
9	1	-0.0 (22)	-0.1 (22)	-0.0 (22)	-43.04 (15)	-498.26 (15)	-44.02 (15)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
9	2	-0.0 (16)	-0.1 (22)	-0.0 (23-II-2)	-29.05 (15)	-448.37 (15)	-12.62 (23-II-3)
9	3	-0.0 (16)	-0.1 (16)	0.0 (16)	67.07 (23-II-3)	657.14 (23-II-3)	-155.80 (23-II-3)
9	4	0.1 (23-I-2)	-0.3 (23-I-2)	0.1 (23-I-2)	-156.00 (23-I-3)	1066.27 (23-II-3)	-357.26 (23-II-3)
9	5	-0.0 (16)	-0.1 (13)	-0.0 (13)	-55.95 (15)	-456.77 (15)	-34.99 (15)
9	6	-0.0 (16)	-0.1 (13)	-0.0 (22)	-58.12 (15)	-396.78 (15)	-18.37 (22)
9	7	-0.0 (16)	-0.1 (23-I-2)	0.0 (23-II-2)	-85.82 (15)	-246.96 (15)	-50.42 (23-II-3)
9	8	0.1 (16)	0.0 (23-I-2)	0.0 (23-II-2)	-132.76 (23-I-3)	-17.33 (15)	31.28 (23-I-3)
9	9	-0.0 (23-I-2)	-0.1 (13)	-0.0 (13)	-56.21 (15)	-445.69 (15)	-34.48 (15)
9	10	-0.0 (23-II-2)	-0.0 (13)	-0.0 (13)	-55.45 (15)	-382.20 (15)	-41.85 (15)
9	11	-0.0 (13)	-0.0 (16)	-0.0 (13)	-83.79 (15)	273.23 (23-II-3)	-80.67 (15)
9	12	0.0 (16)	-0.0 (23-I-2)	-0.0 (13)	-58.29 (23-I-3)	-31.55 (15)	-34.45 (15)
9	13	-0.0 (23-II-2)	-0.1 (13)	-0.0 (13)	-56.29 (15)	-444.71 (15)	-35.80 (15)
9	14	-0.0 (23-II-2)	-0.1 (16)	-0.0 (23-I-2)	-48.49 (15)	-420.08 (15)	-44.04 (15)
9	15	-0.1 (23-II-2)	-0.1 (16)	-0.1 (23-I-2)	-10.70 (15)	622.10 (23-II-3)	-118.05 (15)
9	16	-0.1 (23-II-2)	0.3 (23-II-2)	-0.1 (16)	112.80 (23-II-2)	1030.43 (23-II-3)	516.27 (23-I-2)
10	1	-0.0 (13)	-0.1 (23-II-2)	-0.0 (13)	-55.84 (15)	-439.34 (15)	-34.77 (15)
10	2	-0.0 (13)	-0.1 (23-I-2)	-0.0 (23-I-1)	-48.47 (15)	416.45 (23-II-3)	-42.01 (23-II-3)
10	3	-0.0 (16)	-0.2 (23-I-2)	0.0 (16)	-11.04 (15)	625.47 (23-II-3)	-159.83 (23-II-3)
10	4	-0.1 (23-II-2)	-0.5 (23-II-2)	0.1 (23-II-2)	124.75 (23-I-3)	1031.26 (23-II-3)	-540.37 (23-II-3)
10	5	-0.0 (13)	-0.1 (23-II-2)	-0.0 (13)	-54.41 (15)	-427.99 (15)	-37.02 (15)
10	6	-0.0 (13)	-0.1 (23-II-2)	0.0 (23-I-4)	-55.48 (15)	-371.38 (15)	-45.25 (23-II-3)
10	7	-0.1 (23-II-2)	-0.1 (23-II-2)	0.1 (23-II-2)	-86.76 (15)	284.13 (23-II-3)	-105.77 (23-II-3)
10	8	-0.1 (23-II-2)	0.0 (23-I-2)	0.0 (23-II-2)	-33.83 (15)	-30.68 (15)	-32.94 (23-II-3)
10	9	-0.0 (23-II-2)	-0.1 (16)	-0.0 (13)	-53.96 (15)	-425.44 (15)	-39.48 (15)
10	10	-0.1 (23-II-2)	-0.1 (16)	-0.0 (13)	-54.87 (15)	-369.63 (15)	-49.37 (15)
10	11	-0.1 (13)	-0.0 (16)	0.0 (23-II-1)	87.61 (23-II-3)	285.09 (23-II-3)	-89.16 (15)
10	12	-0.1 (22)	-0.0 (23-I-2)	0.0 (23-II-2)	-32.83 (15)	-30.40 (15)	-40.99 (15)
10	13	-0.0 (23-II-2)	-0.1 (16)	-0.0 (13)	-54.37 (15)	-430.53 (15)	-41.54 (15)
10	14	-0.0 (23-II-2)	-0.1 (16)	-0.0 (23-II-4)	50.59 (23-I-2)	420.01 (23-II-4)	-51.86 (15)
10	15	-0.1 (23-II-2)	-0.1 (16)	-0.1 (23-I-1)	19.32 (23-II-2)	628.40 (23-II-4)	-126.69 (15)
10	16	-0.1 (13)	0.3 (23-I-2)	-0.1 (13)	135.60 (23-II-2)	1032.07 (23-II-2)	507.15 (23-II-2)
11	1	-0.2 (22)	-0.0 (22)	-0.0 (22)	341.66 (15)	28.45 (15)	-27.54 (23-I-1)
11	2	-0.1 (22)	-0.0 (16)	-0.0 (22)	341.43 (15)	40.51 (15)	-9.77 (23-I-1)
11	3	-0.1 (13)	-0.0 (23-I-1)	-0.0 (22)	339.99 (15)	41.68 (15)	7.67 (23-II-1)
11	4	-0.1 (13)	-0.0 (23-II-2)	-0.0 (22)	336.89 (15)	43.79 (15)	9.49 (23-II-2)
11	5	-0.1 (16)	-0.0 (16)	-0.0 (23-II-2)	-313.04 (23-I-1)	14.03 (15)	-21.69 (23-I-1)
11	6	-0.1 (22)	-0.1 (16)	-0.0 (22)	-301.02 (23-I-1)	31.49 (15)	-15.54 (23-I-1)
11	7	-0.0 (13)	-0.0 (23-I-1)	-0.0 (22)	-302.98 (23-I-1)	33.09 (15)	7.61 (23-II-1)
11	8	-0.1 (16)	-0.0 (23-II-2)	-0.0 (23-I-1)	-318.53 (23-I-1)	-50.96 (23-I-1)	14.71 (23-I-2)
11	9	-0.1 (16)	-0.0 (16)	0.0 (16)	-420.01 (23-I-1)	-37.22 (23-I-1)	-49.15 (15)
11	10	-0.1 (23-I-1)	-0.0 (16)	-0.0 (22)	-263.65 (23-I-1)	42.47 (15)	-21.06 (15)
11	11	-0.0 (16)	-0.0 (22)	-0.1 (16)	-264.91 (23-I-1)	43.83 (15)	-27.41 (23-I-1)
11	12	-0.1 (16)	-0.1 (23-II-2)	-0.1 (23-I-1)	-415.90 (23-I-1)	-36.19 (23-I-1)	30.26 (15)
11	13	-0.3 (23-I-1)	0.1 (23-I-2)	0.1 (23-II-2)	-708.48 (23-I-1)	21.50 (23-I-2)	285.38 (23-I-1)
11	14	0.0 (23-I-2)	0.0 (16)	-0.0 (16)	-42.12 (23-I-1)	54.70 (15)	42.12 (23-II-1)
11	15	-0.0 (23-I-1)	-0.0 (23-II-2)	-0.0 (22)	-46.90 (23-I-1)	54.68 (15)	-48.84 (23-I-1)
11	16	0.3 (23-II-1)	-0.1 (23-II-2)	-0.1 (16)	-696.40 (23-I-1)	-9.20 (23-I-1)	-315.31 (23-I-1)
12	1	-0.1 (23-II-2)	-0.0 (22)	-0.0 (22)	336.13 (15)	43.67 (15)	5.33 (15)
12	2	-0.1 (23-II-2)	-0.0 (22)	-0.0 (22)	337.57 (15)	41.31 (15)	6.63 (15)
12	3	-0.1 (13)	-0.0 (23-II-2)	-0.0 (13)	337.67 (15)	41.21 (15)	11.64 (23-II-2)
12	4	-0.1 (13)	-0.0 (23-I-1)	-0.0 (13)	336.15 (15)	43.43 (15)	12.69 (23-II-2)
12	5	-0.1 (23-II-2)	-0.0 (22)	-0.0 (23-I-1)	-317.11 (23-I-1)	-55.09 (23-I-1)	4.69 (15)
12	6	-0.1 (23-II-2)	-0.0 (22)	0.0 (23-II-1)	-301.46 (23-I-1)	32.89 (15)	5.00 (15)
12	7	-0.1 (13)	-0.1 (23-I-1)	-0.0 (13)	-301.28 (23-I-1)	32.49 (15)	13.31 (23-II-2)
12	8	-0.1 (16)	-0.1 (23-I-1)	-0.0 (13)	-315.09 (23-I-1)	-52.86 (23-I-1)	16.72 (23-II-2)
12	9	-0.2 (23-II-2)	-0.0 (16)	0.0 (16)	-415.82 (23-I-1)	-47.45 (23-I-1)	46.26 (23-II-2)
12	10	-0.1 (23-II-2)	-0.1 (23-II-2)	0.1 (23-II-2)	-265.40 (23-I-1)	-43.54 (23-I-1)	31.95 (23-II-2)
12	11	-0.0 (16)	-0.1 (22)	0.0 (23-II-1)	-265.95 (23-I-1)	42.79 (15)	26.33 (15)
12	12	-0.1 (16)	-0.1 (23-I-1)	-0.1 (23-I-1)	-415.77 (23-I-1)	-40.75 (23-I-1)	34.00 (15)
12	13	-0.5 (23-II-2)	-0.1 (23-II-2)	0.1 (23-II-2)	-702.75 (23-I-2)	-62.60 (23-I-1)	348.81 (23-II-2)
12	14	0.0 (23-I-1)	-0.1 (23-II-2)	0.0 (23-II-1)	-48.07 (23-I-1)	-57.33 (23-I-1)	53.53 (23-II-2)
12	15	-0.0 (23-I-1)	-0.1 (22)	0.0 (23-II-1)	-47.17 (23-I-1)	53.23 (15)	-42.04 (23-I-2)
12	16	0.3 (23-II-1)	-0.1 (22)	-0.1 (13)	-697.03 (23-II-2)	-16.55 (23-I-1)	-311.17 (23-I-2)
13	1	0.0 (22)	-0.0 (15)	0.0 (15)	28.48 (22)	150.10 (15)	-32.92 (15)
13	2	0.0 (22)	-0.0 (15)	0.0 (15)	44.36 (22)	113.79 (15)	-18.85 (22)
13	3	0.0 (22)	-0.0 (15)	0.0 (15)	35.90 (22)	70.11 (15)	-15.36 (22)
13	4	0.0 (22)	-0.0 (15)	0.0 (15)	9.92 (22)	-21.23 (23-II-3)	-21.60 (22)
13	5	0.0 (22)	-0.0 (15)	0.0 (15)	22.93 (22)	173.95 (15)	-59.45 (15)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
13	6	0.0 (22)	-0.0 (15)	0.0 (15)	24.47 (22)	120.78 (15)	-81.32 (15)
13	7	0.0 (22)	-0.0 (15)	0.0 (15)	5.65 (22)	66.91 (15)	-73.40 (15)
13	8	0.0 (22)	-0.0 (15)	0.0 (15)	-25.36 (15)	-42.68 (23-II-3)	-69.64 (15)
13	9	0.0 (22)	-0.0 (15)	0.0 (15)	-19.09 (22)	123.47 (15)	-62.21 (15)
13	10	0.0 (22)	-0.0 (15)	0.0 (15)	-30.21 (22)	123.47 (15)	-104.05 (15)
13	11	0.0 (22)	-0.0 (15)	0.0 (15)	-53.74 (22)	84.94 (15)	-82.25 (15)
13	12	0.0 (22)	-0.0 (15)	0.0 (15)	-60.79 (22)	-16.70 (23-II-3)	-65.17 (15)
13	13	0.0 (22)	-0.0 (15)	0.0 (15)	-126.20 (22)	77.96 (15)	-111.33 (15)
13	14	0.0 (22)	-0.0 (15)	0.0 (15)	-159.38 (22)	114.05 (15)	-112.70 (15)
13	15	0.0 (22)	-0.0 (15)	0.0 (15)	-136.43 (22)	99.31 (15)	-90.26 (15)
13	16	0.0 (22)	-0.0 (15)	0.0 (15)	-111.99 (22)	40.95 (16)	-70.93 (15)
14	1	0.0 (22)	0.0 (23-II-3)	0.0 (15)	26.18 (22)	28.56 (15)	-13.04 (13)
14	2	0.0 (22)	0.0 (23-II-3)	0.0 (15)	53.12 (22)	-10.50 (23-II-3)	-19.69 (22)
14	3	0.0 (22)	0.0 (23-II-3)	0.0 (15)	48.31 (22)	-12.41 (13)	-15.13 (22)
14	4	0.0 (22)	-0.0 (15)	0.0 (13)	18.25 (22)	-11.27 (15)	-11.58 (22)
14	5	0.0 (22)	0.0 (23-II-3)	0.0 (15)	8.71 (16)	43.39 (15)	-38.02 (15)
14	6	0.0 (22)	0.0 (23-II-3)	0.0 (15)	13.05 (14)	-22.02 (23-II-3)	-47.85 (15)
14	7	0.0 (22)	0.0 (23-II-3)	0.0 (15)	-15.14 (13)	-25.58 (15)	-43.35 (22)
14	8	0.0 (15)	-0.0 (15)	0.0 (13)	-26.20 (15)	-21.81 (15)	-35.56 (22)
14	9	0.0 (22)	0.0 (23-II-3)	0.0 (15)	-44.15 (22)	20.63 (15)	-37.56 (15)
14	10	0.0 (22)	0.0 (23-II-3)	0.0 (15)	-56.69 (22)	-32.25 (23-II-3)	-61.18 (15)
14	11	0.0 (22)	0.0 (23-II-3)	0.0 (15)	-71.41 (22)	-26.18 (23-II-2)	-52.72 (22)
14	12	0.0 (22)	0.0 (23-II-3)	0.0 (13)	-70.01 (15)	-18.64 (15)	-43.38 (22)
14	13	0.0 (22)	0.0 (23-II-3)	0.0 (15)	-140.59 (22)	-39.77 (23-II-3)	-76.63 (15)
14	14	0.0 (22)	0.0 (23-II-3)	0.0 (22)	-182.86 (22)	-46.74 (23-II-3)	-70.72 (15)
14	15	0.0 (22)	0.0 (23-II-3)	0.0 (23-II-3)	-166.43 (22)	-32.34 (23-II-2)	-56.47 (15)
14	16	0.0 (22)	0.0 (23-II-3)	0.0 (23-II-2)	-131.46 (22)	-12.79 (15)	-36.90 (23-II-2)
15	1	0.0 (15)	-0.0 (15)	0.0 (15)	8.50 (22)	53.90 (15)	-21.60 (15)
15	2	0.0 (15)	-0.0 (15)	0.0 (15)	3.71 (22)	-33.64 (23-II-3)	-38.31 (15)
15	3	0.0 (15)	-0.0 (15)	0.0 (15)	-5.11 (15)	72.28 (15)	-40.14 (15)
15	4	0.0 (22)	-0.0 (15)	0.0 (15)	-10.43 (15)	-38.96 (23-II-3)	-62.33 (15)
15	5	0.0 (22)	-0.0 (15)	0.0 (15)	-38.88 (22)	75.70 (15)	-17.48 (15)
15	6	0.0 (22)	-0.0 (15)	0.0 (15)	-43.39 (22)	-39.24 (22)	-60.89 (15)
15	7	0.0 (22)	-0.0 (16)	0.0 (15)	-115.46 (22)	53.49 (15)	-38.42 (15)
15	8	0.0 (22)	0.0 (22)	0.0 (15)	-123.02 (22)	-55.13 (22)	-55.06 (15)
16	1	0.0 (13)	-0.0 (15)	0.0 (15)	27.61 (22)	35.97 (15)	-33.12 (15)
16	2	0.0 (22)	-0.0 (15)	0.0 (15)	49.23 (22)	131.04 (15)	-42.56 (15)
16	3	0.0 (22)	-0.0 (15)	0.0 (15)	47.80 (22)	146.99 (15)	-25.39 (15)
16	4	0.0 (22)	-0.0 (15)	0.0 (15)	21.82 (22)	87.60 (15)	-24.33 (15)
16	5	0.0 (13)	-0.0 (15)	0.0 (15)	23.09 (15)	21.68 (22)	-59.85 (15)
16	6	0.0 (13)	-0.0 (15)	0.0 (15)	35.99 (22)	158.29 (15)	-77.05 (15)
16	7	0.0 (22)	-0.0 (15)	0.0 (15)	29.70 (22)	162.20 (15)	-54.22 (15)
16	8	0.0 (22)	-0.0 (15)	0.0 (15)	9.93 (22)	62.67 (15)	-66.57 (15)
16	9	0.0 (13)	-0.0 (15)	0.0 (15)	-30.15 (13)	10.60 (15)	-94.98 (15)
16	10	0.0 (13)	-0.0 (15)	0.0 (15)	-32.17 (13)	186.67 (15)	-93.93 (15)
16	11	0.0 (13)	-0.0 (15)	0.0 (15)	-30.28 (13)	177.43 (15)	-42.16 (15)
16	12	0.0 (22)	-0.0 (15)	0.0 (15)	-30.98 (22)	44.57 (15)	-60.82 (15)
16	13	0.0 (13)	-0.0 (15)	0.0 (15)	-134.56 (13)	62.17 (15)	-138.94 (15)
16	14	0.0 (13)	-0.0 (15)	0.0 (15)	-140.47 (22)	191.51 (15)	-92.54 (15)
16	15	0.0 (13)	-0.0 (15)	0.0 (15)	-143.21 (22)	169.91 (15)	-61.05 (15)
16	16	0.0 (22)	-0.0 (15)	0.0 (15)	-124.90 (22)	33.75 (15)	-43.70 (15)
17	1	0.0 (13)	-0.0 (15)	0.0 (15)	-119.68 (13)	148.25 (15)	-83.98 (15)
17	2	0.0 (13)	-0.1 (15)	0.0 (15)	-94.75 (13)	294.16 (15)	-82.86 (23-I-2)
17	3	0.0 (13)	-0.0 (15)	0.0 (15)	-102.61 (13)	229.15 (15)	50.06 (13)
17	4	0.0 (23-II-2)	-0.0 (15)	0.0 (15)	-135.10 (23-II-2)	-85.71 (13)	29.28 (13)
17	5	0.0 (13)	-0.0 (15)	0.0 (15)	-133.13 (13)	126.27 (15)	-64.86 (15)
17	6	0.0 (13)	-0.0 (15)	0.0 (15)	-100.01 (13)	348.81 (15)	-80.22 (15)
17	7	0.0 (13)	-0.0 (15)	0.0 (15)	-104.73 (13)	274.14 (15)	-61.91 (15)
17	8	0.0 (23-II-2)	-0.0 (15)	0.0 (15)	-154.68 (23-II-2)	-157.63 (13)	-69.69 (15)
17	9	0.0 (13)	-0.0 (15)	0.0 (15)	-140.37 (13)	125.59 (15)	-60.93 (15)
17	10	0.0 (13)	-0.0 (15)	0.0 (15)	-109.17 (13)	350.73 (15)	-83.06 (15)
17	11	0.0 (13)	-0.0 (15)	0.0 (15)	-111.88 (13)	275.72 (15)	-88.92 (15)
17	12	0.0 (13)	-0.0 (15)	0.0 (15)	-159.82 (13)	-160.64 (13)	-88.12 (15)
17	13	0.0 (13)	-0.0 (15)	0.0 (15)	-143.02 (13)	146.58 (15)	-45.05 (15)
17	14	0.0 (13)	-0.1 (15)	0.0 (23-I-2)	-121.92 (13)	297.92 (15)	-88.59 (15)
17	15	0.0 (13)	-0.0 (15)	0.0 (23-I-2)	-123.33 (13)	232.85 (15)	-167.70 (15)
17	16	0.0 (13)	-0.0 (15)	0.0 (23-I-2)	-151.03 (13)	-92.63 (13)	-147.43 (15)
18	1	0.0 (23-I-1)	-0.0 (16)	0.0 (23-II-2)	-165.86 (23-I-1)	86.40 (16)	-81.56 (23-II-2)
18	2	0.0 (23-I-1)	0.0 (13)	0.0 (23-II-2)	-193.80 (23-I-1)	-133.46 (15)	-85.26 (23-II-2)
18	3	0.0 (23-I-1)	0.0 (15)	0.0 (23-II-2)	-153.25 (23-I-1)	140.77 (15)	-112.66 (23-I-2)
18	4	0.0 (23-I-1)	0.0 (13)	0.0 (23-II-2)	-189.66 (23-I-1)	-197.24 (15)	-110.20 (23-II-2)
18	5	0.0 (23-I-1)	0.0 (15)	0.0 (23-II-2)	-142.85 (23-I-1)	137.43 (15)	-117.35 (23-I-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
18	6	0.0 (23-I-1)	0.0 (13)	0.0 (23-II-2)	-173.54 (23-I-1)	-198.41 (15)	-115.07 (23-II-2)
18	7	0.0 (23-I-1)	-0.0 (16)	0.0 (23-II-2)	-137.85 (23-I-1)	78.97 (16)	-140.45 (15)
18	8	0.0 (23-I-1)	0.0 (15)	0.0 (23-II-2)	-153.29 (23-I-1)	-137.88 (15)	-133.88 (15)
19	1	0.0 (23-I-1)	0.0 (23-II-3)	0.0 (15)	-232.77 (23-I-1)	-111.72 (23-II-3)	-130.51 (23-II-2)
19	2	0.0 (23-I-1)	0.0 (23-I-3)	0.0 (15)	-276.88 (23-I-1)	-68.53 (23-I-3)	-132.41 (23-II-2)
19	3	0.0 (23-I-1)	0.0 (23-I-3)	0.0 (15)	-330.48 (23-I-1)	-42.44 (23-I-3)	-121.76 (23-II-2)
19	4	0.0 (23-I-1)	0.0 (23-I-3)	0.0 (23-II-2)	-300.20 (23-I-1)	-19.62 (15)	-63.99 (23-II-2)
19	5	0.0 (23-I-1)	0.0 (23-I-3)	0.0 (23-II-2)	-199.42 (23-I-1)	-124.87 (23-II-4)	-131.91 (23-II-2)
19	6	0.0 (23-I-1)	0.0 (23-I-3)	0.0 (23-II-2)	-207.94 (23-I-1)	-54.21 (23-I-3)	-125.94 (23-II-2)
19	7	0.0 (23-I-1)	0.0 (23-I-3)	0.0 (23-II-2)	-226.58 (23-I-1)	-21.91 (16)	-122.69 (23-II-2)
19	8	0.0 (23-I-1)	0.0 (23-I-3)	0.0 (23-II-2)	-218.95 (23-I-1)	-12.43 (15)	-43.60 (23-II-2)
19	9	0.0 (23-I-1)	0.0 (23-I-3)	0.0 (23-II-2)	-166.65 (23-I-1)	-126.34 (23-II-4)	-129.95 (23-II-2)
19	10	0.0 (23-I-1)	0.0 (23-I-3)	0.0 (23-II-2)	-146.04 (23-I-1)	-41.59 (23-I-3)	-121.84 (23-II-2)
19	11	0.0 (23-I-1)	0.0 (23-I-3)	0.0 (23-II-2)	-136.84 (23-I-1)	11.11 (13)	-121.99 (23-II-2)
19	12	0.0 (23-I-1)	0.0 (23-I-3)	0.0 (23-II-2)	-150.87 (23-I-1)	16.56 (23-II-2)	-45.18 (23-II-2)
19	13	0.0 (23-I-1)	0.0 (23-II-4)	0.0 (23-II-2)	-133.61 (23-I-1)	-106.94 (23-II-4)	-116.78 (15)
19	14	0.0 (23-I-1)	0.0 (23-I-4)	0.0 (23-II-2)	-111.31 (13)	-35.83 (23-II-4)	-116.15 (15)
19	15	0.0 (23-I-1)	0.0 (23-I-3)	0.0 (23-II-2)	-95.41 (13)	11.15 (15)	-111.98 (15)
19	16	0.0 (23-I-1)	0.0 (23-I-3)	0.0 (23-II-2)	-94.58 (13)	15.95 (23-II-2)	-62.72 (15)
20	1	0.0 (23-II-2)	0.0 (23-II-3)	0.0 (15)	-156.03 (23-II-2)	-164.66 (23-I-2)	-124.20 (23-I-2)
20	2	0.0 (23-I-1)	-0.0 (15)	0.0 (15)	-132.39 (23-II-2)	151.86 (15)	-159.24 (23-II-2)
20	3	0.0 (23-I-1)	-0.0 (15)	0.0 (15)	-133.31 (23-II-2)	159.72 (15)	-128.39 (23-II-2)
20	4	0.0 (23-I-1)	-0.0 (15)	0.0 (15)	-150.49 (23-I-1)	84.47 (16)	-104.53 (23-II-2)
20	5	0.0 (23-I-1)	-0.0 (15)	0.0 (15)	-174.95 (23-II-2)	-237.72 (23-II-2)	-92.50 (15)
20	6	0.0 (23-I-1)	-0.0 (15)	0.0 (15)	-139.12 (23-II-2)	177.66 (15)	-105.00 (23-II-2)
20	7	0.0 (23-I-1)	-0.0 (15)	0.0 (15)	-136.27 (23-I-1)	188.70 (15)	-107.35 (23-II-2)
20	8	0.0 (23-I-1)	-0.0 (15)	0.0 (15)	-148.44 (23-I-1)	80.79 (16)	-106.55 (23-II-2)
20	9	0.0 (23-I-1)	-0.0 (15)	0.0 (23-I-2)	-171.75 (23-I-1)	-244.87 (23-II-2)	-87.12 (15)
20	10	0.0 (23-I-1)	-0.0 (15)	0.0 (23-I-2)	-141.45 (23-I-1)	176.35 (15)	-94.28 (15)
20	11	0.0 (23-I-1)	-0.0 (15)	0.0 (23-I-2)	-136.22 (23-I-1)	188.58 (15)	-100.94 (15)
20	12	0.0 (23-I-1)	-0.0 (15)	0.0 (23-I-2)	-144.36 (23-I-1)	80.26 (16)	-105.20 (23-II-2)
20	13	0.0 (23-I-1)	0.0 (23-II-3)	0.0 (23-I-2)	-160.90 (23-I-1)	-184.10 (23-II-2)	-68.20 (15)
20	14	0.0 (23-I-1)	-0.0 (15)	0.0 (23-I-2)	-144.47 (23-I-1)	147.75 (15)	-68.21 (15)
20	15	0.0 (23-I-1)	-0.0 (15)	0.0 (23-I-2)	-131.33 (23-I-1)	158.81 (15)	-108.58 (15)
20	16	0.0 (23-I-1)	-0.0 (15)	0.0 (23-I-2)	-138.40 (23-I-1)	80.71 (16)	-116.18 (15)
21	1	0.0 (13)	0.0 (15)	0.0 (15)	-123.38 (13)	3.33 (15)	2.40 (23-II-3)
21	2	0.0 (13)	0.0 (15)	0.0 (15)	-125.15 (13)	-3.86 (13)	-46.28 (15)
21	3	0.0 (13)	0.0 (15)	0.0 (15)	-132.63 (13)	2.65 (15)	14.06 (15)
21	4	0.0 (13)	0.0 (15)	0.0 (15)	-135.71 (13)	-5.37 (15)	-58.39 (15)
21	5	0.0 (13)	0.0 (15)	0.0 (15)	-134.90 (13)	2.49 (15)	14.71 (15)
21	6	0.0 (13)	0.0 (15)	0.0 (15)	-137.79 (13)	-5.02 (15)	-59.58 (15)
21	7	0.0 (13)	0.0 (23-II-3)	0.0 (15)	-147.68 (13)	0	3.40 (23-II-3)
21	8	0.0 (13)	0.0 (13)	0.0 (15)	-147.99 (13)	-6.10 (15)	-44.60 (15)
22	1	-0.0 (22)	0.0 (15)	0.0 (15)	9.12 (15)	1.28 (15)	6.44 (15)
22	2	-0.0 (15)	-0.0 (15)	0.0 (15)	12.48 (15)	4.18 (15)	-15.86 (15)
22	3	-0.0 (23-II-2)	-0.0 (22)	0.0 (15)	9.39 (23-II-2)	-1.76 (15)	13.06 (13)
22	4	-0.0 (15)	-0.0 (15)	0.0 (15)	17.60 (15)	11.10 (15)	-52.40 (15)
22	5	0.0 (13)	-0.0 (15)	0.0 (15)	-21.98 (13)	-5.12 (15)	52.32 (15)
22	6	0.0 (13)	-0.0 (15)	0.0 (15)	9.84 (23-II-2)	16.51 (15)	-116.84 (15)
22	7	0.0 (13)	-0.0 (15)	0.0 (15)	-127.77 (13)	1.97 (23-II-3)	10.48 (22)
22	8	0.0 (13)	-0.0 (15)	0.0 (15)	-125.65 (13)	30.72 (15)	-128.30 (15)
23	1	0.0 (13)	0.0 (23-II-3)	0.0 (15)	-137.02 (13)	3.35 (23-II-3)	1.21 (23-II-3)
23	2	0.0 (13)	0.0 (13)	0.0 (15)	-137.29 (13)	-4.39 (13)	-43.55 (15)
23	3	0.0 (13)	0.0 (13)	0.0 (15)	-144.29 (13)	2.71 (23-II-3)	12.15 (15)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
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BTK3**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
23	4	0.0 (13)	0.0 (13)	0.0 (15)	-146.79 (13)	-5.42 (15)	-54.14 (15)
23	5	0.0 (13)	0.0 (15)	0.0 (15)	-146.07 (13)	2.65 (15)	12.89 (15)
23	6	0.0 (13)	0.0 (13)	0.0 (15)	-148.76 (13)	-5.27 (13)	-55.90 (15)
23	7	0.0 (13)	0.0 (13)	0.0 (15)	-155.78 (13)	0	2.06 (13)
23	8	0.0 (13)	0.0 (13)	0.0 (15)	-155.93 (13)	-6.27 (15)	-42.08 (15)
24	1	0.0 (13)	-0.0 (23-II-2)	0.0 (15)	-166.83 (13)	5.00 (15)	10.28 (23-II-2)
24	2	0.0 (13)	-0.0 (23-II-2)	0.0 (15)	-176.34 (13)	26.48 (23-II-2)	-63.22 (15)
24	3	0.0 (13)	0.0 (15)	0.0 (15)	-152.17 (13)	-3.89 (23-II-3)	5.01 (15)
24	4	0.0 (13)	0.0 (15)	0.0 (15)	-154.99 (13)	9.42 (23-II-2)	-68.69 (15)
24	5	0.0 (13)	0.0 (15)	0.0 (15)	-134.90 (13)	2.96 (15)	12.46 (15)
24	6	0.0 (13)	0.0 (15)	0.0 (15)	-140.51 (13)	-7.56 (15)	-69.08 (15)
24	7	0.0 (13)	0.0 (23-I-3)	0.0 (15)	-137.14 (13)	-1.60 (23-II-2)	3.52 (23-II-2)
24	8	0.0 (13)	0.0 (15)	0.0 (15)	-138.01 (13)	-5.38 (15)	-47.75 (15)
25	1	-0.0 (13)	-0.1 (23-I-3)	-0.0 (13)	-69.81 (15)	-533.56 (15)	-8.83 (15)
25	2	-0.0 (13)	-0.1 (23-I-3)	-0.0 (13)	-73.71 (15)	-508.15 (15)	-7.51 (15)
25	3	-0.0 (13)	-0.2 (23-I-3)	0.0 (16)	-42.12 (15)	-545.47 (15)	48.69 (15)
25	4	-0.1 (23-II-2)	-0.5 (23-I-3)	0.1 (23-II-2)	-11.32 (15)	-772.10 (15)	369.74 (15)
25	5	-0.0 (13)	-0.1 (23-I-3)	-0.0 (13)	-63.80 (15)	-536.96 (15)	-8.68 (15)
25	6	-0.0 (13)	-0.1 (23-I-3)	0.0 (23-II-3)	-50.00 (15)	-486.08 (15)	-5.95 (15)
25	7	-0.1 (23-II-2)	-0.1 (23-I-3)	0.1 (23-II-3)	-71.67 (15)	-372.79 (15)	35.12 (15)
25	8	-0.1 (23-II-2)	0.0 (23-I-3)	0.0 (23-II-3)	-90.99 (15)	-71.03 (15)	63.01 (15)
25	9	-0.0 (23-II-3)	-0.1 (16)	-0.0 (13)	-63.65 (15)	-535.13 (15)	-7.05 (23-I-2)
25	10	-0.1 (23-II-2)	-0.1 (16)	-0.0 (13)	-50.17 (15)	-484.83 (15)	-8.86 (23-I-2)
25	11	-0.1 (13)	-0.0 (16)	0.0 (23-I-3)	-72.11 (15)	-372.00 (15)	-41.23 (15)
25	12	-0.1 (13)	-0.0 (23-I-3)	0.0 (23-II-3)	-91.78 (15)	-71.10 (15)	-64.26 (15)
25	13	-0.0 (23-II-3)	-0.1 (16)	-0.0 (13)	-69.37 (15)	-528.16 (15)	-6.31 (23-I-2)
25	14	-0.0 (23-II-2)	-0.1 (16)	-0.0 (13)	-74.04 (15)	-504.67 (15)	-7.46 (23-I-2)
25	15	-0.1 (23-II-2)	-0.1 (16)	-0.1 (23-I-3)	-43.49 (15)	-543.21 (15)	-55.67 (15)
25	16	-0.1 (13)	0.3 (23-II-3)	-0.1 (13)	50.50 (23-II-3)	-770.10 (15)	-369.69 (15)
26	1	-0.0 (13)	-0.1 (13)	-0.0 (13)	-42.51 (15)	-535.50 (15)	-34.41 (15)
26	2	-0.0 (16)	-0.1 (13)	0.0 (16)	-22.00 (15)	-514.23 (15)	22.42 (23-I-2)
26	3	-0.0 (16)	-0.1 (16)	0.1 (16)	-55.33 (15)	-556.63 (15)	80.85 (15)
26	4	0.1 (23-I-2)	-0.3 (23-I-3)	0.1 (23-II-3)	-69.57 (23-II-2)	-790.25 (15)	333.27 (15)
26	5	-0.0 (13)	-0.1 (13)	-0.0 (13)	-61.16 (15)	-543.01 (15)	-12.94 (15)
26	6	-0.0 (16)	-0.1 (13)	-0.0 (13)	-43.97 (15)	-491.87 (15)	14.21 (23-I-2)
26	7	-0.0 (16)	-0.1 (23-I-3)	0.0 (23-II-3)	-62.85 (15)	-375.39 (15)	32.53 (15)
26	8	0.1 (16)	0.0 (23-I-2)	0.0 (23-II-3)	-82.03 (15)	-66.28 (15)	60.31 (15)
26	9	-0.0 (13)	-0.1 (16)	-0.0 (13)	-64.05 (15)	-543.42 (15)	-3.80 (23-II-2)
26	10	-0.0 (23-I-3)	-0.0 (16)	-0.0 (13)	-48.38 (15)	-488.99 (15)	-3.31 (23-II-2)
26	11	-0.0 (13)	-0.0 (16)	-0.0 (13)	-68.94 (15)	-374.27 (15)	-42.49 (15)
26	12	0.0 (16)	-0.0 (23-I-2)	-0.0 (13)	-87.90 (15)	-72.23 (15)	-66.60 (15)
26	13	-0.0 (23-II-2)	-0.1 (16)	-0.0 (13)	-70.10 (15)	-535.72 (15)	-5.20 (23-II-2)
26	14	-0.0 (23-II-2)	-0.1 (16)	-0.0 (13)	-73.82 (15)	-509.28 (15)	-5.12 (23-II-2)
26	15	-0.1 (23-II-2)	-0.1 (16)	-0.1 (23-I-3)	-42.13 (15)	-545.85 (15)	-56.00 (15)
26	16	-0.1 (13)	0.3 (23-II-3)	-0.1 (16)	46.71 (23-I-3)	-772.24 (15)	-373.01 (15)
27	1	-0.0 (13)	-0.1 (23-II-3)	0.0 (16)	-69.23 (15)	-527.13 (15)	-8.85 (15)
27	2	-0.0 (13)	-0.1 (23-II-3)	0.0 (16)	-73.88 (15)	-503.99 (15)	-8.16 (15)
27	3	-0.1 (13)	-0.2 (23-II-3)	0.0 (16)	-43.36 (15)	-542.91 (15)	47.62 (15)
27	4	-0.1 (13)	-0.5 (23-II-3)	0.1 (23-II-3)	-15.08 (15)	-769.99 (15)	368.72 (15)
27	5	-0.0 (13)	-0.1 (23-II-3)	0.0 (23-I-4)	-63.25 (15)	-531.96 (15)	-8.94 (15)
27	6	-0.1 (13)	-0.1 (23-II-3)	0.0 (23-I-4)	-49.82 (15)	-482.68 (15)	-6.97 (15)
27	7	-0.1 (23-II-3)	-0.1 (23-II-3)	0.1 (23-II-2)	-71.80 (15)	-370.95 (15)	33.44 (15)
27	8	-0.1 (13)	0.0 (23-I-3)	0.0 (23-II-3)	-91.30 (15)	-70.80 (15)	61.38 (15)
27	9	-0.0 (23-II-3)	-0.1 (16)	0.0 (23-I-4)	-63.18 (15)	-531.52 (15)	-7.63 (23-II-2)
27	10	-0.1 (23-II-3)	-0.1 (16)	0.0 (23-I-4)	-49.73 (15)	-482.32 (15)	-9.83 (23-II-2)
27	11	-0.1 (13)	-0.0 (16)	0.0 (23-I-4)	-71.57 (15)	-370.69 (15)	-42.70 (15)
27	12	-0.1 (13)	-0.0 (23-I-3)	0.0 (23-II-3)	-91.13 (15)	-70.80 (15)	-65.59 (15)
27	13	-0.0 (23-II-3)	-0.1 (16)	0.0 (16)	-69.00 (15)	-525.72 (15)	-6.81 (23-II-2)
27	14	-0.0 (23-II-3)	-0.1 (16)	-0.0 (13)	-73.57 (15)	-502.90 (15)	-8.19 (23-II-2)
27	15	-0.1 (23-II-3)	-0.1 (16)	-0.1 (23-II-4)	-42.82 (15)	-542.24 (15)	-56.76 (15)
27	16	-0.1 (13)	0.3 (23-I-3)	-0.1 (13)	50.33 (23-I-3)	-769.88 (15)	-370.56 (15)
28	1	-0.0 (13)	-0.1 (23-II-2)	0.0 (16)	-54.06 (15)	-429.16 (15)	-40.31 (15)
28	2	-0.0 (13)	-0.1 (23-II-2)	0.0 (16)	51.02 (23-I-2)	420.14 (23-I-2)	-52.41 (23-II-3)
28	3	-0.1 (13)	-0.2 (23-II-2)	0.0 (16)	19.85 (23-II-2)	628.57 (23-I-2)	-170.32 (23-II-3)
28	4	-0.1 (23-II-2)	-0.5 (23-II-2)	0.1 (23-II-2)	136.24 (23-II-2)	1032.09 (23-I-2)	-546.17 (23-II-3)
28	5	-0.0 (13)	-0.1 (23-II-2)	0.0 (23-I-4)	-53.04 (15)	-421.05 (15)	-41.89 (15)
28	6	-0.1 (13)	-0.1 (23-II-2)	0.0 (23-I-4)	-53.29 (15)	-366.61 (15)	-52.11 (23-II-3)
28	7	-0.1 (23-II-2)	-0.1 (23-II-2)	0.1 (23-II-2)	89.73 (23-I-2)	285.97 (23-I-2)	-112.86 (23-II-3)
28	8	-0.1 (23-II-2)	0.0 (23-I-1)	0.0 (23-II-2)	-30.60 (15)	-30.14 (15)	-37.31 (23-II-3)
28	9	-0.0 (23-II-2)	-0.1 (16)	0.0 (23-I-4)	-52.88 (15)	-420.28 (15)	-43.28 (15)
28	10	-0.1 (23-II-2)	-0.1 (16)	0.0 (23-I-4)	-53.08 (15)	-365.95 (15)	-53.72 (15)
28	11	-0.1 (13)	-0.0 (16)	0.0 (23-I-4)	90.04 (23-I-2)	286.27 (23-I-2)	-93.64 (15)



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
28	12	-0.1 (13)	-0.0 (23-I-2)	0.0 (23-II-4)	-30.04 (15)	-29.98 (15)	-43.76 (15)
28	13	-0.0 (23-I-1)	-0.1 (16)	0.0 (16)	-53.52 (15)	-426.68 (15)	-44.65 (15)
28	14	-0.0 (23-I-1)	-0.1 (16)	-0.0 (13)	51.47 (23-I-2)	421.22 (23-I-3)	-55.28 (15)
28	15	-0.1 (23-I-1)	-0.1 (16)	-0.0 (23-II-4)	20.85 (23-I-2)	629.32 (23-I-3)	-130.16 (15)
28	16	-0.1 (13)	0.3 (23-I-2)	-0.1 (13)	137.42 (23-I-2)	1032.41 (23-I-3)	504.92 (23-I-3)
29	1	-0.1 (23-II-2)	-0.0 (22)	0.0 (16)	336.03 (15)	43.38 (15)	8.05 (15)
29	2	-0.1 (23-I-1)	-0.0 (22)	0.0 (23-I-4)	337.28 (15)	41.01 (15)	8.35 (15)
29	3	-0.1 (16)	-0.0 (23-I-1)	0.0 (23-I-4)	336.84 (15)	40.90 (15)	12.37 (23-II-2)
29	4	-0.1 (16)	-0.0 (23-I-1)	0.0 (16)	334.99 (15)	43.12 (15)	13.16 (23-II-2)
29	5	-0.1 (23-II-2)	-0.0 (22)	0.0 (16)	-313.49 (23-I-1)	-55.63 (23-I-1)	7.03 (15)
29	6	-0.1 (23-II-2)	-0.1 (22)	0.0 (23-I-4)	-298.52 (23-I-4)	31.99 (15)	6.56 (15)
29	7	-0.1 (16)	-0.1 (23-I-1)	0.0 (23-I-4)	-299.51 (23-I-4)	31.84 (15)	13.11 (23-II-2)
29	8	-0.1 (16)	-0.1 (23-I-1)	0.0 (16)	-314.31 (23-I-4)	-52.82 (23-I-1)	16.60 (23-II-2)
29	9	-0.2 (23-II-2)	-0.1 (16)	0.0 (16)	-414.90 (23-I-1)	-49.32 (23-I-1)	46.60 (23-II-2)
29	10	-0.1 (23-I-1)	-0.1 (23-I-1)	0.1 (23-I-1)	-264.42 (23-II-4)	-43.84 (23-I-1)	31.36 (23-II-2)
29	11	-0.0 (16)	-0.1 (22)	0.0 (23-II-1)	-265.23 (23-II-4)	41.83 (15)	27.33 (15)
29	12	-0.1 (16)	-0.1 (23-I-1)	-0.0 (23-I-1)	-415.39 (23-II-4)	-40.58 (23-I-1)	34.71 (15)
29	13	-0.5 (23-II-2)	-0.1 (23-I-1)	0.1 (23-I-1)	-703.05 (23-II-2)	-66.80 (23-I-1)	349.84 (23-I-1)
29	14	0.0 (23-I-1)	-0.1 (23-I-1)	0.0 (23-II-1)	-48.01 (23-II-4)	-57.99 (23-I-1)	53.00 (23-II-2)
29	15	-0.0 (23-II-1)	-0.1 (22)	0.0 (23-II-1)	-47.05 (23-I-4)	52.08 (15)	-42.45 (23-I-2)
29	16	0.3 (23-II-1)	-0.1 (22)	-0.1 (13)	-696.96 (23-I-1)	-15.90 (23-I-1)	-311.36 (23-II-2)
30	1	-0.0 (13)	-0.1 (23-I-1)	0.0 (16)	-53.36 (15)	-426.12 (15)	-42.73 (15)
30	2	-0.0 (13)	-0.1 (23-II-2)	0.0 (16)	51.72 (23-I-2)	421.56 (23-I-3)	-56.33 (23-II-3)
30	3	-0.1 (13)	-0.2 (23-II-2)	0.0 (16)	20.98 (23-I-2)	629.46 (23-I-3)	-173.86 (23-II-3)
30	4	-0.1 (23-I-1)	-0.5 (23-I-1)	0.1 (23-II-2)	137.56 (23-I-2)	1032.37 (23-I-3)	-548.13 (23-I-2)
30	5	-0.0 (13)	-0.1 (23-I-1)	0.0 (23-I-4)	-52.45 (15)	-418.51 (15)	-43.79 (15)
30	6	-0.1 (13)	-0.1 (23-I-1)	0.0 (23-II-2)	-52.26 (15)	-364.78 (15)	-55.58 (23-I-2)
30	7	-0.1 (23-I-1)	-0.1 (23-I-1)	0.1 (23-II-2)	90.63 (23-I-3)	286.83 (23-I-3)	-115.95 (23-I-2)
30	8	-0.1 (23-I-1)	0.0 (23-I-4)	0.0 (23-II-2)	-29.00 (15)	-29.92 (15)	-39.15 (23-I-2)
30	9	-0.0 (23-I-1)	-0.1 (16)	0.0 (23-I-4)	-52.35 (15)	-417.92 (15)	-46.56 (23-I-2)
30	10	-0.1 (23-I-1)	-0.1 (16)	0.0 (23-I-4)	-52.16 (15)	-364.33 (15)	-55.17 (15)
30	11	-0.1 (13)	-0.0 (16)	0.0 (23-I-4)	90.92 (23-I-2)	287.23 (23-I-3)	-95.06 (15)
30	12	-0.1 (13)	-0.0 (23-II-1)	0.0 (23-I-4)	-28.64 (15)	-29.80 (15)	-44.63 (15)
30	13	-0.0 (23-II-4)	-0.1 (16)	0.0 (16)	-53.02 (15)	-424.42 (15)	-47.48 (23-I-2)
30	14	-0.0 (23-II-4)	-0.1 (16)	0.0 (16)	52.10 (23-I-2)	423.22 (23-I-3)	-56.21 (15)
30	15	-0.1 (23-II-4)	-0.1 (16)	-0.0 (23-II-4)	21.83 (23-II-3)	630.44 (23-I-3)	-131.08 (15)
30	16	-0.1 (13)	0.3 (23-II-1)	-0.1 (13)	138.57 (23-II-3)	1032.77 (23-I-3)	503.43 (23-I-3)
31	1	-0.1 (23-I-1)	-0.0 (22)	0.0 (16)	334.93 (15)	43.11 (15)	8.45 (15)
31	2	-0.1 (23-I-1)	-0.0 (22)	0.0 (23-II-2)	336.44 (15)	40.82 (15)	8.50 (15)
31	3	-0.1 (16)	-0.0 (23-I-1)	0.0 (23-I-4)	336.27 (15)	40.78 (15)	12.35 (23-I-2)
31	4	-0.1 (16)	-0.0 (23-I-1)	0.0 (16)	334.55 (15)	43.03 (15)	13.10 (23-I-2)
31	5	-0.1 (23-I-1)	-0.0 (22)	0.0 (16)	-313.36 (23-I-4)	-55.69 (23-I-1)	7.50 (15)
31	6	-0.1 (23-I-1)	-0.0 (22)	0.0 (23-II-2)	-298.69 (23-I-4)	31.67 (15)	6.83 (15)
31	7	-0.1 (16)	-0.1 (23-I-1)	0.0 (23-I-4)	-299.80 (23-I-4)	31.61 (15)	12.99 (23-I-2)
31	8	-0.1 (16)	-0.0 (23-I-1)	0.0 (16)	-314.65 (23-I-4)	-52.89 (23-II-4)	16.47 (23-I-2)
31	9	-0.2 (23-I-1)	-0.1 (22)	0.0 (16)	-414.81 (23-II-4)	-49.34 (23-I-1)	46.18 (23-II-1)
31	10	-0.1 (23-I-1)	-0.1 (23-I-1)	0.1 (23-I-1)	-264.46 (23-I-4)	-43.88 (23-II-4)	31.10 (23-II-1)
31	11	-0.0 (16)	-0.1 (13)	0.0 (23-II-1)	-265.35 (23-I-4)	41.50 (15)	27.49 (15)
31	12	-0.1 (16)	-0.1 (23-I-1)	-0.0 (23-I-1)	-415.56 (23-I-4)	-40.60 (23-I-1)	34.74 (15)
31	13	-0.5 (23-I-1)	-0.1 (23-I-1)	0.1 (23-I-1)	-703.06 (23-I-1)	-66.68 (23-I-1)	349.58 (23-I-1)
31	14	0.0 (23-I-1)	-0.1 (23-I-1)	0.0 (23-II-1)	-48.00 (23-I-4)	-57.97 (23-II-4)	52.75 (23-I-1)
31	15	-0.0 (23-II-1)	-0.1 (13)	0.0 (23-II-1)	-47.07 (23-I-4)	51.67 (15)	-42.42 (23-II-2)
31	16	0.3 (23-II-1)	-0.1 (13)	-0.1 (13)	-697.26 (23-I-1)	-15.92 (23-I-1)	-311.48 (23-II-2)
32	1	0.0 (23-I-1)	0.0 (23-II-4)	0.0 (23-II-2)	-184.33 (23-I-1)	-118.38 (23-II-4)	-142.01 (23-II-2)
32	2	0.0 (23-I-1)	0.0 (23-I-4)	0.0 (15)	-203.23 (23-I-1)	-47.39 (23-I-4)	-152.85 (23-II-2)
32	3	0.0 (23-I-1)	0.0 (23-I-4)	0.0 (15)	-244.28 (23-I-1)	-21.11 (23-I-3)	-140.81 (23-II-2)
32	4	0.0 (23-I-1)	0.0 (23-I-4)	0.0 (23-II-2)	-217.39 (23-I-1)	-11.43 (15)	-77.66 (23-II-2)
32	5	0.0 (23-I-1)	0.0 (23-I-4)	0.0 (23-II-2)	-159.75 (23-I-1)	-141.48 (23-II-4)	-130.70 (23-II-2)
32	6	0.0 (23-I-1)	0.0 (23-I-4)	0.0 (23-II-2)	-153.75 (23-I-1)	-34.86 (23-I-4)	-129.75 (23-II-2)
32	7	0.0 (23-I-1)	0.0 (23-I-4)	0.0 (23-II-2)	-162.10 (23-I-1)	11.83 (13)	-134.01 (23-II-2)
32	8	0.0 (23-I-1)	0.0 (23-II-4)	0.0 (23-II-2)	-151.72 (23-I-1)	12.40 (23-I-1)	-55.61 (23-II-2)



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
32	9	0.0 (23-I-1)	0.0 (23-I-4)	0.0 (23-II-2)	-131.37 (23-I-1)	-141.93 (23-II-4)	-125.77 (23-I-2)
32	10	0.0 (23-I-1)	0.0 (23-I-4)	0.0 (23-II-2)	-108.15 (13)	-27.89 (23-I-4)	-120.04 (23-II-2)
32	11	0.0 (23-I-1)	0.0 (23-I-4)	0.0 (23-II-2)	-100.96 (13)	13.06 (13)	-128.26 (23-II-2)
32	12	0.0 (23-I-1)	0.0 (23-I-4)	0.0 (23-II-2)	-100.14 (13)	20.72 (23-I-1)	-53.96 (23-II-2)
32	13	0.0 (23-I-1)	0.0 (23-I-4)	0.0 (23-II-2)	-117.04 (13)	-115.10 (23-II-4)	-108.45 (15)
32	14	0.0 (23-I-1)	0.0 (23-I-4)	0.0 (23-II-2)	-106.18 (13)	-28.79 (23-I-4)	-107.32 (15)
32	15	0.0 (23-I-1)	0.0 (23-I-4)	0.0 (23-II-2)	-92.00 (13)	18.42 (15)	-111.23 (15)
32	16	0.0 (23-I-1)	0.0 (23-I-4)	0.0 (23-II-2)	-92.68 (13)	17.66 (23-I-1)	-65.97 (15)
33	1	0.0 (23-I-1)	-0.0 (16)	0.0 (23-II-2)	-145.88 (23-I-1)	73.21 (16)	-95.88 (23-I-2)
33	2	0.0 (23-I-1)	0.0 (15)	0.0 (23-II-2)	-165.84 (23-I-1)	-139.96 (15)	-94.52 (23-II-2)
33	3	0.0 (23-I-1)	0.0 (15)	0.0 (23-II-2)	-125.32 (23-I-1)	127.57 (15)	-121.36 (23-I-2)
33	4	0.0 (23-I-1)	0.0 (15)	0.0 (23-I-2)	-155.11 (23-I-1)	-198.11 (15)	-111.37 (23-II-2)
33	5	0.0 (23-I-1)	0.0 (15)	0.0 (23-I-2)	-110.08 (23-I-1)	126.29 (15)	-122.66 (23-I-2)
33	6	0.0 (23-I-1)	0.0 (15)	0.0 (23-I-2)	-139.80 (13)	-197.97 (15)	-114.74 (23-II-2)
33	7	0.0 (13)	0.0 (23-II-4)	0.0 (23-I-2)	-114.69 (13)	70.37 (16)	-139.39 (15)
33	8	0.0 (13)	0.0 (15)	0.0 (23-I-2)	-132.92 (13)	-139.25 (15)	-132.08 (23-I-2)
34	1	0.0 (13)	-0.0 (15)	0.0 (15)	-131.16 (13)	148.02 (15)	-86.52 (23-I-2)
34	2	0.0 (13)	-0.1 (15)	0.0 (15)	-106.79 (13)	300.16 (15)	-87.44 (23-I-2)
34	3	0.0 (13)	-0.0 (15)	0.0 (15)	-114.58 (13)	231.18 (15)	57.71 (13)
34	4	0.0 (13)	-0.0 (15)	0.0 (15)	-145.26 (13)	-94.24 (22)	36.73 (13)
34	5	0.0 (13)	-0.0 (15)	0.0 (15)	-140.95 (13)	125.56 (15)	-63.88 (15)
34	6	0.0 (13)	-0.0 (15)	0.0 (15)	-107.55 (13)	356.37 (15)	-79.58 (15)
34	7	0.0 (13)	-0.0 (15)	0.0 (15)	-111.81 (13)	277.28 (15)	-65.41 (23-I-2)
34	8	0.0 (13)	-0.0 (15)	0.0 (15)	-161.85 (13)	-166.98 (13)	-74.83 (23-I-2)
34	9	0.0 (13)	-0.0 (15)	0.0 (15)	-144.37 (13)	125.34 (15)	-59.93 (15)
34	10	0.0 (13)	-0.0 (15)	0.0 (23-I-2)	-111.63 (13)	357.49 (15)	-82.42 (15)
34	11	0.0 (13)	-0.0 (15)	0.0 (23-I-2)	-113.98 (13)	278.34 (15)	-92.50 (15)
34	12	0.0 (13)	-0.0 (15)	0.0 (23-I-2)	-163.23 (13)	-168.37 (13)	-90.69 (15)
34	13	0.0 (13)	-0.0 (15)	0.0 (23-I-2)	-142.64 (13)	147.23 (15)	-42.91 (15)
34	14	0.0 (13)	-0.1 (15)	0.0 (23-I-2)	-119.26 (13)	302.54 (15)	-88.26 (15)
34	15	0.0 (13)	-0.0 (15)	0.0 (23-I-2)	-120.63 (13)	234.06 (15)	-172.30 (15)
34	16	0.0 (13)	-0.0 (15)	0.0 (23-I-2)	-149.99 (13)	-102.21 (22)	-151.30 (15)
35	1	0.0 (23-I-1)	0.0 (23-II-3)	0.0 (15)	-160.92 (23-I-1)	-192.10 (23-II-2)	-135.90 (23-I-2)
35	2	0.0 (23-I-1)	-0.0 (15)	0.0 (15)	-143.58 (23-II-2)	142.77 (15)	-172.38 (23-II-2)
35	3	0.0 (23-I-1)	-0.0 (15)	0.0 (15)	-138.11 (23-I-1)	154.14 (15)	-143.77 (23-II-2)
35	4	0.0 (23-I-1)	-0.0 (15)	0.0 (15)	-139.95 (23-I-1)	79.19 (16)	-117.18 (23-II-2)
35	5	0.0 (23-I-1)	-0.0 (15)	0.0 (15)	-166.86 (23-I-1)	-267.25 (23-II-2)	-98.57 (23-I-2)
35	6	0.0 (23-I-1)	-0.0 (15)	0.0 (15)	-129.83 (23-I-1)	168.62 (15)	-110.48 (23-I-2)
35	7	0.0 (23-I-1)	-0.0 (15)	0.0 (15)	-122.84 (23-I-1)	184.26 (15)	-114.34 (23-I-2)
35	8	0.0 (23-I-1)	-0.0 (15)	0.0 (23-I-2)	-126.37 (23-I-1)	79.96 (16)	-110.70 (23-II-2)
35	9	0.0 (13)	-0.0 (15)	0.0 (23-I-2)	-152.94 (13)	-271.32 (23-II-2)	-90.36 (15)
35	10	0.0 (23-I-1)	-0.0 (15)	0.0 (23-I-2)	-117.51 (13)	167.64 (15)	-94.66 (15)
35	11	0.0 (23-I-1)	-0.0 (15)	0.0 (23-I-2)	-109.67 (13)	184.43 (15)	-102.34 (23-I-2)
35	12	0.0 (23-I-1)	-0.0 (15)	0.0 (23-I-2)	-116.57 (13)	80.12 (16)	-106.04 (23-I-2)
35	13	0.0 (13)	0.0 (23-II-3)	0.0 (23-I-2)	-143.82 (13)	-203.90 (23-I-1)	-67.27 (15)
35	14	0.0 (13)	-0.0 (15)	0.0 (23-I-2)	-122.81 (13)	140.20 (15)	-63.44 (15)
35	15	0.0 (23-I-1)	-0.0 (15)	0.0 (23-I-2)	-111.55 (13)	154.37 (15)	-104.42 (15)
35	16	0.0 (23-I-1)	-0.0 (15)	0.0 (23-I-2)	-116.76 (13)	77.43 (16)	-114.00 (15)
36	1	0.0 (13)	0.0 (23-II-4)	0.0 (15)	-147.26 (13)	3.37 (23-II-2)	-1.29 (16)
36	2	0.0 (13)	0.0 (13)	0.0 (15)	-147.49 (13)	-4.85 (13)	-41.05 (15)
36	3	0.0 (13)	0.0 (13)	0.0 (15)	-150.84 (13)	2.90 (23-II-3)	10.16 (15)
36	4	0.0 (13)	0.0 (13)	0.0 (15)	-153.42 (13)	-5.60 (15)	-50.63 (15)
36	5	0.0 (13)	0.0 (15)	0.0 (15)	-151.01 (13)	2.76 (15)	11.01 (15)
36	6	0.0 (13)	0.0 (13)	0.0 (23-I-2)	-153.72 (13)	-5.47 (15)	-52.68 (15)
36	7	0.0 (13)	0.0 (13)	0.0 (15)	-157.22 (13)	1.13 (13)	1.46 (13)
36	8	0.0 (13)	0.0 (13)	0.0 (15)	-157.31 (13)	-6.34 (15)	-39.82 (15)
37	1	-0.0 (13)	-0.1 (23-II-3)	0.0 (16)	-68.97 (15)	-525.56 (15)	-8.97 (15)
37	2	-0.0 (13)	-0.1 (23-II-3)	0.0 (16)	-73.49 (15)	-502.77 (15)	-8.66 (15)
37	3	-0.1 (13)	-0.2 (23-II-3)	0.0 (16)	-42.78 (15)	-542.21 (15)	46.88 (15)
37	4	-0.1 (13)	-0.5 (23-II-3)	0.1 (23-II-3)	-14.36 (15)	-769.82 (15)	368.13 (15)
37	5	-0.0 (13)	-0.1 (23-II-3)	0.0 (23-II-2)	-63.08 (15)	-530.97 (15)	-8.97 (15)
37	6	-0.1 (13)	-0.1 (23-II-3)	0.0 (23-II-2)	-49.54 (15)	-481.87 (15)	-7.25 (15)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
37	7	-0.1 (13)	-0.1 (23-II-3)	0.1 (23-II-2)	-71.37 (15)	-370.46 (15)	32.99 (15)
37	8	-0.1 (13)	0.0 (23-I-4)	0.0 (23-II-3)	-90.75 (15)	-70.67 (15)	60.96 (15)
37	9	-0.0 (23-II-3)	-0.1 (16)	0.0 (23-II-2)	-63.07 (15)	-530.89 (15)	-7.96 (23-I-2)
37	10	-0.1 (23-II-3)	-0.1 (16)	0.0 (23-I-4)	-49.54 (15)	-481.78 (15)	-10.21 (23-I-2)
37	11	-0.1 (13)	-0.0 (16)	0.0 (23-I-4)	-71.27 (15)	-370.35 (15)	-42.95 (15)
37	12	-0.1 (13)	-0.0 (23-I-3)	0.0 (23-II-4)	-90.74 (15)	-70.71 (15)	-65.83 (15)
37	13	-0.0 (23-II-3)	-0.1 (16)	0.0 (16)	-68.93 (15)	-525.32 (15)	-7.10 (23-I-2)
37	14	-0.0 (13)	-0.1 (16)	-0.0 (13)	-73.44 (15)	-502.55 (15)	-8.52 (23-I-2)
37	15	-0.1 (23-II-3)	-0.1 (16)	-0.0 (23-II-4)	-42.61 (15)	-542.02 (15)	-56.86 (15)
37	16	-0.1 (13)	0.3 (23-I-3)	-0.1 (13)	50.45 (23-II-3)	-769.82 (15)	-370.65 (15)
38	1	-0.0 (13)	-0.1 (23-II-4)	0.0 (16)	-68.88 (15)	-525.09 (15)	-8.40 (15)
38	2	-0.0 (13)	-0.1 (23-II-4)	0.0 (16)	-73.34 (15)	-502.38 (15)	-8.15 (15)
38	3	-0.1 (13)	-0.2 (23-II-4)	0.0 (16)	-42.54 (15)	-541.97 (15)	47.34 (15)
38	4	-0.1 (13)	-0.5 (23-II-4)	0.1 (23-II-4)	-14.05 (15)	-769.75 (15)	368.45 (15)
38	5	-0.0 (13)	-0.1 (23-II-4)	0.0 (23-II-3)	-63.01 (15)	-530.59 (15)	-8.34 (15)
38	6	-0.1 (13)	-0.1 (23-II-4)	0.0 (23-II-3)	-49.41 (15)	-481.56 (15)	-6.65 (15)
38	7	-0.1 (13)	-0.1 (23-II-4)	0.1 (23-II-4)	-71.17 (15)	-370.27 (15)	33.56 (15)
38	8	-0.1 (13)	0.0 (23-II-4)	0.0 (23-I-1)	-90.50 (15)	-70.62 (15)	61.41 (15)
38	9	-0.0 (13)	-0.1 (16)	0.0 (23-II-3)	-63.00 (15)	-530.55 (15)	-8.40 (23-II-3)
38	10	-0.1 (13)	-0.1 (16)	0.0 (23-II-3)	-49.42 (15)	-481.51 (15)	-10.72 (23-II-3)
38	11	-0.1 (13)	-0.0 (16)	0.0 (23-II-2)	-71.09 (15)	-370.19 (15)	-42.28 (15)
38	12	-0.1 (13)	-0.0 (23-II-2)	0.0 (23-II-2)	-90.51 (15)	-70.66 (15)	-65.29 (15)
38	13	-0.0 (13)	-0.1 (16)	0.0 (16)	-68.86 (15)	-524.96 (15)	-7.46 (23-II-3)
38	14	-0.0 (13)	-0.1 (16)	-0.0 (13)	-73.32 (15)	-502.28 (15)	-8.94 (23-II-3)
38	15	-0.1 (23-II-4)	-0.1 (16)	-0.0 (23-I-2)	-42.43 (15)	-541.86 (15)	-56.11 (15)
38	16	-0.1 (13)	0.3 (23-I-4)	-0.1 (16)	50.95 (23-II-3)	-769.78 (15)	-370.10 (15)
39	1	-0.0 (13)	-0.1 (23-II-4)	0.0 (16)	-52.60 (15)	-422.62 (15)	-45.39 (23-I-3)
39	2	-0.0 (13)	-0.1 (23-II-4)	0.0 (16)	52.90 (23-II-2)	423.99 (23-I-3)	-60.07 (23-I-3)
39	3	-0.1 (13)	-0.2 (23-II-4)	0.0 (16)	22.60 (23-II-3)	630.74 (23-I-3)	-177.50 (23-I-3)
39	4	-0.1 (13)	-0.5 (23-II-4)	0.1 (23-II-4)	139.39 (23-II-3)	1032.73 (23-I-3)	-550.32 (23-I-3)
39	5	-0.0 (13)	-0.1 (23-II-4)	0.0 (23-II-2)	-51.77 (15)	-415.43 (15)	-46.06 (23-I-3)
39	6	-0.1 (13)	-0.1 (23-II-4)	0.0 (23-II-2)	-51.12 (15)	-362.74 (15)	-58.74 (23-I-3)
39	7	-0.1 (13)	-0.1 (23-II-4)	0.1 (23-I-1)	92.11 (23-I-4)	287.83 (23-I-4)	-119.05 (23-I-3)
39	8	-0.1 (13)	0.0 (23-II-4)	0.0 (23-II-4)	-27.30 (15)	-29.70 (15)	-41.06 (23-I-3)
39	9	-0.0 (13)	-0.1 (16)	0.0 (23-II-2)	-51.74 (15)	-415.23 (15)	-49.01 (23-I-3)
39	10	-0.1 (13)	-0.1 (16)	0.0 (23-II-2)	-51.15 (15)	-362.53 (15)	-53.31 (15)
39	11	-0.1 (13)	-0.0 (16)	0.0 (23-II-2)	92.29 (23-I-4)	288.01 (23-I-4)	-93.41 (15)
39	12	-0.1 (13)	-0.0 (23-I-4)	0.0 (23-I-4)	-27.12 (15)	-29.60 (15)	-43.65 (15)
39	13	-0.0 (13)	-0.1 (16)	0.0 (16)	-52.49 (15)	-422.03 (15)	-49.43 (23-I-3)
39	14	-0.0 (13)	-0.1 (16)	0.0 (16)	52.98 (23-II-2)	424.42 (23-I-4)	-53.81 (15)
39	15	-0.1 (23-II-4)	-0.1 (16)	-0.0 (23-I-2)	22.85 (23-II-2)	630.95 (23-I-4)	-128.91 (15)
39	16	-0.1 (13)	0.3 (23-I-4)	-0.1 (13)	139.65 (23-II-4)	1032.79 (23-I-4)	502.63 (23-II-2)
40	1	-0.0 (13)	-0.1 (23-II-3)	0.0 (16)	-68.93 (15)	-525.30 (15)	-8.85 (15)
40	2	-0.0 (13)	-0.1 (23-II-3)	0.0 (16)	-73.41 (15)	-502.54 (15)	-8.60 (15)
40	3	-0.1 (13)	-0.2 (23-II-3)	0.0 (16)	-42.65 (15)	-542.06 (15)	46.89 (15)
40	4	-0.1 (13)	-0.5 (23-II-3)	0.1 (23-II-3)	-14.18 (15)	-769.77 (15)	368.12 (15)
40	5	-0.0 (13)	-0.1 (23-II-3)	0.0 (23-II-2)	-63.05 (15)	-530.80 (15)	-8.83 (15)
40	6	-0.1 (13)	-0.1 (23-II-3)	0.0 (23-II-2)	-49.48 (15)	-481.71 (15)	-7.15 (15)
40	7	-0.1 (13)	-0.1 (23-II-3)	0.1 (23-II-3)	-71.28 (15)	-370.36 (15)	33.06 (15)
40	8	-0.1 (13)	0.0 (23-II-4)	0.0 (23-II-3)	-90.63 (15)	-70.65 (15)	61.00 (15)
40	9	-0.0 (13)	-0.1 (16)	0.0 (23-II-2)	-63.04 (15)	-530.76 (15)	-8.16 (23-II-2)
40	10	-0.1 (13)	-0.1 (16)	0.0 (23-II-2)	-49.50 (15)	-481.67 (15)	-10.38 (23-II-2)
40	11	-0.1 (13)	-0.0 (16)	0.0 (23-I-4)	-71.20 (15)	-370.28 (15)	-42.83 (15)
40	12	-0.1 (13)	-0.0 (23-I-3)	0.0 (23-I-4)	-90.65 (15)	-70.69 (15)	-65.73 (15)
40	13	-0.0 (13)	-0.1 (16)	0.0 (16)	-68.91 (15)	-525.21 (15)	-7.28 (23-I-3)
40	14	-0.0 (13)	-0.1 (16)	0.0 (16)	-73.41 (15)	-502.46 (15)	-8.68 (23-I-3)
40	15	-0.1 (23-II-4)	-0.1 (16)	-0.0 (23-II-4)	-42.56 (15)	-541.96 (15)	-56.71 (15)
40	16	-0.1 (13)	0.3 (23-I-3)	-0.1 (13)	50.75 (23-II-3)	-769.81 (15)	-370.54 (15)
41	1	-0.1 (23-I-1)	-0.0 (13)	0.0 (16)	334.43 (15)	43.00 (15)	7.99 (15)
41	2	-0.1 (23-I-1)	-0.0 (13)	0.0 (23-II-2)	336.07 (15)	40.74 (15)	7.94 (15)
41	3	-0.1 (16)	-0.0 (13)	0.0 (23-II-2)	336.04 (15)	40.73 (15)	11.97 (23-I-2)
41	4	-0.1 (16)	-0.0 (23-II-4)	0.0 (16)	334.40 (15)	43.00 (15)	12.71 (23-I-2)
41	5	-0.1 (23-I-1)	-0.0 (13)	0.0 (16)	-313.86 (23-II-4)	-55.80 (23-I-4)	7.10 (15)
41	6	-0.1 (23-I-1)	-0.0 (13)	0.0 (23-II-2)	-299.11 (23-II-4)	31.54 (15)	6.34 (15)
41	7	-0.1 (16)	-0.0 (23-II-4)	0.0 (23-II-2)	-300.12 (23-II-4)	31.53 (15)	12.62 (23-I-2)
41	8	-0.1 (16)	-0.0 (13)	0.0 (16)	-314.88 (23-II-4)	-52.92 (23-II-4)	16.10 (23-I-2)
41	9	-0.2 (23-I-1)	-0.1 (13)	0.0 (16)	-415.10 (23-II-4)	-49.25 (23-II-2)	45.90 (23-I-2)
41	10	-0.1 (23-I-1)	-0.1 (13)	0.1 (23-I-1)	-264.69 (23-II-4)	-44.01 (23-I-4)	30.79 (23-I-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
41	11	-0.0 (16)	-0.1 (13)	0.0 (23-I-4)	-265.52 (23-II-4)	41.37 (15)	26.97 (15)
41	12	-0.1 (16)	-0.1 (23-II-4)	-0.0 (23-I-2)	-415.70 (23-II-4)	-40.65 (23-I-1)	34.17 (15)
41	13	-0.5 (23-I-1)	-0.1 (13)	0.1 (23-II-4)	-702.90 (23-I-1)	-66.40 (23-II-2)	349.10 (23-II-4)
41	14	0.0 (23-I-1)	-0.1 (13)	0.0 (23-II-4)	-48.05 (23-II-4)	-58.11 (23-I-4)	52.50 (23-I-2)
41	15	-0.0 (23-I-4)	-0.1 (13)	0.0 (23-II-1)	-47.11 (23-II-4)	51.51 (15)	-42.63 (23-II-2)
41	16	0.3 (23-I-4)	-0.1 (13)	-0.1 (13)	-696.75 (23-II-4)	-16.26 (23-I-1)	-311.59 (23-II-4)
42	1	-0.0 (13)	-0.1 (23-I-1)	0.0 (16)	-52.90 (15)	-424.00 (15)	-44.23 (23-I-2)
42	2	-0.0 (13)	-0.1 (23-I-1)	0.0 (16)	52.37 (23-I-4)	423.44 (23-I-3)	-58.84 (23-I-2)
42	3	-0.1 (13)	-0.2 (23-I-1)	0.0 (16)	21.95 (23-II-3)	630.51 (23-I-3)	-176.21 (23-I-2)
42	4	-0.1 (13)	-0.5 (23-I-1)	0.1 (23-I-1)	138.70 (23-II-3)	1032.72 (23-I-3)	-549.53 (23-I-3)
42	5	-0.0 (13)	-0.1 (23-I-1)	0.0 (23-II-2)	-52.03 (15)	-416.60 (15)	-45.13 (23-I-2)
42	6	-0.1 (13)	-0.1 (23-I-1)	0.0 (23-II-2)	-51.56 (15)	-363.52 (15)	-57.73 (23-I-2)
42	7	-0.1 (13)	-0.1 (23-I-1)	0.1 (23-II-2)	91.51 (23-I-4)	287.65 (23-I-3)	-117.99 (23-I-2)
42	8	-0.1 (13)	0.0 (23-II-4)	0.0 (23-I-1)	-27.95 (15)	-29.78 (15)	-40.39 (23-I-2)
42	9	-0.0 (23-II-4)	-0.1 (16)	0.0 (23-II-2)	-51.97 (15)	-416.21 (15)	-48.31 (23-I-2)
42	10	-0.1 (23-II-4)	-0.1 (16)	0.0 (23-II-2)	-51.53 (15)	-363.19 (15)	-54.82 (15)
42	11	-0.1 (13)	-0.0 (16)	0.0 (23-I-4)	91.77 (23-I-3)	287.84 (23-I-3)	-94.78 (15)
42	12	-0.1 (13)	-0.0 (23-II-1)	0.0 (23-I-4)	-27.68 (15)	-29.67 (15)	-44.47 (15)
42	13	-0.0 (23-II-4)	-0.1 (16)	0.0 (16)	-52.68 (15)	-422.87 (15)	-48.93 (23-I-3)
42	14	-0.0 (13)	-0.1 (16)	0.0 (16)	52.69 (23-II-2)	424.12 (23-I-3)	-55.52 (15)
42	15	-0.1 (23-II-4)	-0.1 (16)	-0.0 (23-II-4)	22.50 (23-II-3)	630.84 (23-I-3)	-130.47 (15)
42	16	-0.1 (13)	0.3 (23-I-4)	-0.1 (13)	139.28 (23-II-3)	1032.82 (23-I-3)	502.69 (23-II-2)
43	1	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-2)	-141.99 (23-I-1)	-122.73 (23-II-4)	-142.97 (23-II-2)
43	2	0.0 (13)	0.0 (23-I-4)	0.0 (15)	-151.11 (23-I-1)	-40.09 (23-I-4)	-156.68 (23-II-3)
43	3	0.0 (13)	0.0 (23-I-4)	0.0 (15)	-184.68 (23-I-1)	-12.08 (23-I-4)	-144.89 (23-II-3)
43	4	0.0 (13)	-0.0 (15)	0.0 (23-I-2)	-160.83 (23-I-1)	-7.69 (15)	-80.47 (23-II-2)
43	5	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-2)	-120.49 (23-I-1)	-149.37 (23-II-4)	-126.64 (23-I-2)
43	6	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-2)	-109.27 (23-I-1)	-28.72 (23-I-4)	-126.75 (23-I-2)
43	7	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-2)	-113.85 (23-I-1)	13.09 (13)	-133.56 (23-I-2)
43	8	0.0 (13)	0.0 (23-I-4)	0.0 (23-II-2)	-103.46 (23-I-1)	15.23 (23-I-1)	-58.32 (23-I-2)
43	9	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-2)	-117.29 (13)	-149.30 (23-II-4)	-120.62 (23-I-2)
43	10	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-2)	-104.14 (13)	-23.79 (23-I-4)	-115.25 (23-I-2)
43	11	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-2)	-97.28 (13)	15.67 (15)	-125.92 (23-I-2)
43	12	0.0 (13)	0.0 (23-I-4)	0.0 (23-II-3)	-96.64 (13)	22.27 (23-I-1)	-55.50 (23-I-2)
43	13	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-2)	-112.35 (13)	-119.60 (23-II-4)	-100.98 (15)
43	14	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-100.42 (13)	-27.16 (23-I-4)	-99.32 (15)
43	15	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-88.35 (13)	20.20 (15)	-105.72 (15)
43	16	0.0 (13)	0.0 (23-I-4)	0.0 (23-II-3)	-89.62 (13)	17.92 (23-II-1)	-64.37 (23-I-2)
44	1	0.0 (13)	-0.0 (15)	0.0 (15)	-136.54 (13)	147.95 (15)	-89.85 (23-I-2)
44	2	0.0 (13)	-0.1 (15)	0.0 (15)	-113.49 (13)	302.49 (15)	-91.37 (23-I-2)
44	3	0.0 (13)	-0.0 (15)	0.0 (15)	-120.21 (13)	230.24 (15)	64.69 (13)
44	4	0.0 (13)	-0.0 (15)	0.0 (15)	-149.05 (13)	-107.35 (22)	43.71 (13)
44	5	0.0 (13)	-0.0 (15)	0.0 (15)	-142.58 (13)	125.37 (15)	-63.81 (23-I-3)
44	6	0.0 (13)	-0.0 (15)	0.0 (15)	-109.38 (13)	359.70 (15)	-82.23 (23-II-3)
44	7	0.0 (13)	-0.0 (15)	0.0 (15)	-113.03 (13)	277.12 (15)	-71.64 (23-II-3)
44	8	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-162.52 (13)	-175.49 (22)	-78.22 (23-II-3)
44	9	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-142.85 (13)	125.37 (15)	-58.83 (23-I-3)
44	10	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-109.09 (13)	360.58 (15)	-80.58 (15)
44	11	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-111.35 (13)	278.10 (15)	-92.39 (15)
44	12	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-161.27 (13)	-177.45 (22)	-93.17 (23-I-3)
44	13	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-137.94 (13)	147.57 (15)	-40.72 (15)
44	14	0.0 (13)	-0.1 (15)	0.0 (23-I-3)	-112.80 (13)	304.52 (15)	-86.61 (15)
44	15	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-114.79 (13)	233.19 (15)	-172.81 (15)
44	16	0.0 (13)	0.0 (22)	0.0 (23-I-3)	-145.44 (13)	-112.24 (22)	-150.96 (15)
45	1	0.0 (13)	0.0 (23-II-3)	0.0 (15)	-143.38 (23-I-1)	-211.77 (23-I-1)	-142.29 (23-I-2)
45	2	0.0 (13)	-0.0 (15)	0.0 (15)	-128.25 (23-I-1)	134.11 (15)	-178.80 (23-I-2)
45	3	0.0 (13)	-0.0 (15)	0.0 (15)	-118.00 (23-I-1)	148.71 (15)	-149.77 (23-I-2)
45	4	0.0 (13)	-0.0 (15)	0.0 (15)	-116.84 (13)	75.09 (16)	-120.21 (23-I-2)
45	5	0.0 (13)	0.0 (23-II-4)	0.0 (23-I-2)	-151.95 (13)	-287.89 (23-I-1)	-103.74 (23-II-3)
45	6	0.0 (13)	-0.0 (15)	0.0 (23-I-2)	-115.98 (13)	160.29 (15)	-111.63 (23-I-2)
45	7	0.0 (13)	-0.0 (15)	0.0 (23-I-2)	-108.39 (13)	179.89 (15)	-114.93 (23-I-2)
45	8	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-115.24 (13)	79.19 (16)	-109.39 (23-I-2)
45	9	0.0 (13)	0.0 (23-II-4)	0.0 (23-I-2)	-150.76 (13)	-289.82 (23-I-1)	-92.24 (23-II-3)
45	10	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-114.18 (13)	159.91 (15)	-92.84 (23-I-2)
45	11	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-106.34 (13)	180.38 (15)	-100.86 (23-I-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
45	12	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-113.64 (13)	79.53 (16)	-103.41 (23-I-2)
45	13	0.0 (13)	0.0 (23-II-4)	0.0 (23-I-3)	-139.14 (13)	-218.11 (23-II-4)	-63.63 (15)
45	14	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-116.21 (13)	133.38 (15)	-56.93 (15)
45	15	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-105.33 (13)	150.03 (15)	-97.51 (15)
45	16	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-112.19 (13)	74.55 (16)	-108.56 (15)
46	1	0.0 (13)	0.0 (23-II-4)	0.0 (23-I-2)	-114.87 (13)	66.08 (16)	-97.66 (23-I-2)
46	2	0.0 (13)	0.0 (15)	0.0 (23-I-2)	-133.49 (13)	-141.48 (15)	-94.78 (23-I-2)
46	3	0.0 (13)	0.0 (15)	0.0 (23-I-2)	-105.52 (13)	120.75 (15)	-120.83 (23-II-3)
46	4	0.0 (13)	0.0 (15)	0.0 (23-I-2)	-138.38 (13)	-197.82 (15)	-108.87 (23-I-2)
46	5	0.0 (13)	0.0 (15)	0.0 (23-I-2)	-104.02 (13)	120.17 (15)	-121.09 (23-II-3)
46	6	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-136.86 (13)	-197.72 (15)	-111.87 (23-I-2)
46	7	0.0 (13)	0.0 (23-II-4)	0.0 (23-I-3)	-110.42 (13)	64.90 (16)	-135.66 (23-I-3)
46	8	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-128.50 (13)	-140.45 (15)	-128.67 (23-I-2)
47	1	-0.0 (13)	-0.1 (23-II-4)	0.0 (16)	-52.44 (15)	-421.91 (15)	-45.67 (23-I-3)
47	2	-0.0 (13)	-0.1 (23-II-4)	0.0 (16)	53.14 (23-II-2)	424.30 (23-I-4)	-60.43 (23-I-3)
47	3	-0.1 (13)	-0.2 (23-II-4)	0.0 (16)	22.88 (23-II-4)	630.85 (23-I-4)	-177.84 (23-I-3)
47	4	-0.1 (13)	-0.5 (23-II-4)	0.1 (23-II-4)	139.66 (23-II-4)	1032.71 (23-I-4)	-550.41 (23-I-3)
47	5	-0.0 (13)	-0.1 (23-II-4)	0.0 (23-I-1)	-51.63 (15)	-414.84 (15)	-46.17 (23-I-3)
47	6	-0.1 (13)	-0.1 (23-II-4)	0.0 (23-I-1)	-50.89 (15)	-362.33 (15)	-58.91 (23-I-3)
47	7	-0.1 (13)	-0.1 (23-II-4)	0.1 (23-II-4)	92.43 (23-II-2)	287.92 (23-I-4)	-119.23 (23-I-3)
47	8	-0.1 (13)	0.0 (23-II-4)	0.0 (23-I-1)	-26.94 (15)	-29.65 (15)	-41.17 (23-I-3)
47	9	-0.0 (13)	-0.1 (16)	0.0 (23-I-1)	-51.63 (15)	-414.72 (15)	-48.97 (23-I-3)
47	10	-0.1 (13)	-0.1 (16)	0.0 (23-I-1)	-50.95 (15)	-362.18 (15)	-51.17 (15)
47	11	-0.1 (13)	-0.0 (16)	0.0 (23-II-2)	92.56 (23-I-4)	287.95 (23-I-4)	-91.42 (15)
47	12	-0.1 (13)	-0.0 (23-II-2)	0.0 (23-II-2)	-26.82 (15)	-29.56 (15)	-42.45 (15)
47	13	-0.0 (13)	-0.1 (16)	0.0 (16)	-52.38 (15)	-421.57 (15)	-49.24 (23-I-3)
47	14	-0.0 (13)	-0.1 (16)	-0.0 (13)	53.17 (23-II-2)	424.40 (23-II-2)	-51.55 (15)
47	15	-0.1 (23-II-4)	-0.1 (16)	-0.0 (23-I-2)	23.12 (23-I-2)	630.90 (23-II-2)	-126.82 (15)
47	16	-0.1 (13)	0.3 (23-I-4)	-0.1 (13)	139.90 (23-I-2)	1032.74 (23-II-2)	502.87 (23-II-3)
48	1	-0.1 (23-I-1)	-0.0 (13)	0.0 (16)	334.55 (15)	43.03 (15)	8.30 (15)
48	2	-0.1 (23-I-1)	-0.0 (13)	0.0 (23-II-2)	336.14 (15)	40.75 (15)	8.28 (15)
48	3	-0.1 (16)	-0.0 (23-I-1)	0.0 (23-II-2)	336.06 (15)	40.73 (15)	12.16 (23-II-2)
48	4	-0.1 (16)	-0.0 (23-II-4)	0.0 (16)	334.40 (15)	43.00 (15)	12.90 (23-II-2)
48	5	-0.1 (23-I-1)	-0.0 (13)	0.0 (16)	-313.69 (23-I-4)	-55.77 (23-II-4)	7.39 (15)
48	6	-0.1 (23-I-1)	-0.0 (13)	0.0 (23-II-2)	-299.00 (23-I-4)	31.56 (15)	6.65 (15)
48	7	-0.1 (16)	-0.1 (23-I-1)	0.0 (23-II-2)	-300.06 (23-I-4)	31.54 (15)	12.76 (23-II-2)
48	8	-0.1 (16)	-0.0 (23-II-4)	0.0 (16)	-314.86 (23-I-4)	-52.94 (23-I-4)	16.23 (23-II-2)
48	9	-0.2 (23-I-1)	-0.1 (13)	0.0 (16)	-414.98 (23-I-4)	-49.28 (23-I-1)	46.04 (23-II-1)
48	10	-0.1 (23-I-1)	-0.1 (23-I-1)	0.1 (23-I-1)	-264.62 (23-I-4)	-43.98 (23-II-4)	30.94 (23-II-1)
48	11	-0.0 (16)	-0.1 (13)	0.0 (23-I-4)	-265.48 (23-II-4)	41.39 (15)	27.28 (15)
48	12	-0.1 (16)	-0.1 (23-II-4)	-0.0 (23-II-4)	-415.69 (23-II-4)	-40.65 (23-I-1)	34.49 (15)
48	13	-0.5 (23-I-1)	-0.1 (23-I-1)	0.1 (23-I-1)	-703.29 (23-I-1)	-66.32 (23-II-4)	349.48 (23-I-1)
48	14	0.0 (23-I-1)	-0.1 (23-I-1)	0.0 (23-II-1)	-48.04 (23-I-4)	-58.08 (23-II-4)	52.62 (23-I-1)
48	15	-0.0 (23-II-1)	-0.1 (13)	0.0 (23-II-1)	-47.10 (23-II-4)	51.54 (15)	-42.42 (23-I-2)
48	16	0.3 (23-II-1)	-0.1 (13)	-0.1 (13)	-696.95 (23-I-1)	-16.16 (23-I-1)	-311.51 (23-I-1)
49	1	-0.1 (23-II-4)	-0.0 (13)	0.0 (16)	334.44 (15)	43.01 (15)	7.65 (15)
49	2	-0.1 (23-II-4)	-0.0 (13)	0.0 (23-I-1)	336.10 (15)	40.74 (15)	7.60 (15)
49	3	-0.1 (16)	-0.0 (13)	0.0 (23-I-1)	336.09 (15)	40.74 (15)	11.79 (23-I-2)
49	4	-0.1 (16)	-0.0 (13)	0.0 (16)	334.47 (15)	43.01 (15)	12.55 (23-I-2)
49	5	-0.1 (23-II-4)	-0.0 (13)	0.0 (16)	-313.86 (23-I-4)	-55.78 (23-I-4)	6.77 (15)
49	6	-0.1 (23-II-4)	-0.0 (13)	0.0 (23-I-1)	-299.10 (23-I-4)	31.55 (15)	6.02 (15)
49	7	-0.1 (16)	-0.0 (13)	0.0 (23-I-1)	-300.10 (23-I-4)	31.55 (15)	12.48 (23-II-1)
49	8	-0.1 (16)	-0.0 (13)	-0.0 (13)	-314.87 (23-I-4)	-52.91 (23-II-4)	15.95 (23-I-2)
49	9	-0.2 (23-II-4)	-0.1 (13)	0.0 (16)	-415.10 (23-II-4)	-49.28 (23-II-1)	45.79 (23-II-1)
49	10	-0.1 (23-II-4)	-0.1 (13)	0.1 (23-II-4)	-264.68 (23-II-4)	-43.99 (23-I-4)	30.68 (23-II-1)
49	11	-0.0 (16)	-0.1 (13)	0.0 (23-II-2)	-265.51 (23-I-4)	41.40 (15)	26.66 (15)
49	12	-0.1 (16)	-0.1 (23-II-4)	-0.0 (23-I-2)	-415.67 (23-I-4)	-40.58 (23-I-1)	33.86 (15)
49	13	-0.5 (23-II-4)	-0.1 (13)	0.1 (23-I-2)	-702.73 (23-II-4)	-66.48 (23-II-1)	348.96 (23-I-2)
49	14	0.0 (23-I-1)	-0.1 (13)	0.0 (23-II-1)	-48.05 (23-I-4)	-58.09 (23-I-4)	52.41 (23-II-1)
49	15	-0.0 (23-I-1)	-0.1 (13)	0.0 (23-II-1)	-47.11 (23-II-4)	51.54 (15)	-42.80 (23-II-1)
49	16	0.3 (23-I-4)	-0.1 (13)	-0.1 (16)	-696.56 (23-II-2)	-16.11 (23-I-1)	-311.56 (23-II-4)
50	1	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-2)	-116.70 (13)	-125.24 (23-II-4)	-140.27 (23-I-3)
50	2	0.0 (13)	0.0 (23-I-4)	0.0 (15)	-110.05 (13)	-37.35 (23-I-4)	-154.87 (23-I-3)
50	3	0.0 (13)	0.0 (23-I-4)	0.0 (15)	-136.56 (23-I-1)	-8.22 (23-I-4)	-142.69 (23-I-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
50	4	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-115.94 (23-I-1)	-5.79 (15)	-79.34 (23-I-3)
50	5	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-2)	-115.50 (13)	-153.35 (23-II-4)	-121.73 (23-I-3)
50	6	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-104.34 (13)	-26.62 (23-I-4)	-122.47 (23-I-2)
50	7	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-100.47 (13)	13.83 (13)	-129.55 (23-I-3)
50	8	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-98.00 (13)	16.30 (23-II-4)	-58.05 (23-I-2)
50	9	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-112.58 (13)	-153.24 (23-II-4)	-115.50 (23-I-3)
50	10	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-99.29 (13)	-22.75 (23-I-4)	-110.52 (23-I-3)
50	11	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-92.98 (13)	17.15 (15)	-121.39 (23-I-3)
50	12	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-92.31 (13)	22.47 (23-II-4)	-54.88 (23-I-2)
50	13	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-107.44 (13)	-122.66 (23-II-4)	-94.36 (15)
50	14	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-95.53 (13)	-27.46 (23-I-4)	-92.58 (15)
50	15	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-85.77 (13)	19.76 (15)	-99.36 (15)
50	16	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-86.89 (13)	17.39 (23-II-1)	-62.08 (23-I-3)
51	1	0.0 (13)	0.0 (23-II-3)	0.0 (15)	-150.91 (13)	3.42 (23-I-2)	-1.68 (16)
51	2	0.0 (13)	0.0 (15)	0.0 (15)	-151.16 (13)	-5.09 (13)	-38.94 (15)
51	3	0.0 (13)	0.0 (13)	0.0 (15)	-151.32 (13)	3.04 (23-II-3)	8.87 (15)
51	4	0.0 (13)	0.0 (13)	0.0 (23-II-3)	-153.93 (13)	-5.70 (15)	-47.84 (15)
51	5	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-150.44 (13)	2.85 (15)	9.89 (15)
51	6	0.0 (13)	0.0 (13)	0.0 (23-II-3)	-153.14 (13)	-5.63 (15)	-52.81 (23-I-3)
51	7	0.0 (13)	0.0 (13)	0.0 (23-I-3)	-154.02 (13)	1.36 (13)	1.04 (13)
51	8	0.0 (13)	0.0 (13)	0.0 (23-I-3)	-154.09 (13)	-6.42 (22)	-39.16 (23-I-3)
52	1	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-111.46 (13)	-126.85 (23-II-4)	-137.01 (23-I-3)
52	2	0.0 (13)	0.0 (23-I-4)	0.0 (15)	-104.30 (13)	-36.00 (23-I-4)	-151.78 (23-I-3)
52	3	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-101.06 (13)	8.33 (13)	-138.77 (23-I-3)
52	4	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-97.45 (13)	-4.56 (15)	-77.06 (23-I-3)
52	5	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-110.47 (13)	-155.74 (23-II-4)	-117.19 (23-I-3)
52	6	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-99.03 (13)	-25.79 (23-I-4)	-118.69 (23-I-3)
52	7	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-94.54 (13)	14.10 (13)	-124.93 (23-I-3)
52	8	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-92.27 (13)	16.77 (23-II-2)	-57.14 (23-I-3)
52	9	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-107.84 (13)	-155.89 (23-I-4)	-111.09 (23-I-3)
52	10	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-94.82 (13)	-22.67 (23-I-4)	-106.76 (23-I-3)
52	11	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-89.22 (13)	17.31 (22)	-116.70 (23-I-3)
52	12	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-88.38 (13)	22.18 (23-II-4)	-53.91 (23-I-3)
52	13	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-103.12 (13)	-125.20 (23-I-4)	-89.43 (23-I-3)
52	14	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-91.86 (13)	-28.39 (23-I-4)	-86.87 (15)
52	15	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-84.53 (13)	18.60 (15)	-93.12 (15)
52	16	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-85.10 (13)	16.56 (23-II-4)	-59.60 (23-I-3)
53	1	0.0 (13)	0.0 (23-II-4)	0.0 (23-I-3)	-111.75 (13)	61.70 (14)	-95.41 (23-I-3)
53	2	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-130.24 (13)	-142.67 (15)	-92.42 (23-I-2)
53	3	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-101.36 (13)	116.65 (15)	-117.42 (23-I-3)
53	4	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-134.15 (13)	-198.54 (15)	-106.06 (23-I-2)
53	5	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-99.25 (13)	116.24 (15)	-117.44 (23-I-3)
53	6	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-132.12 (13)	-198.71 (15)	-109.22 (23-I-3)
53	7	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-105.29 (13)	60.79 (16)	-132.34 (23-I-3)
53	8	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-123.39 (13)	-142.35 (15)	-125.74 (23-I-3)
54	1	0.0 (13)	-0.0 (15)	0.0 (15)	-136.64 (13)	148.03 (15)	-92.09 (23-I-3)
54	2	0.0 (13)	-0.1 (15)	0.0 (15)	-114.32 (13)	303.70 (15)	-93.73 (23-I-3)
54	3	0.0 (13)	-0.0 (15)	0.0 (15)	-119.75 (13)	228.80 (15)	71.92 (13)
54	4	0.0 (13)	0.0 (22)	0.0 (15)	-147.49 (13)	-117.00 (22)	50.94 (13)
54	5	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-140.21 (13)	125.37 (15)	-66.06 (23-I-3)
54	6	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-107.10 (13)	361.47 (15)	-85.18 (23-I-3)
54	7	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-110.20 (13)	275.96 (15)	-74.56 (23-I-3)
54	8	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-159.35 (13)	-185.84 (22)	-79.94 (23-I-3)
54	9	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-138.57 (13)	125.31 (15)	-60.82 (23-I-3)
54	10	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-104.25 (13)	362.03 (15)	-81.84 (23-I-3)
54	11	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-106.63 (13)	276.64 (15)	-92.70 (23-I-3)
54	12	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-156.90 (13)	-187.34 (22)	-94.73 (23-I-3)
54	13	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-131.76 (13)	147.44 (15)	-37.81 (15)
54	14	0.0 (13)	-0.1 (15)	0.0 (23-I-3)	-105.74 (13)	304.87 (15)	-83.59 (15)
54	15	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-108.73 (13)	230.94 (15)	-170.78 (15)
54	16	0.0 (13)	0.0 (23-II-4)	0.0 (23-I-3)	-139.98 (13)	-120.72 (22)	-148.37 (15)
55	1	0.0 (13)	0.0 (23-II-4)	0.0 (15)	-140.76 (13)	-225.19 (23-II-4)	-144.76 (23-I-3)
55	2	0.0 (13)	-0.0 (15)	0.0 (15)	-120.35 (13)	127.65 (15)	-181.06 (23-I-3)
55	3	0.0 (13)	-0.0 (15)	0.0 (15)	-109.98 (13)	144.70 (15)	-151.00 (23-I-3)
55	4	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-114.08 (13)	71.94 (16)	-119.67 (23-I-3)
55	5	0.0 (13)	0.0 (23-II-4)	0.0 (23-I-3)	-148.55 (13)	-302.00 (23-II-4)	-104.86 (23-I-3)
55	6	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-112.54 (13)	153.80 (15)	-110.87 (23-I-3)
55	7	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-104.81 (13)	176.25 (15)	-113.38 (23-I-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
55	8	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-111.32 (13)	77.75 (16)	-107.27 (23-I-3)
55	9	0.0 (13)	0.0 (23-II-4)	0.0 (23-I-3)	-146.27 (13)	-302.85 (23-II-4)	-92.57 (23-I-3)
55	10	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-109.15 (13)	153.47 (15)	-91.43 (23-I-3)
55	11	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-101.32 (13)	176.56 (15)	-98.47 (23-I-3)
55	12	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-108.83 (13)	77.88 (16)	-100.94 (23-I-3)
55	13	0.0 (13)	0.0 (23-II-4)	0.0 (23-I-3)	-133.68 (13)	-228.84 (23-II-4)	-58.67 (15)
55	14	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-109.97 (13)	126.98 (15)	-50.59 (15)
55	15	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-99.34 (13)	145.52 (15)	-90.74 (15)
55	16	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-106.88 (13)	71.36 (16)	-102.97 (15)
56	1	0.0 (13)	0.0 (23-I-2)	0.0 (15)	-150.02 (13)	3.52 (23-I-2)	-1.70 (16)
56	2	0.0 (13)	0.0 (15)	0.0 (15)	-150.29 (13)	-5.28 (13)	-37.20 (15)
56	3	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-148.18 (13)	3.16 (23-II-4)	8.39 (15)
56	4	0.0 (13)	0.0 (13)	0.0 (23-I-3)	-150.81 (13)	-5.85 (15)	-48.10 (23-I-3)
56	5	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-146.87 (13)	2.95 (15)	9.58 (15)
56	6	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-149.56 (13)	-5.78 (15)	-54.40 (23-I-3)
56	7	0.0 (13)	0.0 (13)	0.0 (23-I-3)	-148.57 (13)	1.55 (13)	0
56	8	0.0 (13)	0.0 (13)	0.0 (23-I-3)	-148.67 (13)	-6.62 (22)	-40.39 (23-I-3)
57	1	0.0 (13)	0.0 (23-II-4)	0.0 (23-I-3)	-136.40 (13)	-234.92 (23-II-4)	-145.11 (23-I-3)
57	2	0.0 (13)	-0.0 (15)	0.0 (15)	-116.11 (13)	122.45 (15)	-181.91 (23-I-3)
57	3	0.0 (13)	-0.0 (15)	0.0 (15)	-105.46 (13)	141.36 (15)	-150.82 (23-I-3)
57	4	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-109.33 (13)	69.15 (14)	-118.65 (23-I-3)
57	5	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-143.72 (13)	-312.53 (23-II-4)	-103.58 (23-I-3)
57	6	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-107.65 (13)	147.95 (15)	-110.02 (23-I-3)
57	7	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-99.88 (13)	172.62 (15)	-111.89 (23-I-3)
57	8	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-106.36 (13)	75.71 (14)	-106.38 (23-I-3)
57	9	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-141.17 (13)	-313.40 (23-II-2)	-90.84 (23-I-3)
57	10	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-103.94 (13)	146.97 (15)	-90.31 (23-I-3)
57	11	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-96.19 (13)	172.24 (15)	-96.62 (23-I-3)
57	12	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-103.80 (13)	75.40 (14)	-100.06 (23-I-3)
57	13	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-128.36 (13)	-239.02 (23-II-2)	-53.18 (15)
57	14	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-104.60 (13)	119.65 (15)	52.71 (13)
57	15	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-94.22 (13)	140.02 (15)	-84.92 (15)
57	16	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-101.91 (13)	67.55 (14)	-98.34 (15)
58	1	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-106.91 (13)	58.41 (14)	-92.21 (23-I-3)
58	2	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-125.35 (13)	-144.24 (15)	-90.24 (23-I-3)
58	3	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-96.35 (13)	113.35 (15)	-113.45 (23-I-3)
58	4	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-129.17 (13)	-200.21 (15)	-104.63 (23-I-3)
58	5	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-94.26 (13)	112.75 (15)	-113.57 (23-I-3)
58	6	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-127.20 (13)	-200.62 (15)	-108.16 (23-I-3)
58	7	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-100.43 (13)	56.92 (16)	-129.38 (23-I-3)
58	8	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-118.64 (13)	-144.94 (15)	-124.08 (23-I-3)
59	1	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-146.99 (13)	3.64 (23-I-3)	-1.38 (13)
59	2	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-147.25 (13)	-5.44 (13)	-38.39 (23-I-3)
59	3	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-143.50 (13)	3.26 (23-II-4)	8.65 (15)
59	4	0.0 (13)	0.0 (15)	0.0 (23-II-3)	-146.15 (13)	-6.08 (15)	-49.67 (23-I-3)
59	5	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-142.15 (13)	3.07 (15)	9.96 (15)
59	6	0.0 (13)	0.0 (15)	0.0 (23-II-3)	-144.82 (13)	-5.94 (15)	-56.00 (23-I-3)
59	7	0.0 (13)	0.0 (13)	0.0 (23-I-3)	-142.34 (13)	1.73 (13)	1.07 (23-I-3)
59	8	0.0 (13)	0.0 (13)	0.0 (23-I-3)	-142.47 (13)	-6.84 (22)	-41.50 (23-I-3)
60	1	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-133.98 (13)	148.33 (15)	-93.03 (23-I-3)
60	2	0.0 (13)	-0.1 (15)	0.0 (15)	-111.85 (13)	304.61 (15)	-94.37 (23-I-3)
60	3	0.0 (13)	-0.0 (15)	0.0 (15)	-115.93 (13)	227.31 (15)	79.35 (13)
60	4	0.0 (13)	0.0 (22)	0.0 (23-I-3)	-143.31 (13)	-124.76 (22)	58.32 (13)
60	5	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-136.07 (13)	125.51 (15)	-65.99 (23-I-3)
60	6	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-102.97 (13)	362.39 (15)	-85.97 (23-I-3)
60	7	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-105.61 (13)	274.06 (15)	-74.92 (23-I-3)
60	8	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-154.63 (13)	-194.82 (22)	-80.85 (23-I-3)
60	9	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-133.30 (13)	125.14 (15)	-60.43 (23-I-3)
60	10	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-98.75 (13)	362.22 (15)	-82.38 (23-I-3)
60	11	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-101.41 (13)	273.86 (15)	-92.97 (23-I-3)
60	12	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-151.82 (13)	-196.62 (22)	-95.62 (23-I-3)
60	13	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-125.26 (13)	146.77 (15)	-36.50 (23-I-3)
60	14	0.0 (13)	-0.1 (15)	0.0 (23-I-3)	-98.98 (13)	303.56 (15)	-79.19 (15)
60	15	0.0 (13)	-0.0 (15)	-0.0 (13)	-103.17 (13)	226.79 (15)	-167.02 (15)
60	16	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-134.59 (13)	-129.47 (22)	-144.66 (15)
61	1	-0.0 (13)	-0.1 (23-II-4)	0.0 (16)	-68.91 (15)	-525.20 (15)	-8.66 (15)
61	2	-0.0 (13)	-0.1 (23-II-4)	0.0 (16)	-73.38 (15)	-502.46 (15)	-8.42 (15)
61	3	-0.1 (13)	-0.2 (23-II-4)	0.0 (16)	-42.60 (15)	-542.02 (15)	47.07 (15)
61	4	-0.1 (13)	-0.5 (23-II-4)	0.1 (23-II-4)	-14.12 (15)	-769.76 (15)	368.25 (15)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
61	5	-0.0 (13)	-0.1 (23-II-4)	0.0 (23-II-2)	-63.03 (15)	-530.71 (15)	-8.62 (15)
61	6	-0.1 (13)	-0.1 (23-II-4)	0.0 (23-II-2)	-49.45 (15)	-481.64 (15)	-6.94 (15)
61	7	-0.1 (13)	-0.1 (23-II-4)	0.1 (23-II-3)	-71.23 (15)	-370.32 (15)	33.27 (15)
61	8	-0.1 (13)	0.0 (23-II-4)	0.0 (23-II-4)	-90.57 (15)	-70.63 (15)	61.17 (15)
61	9	-0.0 (13)	-0.1 (16)	0.0 (23-II-2)	-63.02 (15)	-530.67 (15)	-8.33 (23-I-3)
61	10	-0.1 (13)	-0.1 (16)	0.0 (23-II-2)	-49.47 (15)	-481.60 (15)	-10.57 (23-I-3)
61	11	-0.1 (13)	-0.0 (16)	0.0 (23-II-2)	-71.16 (15)	-370.24 (15)	-42.60 (15)
61	12	-0.1 (13)	-0.0 (23-I-4)	0.0 (23-I-4)	-90.59 (15)	-70.68 (15)	-65.55 (15)
61	13	-0.0 (13)	-0.1 (16)	0.0 (16)	-68.89 (15)	-525.11 (15)	-7.42 (23-I-3)
61	14	-0.0 (13)	-0.1 (16)	0.0 (16)	-73.37 (15)	-502.38 (15)	-8.86 (23-I-3)
61	15	-0.1 (23-II-4)	-0.1 (16)	-0.0 (23-I-2)	-42.51 (15)	-541.92 (15)	-56.46 (15)
61	16	-0.1 (13)	0.3 (23-I-4)	-0.1 (13)	50.94 (23-I-3)	-769.80 (15)	-370.36 (15)
62	1	-0.0 (13)	-0.1 (23-I-3)	0.0 (13)	-68.67 (15)	-524.09 (15)	-6.68 (15)
62	2	-0.0 (13)	-0.1 (23-I-3)	0.0 (16)	-73.00 (15)	-501.72 (15)	-6.37 (15)
62	3	-0.1 (13)	-0.2 (23-I-3)	0.0 (16)	-42.07 (15)	-541.61 (15)	49.16 (15)
62	4	-0.1 (13)	-0.5 (23-I-3)	0.1 (23-I-3)	-13.51 (15)	-769.67 (15)	369.78 (15)
62	5	-0.0 (13)	-0.1 (23-I-3)	0.0 (23-II-4)	-62.77 (15)	-529.50 (15)	-6.39 (15)
62	6	-0.1 (13)	-0.1 (23-I-3)	0.0 (23-II-4)	-49.04 (15)	-480.84 (15)	-4.68 (15)
62	7	-0.1 (13)	-0.1 (23-I-3)	0.1 (23-I-2)	-70.66 (15)	-369.87 (15)	35.56 (15)
62	8	-0.1 (13)	0.0 (23-I-3)	0.0 (23-II-2)	-89.90 (15)	-70.53 (15)	63.05 (15)
62	9	-0.0 (13)	-0.1 (16)	-0.0 (18)	-62.77 (15)	-529.46 (15)	-7.19 (23-I-4)
62	10	-0.1 (13)	-0.1 (16)	-0.0 (18)	-49.04 (15)	-480.75 (15)	-9.48 (23-I-4)
62	11	-0.1 (13)	-0.0 (16)	0.0 (23-II-4)	-70.56 (15)	-369.78 (15)	-40.08 (15)
62	12	-0.1 (13)	-0.0 (23-I-2)	0.0 (23-II-3)	-89.87 (15)	-70.56 (15)	-63.48 (15)
62	13	-0.0 (23-I-3)	-0.1 (16)	-0.0 (18)	-68.60 (15)	-523.77 (15)	-6.06 (23-I-4)
62	14	-0.0 (13)	-0.1 (16)	-0.0 (23-I-4)	-72.90 (15)	-501.48 (15)	-7.46 (23-I-4)
62	15	-0.1 (23-I-3)	-0.1 (16)	-0.1 (23-I-4)	-41.87 (15)	-541.45 (15)	-53.69 (15)
62	16	-0.1 (13)	0.3 (23-II-3)	-0.1 (16)	52.37 (23-II-3)	-769.68 (15)	-368.34 (15)
63	1	-0.1 (23-II-1)	-0.0 (13)	0.0 (16)	334.51 (15)	43.02 (15)	6.90 (15)
63	2	-0.1 (23-II-1)	-0.0 (13)	0.0 (23-II-4)	336.11 (15)	40.75 (15)	6.86 (15)
63	3	-0.1 (16)	-0.0 (13)	0.0 (23-II-4)	336.02 (15)	40.73 (15)	11.46 (23-I-4)
63	4	-0.1 (16)	-0.0 (23-II-1)	-0.0 (15)	334.25 (15)	42.97 (15)	12.20 (23-I-4)
63	5	-0.1 (23-II-1)	-0.0 (13)	0.0 (16)	-313.95 (23-II-2)	-55.77 (23-I-2)	5.98 (15)
63	6	-0.1 (23-II-1)	-0.0 (13)	0.0 (23-II-4)	-299.21 (23-II-2)	31.55 (15)	5.24 (15)
63	7	-0.1 (16)	-0.0 (13)	0.0 (23-II-4)	-300.25 (23-II-2)	31.51 (15)	12.04 (23-II-1)
63	8	-0.1 (16)	-0.0 (13)	-0.0 (23-I-4)	-315.10 (23-II-2)	-53.05 (23-II-1)	15.45 (23-I-4)
63	9	-0.2 (23-II-1)	0.1 (23-I-1)	0.0 (16)	-415.18 (23-I-2)	-49.29 (23-II-1)	45.40 (23-II-4)
63	10	-0.1 (23-II-1)	-0.1 (13)	0.1 (23-II-1)	-264.77 (23-II-2)	-44.02 (23-I-2)	30.23 (23-I-4)
63	11	-0.0 (16)	-0.1 (13)	0.0 (23-I-1)	-265.63 (23-II-2)	41.34 (15)	25.82 (15)
63	12	-0.1 (16)	-0.1 (23-II-1)	-0.1 (23-II-1)	-415.86 (23-II-2)	-40.93 (23-II-1)	32.97 (15)
63	13	-0.5 (23-II-1)	-0.1 (13)	0.1 (23-II-1)	-703.41 (23-II-1)	-66.37 (23-II-1)	349.09 (23-II-1)
63	14	0.0 (23-II-1)	-0.0 (13)	0.0 (23-II-1)	-48.07 (23-II-2)	-58.13 (23-I-2)	52.05 (23-I-4)
63	15	-0.0 (23-I-1)	-0.0 (13)	0.0 (23-II-1)	-47.14 (23-II-2)	51.46 (15)	-43.17 (23-II-1)
63	16	0.3 (23-I-1)	-0.1 (13)	-0.1 (16)	-697.42 (23-II-1)	-16.56 (23-I-1)	-312.30 (23-II-1)
64	1	-0.0 (13)	-0.1 (23-II-1)	0.0 (16)	-51.98 (15)	-419.92 (15)	-42.60 (23-I-3)
64	2	-0.0 (13)	-0.1 (23-II-1)	0.0 (16)	54.08 (23-I-2)	426.00 (23-II-3)	-57.21 (23-I-3)
64	3	0.1 (23-II-2)	-0.2 (23-II-1)	0.0 (16)	24.28 (23-I-3)	631.77 (23-II-3)	-174.59 (23-II-3)
64	4	-0.1 (13)	-0.5 (23-II-1)	0.1 (23-II-1)	141.23 (23-I-3)	1032.94 (23-II-3)	-548.51 (23-II-3)
64	5	-0.0 (13)	-0.1 (23-II-1)	0.0 (23-II-4)	-51.11 (15)	-412.58 (15)	-42.58 (23-II-3)
64	6	-0.0 (13)	-0.1 (23-II-1)	0.0 (23-I-2)	-49.99 (15)	362.45 (23-II-3)	-55.05 (23-II-3)
64	7	-0.1 (13)	-0.1 (23-II-1)	0.1 (23-I-2)	93.95 (23-I-2)	289.01 (23-II-3)	-115.36 (23-II-3)
64	8	-0.1 (13)	0.0 (23-II-1)	0.0 (23-I-2)	-25.54 (15)	-29.45 (15)	-38.78 (23-II-3)
64	9	-0.0 (13)	-0.1 (16)	0.0 (23-II-4)	-50.99 (15)	-411.87 (15)	-44.71 (23-II-3)
64	10	-0.0 (13)	-0.1 (16)	0.0 (23-II-4)	-49.87 (15)	362.97 (23-II-3)	-41.54 (15)
64	11	-0.1 (13)	-0.0 (16)	0.0 (23-II-4)	94.42 (23-I-2)	289.29 (23-II-3)	-82.33 (15)
64	12	-0.1 (13)	-0.0 (23-I-1)	0.0 (23-II-4)	-25.20 (15)	-29.36 (15)	-36.94 (15)
64	13	-0.0 (23-II-1)	-0.1 (16)	-0.0 (15)	-51.64 (15)	-418.19 (15)	-44.05 (23-II-3)
64	14	-0.0 (13)	-0.1 (16)	-0.0 (23-I-4)	54.82 (23-I-2)	427.28 (23-II-3)	-41.21 (15)
64	15	-0.1 (23-II-1)	-0.1 (16)	-0.1 (23-I-4)	25.44 (23-I-4)	632.37 (23-II-3)	-117.06 (15)
64	16	-0.1 (13)	0.3 (23-I-1)	-0.1 (16)	142.45 (23-I-4)	1033.05 (23-II-3)	505.43 (23-II-3)
65	1	-0.1 (23-I-2)	-0.0 (13)	0.0 (16)	334.51 (15)	43.02 (15)	7.36 (15)
65	2	-0.1 (23-I-2)	-0.0 (13)	0.0 (23-I-1)	336.17 (15)	40.76 (15)	7.32 (15)



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
65	3	-0.1 (16)	-0.0 (13)	0.0 (23-I-1)	336.17 (15)	40.76 (15)	11.64 (23-I-4)
65	4	-0.1 (16)	-0.0 (13)	0.0 (16)	334.54 (15)	43.03 (15)	12.42 (23-I-3)
65	5	-0.1 (23-I-2)	-0.0 (13)	0.0 (16)	-313.87 (23-II-2)	-55.76 (23-II-4)	6.47 (15)
65	6	-0.1 (23-I-2)	-0.0 (13)	0.0 (23-II-4)	-299.13 (23-II-2)	31.57 (15)	5.74 (15)
65	7	-0.1 (16)	-0.0 (13)	0.0 (23-I-1)	-300.16 (23-I-2)	31.57 (15)	12.27 (23-II-2)
65	8	-0.1 (16)	-0.0 (13)	-0.0 (23-II-1)	-314.95 (23-I-2)	-52.88 (23-II-2)	15.76 (23-II-1)
65	9	-0.2 (23-I-2)	0.1 (23-II-4)	0.0 (16)	-415.07 (23-II-2)	-49.27 (23-II-1)	45.59 (23-II-2)
65	10	-0.1 (23-I-2)	-0.1 (13)	0.1 (23-II-4)	-264.69 (23-I-2)	-43.96 (23-II-4)	30.44 (23-I-4)
65	11	-0.0 (16)	-0.1 (13)	0.0 (23-I-1)	-265.54 (23-I-2)	41.43 (15)	26.39 (15)
65	12	-0.1 (16)	-0.1 (23-I-2)	-0.0 (23-II-1)	-415.74 (23-I-2)	-40.48 (23-I-4)	33.60 (15)
65	13	-0.5 (23-I-2)	-0.1 (13)	0.1 (23-II-1)	-702.65 (23-I-2)	-66.60 (23-II-1)	348.98 (23-II-2)
65	14	0.0 (23-II-2)	-0.1 (13)	0.0 (23-II-1)	-48.05 (23-I-2)	-58.04 (23-II-4)	52.22 (23-I-4)
65	15	-0.0 (23-I-1)	-0.1 (13)	0.0 (23-I-3)	-47.11 (23-I-2)	51.58 (15)	-42.82 (23-I-2)
65	16	0.3 (23-II-2)	-0.1 (13)	-0.1 (16)	-696.82 (23-I-2)	-15.92 (23-I-4)	-311.65 (23-I-2)
66	1	-0.0 (13)	-0.1 (23-I-2)	0.0 (16)	-68.78 (15)	-524.59 (15)	-7.51 (15)
66	2	-0.0 (13)	-0.1 (23-I-2)	0.0 (16)	-73.17 (15)	-502.05 (15)	-7.22 (15)
66	3	-0.1 (13)	-0.2 (23-I-2)	0.0 (16)	-42.31 (15)	-541.78 (15)	48.29 (15)
66	4	-0.1 (13)	-0.5 (23-I-2)	0.1 (23-I-3)	-13.78 (15)	-769.71 (15)	369.15 (15)
66	5	-0.0 (13)	-0.1 (23-I-2)	0.0 (23-II-4)	-62.89 (15)	-530.04 (15)	-7.34 (15)
66	6	-0.1 (13)	-0.1 (23-I-2)	0.0 (23-II-4)	-49.22 (15)	-481.18 (15)	-5.63 (15)
66	7	-0.1 (13)	-0.1 (23-I-3)	0.1 (23-I-2)	-70.91 (15)	-370.05 (15)	34.61 (15)
66	8	-0.1 (13)	0.0 (23-I-2)	0.0 (23-I-2)	-90.19 (15)	-70.57 (15)	62.27 (15)
66	9	-0.0 (13)	-0.1 (16)	0.0 (23-II-4)	-62.88 (15)	-529.97 (15)	-7.92 (23-II-3)
66	10	-0.1 (13)	-0.1 (16)	0.0 (23-II-4)	-49.22 (15)	-481.09 (15)	-10.22 (23-II-3)
66	11	-0.1 (13)	-0.0 (16)	0.0 (23-II-3)	-70.80 (15)	-369.95 (15)	-41.12 (15)
66	12	-0.1 (13)	-0.0 (23-II-3)	0.0 (23-II-3)	-90.15 (15)	-70.60 (15)	-64.33 (15)
66	13	-0.0 (13)	-0.1 (16)	-0.0 (18)	-68.71 (15)	-524.29 (15)	-6.88 (23-II-3)
66	14	-0.0 (13)	-0.1 (16)	-0.0 (23-I-4)	-73.08 (15)	-501.80 (15)	-8.29 (23-II-3)
66	15	-0.1 (23-I-2)	-0.1 (16)	-0.1 (23-I-3)	-42.10 (15)	-541.60 (15)	-54.81 (15)
66	16	-0.1 (13)	0.3 (23-II-3)	-0.1 (16)	51.19 (23-II-2)	-769.72 (15)	-369.15 (15)
67	1	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-101.62 (13)	-128.95 (23-I-2)	-132.91 (23-I-3)
67	2	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-93.91 (13)	-32.85 (23-II-2)	-147.09 (23-I-4)
67	3	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-86.53 (13)	9.62 (15)	-130.55 (23-I-4)
67	4	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-84.05 (13)	4.46 (23-I-3)	-71.82 (23-I-3)
67	5	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-101.27 (13)	-159.62 (23-I-2)	-110.52 (23-I-3)
67	6	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-89.92 (13)	-23.29 (23-II-2)	-113.29 (23-I-4)
67	7	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-84.63 (13)	15.90 (15)	-115.53 (23-I-3)
67	8	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-3)	-82.82 (13)	17.84 (23-II-1)	-55.07 (23-I-4)
67	9	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-4)	-98.99 (13)	-160.54 (23-I-2)	-104.56 (23-I-3)
67	10	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-87.03 (13)	21.98 (15)	-101.08 (23-I-3)
67	11	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-83.15 (13)	18.59 (22)	-106.93 (23-I-3)
67	12	0.0 (13)	0.0 (23-II-2)	0.0 (23-II-3)	-82.14 (13)	21.80 (23-II-1)	-51.59 (23-I-4)
67	13	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-4)	-94.44 (13)	-129.08 (23-I-2)	-84.46 (23-II-3)
67	14	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-4)	-84.59 (13)	-28.40 (23-II-2)	-75.80 (15)
67	15	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-4)	-82.24 (13)	17.78 (15)	-79.87 (15)
67	16	0.0 (13)	0.0 (23-II-2)	0.0 (23-II-3)	-82.23 (13)	15.16 (23-II-1)	-53.70 (23-II-3)
68	1	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-106.23 (13)	-128.01 (23-I-4)	-134.44 (23-I-3)
68	2	0.0 (13)	0.0 (23-I-4)	0.0 (15)	-98.57 (13)	-34.75 (23-II-2)	-149.03 (23-I-3)
68	3	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-93.14 (13)	8.56 (13)	-134.66 (23-I-3)
68	4	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-90.21 (13)	-3.49 (15)	-74.56 (23-I-3)
68	5	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-105.73 (13)	-157.70 (23-II-2)	-113.46 (23-I-3)
68	6	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-94.17 (13)	-25.01 (23-II-2)	-115.73 (23-I-3)
68	7	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-89.20 (13)	14.29 (15)	-120.38 (23-I-3)
68	8	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-87.21 (13)	17.21 (23-I-2)	-56.23 (23-I-3)
68	9	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-103.50 (13)	-158.32 (23-I-2)	-107.53 (23-I-3)
68	10	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-90.97 (13)	-22.53 (23-II-2)	-103.84 (23-I-3)
68	11	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-86.18 (13)	17.44 (22)	-112.10 (23-I-3)
68	12	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-85.18 (13)	21.84 (23-I-2)	-52.95 (23-I-3)
68	13	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-99.19 (13)	-127.55 (23-I-2)	-86.91 (23-I-3)
68	14	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-88.74 (13)	-29.09 (23-II-2)	-81.69 (15)
68	15	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-83.89 (13)	17.63 (15)	-86.95 (15)
68	16	0.0 (13)	0.0 (23-II-4)	0.0 (23-I-3)	-83.95 (13)	15.71 (23-II-4)	-57.00 (23-I-3)
69	1	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-131.41 (13)	-244.25 (23-II-2)	-144.55 (23-I-3)
69	2	0.0 (13)	-0.0 (15)	0.0 (15)	-111.16 (13)	116.92 (15)	-183.03 (23-I-3)
69	3	0.0 (13)	-0.0 (15)	0.0 (15)	-100.38 (13)	137.70 (15)	-151.11 (23-I-3)
69	4	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-104.33 (13)	66.39 (14)	-118.57 (23-I-3)
69	5	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-138.59 (13)	-324.27 (23-I-2)	-100.75 (23-I-3)
69	6	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-102.64 (13)	140.97 (15)	-109.84 (23-I-3)
69	7	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-94.91 (13)	168.10 (15)	-111.39 (23-I-3)
69	8	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-101.49 (13)	73.47 (14)	-107.35 (23-I-3)



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
69	9	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-135.93 (13)	-326.53 (23-I-2)	-87.60 (23-I-3)
69	10	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-98.85 (13)	138.59 (15)	-89.89 (23-I-3)
69	11	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-91.26 (13)	166.47 (15)	-95.81 (23-I-3)
69	12	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-99.00 (13)	72.52 (14)	-101.11 (23-I-3)
69	13	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-122.91 (13)	-251.92 (23-I-2)	-47.38 (23-I-3)
69	14	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-99.29 (13)	109.69 (15)	60.05 (13)
69	15	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-89.26 (13)	132.47 (15)	-79.66 (15)
69	16	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-97.13 (13)	62.93 (14)	-94.76 (15)
70	1	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-3)	-101.95 (13)	55.15 (14)	-89.41 (23-I-3)
70	2	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-120.40 (13)	-146.13 (15)	-89.22 (23-I-3)
70	3	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-91.55 (13)	109.49 (15)	-109.88 (23-I-3)
70	4	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-124.44 (13)	-202.22 (15)	-104.99 (23-I-3)
70	5	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-89.59 (13)	108.43 (15)	-110.20 (23-I-3)
70	6	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-122.63 (13)	-202.73 (15)	-108.91 (23-I-3)
70	7	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-3)	-95.79 (13)	52.80 (13)	-127.05 (23-I-3)
70	8	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-114.18 (13)	-147.80 (15)	-123.75 (23-I-3)
71	1	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-130.42 (13)	148.79 (15)	-92.17 (23-I-3)
71	2	0.0 (13)	-0.1 (15)	0.0 (23-I-3)	-108.39 (13)	304.96 (15)	-92.84 (23-I-3)
71	3	0.0 (13)	-0.0 (15)	0.0 (15)	-111.14 (13)	225.03 (15)	86.82 (13)
71	4	0.0 (13)	0.0 (22)	0.0 (23-I-3)	-138.40 (13)	-132.47 (22)	65.69 (13)
71	5	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-131.33 (13)	125.76 (15)	-63.32 (23-I-3)
71	6	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-98.33 (13)	362.07 (15)	-84.44 (23-I-3)
71	7	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-100.58 (13)	270.46 (15)	-73.10 (23-I-3)
71	8	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-149.51 (13)	-204.42 (22)	-81.48 (23-I-3)
71	9	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-127.54 (13)	124.78 (15)	-57.35 (23-I-3)
71	10	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-92.94 (13)	360.52 (15)	-80.55 (23-I-3)
71	11	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-95.98 (13)	268.58 (15)	-91.09 (23-I-3)
71	12	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-146.51 (13)	-207.27 (22)	-96.29 (23-I-3)
71	13	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-118.21 (13)	145.35 (15)	-34.53 (23-I-3)
71	14	0.0 (13)	-0.1 (15)	0.0 (23-I-3)	-91.78 (13)	299.72 (15)	-73.12 (15)
71	15	0.0 (13)	-0.0 (15)	-0.0 (13)	-97.33 (13)	219.38 (15)	-161.70 (15)
71	16	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-128.97 (13)	-140.40 (22)	-140.70 (23-I-3)
72	1	-0.0 (13)	-0.1 (23-I-2)	0.0 (16)	-52.23 (15)	-420.99 (15)	-44.36 (23-I-3)
72	2	-0.0 (13)	-0.1 (23-I-2)	0.0 (16)	53.54 (23-I-4)	424.82 (23-II-2)	-59.04 (23-I-3)
72	3	0.1 (23-II-2)	-0.2 (23-I-2)	0.0 (16)	23.42 (23-I-3)	631.09 (23-II-2)	-176.32 (23-I-3)
72	4	-0.1 (13)	-0.5 (23-I-2)	0.1 (23-I-2)	140.24 (23-I-3)	1032.72 (23-II-2)	-549.48 (23-I-4)
72	5	-0.0 (13)	-0.1 (23-I-2)	0.0 (23-II-4)	-51.40 (15)	-413.84 (15)	-44.60 (23-I-3)
72	6	-0.0 (13)	-0.1 (23-I-2)	0.0 (23-II-4)	-50.49 (15)	-361.62 (15)	-57.17 (23-I-3)
72	7	-0.1 (13)	-0.1 (23-I-2)	0.1 (23-I-2)	93.05 (23-II-2)	288.32 (23-II-3)	-117.41 (23-I-4)
72	8	-0.1 (13)	0.0 (23-I-2)	0.0 (23-I-2)	-26.31 (15)	-29.56 (15)	-40.04 (23-I-4)
72	9	-0.0 (13)	-0.1 (16)	0.0 (23-II-4)	-51.35 (15)	-413.51 (15)	-47.09 (23-I-3)
72	10	-0.0 (13)	-0.1 (16)	0.0 (23-II-4)	-50.48 (15)	361.67 (23-II-3)	-45.58 (15)
72	11	-0.1 (13)	-0.0 (16)	0.0 (23-II-4)	93.31 (23-II-2)	288.63 (23-II-3)	-86.17 (15)
72	12	-0.1 (13)	-0.0 (23-II-2)	0.0 (23-II-1)	-26.11 (15)	-29.47 (15)	-39.27 (15)
72	13	-0.0 (13)	-0.1 (16)	-0.0 (15)	-52.07 (15)	-420.15 (15)	-46.97 (23-I-3)
72	14	-0.0 (13)	-0.1 (16)	-0.0 (23-I-4)	53.82 (23-II-2)	425.86 (23-II-3)	-45.65 (15)
72	15	-0.1 (23-I-2)	-0.1 (16)	-0.1 (23-I-4)	24.10 (23-I-3)	631.72 (23-II-3)	-121.27 (15)
72	16	-0.1 (13)	0.3 (23-II-2)	-0.1 (16)	141.04 (23-I-3)	1032.99 (23-II-3)	503.96 (23-II-3)
73	1	-0.0 (13)	-0.1 (23-I-2)	0.0 (16)	-68.84 (15)	-524.91 (15)	-8.04 (15)
73	2	-0.0 (13)	-0.1 (23-I-2)	0.0 (16)	-73.28 (15)	-502.26 (15)	-7.78 (15)
73	3	-0.1 (13)	-0.2 (23-I-2)	0.0 (16)	-42.45 (15)	-541.90 (15)	47.72 (15)
73	4	-0.1 (13)	-0.5 (23-I-2)	0.1 (23-I-2)	-13.95 (15)	-769.74 (15)	368.73 (15)
73	5	-0.0 (13)	-0.1 (23-I-2)	0.0 (23-II-4)	-62.96 (15)	-530.39 (15)	-7.94 (15)
73	6	-0.1 (13)	-0.1 (23-I-2)	0.0 (23-II-4)	-49.34 (15)	-481.42 (15)	-6.25 (15)
73	7	-0.1 (13)	-0.1 (23-I-2)	0.1 (23-II-4)	-71.08 (15)	-370.19 (15)	33.98 (15)
73	8	-0.1 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-90.38 (15)	-70.60 (15)	61.75 (15)
73	9	-0.0 (13)	-0.1 (16)	0.0 (23-II-4)	-62.95 (15)	-530.34 (15)	-8.29 (23-I-3)
73	10	-0.1 (13)	-0.1 (16)	0.0 (23-II-3)	-49.35 (15)	-481.35 (15)	-10.60 (23-I-3)
73	11	-0.1 (13)	-0.0 (16)	0.0 (23-II-3)	-70.98 (15)	-370.10 (15)	-41.82 (15)
73	12	-0.1 (13)	-0.0 (23-II-2)	0.0 (23-II-2)	-90.38 (15)	-70.64 (15)	-64.91 (15)
73	13	-0.0 (13)	-0.1 (16)	0.0 (16)	-68.80 (15)	-524.71 (15)	-7.31 (23-I-3)
73	14	-0.0 (13)	-0.1 (16)	-0.0 (23-I-3)	-73.23 (15)	-502.10 (15)	-8.78 (23-I-3)
73	15	-0.1 (23-I-2)	-0.1 (16)	-0.1 (23-I-3)	-42.31 (15)	-541.76 (15)	-55.59 (15)
73	16	-0.1 (13)	0.3 (23-II-2)	-0.1 (16)	50.75 (23-I-3)	-769.76 (15)	-369.72 (15)
74	1	-0.1 (23-II-1)	-0.0 (13)	0.0 (16)	334.56 (15)	43.03 (15)	7.12 (15)
74	2	-0.1 (23-II-1)	-0.0 (13)	0.0 (23-II-4)	336.21 (15)	40.77 (15)	7.09 (15)
74	3	-0.1 (16)	-0.0 (13)	0.0 (23-II-4)	336.19 (15)	40.76 (15)	11.57 (23-I-3)
74	4	-0.1 (16)	-0.0 (13)	0.0 (16)	334.53 (15)	43.03 (15)	12.35 (23-I-3)
74	5	-0.1 (23-II-1)	-0.0 (13)	0.0 (16)	-313.94 (23-I-2)	-55.74 (23-II-2)	6.23 (15)
74	6	-0.1 (23-II-1)	-0.0 (13)	0.0 (23-II-4)	-299.18 (23-I-2)	31.59 (15)	5.50 (15)
74	7	-0.1 (16)	-0.0 (13)	0.0 (23-II-4)	-300.18 (23-II-2)	31.58 (15)	12.18 (23-II-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
74	8	-0.1 (16)	-0.0 (13)	-0.0 (23-I-4)	-314.95 (23-II-2)	-52.90 (23-I-2)	15.66 (23-II-1)
74	9	-0.2 (23-II-1)	0.1 (23-II-2)	0.0 (16)	-415.14 (23-I-2)	-49.24 (23-II-1)	45.45 (23-I-4)
74	10	-0.1 (23-II-1)	-0.1 (13)	0.1 (23-II-1)	-264.72 (23-I-2)	-43.95 (23-II-2)	30.32 (23-II-1)
74	11	-0.0 (16)	-0.1 (13)	0.0 (23-I-1)	-265.56 (23-I-2)	41.44 (15)	26.14 (15)
74	12	-0.1 (16)	-0.1 (23-II-1)	-0.1 (23-II-1)	-415.76 (23-I-2)	-40.56 (23-II-1)	33.35 (15)
74	13	-0.5 (23-II-1)	-0.1 (13)	0.1 (23-II-1)	-702.91 (23-II-1)	-66.51 (23-II-1)	349.06 (23-II-1)
74	14	0.0 (23-I-1)	-0.1 (13)	0.0 (23-II-1)	-48.06 (23-I-2)	-58.03 (23-II-2)	52.10 (23-II-4)
74	15	-0.0 (23-I-1)	-0.1 (13)	0.0 (23-II-1)	-47.12 (23-I-2)	51.58 (15)	-42.91 (23-II-1)
74	16	0.3 (23-I-1)	-0.1 (13)	-0.1 (16)	-697.33 (23-II-1)	-15.86 (23-I-1)	-311.90 (23-II-1)
75	1	-0.0 (13)	-0.1 (23-I-2)	0.0 (16)	-52.34 (15)	-421.50 (15)	-45.30 (23-I-3)
75	2	-0.0 (13)	-0.1 (23-I-2)	0.0 (16)	53.32 (23-II-2)	424.40 (23-II-2)	-60.06 (23-I-3)
75	3	-0.1 (13)	-0.2 (23-I-2)	0.0 (16)	23.09 (23-I-2)	630.86 (23-II-2)	-177.38 (23-I-3)
75	4	-0.1 (13)	-0.5 (23-I-2)	0.1 (23-I-2)	139.86 (23-I-2)	1032.67 (23-II-2)	-550.04 (23-I-4)
75	5	-0.0 (13)	-0.1 (23-I-2)	0.0 (23-II-4)	-51.54 (15)	-414.44 (15)	-45.68 (23-I-3)
75	6	-0.1 (13)	-0.1 (23-I-2)	0.0 (23-II-4)	-50.73 (15)	-362.05 (15)	-58.37 (23-I-3)
75	7	-0.1 (13)	-0.1 (23-I-2)	0.1 (23-II-4)	92.67 (23-II-2)	288.06 (23-II-2)	-118.62 (23-I-3)
75	8	-0.1 (13)	0.0 (23-I-2)	0.0 (23-I-2)	-26.69 (15)	-29.61 (15)	-40.77 (23-I-3)
75	9	-0.0 (13)	-0.1 (16)	0.0 (23-II-4)	-51.53 (15)	-414.29 (15)	-48.35 (23-I-3)
75	10	-0.1 (13)	-0.1 (16)	0.0 (23-II-4)	-50.78 (15)	-361.88 (15)	-48.62 (15)
75	11	-0.1 (13)	-0.0 (16)	0.0 (23-I-1)	92.83 (23-II-2)	288.23 (23-II-2)	-89.04 (15)
75	12	-0.1 (13)	-0.0 (23-II-2)	0.0 (23-II-2)	-26.56 (15)	-29.53 (15)	-41.01 (15)
75	13	-0.0 (13)	-0.1 (16)	0.0 (16)	-52.28 (15)	-421.09 (15)	-48.47 (23-I-3)
75	14	-0.0 (13)	-0.1 (16)	-0.0 (23-I-4)	53.37 (23-I-4)	424.87 (23-II-2)	-48.89 (15)
75	15	-0.1 (23-I-2)	-0.1 (16)	-0.0 (23-II-1)	23.45 (23-I-3)	631.15 (23-II-2)	-124.33 (15)
75	16	-0.1 (13)	0.3 (23-II-2)	-0.1 (16)	140.26 (23-I-3)	1032.80 (23-II-2)	503.34 (23-II-3)
76	1	0.0 (13)	0.0 (23-I-3)	0.0 (23-I-3)	-138.94 (13)	3.97 (23-I-3)	-1.73 (13)
76	2	0.0 (13)	0.0 (23-I-3)	0.0 (23-I-3)	-139.17 (13)	-5.75 (13)	-39.73 (23-I-3)
76	3	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-132.23 (13)	3.50 (23-I-2)	12.57 (23-I-3)
76	4	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-134.93 (13)	-7.01 (15)	-51.26 (23-I-3)
76	5	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-130.64 (13)	3.42 (15)	13.38 (23-I-3)
76	6	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-133.29 (13)	-6.55 (15)	-57.00 (23-I-3)
76	7	0.0 (13)	0.0 (13)	0.0 (23-I-3)	-127.17 (13)	2.09 (13)	3.37 (23-I-4)
76	8	0.0 (13)	0.0 (13)	0.0 (23-II-3)	-127.37 (13)	-7.51 (22)	-41.63 (23-I-3)
77	1	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-143.24 (13)	3.80 (23-I-3)	-1.53 (13)
77	2	0.0 (13)	0.0 (22)	0.0 (23-I-3)	-143.48 (13)	-5.60 (13)	-39.38 (23-I-3)
77	3	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-138.27 (13)	3.37 (23-I-2)	10.33 (23-I-3)
77	4	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-140.94 (13)	-6.44 (15)	-50.94 (23-I-3)
77	5	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-136.94 (13)	3.22 (15)	11.10 (16)
77	6	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-139.59 (13)	-6.17 (15)	-57.14 (23-I-3)
77	7	0.0 (13)	0.0 (13)	0.0 (23-I-3)	-135.55 (13)	1.90 (13)	1.99 (23-I-3)
77	8	0.0 (13)	0.0 (13)	0.0 (23-I-3)	-135.72 (13)	-7.12 (22)	-42.15 (23-I-3)
78	1	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-126.61 (13)	149.23 (15)	-88.64 (23-I-3)
78	2	0.0 (13)	-0.1 (15)	0.0 (23-I-3)	-105.08 (13)	303.67 (15)	-88.34 (23-I-3)
78	3	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-106.55 (13)	220.43 (15)	94.09 (13)
78	4	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-133.49 (13)	-141.92 (22)	72.85 (13)
78	5	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-125.89 (13)	126.09 (15)	-57.13 (23-I-3)
78	6	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-93.26 (13)	358.98 (15)	-79.88 (23-I-3)
78	7	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-95.21 (13)	263.23 (15)	-69.16 (23-I-3)
78	8	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-143.98 (13)	-216.35 (22)	-82.05 (23-I-3)
78	9	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-120.51 (13)	124.14 (15)	-50.49 (23-I-3)
78	10	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-85.85 (13)	354.98 (15)	-75.56 (23-I-3)
78	11	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-89.41 (13)	258.48 (15)	-87.07 (23-I-3)
78	12	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-140.26 (13)	-220.88 (22)	-96.89 (23-I-3)
78	13	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-109.11 (13)	142.72 (15)	37.12 (13)
78	14	0.0 (13)	-0.1 (15)	0.0 (23-I-3)	-82.20 (13)	291.12 (15)	-64.52 (15)
78	15	0.0 (13)	-0.0 (15)	-0.0 (13)	-89.27 (13)	206.18 (15)	-154.58 (15)
78	16	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-121.69 (13)	-155.06 (22)	-139.17 (23-I-3)
79	1	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-121.84 (13)	149.45 (15)	-80.31 (23-I-3)
79	2	0.0 (13)	-0.1 (15)	0.0 (23-II-3)	-101.54 (13)	298.15 (15)	-79.22 (23-I-3)
79	3	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-101.90 (13)	210.83 (15)	100.75 (13)
79	4	0.0 (13)	0.0 (23-I-3)	0.0 (23-I-3)	-128.04 (13)	-153.99 (22)	79.41 (13)
79	5	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-118.36 (13)	126.76 (15)	-44.94 (23-II-3)
79	6	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-86.51 (13)	349.08 (15)	-70.56 (23-I-3)
79	7	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-88.36 (13)	248.45 (15)	-63.64 (23-I-3)
79	8	0.0 (13)	-0.0 (13)	0.0 (23-I-3)	-136.84 (13)	-230.49 (22)	-83.19 (23-II-3)
79	9	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-110.27 (13)	123.49 (15)	-37.16 (23-II-3)
79	10	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-75.49 (13)	340.24 (15)	-65.58 (23-II-3)
79	11	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-79.77 (13)	238.58 (15)	-81.50 (23-II-3)
79	12	0.0 (13)	-0.0 (13)	0.0 (23-II-3)	-131.32 (13)	-236.52 (22)	-98.00 (23-II-3)
79	13	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-103.67 (22)	138.12 (15)	43.62 (13)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
79	14	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-100.18 (22)	271.83 (15)	-53.86 (23-II-4)
79	15	0.0 (13)	-0.0 (13)	-0.0 (13)	-97.36 (22)	192.40 (13)	-145.41 (15)
79	16	0.0 (13)	0.0 (23-I-3)	-0.0 (13)	-110.55 (13)	-172.73 (22)	-135.71 (23-II-3)
80	1	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-126.48 (13)	-256.23 (23-I-2)	-143.48 (23-I-3)
80	2	0.0 (13)	-0.0 (15)	0.0 (15)	-106.70 (13)	109.33 (15)	-185.21 (23-I-3)
80	3	0.0 (13)	-0.0 (15)	0.0 (15)	-95.87 (13)	132.61 (15)	-152.90 (23-I-3)
80	4	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-99.69 (13)	63.48 (14)	-120.16 (23-I-3)
80	5	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-133.14 (13)	-339.68 (23-I-2)	-96.25 (23-I-3)
80	6	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-97.63 (13)	130.89 (15)	-110.20 (23-I-3)
80	7	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-90.03 (13)	161.49 (15)	-111.97 (23-I-3)
80	8	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-96.69 (13)	71.51 (14)	-110.41 (23-I-3)
80	9	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-129.88 (13)	-343.74 (23-I-2)	-82.40 (23-I-3)
80	10	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-93.04 (13)	126.26 (15)	-89.53 (23-I-3)
80	11	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-85.70 (13)	157.90 (15)	-95.63 (23-I-3)
80	12	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-93.80 (13)	69.65 (14)	-104.06 (23-I-3)
80	13	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-115.97 (13)	-269.19 (23-II-1)	48.04 (13)
80	14	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-92.19 (13)	95.11 (15)	66.81 (13)
80	15	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-82.71 (13)	122.63 (13)	-73.61 (15)
80	16	0.0 (13)	-0.0 (13)	0.0 (23-I-3)	-91.30 (13)	58.76 (13)	-91.53 (15)
81	1	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-3)	-97.24 (13)	-128.95 (23-I-2)	-132.16 (23-I-4)
81	2	0.0 (13)	0.0 (23-II-2)	0.0 (23-II-3)	-90.35 (13)	-29.11 (23-II-2)	-145.34 (23-I-4)
81	3	0.0 (13)	-0.0 (15)	0.0 (23-I-3)	-81.31 (13)	12.75 (15)	-125.54 (23-I-4)
81	4	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-78.69 (13)	5.94 (23-II-1)	-68.19 (23-I-4)
81	5	0.0 (13)	0.0 (23-II-2)	0.0 (23-I-4)	-96.09 (13)	-160.90 (23-II-1)	-107.64 (23-I-4)
81	6	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-4)	-85.47 (13)	24.66 (15)	-110.04 (23-I-4)
81	7	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-3)	-80.08 (13)	19.27 (15)	-108.96 (23-I-4)
81	8	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-3)	-78.26 (13)	18.91 (23-II-1)	-52.67 (23-I-4)
81	9	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-4)	-92.80 (13)	-161.63 (23-II-1)	-101.01 (23-II-3)
81	10	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-4)	-81.43 (13)	25.69 (15)	-96.58 (23-II-4)
81	11	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-4)	-78.61 (13)	22.31 (23-I-2)	-99.35 (23-II-4)
81	12	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-4)	-77.88 (13)	22.30 (23-II-1)	-48.63 (23-II-4)
81	13	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-4)	-86.85 (13)	-127.97 (23-I-2)	-79.88 (23-II-3)
81	14	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-4)	-77.12 (13)	-24.35 (23-I-2)	-66.53 (15)
81	15	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-77.31 (13)	20.05 (15)	-69.72 (15)
81	16	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-78.04 (13)	15.22 (23-II-1)	-48.42 (23-II-3)
82	1	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-97.33 (13)	52.31 (13)	-87.56 (23-I-3)
82	2	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-115.87 (13)	-147.84 (15)	-89.78 (23-I-3)
82	3	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-86.86 (13)	103.75 (15)	-106.98 (23-I-3)
82	4	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-119.87 (13)	-203.44 (15)	-107.13 (23-I-3)
82	5	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-84.64 (13)	102.83 (13)	-107.48 (23-I-3)
82	6	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-117.87 (13)	-203.69 (15)	-111.39 (23-I-4)
82	7	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-90.30 (13)	52.05 (13)	-124.91 (23-I-3)
82	8	0.0 (13)	0.0 (15)	0.0 (23-I-3)	-108.93 (13)	-149.95 (15)	-124.24 (23-I-3)
83	1	0.0 (13)	0.0 (23-I-3)	0.0 (23-II-3)	-133.02 (13)	4.13 (23-I-3)	2.84 (23-I-4)
83	2	0.0 (13)	0.0 (23-I-3)	0.0 (23-II-3)	-133.27 (13)	-6.19 (23-I-3)	-38.60 (23-II-3)
83	3	0.0 (13)	0.0 (15)	0.0 (23-II-3)	-123.88 (13)	3.66 (23-I-3)	15.36 (23-I-4)
83	4	0.0 (13)	0.0 (15)	0.0 (23-II-3)	-126.62 (13)	-7.96 (15)	-49.39 (23-II-3)
83	5	0.0 (13)	0.0 (15)	0.0 (23-II-3)	-121.47 (13)	3.72 (15)	16.22 (23-I-4)
83	6	0.0 (13)	0.0 (15)	0.0 (23-II-3)	-124.12 (13)	-7.17 (15)	-54.09 (23-II-3)
83	7	0.0 (13)	0.0 (23-I-4)	0.0 (23-I-4)	-115.01 (13)	2.32 (13)	5.25 (23-I-4)
83	8	0.0 (13)	0.0 (13)	0.0 (23-II-3)	-115.24 (13)	-8.04 (23-II-3)	-38.82 (23-I-4)
84	1	0.0 (13)	0.0 (23-II-1)	0.0 (23-II-3)	-121.16 (13)	-271.98 (23-II-1)	-140.86 (23-I-3)
84	2	0.0 (13)	0.0 (23-I-2)	0.0 (15)	-102.70 (13)	97.70 (15)	-187.52 (23-I-3)
84	3	0.0 (13)	-0.0 (13)	0.0 (15)	-91.79 (13)	124.28 (15)	-156.12 (23-I-3)
84	4	0.0 (13)	-0.0 (13)	0.0 (23-II-3)	-94.81 (13)	59.97 (14)	-123.72 (23-I-3)
84	5	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-3)	-126.23 (13)	-359.88 (23-II-1)	-88.20 (23-I-3)
84	6	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-3)	-91.66 (13)	115.13 (15)	-109.02 (23-II-3)
84	7	0.0 (13)	-0.0 (13)	0.0 (23-II-3)	-84.24 (13)	153.39 (13)	-112.54 (23-II-3)
84	8	0.0 (13)	-0.0 (13)	0.0 (23-II-3)	-90.85 (13)	69.95 (14)	-115.70 (23-I-4)
84	9	0.0 (13)	0.0 (23-I-3)	0.0 (23-II-3)	-121.32 (13)	-365.79 (23-II-1)	-72.83 (23-II-3)
84	10	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-3)	-84.70 (13)	108.97 (13)	-86.39 (23-II-3)
84	11	0.0 (13)	-0.0 (13)	0.0 (23-II-3)	-77.71 (13)	153.44 (13)	-94.42 (23-II-3)
84	12	0.0 (13)	-0.0 (13)	0.0 (23-II-3)	-86.52 (13)	66.49 (14)	-108.89 (23-I-4)
84	13	0.0 (13)	0.0 (23-II-1)	0.0 (23-II-3)	-105.29 (13)	-290.93 (23-I-4)	54.04 (13)
84	14	0.0 (13)	0.0 (23-I-3)	0.0 (23-II-3)	-89.18 (22)	86.16 (13)	72.76 (13)
84	15	0.0 (13)	-0.0 (13)	0.0 (23-II-3)	-72.07 (13)	121.33 (13)	-64.30 (15)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
84	16	0.0 (13)	-0.0 (13)	0.0 (23-II-3)	-82.35 (13)	57.28 (13)	-88.75 (23-II-3)
85	1	0.0 (13)	0.0 (23-I-2)	0.0 (23-I-3)	-92.42 (13)	51.40 (13)	-86.88 (23-I-3)
85	2	0.0 (13)	0.0 (15)	0.0 (23-II-3)	-111.19 (13)	-147.92 (15)	-92.07 (23-I-3)
85	3	0.0 (13)	0.0 (15)	0.0 (23-I-4)	-81.18 (13)	102.02 (13)	-104.66 (23-II-3)
85	4	0.0 (13)	0.0 (15)	0.0 (23-II-3)	-114.35 (13)	-201.12 (15)	-110.86 (23-I-4)
85	5	0.0 (13)	0.0 (15)	0.0 (23-I-4)	-77.87 (13)	101.86 (13)	-105.19 (23-II-3)
85	6	0.0 (13)	0.0 (15)	0.0 (23-II-3)	-111.39 (13)	-199.94 (15)	-115.24 (23-I-4)
85	7	0.0 (13)	0.0 (23-II-1)	0.0 (23-II-4)	-81.93 (13)	51.25 (13)	-121.38 (23-II-3)
85	8	0.0 (13)	0.0 (15)	0.0 (23-II-4)	-100.90 (13)	-148.37 (15)	-124.04 (23-II-4)
86	1	-0.0 (16)	-0.1 (13)	0.0 (16)	-68.58 (15)	-525.87 (15)	3.12 (23-II-4)
86	2	-0.0 (22)	-0.1 (23-II-3)	0.0 (16)	-72.06 (15)	-501.97 (15)	7.46 (23-II-4)
86	3	-0.0 (16)	-0.2 (23-II-3)	0.1 (16)	-40.21 (15)	-541.19 (15)	53.38 (15)
86	4	-0.1 (22)	-0.5 (23-II-3)	0.1 (23-II-3)	-11.07 (15)	-769.32 (15)	372.88 (15)
86	5	-0.0 (23-II-3)	-0.1 (23-II-3)	0.0 (16)	-62.15 (15)	-531.24 (15)	2.29 (23-I-4)
86	6	-0.0 (22)	-0.1 (23-II-3)	0.1 (23-II-3)	-46.05 (15)	-480.33 (15)	4.34 (23-I-4)
86	7	-0.1 (23-I-4)	-0.0 (23-II-3)	0.1 (23-II-3)	-65.93 (15)	-369.37 (15)	41.03 (15)
86	8	0.0 (13)	0.0 (23-I-4)	0.0 (23-II-3)	-84.27 (15)	-71.13 (15)	67.10 (15)
86	9	-0.0 (23-II-3)	-0.1 (23-II-3)	0.0 (16)	-58.94 (15)	-528.10 (15)	10.49 (15)
86	10	-0.1 (23-II-3)	-0.1 (23-II-3)	0.0 (23-II-3)	-41.50 (15)	-481.43 (15)	9.40 (15)
86	11	-0.1 (23-I-3)	-0.0 (16)	0.1 (23-II-3)	-59.64 (15)	-369.47 (15)	-32.32 (15)
86	12	0.1 (23-II-4)	0.0 (16)	0.1 (23-II-3)	-78.17 (15)	-65.08 (15)	-57.99 (15)
86	13	-0.0 (23-II-3)	-0.2 (23-II-3)	0.0 (23-II-3)	-40.64 (15)	-517.03 (15)	32.14 (15)
86	14	-0.0 (23-II-3)	-0.2 (23-II-3)	0.0 (16)	-21.02 (15)	-502.27 (15)	-12.98 (23-II-4)
86	15	-0.1 (23-II-3)	-0.2 (23-II-3)	-0.1 (23-II-4)	-53.85 (15)	-549.20 (15)	-79.33 (15)
86	16	-0.1 (23-I-4)	0.2 (23-I-3)	-0.0 (13)	24.14 (16)	-785.07 (15)	-327.91 (15)
87	1	0.0 (13)	0.0 (23-I-3)	0.0 (23-II-4)	-82.68 (13)	-118.75 (23-I-2)	-117.35 (23-II-4)
87	2	0.0 (13)	0.0 (23-II-3)	0.0 (23-II-3)	-81.27 (13)	31.48 (15)	-128.72 (23-II-4)
87	3	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-70.62 (13)	22.60 (15)	-101.88 (23-II-4)
87	4	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-65.22 (13)	9.93 (23-I-4)	-51.76 (23-II-4)
87	5	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-4)	-82.08 (22)	-154.86 (23-II-1)	-83.69 (23-II-4)
87	6	0.0 (13)	0.0 (23-I-3)	0.0 (23-II-4)	-69.09 (13)	40.46 (15)	-84.37 (23-II-4)
87	7	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-64.45 (13)	34.25 (23-I-4)	-77.68 (23-II-4)
87	8	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-61.71 (13)	22.36 (23-I-4)	-36.51 (23-II-4)
87	9	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-4)	-82.73 (22)	-155.24 (23-I-3)	-70.49 (23-II-4)
87	10	0.0 (13)	0.0 (23-I-3)	0.0 (23-II-4)	-57.37 (13)	42.09 (15)	-64.51 (23-II-4)
87	11	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-56.65 (13)	38.15 (23-I-4)	-63.32 (23-II-4)
87	12	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-57.16 (13)	24.89 (23-I-4)	-30.10 (23-II-4)
87	13	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-4)	-75.45 (22)	-116.22 (23-I-3)	-39.36 (23-II-3)
87	14	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-44.30 (13)	35.71 (15)	37.62 (13)
87	15	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-47.64 (13)	28.17 (15)	-31.32 (15)
87	16	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-51.98 (13)	17.08 (23-I-4)	-25.37 (23-II-3)
88	1	0.0 (13)	0.0 (23-II-3)	0.0 (23-II-3)	-123.28 (13)	4.24 (23-II-3)	5.11 (23-II-3)
88	2	0.0 (13)	0.0 (23-I-3)	0.0 (23-II-4)	-123.63 (13)	-7.01 (23-II-3)	-34.87 (23-II-4)
88	3	0.0 (13)	0.0 (15)	0.0 (23-II-4)	-110.70 (13)	3.71 (23-I-3)	18.92 (23-II-4)
88	4	0.0 (13)	0.0 (15)	-0.0 (13)	-113.49 (13)	-9.33 (15)	-43.88 (23-II-4)
88	5	0.0 (22)	0.0 (15)	0.0 (23-II-4)	-121.65 (22)	4.08 (15)	20.24 (23-II-4)
88	6	0.0 (22)	0.0 (15)	0.0 (23-II-4)	-124.28 (22)	-8.06 (15)	-46.80 (23-II-4)
88	7	0.0 (22)	0.0 (13)	0.0 (23-II-4)	-152.87 (22)	2.58 (13)	8.15 (23-II-3)
88	8	0.0 (22)	0.0 (13)	-0.0 (13)	-155.25 (22)	-8.09 (22)	-32.61 (23-II-4)
89	1	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-4)	-91.73 (13)	-126.08 (23-I-2)	-129.81 (23-II-4)
89	2	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-3)	-86.88 (13)	24.26 (15)	-141.03 (23-I-4)
89	3	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-76.59 (13)	17.47 (15)	-117.15 (23-II-4)
89	4	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-73.01 (13)	7.82 (23-II-1)	-62.14 (23-II-4)
89	5	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-4)	-88.36 (13)	-159.32 (23-II-1)	-101.83 (23-II-4)
89	6	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-4)	-79.23 (13)	31.90 (15)	-102.13 (23-II-4)
89	7	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-4)	-74.01 (13)	25.43 (23-I-3)	-97.55 (23-II-4)
89	8	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-4)	-71.96 (13)	20.54 (23-II-1)	-47.18 (23-II-4)
89	9	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-4)	-82.74 (13)	-158.81 (23-II-1)	-92.60 (23-II-4)
89	10	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-4)	-72.08 (13)	33.62 (15)	-85.68 (23-II-4)
89	11	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-4)	-70.48 (13)	29.05 (23-I-3)	-85.96 (23-II-4)
89	12	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-4)	-70.41 (13)	23.54 (23-II-1)	-42.12 (23-II-4)
89	13	0.0 (13)	0.0 (23-I-2)	0.0 (23-II-4)	-74.02 (13)	-121.36 (23-I-2)	-66.61 (23-II-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
89	14	0.0 (13)	0.0 (23-I-3)	0.0 (23-II-4)	-63.89 (13)	28.08 (15)	-49.15 (15)
89	15	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-66.57 (13)	24.41 (15)	-53.69 (15)
89	16	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-68.98 (13)	16.04 (23-I-4)	-39.34 (23-II-3)
90	1	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-3)	-121.49 (22)	-298.57 (23-I-4)	-111.96 (23-II-4)
90	2	0.0 (22)	0.0 (23-I-3)	-0.0 (13)	-86.92 (13)	-108.12 (23-I-3)	-168.94 (23-II-4)
90	3	0.0 (22)	-0.0 (13)	0.0 (23-II-3)	-75.08 (13)	114.47 (13)	-156.69 (23-II-4)
90	4	0.0 (22)	-0.0 (13)	0.0 (23-II-4)	-75.41 (13)	52.16 (13)	-127.19 (23-II-4)
90	5	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-4)	-178.19 (22)	-383.31 (23-I-4)	-54.08 (23-II-4)
90	6	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-4)	-134.70 (22)	-120.40 (23-I-3)	-85.32 (23-II-4)
90	7	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-4)	-115.42 (22)	144.63 (13)	-96.29 (23-II-4)
90	8	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-4)	-98.88 (22)	65.98 (14)	-107.36 (23-II-4)
90	9	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-4)	-203.71 (22)	-388.30 (23-I-4)	-40.50 (23-II-4)
90	10	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-4)	-175.81 (22)	-134.42 (23-I-3)	-59.71 (23-II-4)
90	11	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-4)	-154.64 (22)	143.83 (13)	-67.87 (23-II-4)
90	12	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-4)	-121.26 (22)	61.24 (14)	-86.79 (23-II-4)
90	13	0.0 (22)	0.1 (23-I-4)	0.0 (23-II-4)	-219.52 (23-I-4)	-318.77 (23-I-4)	62.06 (13)
90	14	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-4)	-219.14 (23-II-4)	-146.81 (23-II-3)	80.63 (13)
90	15	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-4)	-181.63 (23-II-1)	113.26 (13)	44.05 (13)
90	16	0.0 (22)	-0.0 (13)	0.0 (23-II-4)	-132.05 (22)	49.47 (13)	-41.18 (23-II-4)
91	1	0.0 (13)	0.0 (23-I-4)	0.0 (23-II-3)	-113.76 (13)	-288.23 (23-I-4)	-131.06 (23-II-3)
91	2	0.0 (13)	0.0 (23-I-3)	-0.0 (13)	-97.61 (13)	83.64 (13)	-184.02 (23-I-4)
91	3	0.0 (13)	-0.0 (13)	0.0 (23-II-3)	-86.35 (13)	118.44 (13)	-159.47 (23-I-4)
91	4	0.0 (13)	-0.0 (13)	0.0 (23-II-3)	-87.82 (13)	55.45 (13)	-130.24 (23-II-4)
91	5	0.0 (13)	0.0 (23-I-3)	0.0 (23-II-3)	-115.70 (13)	-376.96 (23-I-4)	-69.19 (23-II-3)
91	6	0.0 (13)	0.0 (23-I-3)	0.0 (23-II-3)	-82.66 (13)	107.85 (13)	-99.42 (23-II-4)
91	7	0.0 (13)	0.0 (23-I-3)	0.0 (23-II-3)	-75.36 (13)	150.43 (13)	-111.26 (23-II-4)
91	8	0.0 (13)	-0.0 (13)	0.0 (23-II-3)	-81.81 (13)	69.32 (14)	-125.38 (23-II-4)
91	9	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-4)	-135.59 (22)	-381.17 (23-I-4)	-50.41 (23-II-3)
91	10	0.0 (13)	0.0 (23-I-3)	0.0 (23-II-4)	-98.54 (22)	108.51 (13)	-73.25 (23-II-4)
91	11	0.0 (13)	0.0 (23-I-3)	0.0 (23-II-4)	-81.84 (22)	150.38 (13)	-89.85 (23-II-4)
91	12	0.0 (13)	-0.0 (13)	0.0 (23-II-4)	-74.92 (13)	63.36 (14)	-117.61 (23-II-4)
91	13	0.0 (22)	0.0 (23-I-4)	0.0 (23-II-4)	-177.11 (22)	-308.23 (23-I-4)	58.82 (13)
91	14	0.0 (13)	0.0 (23-I-3)	0.0 (23-II-4)	-184.76 (22)	-113.49 (23-I-3)	77.50 (13)
91	15	0.0 (13)	-0.0 (13)	0.0 (23-II-4)	-159.89 (22)	119.05 (13)	-47.36 (15)
91	16	0.0 (13)	-0.0 (13)	0.0 (23-II-4)	-113.34 (22)	54.87 (13)	-81.67 (23-II-4)
92	1	0.0 (22)	-0.0 (15)	-0.0 (13)	-112.97 (22)	145.94 (15)	-40.75 (23-II-3)
92	2	0.0 (22)	-0.0 (13)	0.0 (23-II-4)	-80.13 (13)	241.40 (13)	-40.24 (23-II-3)
92	3	0.0 (22)	-0.0 (13)	0.0 (23-II-4)	-80.22 (13)	181.86 (13)	107.07 (13)
92	4	0.0 (22)	0.0 (23-I-4)	0.0 (23-I-4)	-115.40 (22)	-172.22 (22)	86.04 (13)
92	5	0.0 (22)	-0.0 (15)	0.0 (23-II-4)	-168.15 (22)	135.04 (15)	29.47 (13)
92	6	0.0 (22)	-0.0 (13)	0.0 (23-II-4)	-141.85 (22)	289.95 (13)	-41.74 (23-II-3)
92	7	0.0 (22)	-0.0 (13)	0.0 (23-II-4)	-143.18 (22)	222.56 (13)	-46.03 (23-II-3)
92	8	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-3)	-180.93 (22)	-237.59 (22)	-74.58 (23-II-3)
92	9	0.0 (22)	-0.0 (15)	0.0 (23-II-4)	-199.04 (22)	130.97 (15)	35.57 (13)
92	10	0.0 (22)	-0.0 (13)	0.0 (23-II-3)	-196.41 (22)	286.85 (13)	-43.49 (23-II-4)
92	11	0.0 (22)	-0.0 (13)	-0.0 (13)	-197.49 (22)	220.84 (13)	-57.82 (23-II-3)
92	12	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-3)	-212.41 (22)	-240.09 (22)	-79.69 (23-II-4)
92	13	0.0 (22)	-0.0 (15)	0.0 (23-II-3)	-227.88 (23-II-3)	128.72 (15)	58.82 (13)
92	14	0.0 (22)	-0.0 (13)	-0.0 (13)	-249.61 (23-II-4)	234.51 (13)	-48.53 (23-II-4)
92	15	0.0 (22)	-0.0 (13)	-0.0 (13)	-248.14 (23-II-4)	178.03 (13)	-108.22 (15)
92	16	0.0 (22)	0.0 (23-I-4)	-0.0 (13)	-222.43 (23-I-4)	-191.39 (23-II-4)	-99.12 (23-II-4)
93	1	0.0 (13)	0.0 (23-II-1)	0.0 (23-II-4)	-85.56 (13)	50.18 (13)	-87.56 (23-II-3)
93	2	0.0 (13)	0.0 (15)	0.0 (23-II-4)	-104.74 (13)	-141.51 (15)	-96.28 (23-II-4)
93	3	0.0 (13)	0.0 (15)	0.0 (23-II-4)	-72.48 (13)	100.54 (13)	-102.18 (23-II-3)
93	4	0.0 (13)	0.0 (15)	0.0 (23-II-4)	-105.81 (13)	-186.14 (15)	-114.71 (23-II-4)
93	5	0.0 (13)	0.0 (15)	0.0 (23-II-4)	-67.04 (13)	100.20 (13)	-101.57 (23-II-3)

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
93	6	0.0 (13)	0.0 (15)	0.0 (23-II-4)	-100.86 (13)	-179.49 (15)	-117.29 (23-II-4)
93	7	0.0 (13)	0.0 (23-I-3)	0.0 (23-II-4)	-85.57 (22)	50.06 (13)	-108.48 (23-II-4)
93	8	0.0 (13)	0.0 (15)	0.0 (23-II-4)	-90.19 (22)	-133.27 (15)	-114.53 (23-II-4)
94	1	0.0 (22)	-0.0 (15)	-0.0 (13)	-113.75 (13)	150.36 (15)	-61.89 (23-I-3)
94	2	0.0 (22)	-0.0 (15)	0.0 (23-II-4)	-95.28 (13)	281.80 (15)	-61.80 (23-II-3)
94	3	0.0 (22)	-0.0 (13)	0.0 (23-II-3)	-94.94 (13)	190.63 (15)	105.82 (13)
94	4	0.0 (13)	0.0 (23-I-4)	0.0 (23-II-3)	-120.16 (13)	-165.00 (22)	84.47 (13)
94	5	0.0 (22)	-0.0 (15)	0.0 (23-II-4)	-106.10 (13)	130.90 (15)	21.05 (13)
94	6	0.0 (22)	-0.0 (15)	0.0 (23-II-3)	-75.54 (13)	320.58 (15)	-53.35 (23-II-3)
94	7	0.0 (22)	-0.0 (13)	0.0 (23-II-3)	-77.69 (13)	231.86 (13)	-59.24 (23-II-3)
94	8	0.0 (13)	0.0 (23-I-3)	0.0 (23-II-3)	-125.82 (13)	-238.83 (22)	-88.29 (23-II-3)
94	9	0.0 (22)	-0.0 (15)	0.0 (23-II-4)	-130.78 (22)	126.21 (15)	26.95 (13)
94	10	0.0 (22)	-0.0 (15)	0.0 (23-II-3)	-109.39 (22)	301.99 (13)	-48.81 (23-II-3)
94	11	0.0 (22)	-0.0 (13)	0.0 (23-II-3)	-108.59 (22)	231.33 (13)	-76.24 (23-II-3)
94	12	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-3)	-140.44 (22)	-243.76 (22)	-102.71 (23-II-3)
94	13	0.0 (22)	-0.0 (15)	0.0 (23-II-4)	-189.03 (22)	130.72 (15)	50.30 (13)
94	14	0.0 (22)	-0.0 (13)	0.0 (23-II-3)	-214.47 (22)	249.63 (13)	-45.44 (23-II-4)
94	15	0.0 (22)	-0.0 (13)	-0.0 (13)	-214.02 (22)	187.82 (13)	-132.11 (15)
94	16	0.0 (22)	0.0 (23-I-4)	-0.0 (13)	-188.48 (22)	-185.71 (22)	-128.55 (23-I-4)
95	1	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-4)	-152.81 (22)	4.77 (23-II-4)	6.16 (23-II-3)
95	2	0.0 (22)	0.0 (15)	0.0 (23-II-4)	-152.86 (22)	-8.40 (15)	-28.55 (23-II-4)
95	3	0.0 (22)	0.0 (15)	0.0 (23-II-4)	-173.49 (22)	4.84 (15)	16.08 (23-II-4)
95	4	0.0 (22)	0.0 (15)	-0.0 (13)	-177.00 (22)	-12.12 (15)	-37.10 (23-II-4)
95	5	0.0 (22)	0.0 (15)	0.0 (23-II-4)	-184.59 (22)	5.20 (15)	14.88 (23-II-4)
95	6	0.0 (22)	0.0 (15)	-0.0 (13)	-187.50 (22)	-11.10 (15)	-38.48 (23-II-4)
95	7	0.0 (22)	0.0 (15)	-0.0 (13)	-195.18 (22)	2.86 (15)	5.28 (23-II-3)
95	8	0.0 (22)	0.0 (15)	-0.0 (13)	-197.10 (22)	-8.27 (15)	29.47 (13)
96	1	0.0 (23-II-3)	-0.0 (15)	-0.0 (13)	-203.16 (22)	124.18 (15)	-54.33 (23-II-3)
96	2	0.0 (23-I-4)	-0.0 (13)	-0.0 (13)	-209.35 (22)	222.75 (13)	44.04 (13)
96	3	0.0 (23-I-4)	-0.0 (13)	0.0 (23-II-4)	-216.53 (22)	172.27 (13)	99.29 (13)
96	4	0.0 (23-I-4)	0.0 (23-II-4)	0.0 (23-II-4)	-211.60 (22)	-197.52 (23-II-4)	83.96 (13)
96	5	0.0 (23-II-3)	-0.0 (13)	-0.0 (13)	-222.00 (23-II-3)	107.74 (15)	46.72 (13)
96	6	0.0 (23-I-4)	-0.0 (13)	-0.0 (13)	-192.22 (23-I-4)	259.69 (13)	45.83 (13)
96	7	0.0 (23-I-4)	-0.0 (13)	0.0 (23-II-4)	-196.28 (23-I-4)	209.90 (13)	29.28 (13)
96	8	0.0 (23-I-4)	0.0 (23-II-3)	0.0 (23-II-4)	-234.87 (23-I-4)	-268.74 (23-II-4)	36.88 (13)
96	9	0.0 (23-II-3)	-0.0 (13)	-0.0 (13)	-218.92 (23-II-3)	90.19 (15)	60.46 (13)
96	10	0.0 (23-I-4)	-0.0 (13)	-0.0 (13)	-155.73 (23-II-3)	245.09 (13)	51.64 (13)
96	11	0.0 (23-I-4)	-0.0 (13)	-0.0 (13)	-161.46 (23-II-4)	202.39 (13)	-55.59 (23-II-4)
96	12	0.0 (23-I-4)	0.0 (23-II-3)	0.0 (23-II-4)	-238.41 (23-II-4)	-274.11 (23-II-4)	-38.35 (23-II-4)
96	13	0.0 (23-II-3)	-0.0 (13)	-0.0 (13)	-163.88 (23-II-3)	75.91 (15)	92.38 (13)
96	14	0.0 (23-I-4)	-0.0 (13)	-0.0 (13)	-74.15 (23-II-4)	188.14 (13)	51.59 (13)
96	15	0.0 (23-I-4)	-0.0 (13)	-0.0 (13)	-74.27 (23-II-4)	156.59 (13)	-120.85 (23-II-4)
96	16	0.0 (23-II-4)	0.0 (23-II-4)	-0.0 (13)	-176.28 (23-II-4)	-207.22 (23-II-4)	-115.73 (23-II-4)
97	1	-0.1 (23-II-1)	-0.0 (13)	0.0 (16)	334.11 (15)	42.94 (15)	6.55 (15)
97	2	-0.1 (23-II-1)	-0.0 (13)	0.0 (23-I-2)	335.57 (15)	40.63 (15)	6.42 (15)
97	3	-0.1 (16)	-0.0 (23-II-1)	0.0 (23-I-2)	335.30 (15)	40.57 (15)	10.99 (23-I-4)
97	4	-0.1 (16)	-0.0 (23-II-1)	0.0 (16)	333.38 (15)	42.77 (15)	11.46 (23-II-4)
97	5	-0.1 (23-II-1)	-0.0 (13)	0.0 (16)	-314.21 (23-II-2)	-56.00 (23-II-1)	5.57 (15)
97	6	-0.1 (23-II-1)	-0.0 (13)	0.0 (23-I-2)	-299.63 (23-II-2)	31.36 (15)	4.73 (15)
97	7	-0.1 (16)	-0.0 (23-II-1)	0.0 (23-II-4)	-300.86 (23-II-2)	31.26 (15)	11.46 (23-I-4)
97	8	-0.1 (16)	-0.0 (23-II-1)	-0.0 (23-I-4)	-316.00 (23-II-1)	-53.61 (23-II-1)	14.64 (23-II-4)
97	9	-0.2 (23-II-1)	0.1 (23-I-1)	0.0 (16)	-415.34 (23-II-2)	-49.69 (23-II-1)	45.09 (23-I-4)
97	10	-0.1 (23-II-1)	-0.1 (13)	0.1 (23-II-1)	-265.02 (23-II-2)	-44.45 (23-II-1)	29.81 (23-I-4)
97	11	-0.0 (16)	-0.1 (13)	0.0 (23-I-1)	-265.98 (23-II-1)	41.02 (15)	25.17 (15)

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DEL RECAPITO FINALE DI SQUINZANO (LE)  
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BTK3**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
97	12	-0.1 (16)	-0.1 (23-II-1)	-0.1 (23-I-4)	-416.47 (23-II-1)	-41.62 (23-II-1)	32.23 (15)
97	13	-0.5 (23-II-1)	-0.1 (13)	0.1 (23-II-1)	-703.45 (23-II-1)	-66.79 (23-II-1)	348.70 (23-I-4)
97	14	0.0 (23-II-1)	-0.0 (13)	0.0 (23-II-1)	-48.13 (23-II-2)	-58.66 (23-II-1)	51.69 (23-I-4)
97	15	-0.0 (23-I-1)	-0.0 (13)	0.0 (23-II-1)	-47.22 (23-II-2)	51.09 (15)	-43.99 (23-II-1)
97	16	0.3 (23-I-1)	-0.1 (13)	-0.1 (16)	-697.53 (23-II-1)	-17.47 (23-I-1)	-313.25 (23-II-1)
98	1	-0.1 (23-II-1)	-0.0 (13)	0.0 (16)	333.26 (15)	42.74 (15)	5.58 (15)
98	2	-0.1 (23-II-1)	-0.0 (13)	0.0 (23-II-1)	334.96 (15)	40.48 (15)	5.24 (15)
98	3	-0.1 (13)	-0.0 (23-II-1)	0.0 (23-II-1)	335.17 (15)	40.51 (15)	9.30 (23-II-4)
98	4	-0.1 (13)	-0.0 (23-I-4)	0.0 (16)	334.06 (15)	42.87 (15)	9.75 (23-II-4)
98	5	-0.1 (23-II-1)	-0.0 (13)	0.0 (16)	-315.41 (23-II-1)	-56.64 (23-II-1)	4.68 (15)
98	6	-0.1 (23-II-1)	-0.0 (13)	0.0 (23-II-1)	-301.00 (23-II-1)	31.15 (15)	3.75 (15)
98	7	-0.1 (16)	-0.0 (23-II-1)	0.0 (23-II-1)	-302.10 (23-II-1)	31.22 (15)	10.03 (23-II-4)
98	8	-0.1 (16)	-0.0 (23-I-4)	0.0 (16)	-316.31 (23-II-1)	-52.81 (23-II-1)	13.72 (23-II-4)
98	9	-0.2 (23-II-1)	0.0 (23-I-1)	0.0 (16)	-416.02 (23-II-1)	-50.46 (23-II-1)	43.94 (23-II-4)
98	10	-0.1 (23-II-1)	-0.0 (23-II-1)	0.1 (23-II-1)	-265.51 (23-II-1)	-45.04 (23-II-1)	28.56 (23-II-4)
98	11	-0.0 (16)	-0.0 (22)	0.0 (23-II-4)	-266.04 (23-II-1)	41.06 (15)	24.42 (15)
98	12	-0.1 (16)	-0.1 (23-I-4)	-0.0 (23-I-4)	-415.53 (23-II-1)	-39.49 (23-II-1)	31.69 (15)
98	13	-0.5 (23-II-1)	-0.1 (13)	0.1 (23-II-1)	-703.56 (23-II-1)	-68.01 (23-II-1)	347.93 (23-II-1)
98	14	0.0 (23-II-1)	-0.0 (23-I-4)	0.0 (23-II-1)	-48.18 (23-II-1)	-59.21 (23-II-1)	50.76 (23-II-4)
98	15	-0.0 (23-I-1)	-0.0 (22)	0.0 (23-II-1)	-47.08 (23-II-1)	51.22 (15)	-44.83 (23-I-4)
98	16	0.3 (23-I-1)	-0.1 (22)	-0.1 (16)	-697.26 (23-II-1)	-14.25 (23-I-1)	-313.06 (23-I-4)
99	1	-0.1 (23-II-1)	-0.0 (16)	0.0 (16)	335.23 (15)	43.10 (15)	4.26 (15)
99	2	-0.1 (23-II-1)	-0.0 (23-II-1)	0.0 (16)	338.92 (15)	41.25 (15)	4.25 (15)
99	3	-0.1 (23-II-1)	-0.0 (23-II-1)	0.0 (16)	341.40 (15)	40.50 (15)	19.94 (23-II-1)
99	4	-0.2 (23-II-1)	-0.0 (23-II-1)	0.0 (16)	341.54 (15)	28.47 (15)	38.24 (23-II-1)
99	5	-0.1 (23-II-1)	-0.0 (22)	0.0 (16)	-313.44 (23-II-1)	-53.27 (23-II-1)	4.12 (15)
99	6	-0.1 (23-II-1)	-0.0 (22)	0.1 (23-II-1)	-295.02 (23-II-1)	32.13 (15)	5.08 (16)
99	7	-0.1 (23-II-1)	-0.1 (23-II-1)	0.0 (16)	-291.75 (23-II-1)	31.35 (15)	28.06 (23-II-1)
99	8	-0.2 (23-II-1)	-0.0 (23-II-1)	-0.0 (23-II-4)	-301.88 (23-II-1)	14.04 (15)	36.56 (23-II-1)
99	9	-0.2 (23-II-1)	0.1 (23-II-4)	0.1 (16)	-413.22 (23-II-1)	-44.05 (23-II-1)	46.48 (23-II-1)
99	10	-0.0 (23-II-1)	-0.0 (23-I-4)	0.1 (23-II-1)	-260.70 (23-II-1)	42.34 (15)	36.02 (23-II-1)
99	11	-0.0 (16)	-0.0 (23-I-4)	0.0 (23-II-1)	-259.35 (23-II-1)	42.18 (15)	26.08 (15)
99	12	-0.2 (23-II-1)	-0.1 (23-II-1)	-0.1 (23-II-4)	-419.10 (23-II-1)	31.05 (15)	53.47 (15)
99	13	-0.5 (23-II-1)	-0.0 (16)	0.1 (23-II-1)	-702.74 (23-II-1)	-59.87 (23-II-1)	350.42 (23-II-1)
99	14	0.0 (23-I-1)	0.0 (23-II-4)	0.0 (23-II-1)	-47.15 (23-II-1)	52.83 (15)	56.64 (23-II-1)
99	15	0.0 (16)	0.1 (23-II-4)	0.1 (23-II-1)	-38.58 (23-II-1)	54.37 (15)	39.91 (15)
99	16	0.2 (23-I-1)	-0.1 (23-I-4)	-0.0 (13)	-713.11 (23-II-1)	85.60 (23-II-4)	-251.00 (23-II-1)
100	1	-0.0 (22)	-0.1 (23-I-4)	0.0 (13)	-50.70 (15)	-414.12 (15)	-31.65 (23-II-3)
100	2	-0.0 (22)	-0.1 (23-I-4)	0.0 (13)	57.80 (23-I-4)	432.76 (23-I-2)	-45.73 (23-II-3)
100	3	-0.0 (16)	-0.2 (23-I-4)	0.0 (16)	29.08 (23-I-4)	634.92 (23-I-2)	-163.46 (23-II-3)
100	4	-0.1 (22)	-0.5 (23-I-4)	0.1 (23-II-4)	146.34 (23-I-4)	1033.46 (23-I-2)	-542.18 (23-II-4)
100	5	-0.0 (22)	-0.1 (23-I-4)	0.0 (23-I-2)	-49.72 (15)	-406.45 (15)	-29.58 (23-II-3)
100	6	-0.0 (22)	-0.1 (23-I-4)	0.0 (23-I-2)	50.03 (23-I-2)	370.76 (23-I-2)	-41.58 (23-II-3)
100	7	-0.1 (23-I-4)	-0.1 (23-I-4)	0.1 (23-II-1)	98.94 (23-I-2)	292.82 (23-I-2)	-102.42 (23-II-4)
100	8	-0.1 (23-I-4)	0.0 (23-I-4)	0.0 (23-II-4)	-21.97 (15)	-29.00 (15)	-30.93 (23-II-4)
100	9	-0.0 (23-I-4)	-0.1 (13)	0.0 (23-I-2)	-49.48 (15)	-405.46 (15)	-29.96 (23-II-3)
100	10	-0.1 (23-I-4)	-0.1 (13)	0.0 (23-I-2)	49.63 (23-I-2)	372.76 (23-I-2)	-26.52 (15)
100	11	-0.1 (22)	-0.0 (16)	0.0 (23-II-4)	98.11 (23-I-2)	293.39 (23-I-2)	-68.26 (15)
100	12	-0.1 (22)	-0.0 (23-I-4)	0.0 (23-II-4)	-21.21 (15)	-28.89 (15)	-28.44 (15)
100	13	-0.0 (23-I-4)	-0.1 (13)	0.0 (16)	-49.97 (15)	-411.75 (15)	-28.07 (23-II-3)



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
100	14	-0.0 (23-I-4)	-0.1 (13)	0.0 (16)	55.59 (23-I-4)	437.87 (23-I-2)	-24.47 (15)
100	15	-0.1 (23-I-4)	-0.1 (16)	-0.0 (23-I-4)	24.89 (23-II-3)	636.26 (23-I-2)	112.59 (23-I-3)
100	16	-0.1 (22)	0.3 (23-I-4)	-0.1 (16)	141.32 (23-II-3)	1033.56 (23-I-2)	514.00 (23-I-3)
101	1	-0.0 (13)	-0.1 (23-I-3)	0.0 (13)	-68.55 (15)	-523.57 (15)	-5.40 (15)
101	2	-0.0 (13)	-0.1 (23-I-3)	0.0 (13)	-72.83 (15)	-501.46 (15)	-5.15 (15)
101	3	-0.1 (13)	-0.2 (23-I-3)	0.0 (16)	-41.87 (15)	-541.50 (15)	50.34 (15)
101	4	-0.1 (13)	-0.5 (23-I-3)	0.1 (23-I-3)	-13.30 (15)	-769.65 (15)	370.63 (15)
101	5	-0.0 (13)	-0.1 (23-I-3)	0.0 (13)	-62.69 (15)	-529.17 (15)	-4.99 (15)
101	6	-0.0 (13)	-0.1 (23-I-3)	0.0 (23-I-2)	-48.94 (15)	-480.71 (15)	-3.42 (15)
101	7	-0.1 (13)	-0.1 (23-I-3)	0.1 (23-II-2)	-70.55 (15)	-369.83 (15)	36.76 (15)
101	8	-0.1 (13)	0.0 (23-I-3)	0.0 (23-II-3)	-89.80 (15)	-70.53 (15)	64.01 (15)
101	9	-0.0 (23-I-3)	-0.1 (16)	-0.0 (18)	-62.78 (15)	-529.53 (15)	-6.01 (23-II-4)
101	10	-0.1 (23-I-3)	-0.1 (16)	-0.0 (18)	-49.05 (15)	-480.81 (15)	-8.33 (23-II-4)
101	11	-0.1 (22)	-0.0 (16)	0.0 (23-II-4)	-70.59 (15)	-369.82 (15)	-38.89 (15)
101	12	-0.1 (22)	-0.0 (23-I-3)	0.0 (23-II-3)	-89.90 (15)	-70.57 (15)	-62.53 (15)
101	13	-0.0 (23-I-3)	-0.1 (13)	-0.0 (18)	-68.70 (15)	-524.28 (15)	5.25 (13)
101	14	-0.0 (23-I-3)	-0.1 (16)	-0.0 (23-II-2)	-73.04 (15)	-501.75 (15)	-6.15 (23-II-4)
101	15	-0.1 (23-I-3)	-0.1 (16)	-0.1 (23-I-4)	-42.04 (15)	-541.57 (15)	-52.53 (15)
101	16	-0.1 (22)	0.3 (23-II-3)	-0.1 (16)	52.56 (23-II-4)	-769.70 (15)	-367.50 (15)
102	1	-0.0 (16)	-0.1 (13)	0.0 (16)	-49.50 (15)	-411.31 (15)	-24.63 (23-II-4)
102	2	-0.0 (22)	-0.1 (23-II-4)	0.0 (16)	49.49 (23-I-4)	437.98 (23-I-2)	-39.21 (23-II-4)
102	3	-0.0 (16)	-0.2 (23-II-4)	0.1 (16)	15.38 (23-I-4)	634.93 (23-I-2)	-157.84 (23-II-4)
102	4	-0.1 (22)	-0.5 (23-II-4)	0.1 (23-II-4)	130.66 (23-II-3)	1033.04 (23-I-3)	-538.75 (23-II-4)
102	5	-0.0 (23-II-4)	-0.1 (23-II-4)	0.0 (16)	-48.63 (15)	-404.21 (15)	-29.85 (23-II-4)
102	6	-0.0 (22)	-0.1 (23-II-4)	0.1 (23-II-4)	-44.46 (15)	370.22 (23-I-3)	-44.35 (23-II-4)
102	7	-0.1 (23-I-4)	-0.0 (23-II-4)	0.1 (23-II-4)	-69.40 (15)	289.29 (23-I-3)	-107.21 (23-II-4)
102	8	0.0 (13)	0.0 (23-I-4)	0.0 (23-II-4)	-40.62 (23-II-3)	-28.65 (15)	-31.88 (23-II-4)
102	9	-0.0 (23-II-4)	-0.1 (23-II-4)	0.0 (16)	-47.68 (15)	-404.79 (15)	-42.15 (23-II-4)
102	10	-0.1 (23-II-4)	-0.1 (23-II-4)	0.0 (23-II-1)	-48.49 (15)	374.21 (23-I-3)	-27.61 (23-II-4)
102	11	-0.0 (23-I-4)	-0.0 (16)	0.1 (23-II-4)	-74.38 (15)	264.16 (23-I-3)	-51.62 (15)
102	12	0.1 (23-II-4)	0.0 (16)	0.1 (23-II-4)	-119.47 (23-II-3)	-13.29 (15)	-45.04 (23-II-4)
102	13	-0.0 (23-II-4)	-0.2 (23-II-4)	0.0 (23-II-4)	-34.79 (15)	-419.33 (15)	-52.76 (23-II-4)
102	14	-0.0 (23-II-4)	-0.2 (23-II-4)	0.0 (16)	28.09 (23-I-3)	444.27 (23-I-3)	-23.35 (15)
102	15	-0.1 (23-II-4)	-0.2 (23-II-4)	-0.1 (23-II-4)	71.63 (23-I-3)	680.26 (23-I-3)	142.56 (23-I-3)
102	16	-0.1 (23-I-4)	0.2 (23-I-4)	-0.0 (13)	-151.19 (23-II-3)	1071.17 (23-I-3)	352.24 (23-I-3)
103	1	-0.0 (22)	-0.1 (23-I-3)	0.0 (13)	-68.71 (15)	-524.38 (15)	-4.12 (15)
103	2	-0.0 (22)	-0.1 (23-I-3)	0.0 (13)	-73.05 (15)	-501.89 (15)	4.67 (23-II-4)
103	3	-0.1 (16)	-0.2 (23-I-3)	0.0 (16)	-42.12 (15)	-541.67 (15)	51.46 (15)
103	4	-0.1 (22)	-0.5 (23-I-3)	0.1 (23-II-3)	-13.56 (15)	-769.68 (15)	371.44 (15)
103	5	-0.0 (22)	-0.1 (23-I-3)	0.0 (23-I-2)	-62.87 (15)	-530.15 (15)	-3.86 (15)
103	6	-0.1 (22)	-0.1 (23-I-3)	0.0 (23-I-3)	-49.14 (15)	-481.22 (15)	2.60 (23-II-4)
103	7	-0.1 (23-I-3)	-0.1 (23-I-3)	0.1 (23-II-3)	-70.76 (15)	-370.01 (15)	37.83 (15)
103	8	-0.1 (23-I-4)	0.0 (23-I-3)	0.0 (23-II-3)	-90.01 (15)	-70.55 (15)	64.89 (15)
103	9	-0.0 (23-I-3)	-0.1 (13)	0.0 (23-I-3)	-62.93 (15)	-530.65 (15)	5.63 (13)
103	10	-0.1 (23-I-3)	-0.1 (13)	0.0 (23-I-3)	-49.14 (15)	-481.33 (15)	-5.97 (23-I-4)
103	11	-0.1 (22)	-0.0 (16)	0.0 (23-II-3)	-70.59 (15)	-369.93 (15)	-37.81 (15)
103	12	-0.1 (22)	-0.0 (23-I-3)	0.0 (23-II-3)	-89.83 (15)	-70.55 (15)	-61.61 (15)
103	13	-0.0 (23-I-3)	-0.1 (13)	0.0 (16)	-68.80 (15)	-525.61 (15)	5.79 (13)
103	14	-0.0 (23-I-4)	-0.1 (13)	0.0 (16)	-72.81 (15)	-502.15 (15)	5.23 (13)
103	15	-0.1 (23-I-4)	-0.1 (16)	-0.0 (23-I-3)	-41.47 (15)	-541.48 (15)	-51.24 (15)
103	16	-0.1 (22)	0.3 (23-I-3)	-0.0 (16)	53.95 (23-II-3)	-769.62 (15)	-366.51 (15)
104	1	-0.0 (13)	-0.1 (23-II-1)	0.0 (13)	-51.49 (15)	-417.73 (15)	-39.11 (23-II-3)
104	2	-0.0 (13)	-0.1 (23-I-4)	0.0 (13)	55.33 (23-I-2)	427.68 (23-II-3)	-53.58 (23-II-3)
104	3	-0.0 (13)	-0.2 (23-I-4)	0.0 (16)	25.94 (23-I-4)	632.57 (23-II-3)	-171.11 (23-II-3)
104	4	-0.1 (13)	-0.5 (23-I-4)	0.1 (23-I-4)	143.00 (23-I-4)	1033.04 (23-II-3)	-546.54 (23-II-3)
104	5	-0.0 (13)	-0.1 (23-I-4)	0.0 (23-I-2)	-50.54 (15)	-410.04 (15)	-38.39 (23-II-3)
104	6	-0.0 (13)	-0.1 (23-I-4)	0.0 (23-I-2)	-49.03 (15)	364.59 (23-II-3)	-50.69 (23-II-3)
104	7	-0.1 (13)	-0.1 (23-I-4)	0.1 (23-I-2)	96.07 (23-I-2)	290.12 (23-II-3)	-111.14 (23-II-3)
104	8	-0.1 (13)	0.0 (23-I-4)	0.0 (23-II-1)	-24.09 (15)	-29.26 (15)	-36.22 (23-II-3)
104	9	-0.0 (23-I-4)	-0.1 (16)	-0.0 (18)	-50.32 (15)	-408.79 (15)	-39.69 (23-II-3)
104	10	-0.0 (23-I-4)	-0.1 (16)	-0.0 (18)	-48.76 (15)	365.92 (23-I-2)	-35.58 (15)
104	11	-0.1 (13)	-0.0 (16)	0.0 (23-II-2)	96.94 (23-I-2)	290.78 (23-I-2)	-76.67 (15)
104	12	-0.1 (13)	-0.0 (23-I-1)	0.0 (23-II-4)	-23.57 (15)	-29.15 (15)	-33.51 (15)
104	13	-0.0 (23-I-4)	-0.1 (13)	-0.0 (15)	-50.89 (15)	-414.75 (15)	-37.80 (23-II-3)
104	14	-0.0 (23-I-4)	-0.1 (16)	-0.0 (23-II-2)	57.04 (23-I-4)	431.24 (23-I-2)	-34.55 (15)
104	15	-0.1 (23-I-4)	-0.1 (16)	-0.1 (23-I-4)	28.30 (23-I-4)	634.26 (23-I-2)	-110.79 (15)
104	16	-0.1 (22)	0.3 (23-II-4)	-0.1 (16)	145.53 (23-I-4)	1033.39 (23-I-2)	509.09 (23-I-3)



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
105	1	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-4)	-91.30 (22)	-116.92 (23-I-3)	-96.45 (23-II-4)
105	2	0.0 (13)	-0.0 (15)	-0.0 (13)	-73.20 (13)	36.42 (15)	-105.49 (23-II-4)
105	3	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-61.44 (13)	24.86 (15)	-74.11 (23-II-4)
105	4	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-52.42 (13)	10.66 (23-II-1)	-35.43 (23-II-4)
105	5	0.0 (23-II-1)	0.0 (23-I-3)	0.0 (23-II-4)	-94.92 (23-II-1)	-154.71 (23-I-3)	-63.20 (23-II-4)
105	6	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-55.93 (13)	46.36 (15)	-51.88 (23-II-4)
105	7	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-48.46 (13)	40.74 (23-II-4)	-44.32 (23-II-4)
105	8	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-44.09 (13)	20.89 (23-II-1)	-20.50 (23-II-4)
105	9	0.0 (23-II-1)	-0.0 (15)	0.0 (23-II-4)	-91.65 (23-II-1)	-143.39 (23-II-3)	-46.91 (23-II-4)
105	10	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-37.02 (13)	45.34 (15)	36.09 (13)
105	11	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-32.80 (13)	42.91 (23-II-4)	-29.76 (23-II-4)
105	12	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-34.57 (13)	22.09 (23-II-1)	14.70 (13)
105	13	0.0 (23-II-1)	0.0 (23-I-3)	0.0 (23-II-4)	-59.54 (23-II-1)	-88.83 (23-I-3)	44.47 (13)
105	14	0.0 (22)	-0.0 (15)	0.0 (23-II-4)	-11.71 (15)	34.67 (15)	41.88 (13)
105	15	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	19.51 (23-I-4)	30.60 (23-II-3)	27.81 (13)
105	16	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	-24.37 (13)	15.46 (23-II-4)	13.69 (13)
106	1	0.0 (23-II-1)	0.0 (23-I-3)	0.0 (23-II-4)	-109.73 (22)	43.90 (13)	-50.48 (23-II-4)
106	2	0.0 (22)	0.0 (15)	0.0 (23-II-4)	-102.60 (22)	-118.52 (13)	-51.88 (23-II-4)
106	3	0.0 (23-II-1)	0.0 (23-I-3)	0.0 (23-II-4)	-102.72 (23-II-1)	90.77 (13)	-46.13 (23-II-4)
106	4	0.0 (23-II-1)	0.0 (23-II-1)	0.0 (23-II-4)	-105.43 (23-II-1)	-163.50 (13)	-45.33 (23-II-4)
106	5	0.0 (23-II-1)	0.0 (23-I-3)	0.0 (23-II-4)	-95.87 (23-II-1)	87.82 (13)	-49.76 (23-II-4)
106	6	0.0 (23-II-1)	0.0 (23-II-1)	0.0 (23-II-4)	-111.67 (23-II-1)	-160.39 (13)	-42.34 (23-II-4)
106	7	0.0 (23-II-1)	0.0 (23-I-3)	0.0 (23-II-4)	-66.87 (23-II-1)	44.04 (13)	-57.98 (23-II-4)
106	8	0.0 (23-II-1)	0.0 (23-II-1)	0.0 (23-II-4)	-82.27 (23-II-1)	-107.48 (23-II-1)	-57.43 (23-II-4)
107	1	0.0 (23-I-3)	0.0 (23-II-3)	-0.0 (13)	-191.34 (22)	4.04 (23-II-4)	4.78 (23-II-4)
107	2	0.0 (23-I-3)	0.0 (15)	-0.0 (13)	-193.44 (22)	-9.79 (15)	33.46 (13)
107	3	0.1 (23-II-3)	0.0 (15)	-0.0 (13)	-213.48 (23-II-3)	5.58 (15)	14.76 (23-II-3)
107	4	0.1 (23-II-3)	0.0 (15)	-0.0 (13)	-216.92 (23-II-3)	-16.38 (15)	50.76 (13)
107	5	0.1 (23-II-3)	0.0 (15)	-0.0 (13)	-236.96 (23-II-3)	10.96 (23-II-3)	-14.07 (13)
107	6	0.1 (23-II-3)	0.0 (15)	-0.0 (13)	-239.29 (23-II-3)	-29.60 (15)	63.08 (13)
107	7	0.1 (23-II-3)	0.0 (23-II-4)	-0.0 (13)	-214.19 (23-II-3)	8.16 (23-II-3)	-6.17 (23-I-4)
107	8	0.1 (23-II-3)	0.0 (15)	-0.0 (13)	-222.12 (23-II-3)	-25.76 (23-II-4)	56.82 (13)
108	1	0.0 (23-I-4)	0.1 (23-I-4)	-0.0 (13)	-203.70 (22)	-329.79 (23-I-4)	-117.65 (23-II-4)
108	2	0.0 (23-II-1)	0.0 (23-I-3)	-0.0 (13)	-193.71 (22)	-136.39 (23-I-3)	-164.80 (23-II-4)
108	3	0.0 (23-II-1)	0.0 (23-I-3)	-0.0 (13)	-167.56 (22)	106.44 (13)	-130.10 (23-II-4)
108	4	0.0 (23-II-1)	0.0 (23-I-3)	0.0 (23-II-4)	-129.51 (22)	45.36 (13)	-85.18 (23-II-4)
108	5	0.0 (23-I-4)	0.0 (23-I-3)	-0.0 (13)	-245.05 (23-I-4)	-430.13 (23-II-4)	-75.32 (23-II-4)
108	6	0.0 (23-I-4)	0.0 (23-I-3)	-0.0 (13)	-191.31 (23-I-4)	-118.26 (23-I-3)	-72.46 (23-II-4)
108	7	0.0 (23-II-1)	0.0 (23-I-3)	-0.0 (13)	-151.35 (23-II-1)	129.59 (13)	-52.48 (23-II-4)
108	8	0.0 (23-II-1)	0.0 (23-I-3)	0.0 (23-II-4)	-113.33 (22)	54.44 (14)	-44.25 (23-II-4)
108	9	0.0 (23-II-4)	0.0 (23-I-3)	0.0 (23-II-4)	-254.72 (23-II-4)	-435.99 (23-II-4)	-55.72 (23-II-4)
108	10	0.0 (23-I-4)	0.0 (23-II-3)	0.0 (23-II-4)	-166.95 (23-II-4)	105.34 (13)	63.33 (13)
108	11	0.0 (23-II-1)	0.0 (23-I-3)	0.0 (23-II-4)	-114.20 (23-II-1)	121.64 (13)	43.97 (13)
108	12	0.0 (23-II-1)	0.0 (23-I-3)	0.0 (23-II-4)	-90.37 (23-II-1)	51.32 (14)	28.33 (13)
108	13	0.0 (23-II-4)	0.1 (23-II-4)	0.0 (23-II-4)	-187.83 (23-II-4)	-326.21 (23-II-4)	83.61 (13)
108	14	0.0 (23-I-4)	0.0 (23-I-3)	0.0 (23-II-4)	-73.44 (23-II-4)	-104.37 (23-I-3)	92.89 (13)
108	15	0.0 (23-II-1)	0.0 (23-I-3)	0.0 (23-II-4)	-45.77 (23-II-1)	89.43 (13)	45.48 (13)
108	16	0.0 (23-II-1)	0.0 (23-I-3)	0.0 (23-II-4)	-58.56 (23-II-1)	34.95 (13)	21.68 (13)
109	1	0.0 (22)	0.0 (23-II-3)	0.0 (23-II-4)	-79.08 (22)	47.91 (13)	-84.06 (23-II-4)
109	2	0.0 (22)	0.0 (15)	0.0 (23-II-4)	-93.69 (13)	-122.98 (13)	-91.68 (23-II-4)
109	3	0.0 (22)	0.0 (15)	0.0 (23-II-4)	-90.92 (22)	96.85 (13)	-84.76 (23-II-4)
109	4	0.0 (22)	0.0 (15)	0.0 (23-II-4)	-93.98 (22)	-168.92 (13)	-95.85 (23-II-4)
109	5	0.0 (22)	0.0 (15)	0.0 (23-II-4)	-101.15 (22)	95.79 (13)	-75.31 (23-II-4)
109	6	0.0 (22)	0.0 (15)	0.0 (23-II-4)	-99.70 (22)	-166.92 (13)	-88.62 (23-II-4)
109	7	0.0 (22)	0.0 (23-I-3)	0.0 (23-II-4)	-107.85 (22)	46.80 (13)	-69.92 (23-II-4)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
109	8	0.0 (22)	0.0 (15)	0.0 (23-II-4)	-99.54 (22)	-118.52 (13)	-74.17 (23-II-4)
110	1	0.0 (23-II-1)	0.0 (23-I-3)	0.0 (23-II-4)	-66.33 (23-II-1)	-57.33 (23-I-3)	-49.22 (23-II-4)
110	2	0.0 (23-II-1)	0.0 (23-I-3)	0.0 (23-II-4)	-56.41 (23-II-1)	-66.48 (23-I-3)	-38.70 (23-II-4)
110	3	0.0 (23-II-1)	0.0 (23-I-3)	-0.0 (13)	12.31 (23-II-1)	-54.55 (23-I-3)	-30.66 (23-II-4)
110	4	0.0 (23-II-1)	0.0 (23-I-3)	0.0 (23-II-4)	16.71 (23-II-4)	-41.57 (23-I-3)	15.46 (13)
111	1	0.0 (23-II-3)	-0.0 (13)	-0.0 (13)	-138.62 (23-II-3)	46.42 (13)	76.64 (13)
111	2	0.0 (23-II-4)	-0.0 (13)	-0.0 (13)	-156.38 (23-II-4)	157.83 (13)	50.19 (13)
111	3	0.0 (23-II-4)	-0.0 (13)	0.0 (23-II-4)	-164.74 (23-II-4)	128.79 (13)	-37.32 (23-II-4)
111	4	0.0 (23-II-4)	0.0 (23-II-4)	0.0 (23-II-4)	-142.49 (23-II-4)	-191.13 (23-II-4)	-81.86 (23-II-4)
111	5	0.0 (23-II-3)	-0.0 (13)	-0.0 (13)	30.75 (23-I-4)	35.81 (15)	33.35 (13)
111	6	0.0 (23-II-4)	-0.0 (13)	-0.0 (13)	67.83 (23-II-4)	140.23 (13)	27.46 (13)
111	7	0.0 (23-II-4)	-0.0 (13)	-0.0 (13)	74.18 (23-II-4)	124.12 (13)	-60.97 (23-II-4)
111	8	0.0 (23-II-4)	0.0 (23-II-4)	0.0 (23-II-4)	35.26 (23-II-4)	-163.62 (23-II-3)	-38.54 (23-II-4)
112	1	0.0 (23-II-3)	-0.0 (13)	-0.0 (15)	-112.83 (23-II-3)	-4.07 (15)	-24.65 (23-II-3)
112	2	0.0 (23-II-3)	0.0 (23-II-3)	-0.0 (13)	-108.42 (23-II-3)	7.99 (13)	50.35 (15)
112	3	0.0 (15)	-0.0 (23-II-3)	-0.0 (23-II-3)	9.25 (13)	0	-24.23 (15)
112	4	0.0 (23-II-4)	-0.0 (13)	-0.0 (13)	12.26 (13)	10.78 (15)	34.81 (15)
113	1	0.0 (23-II-4)	0.0 (23-II-3)	-0.0 (13)	-145.65 (23-II-4)	-253.12 (23-II-4)	75.03 (13)
113	2	0.0 (23-II-4)	0.0 (23-I-3)	-0.0 (13)	-164.71 (23-II-4)	-137.38 (23-II-3)	71.67 (13)
113	3	0.0 (23-II-1)	0.0 (23-I-3)	-0.0 (13)	-115.87 (23-II-1)	63.15 (13)	52.51 (13)
113	4	0.0 (23-II-1)	0.0 (23-I-3)	0.0 (23-II-4)	-70.88 (23-II-1)	-16.50 (23-I-3)	35.02 (13)
113	5	0.0 (23-II-4)	0.0 (23-II-3)	-0.0 (13)	37.16 (23-II-1)	-200.72 (23-II-4)	27.08 (13)
113	6	0.0 (23-II-4)	0.0 (23-II-3)	-0.0 (13)	74.23 (23-II-4)	-106.31 (23-II-3)	45.62 (23-I-3)
113	7	0.0 (23-II-1)	0.0 (23-I-3)	-0.0 (13)	49.62 (23-I-4)	55.88 (13)	27.44 (23-I-3)
113	8	0.0 (23-II-1)	0.0 (23-I-3)	0.0 (23-II-4)	20.46 (23-I-4)	-13.84 (23-I-3)	16.58 (13)
114	1	0.0 (23-I-3)	0.0 (23-I-3)	-0.0 (13)	-48.90 (23-II-1)	-76.10 (23-I-3)	46.80 (13)
114	2	0.0 (13)	-0.0 (15)	-0.0 (13)	-41.38 (23-I-3)	23.53 (15)	38.35 (13)
114	3	0.0 (13)	-0.0 (15)	-0.0 (13)	-30.60 (13)	24.25 (23-II-3)	24.84 (13)
114	4	0.0 (13)	-0.0 (15)	0.0 (23-II-3)	-23.97 (13)	11.50 (23-II-4)	-14.58 (23-II-4)
114	5	0.0 (23-I-3)	0.0 (23-I-3)	-0.0 (13)	10.68 (23-II-1)	-64.34 (23-I-3)	18.76 (13)
114	6	0.0 (23-I-3)	0.0 (13)	-0.0 (13)	23.00 (23-II-1)	20.72 (15)	22.11 (13)
114	7	0.0 (13)	-0.0 (15)	-0.0 (13)	14.22 (23-II-1)	25.08 (23-II-3)	14.80 (13)
114	8	0.0 (13)	-0.0 (15)	0.0 (23-II-4)	7.88 (23-II-4)	11.76 (23-II-4)	6.64 (13)

#### Verifica dei Muri in calcestruzzo

Scenario di calcolo: **ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO**

Simbologia:

Muro	Indice del muro in verifica
Nodi	[n1-n2-n3-n4...] Indici dei nodi di attacco del muro
Pann.X	Numero di pannelli in direzione locale X del muro(per muri a pannelli)
Pann.Y	Numero di pannelli in direzione locale Y del muro(per muri a pannelli)
Pann	Numero totale di pannelli (per muri a mesh)
Spess [cm]	Spessore del muro
Criterio	Criterio di verifica adottato per la verifica
Pannello	Indice del pannello
Nx [daN]	Sforzo in direzione x locale per metro lineare (Nx=sxx*spessore)
Ny [daN]	Sforzo in direzione y locale per metro lineare (Ny=syy*spessore)
Nxy [daN]	Sforzo tagliante locale per metro lineare (Nxy=sxy*spessore)
Mx [daN*m]	Momento in direzione x locale per metro lineare
My [daN*m]	Momento in direzione y locale per metro lineare
Mxy [daN*m]	Momento torcente locale per metro lineare
Ax [m^2]	Armatura totale pannello in direzione x locale <sup>(1)</sup>
Ay [m^2]	Armatura totale pannello in direzione y locale <sup>(1)</sup>
εc	Deformazione nel cls <sup>(2)</sup>
εf	Deformazione nell'acciaio <sup>(2)</sup>
Massimi	Armature massime riscontrate nel muro
Massimo	massima sigma ideale riscontrata nel muro
σid+,σid- [MPa]	$(\sigma_x^2 + \sigma_y^2 - \sigma_x \sigma_y + 3 \tau_{xy}^2)^{1/2}$ Tensioni ideali ai lembi della lastra (Acciaio)

$\sigma_{id+}, \sigma_{id-}$  [MPa]  $(\sigma_x^2 + \sigma_y^2 - \sigma_x \sigma_y + 3 \tau_{xy}^2)^{1/2}$  Tensioni ideali ai lembi della lastra (Legno)

Fatt.Ampl.Sisma Fattore moltiplicativo di gruppo per le azioni sismiche (solo se diverso da 1.0)

Cs Coefficiente di sicurezza definito dal rapporto  $|M_r(N)|/|M_d|$  ( $M_r(N)$ =Momento resistente corrispondente allo sforzo normale N,  $M_d$ =momento agente), quando richiesto dal criterio di verifica

$\zeta_E$  Livello di sicurezza sismico definito come rapporto tra l'accelerazione sopportabile e l'accelerazione di progetto, quando richiesto dal criterio di verifica

Note Verifica muri:

(<sup>1</sup>): Le armature  $A_x$  ed  $A_y$  vanno intese come a metro lineare di pannello.

(<sup>2</sup>): Le deformazioni sono stampate a meno del fattore  $10^{-3}$ ; esse si riferiscono alla verifica considerando quali sollecitazioni di progetto  $M_{x,d}=M_x \pm |M_{xy}|$ ,  $M_{y,d}=M_y \pm |M_{xy}|$  scegliendo il segno in modo tale da rendere massimo in valore assoluto il relativo momento flettente, le sollecitazioni stampate si riferiscono alle sollecitazioni in una data combinazione riferite al sistema locale del pannello

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Muro : 9 - Nodi: [63-62-162-163], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=116.738$  [11-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	-3085.97	36654.61	5370.09	301.89	2614.78	1332.48	20.11	20.11	11-I-3	1.6
1	-9.94	12.03	-485.04	53.69	756.53	83.64	20.11	20.11	11-VII-3	15

Muro : 10 - Nodi: [62-61-161-162], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=168.778$  [11-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	-3834.28	36650.62	5209.25	352.34	2618.21	1320.35	20.11	20.11	11-I-3	1.6
1	-32.04	4112.63	-487.44	108.17	846.28	-16.65	20.11	20.11	11-VII-3	15

Muro : 28 - Nodi: [61-60-160-161], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=157.945$  [11-VII-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	-4283.11	36642.63	5264.31	351.48	2618.80	1323.71	20.11	20.11	11-VII-1	1.6
1	-131.96	4330.62	144.39	110.99	836.28	-19.93	20.11	20.11	11-VII-3	15

Muro : 30 - Nodi: [60-59-159-160], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=136.295$  [11-VII-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	-4202.64	36655.24	5318.23	350.68	2619.31	1324.18	20.11	20.11	11-VII-1	1.6
1	-137.04	4286.05	444.10	110.33	832.07	-17.76	20.11	20.11	11-I-3	16

Muro : 39 - Nodi: [58-57-157-158], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=359.258$  [11-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	-3274.17	36630.59	5357.56	352.53	2617.85	1322.25	20.11	20.11	11-I-3	1.6
1	-72.81	4363.88	694.54	110.78	836.69	-17.77	20.11	20.11	11-VII-1	15

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Muro : 42 - Nodi: [59-58-158-159], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=150.082$  [11-VII-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	-3820.70	36649.46	5347.67	351.07	2619.18	1324.25	20.11	20.11	11-VII-1	1.6
1	-126.39	4326.23	605.66	110.86	837.59	-12.91	20.11	20.11	11-VII-1	15

Muro : 47 - Nodi: [57-56-156-157], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=585.539$  [11-II-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	-2686.60	36583.37	5340.31	353.47	2616.88	1326.21	20.11	20.11	11-VII-3	1.6
1	0.85	4404.04	732.54	110.37	832.59	-17.10	20.11	20.11	11-VII-1	16

Muro : 64 - Nodi: [54-53-153-154], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=137.276$  [11-I-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	-646.87	36666.99	5368.11	352.94	2617.94	1326.89	20.11	20.11	11-I-1	1.6
1	292.81	4402.52	726.50	110.72	836.24	-7.43	20.11	20.11	11-VII-3	16

Muro : 72 - Nodi: [55-54-154-155], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=149.433$  [11-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	-1240.52	36642.98	5359.39	351.00	2619.05	1327.15	20.11	20.11	11-VII-3	1.6
1	199.11	4411.85	775.07	110.60	834.99	-7.96	20.11	20.11	11-VII-3	16

Muro : 75 - Nodi: [56-55-155-156], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=215.420$  [11-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	-1937.24	36614.35	5351.10	351.29	2618.67	1326.97	20.11	20.11	11-VII-3	1.6
1	72.77	4443.98	738.24	110.24	831.19	-16.04	20.11	20.11	11-VII-1	16

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Muro : 100 - Nodi: [52-51-151-152], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45,  $\zeta_e=143.053$  [11-I-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	900.83	36691.79	5569.39	336.26	2618.23	1329.50	20.11	20.11	11-VII-1	1.6
1	494.66	4255.75	862.74	112.32	842.97	-8.11	20.11	20.11	11-VII-3	15

Muro : 102 - Nodi: [51-50-150-151], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45,  $\zeta_e=294.268$  [11-VII-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	6123.40	24000.49	1659.30	-382.86	2711.44	897.83	20.11	20.11	11-VII-1	2.4
1	218.16	3906.85	772.64	105.44	860.04	-11.84	20.11	20.11	11-VII-1	15

Muro : 104 - Nodi: [53-52-152-153], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45,  $\zeta_e=147.033$  [11-I-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	-100.40	36661.38	5382.08	355.27	2618.41	1328.91	20.11	20.11	11-I-1	1.6
1	377.09	4374.29	711.42	110.88	835.83	-11.86	20.11	20.11	11-VII-3	16

Muro : 11 - Nodi: [31-131-130-30], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45,  $\zeta_e=150.140$  [11-I-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	18212.64	1550.44	2620.15	1453.90	-21.79	-654.91	20.11	11.31	11-I-1	1.8
1	54.21	-20.30	-257.45	-497.22	-31.73	-57.05	20.11	11.31	11-I-3	9.3

Muro : 12 - Nodi: [30-130-129-29], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45,  $\zeta_e=397.600$  [11-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	18252.75	1888.83	2565.69	1454.10	-30.63	-654.92	20.11	11.31	11-I-1	1.8
1	2098.14	3.72	-140.11	-532.72	-74.99	-0.02	20.11	11.31	11-I-3	9.9

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Muro : 29 - Nodi: [29-129-128-28], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=326.402$  [11-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	18251.4 8	- 2162.62	2600.21	- 1454.18	-27.57	-656.30	20.11	11.31	11-I-1	1.8
1	- 2173.56	-18.51	103.75	-516.23	-73.51	-4.52	20.11	11.31	11-I-3	10

Muro : 31 - Nodi: [28-128-127-27], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=315.199$  [11-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	18240.3 2	- 2171.10	2618.21	- 1454.78	-27.02	-657.33	20.11	11.31	11-I-1	1.8
1	- 2174.28	-47.30	222.18	-513.54	-74.04	-5.38	20.11	11.31	11-I-3	10

Muro : 41 - Nodi: [26-126-125-25], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=388.664$  [11-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	18259.0 0	- 1654.44	2646.64	- 1452.67	-27.60	-657.44	20.11	11.31	11-I-1	1.8
1	- 2207.81	-17.35	347.18	-512.32	-73.88	-6.11	20.11	11.31	11-I-3	10

Muro : 48 - Nodi: [27-127-126-26], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=331.609$  [11-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	18243.0 1	- 1975.49	2632.68	- 1454.07	-27.39	-657.52	20.11	11.31	11-I-1	1.8
1	- 2186.76	-41.84	300.07	-512.86	-73.95	-5.79	20.11	11.31	11-I-3	10

Muro : 49 - Nodi: [25-125-124-24], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=482.547$  [11-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	18284.3 2	- 1284.67	2663.75	- 1451.40	-25.18	-656.87	20.11	11.31	11-VII-1	1.8
1	- 2231.59	16.89	367.24	-511.04	-73.73	-6.34	20.11	11.31	11-I-3	10

Muro : 63 - Nodi: [22-122-121-21], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=268.626$  [11-I-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	18236.04	-525.08	2632.94	1454.96	-23.55	-658.75	20.11	11.31	11-I-3	1.8
1	2278.81	123.92	349.01	-512.61	-73.91	-7.11	20.11	11.31	11-I-3	10

Muro : 65 - Nodi: [24-124-123-23], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=341.464$  [11-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	18261.57	-887.11	2654.90	1453.64	-24.57	-657.19	20.11	11.31	11-I-3	1.8
1	2255.79	60.14	369.08	-511.19	-73.73	-6.67	20.11	11.31	11-I-3	10

Muro : 74 - Nodi: [23-123-122-22], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=372.602$  [11-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	18241.20	-756.86	2639.78	1454.89	-24.43	-658.20	20.11	11.31	11-I-3	1.8
1	2273.48	109.35	360.12	-512.03	-73.83	-6.93	20.11	11.31	11-I-3	10

Muro : 97 - Nodi: [21-121-120-20], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=294.281$  [11-I-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	18242.38	-236.78	2645.70	1454.98	-23.75	-659.74	20.11	11.31	11-I-3	1.8
1	2260.44	163.74	360.53	-513.58	-74.05	-7.24	20.11	11.31	11-I-3	10

Muro : 98 - Nodi: [20-120-119-19], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=372.499$  [11-I-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	18267.19	516.85	2793.55	1454.31	-16.07	-657.26	20.11	11.31	11-I-3	1.8
1	2180.77	231.22	463.99	-516.80	-74.58	-7.76	20.11	11.31	11-I-3	10



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Muro : 99 - Nodi: [19-119-118-18], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45,  $\zeta_e=19.545$  [11-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	11931.0 1	- 2951.83	791.25	- 1488.85	201.83	-520.11	20.11	11.31	11-I-3	2.1
1	- 2051.38	121.27	446.17	-522.18	-73.23	-6.15	20.11	11.31	11-I-3	10.0

Muro : 25 - Nodi: [78-77-177-178], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45,  $\zeta_e=225.952$  [11-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	- 1696.56	18221.4 4	2546.42	135.67	1071.26	525.66	11.31	20.11	11-VII-1	2.4
1	-273.80	- 2153.32	-269.12	-104.73	-800.25	-12.99	11.31	20.11	10	6.5

Muro : 26 - Nodi: [79-78-178-179], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45,  $\zeta_e=120.037$  [11-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	- 1538.24	18250.2 5	2678.39	116.00	1083.89	537.83	11.31	20.11	11-VII-3	2.4
1	-590.19	- 3877.96	-522.84	-63.71	-802.73	-51.40	11.31	20.11	10	6.3

Muro : 27 - Nodi: [77-76-176-177], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45,  $\zeta_e=180.940$  [11-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	- 1992.12	18329.0 9	2628.59	140.45	1068.62	524.15	11.31	20.11	11-I-3	2.4
1	-356.73	- 2171.41	127.44	-103.85	-790.70	-13.04	11.31	20.11	10	6.6

Muro : 37 - Nodi: [76-75-175-176], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45,  $\zeta_e=156.702$  [11-VII-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	- 1995.32	18359.7 0	2667.16	137.31	1070.61	525.09	11.31	20.11	11-VII-1	2.4
1	-370.70	- 2245.88	318.91	-103.47	-788.39	-13.26	11.31	20.11	10	6.6

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Muro : 38 - Nodi: [73-72-172-173], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=543.410$  [11-VII-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	-1388.58	18298.92	2675.50	136.70	1065.61	524.67	11.31	20.11	11-VII-1	2.4
1	-244.52	2329.18	371.12	-103.34	-787.69	-12.53	11.31	20.11	10	6.6

Muro : 40 - Nodi: [75-74-174-175], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=174.372$  [11-VII-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	-1866.05	18354.15	2684.95	136.76	1069.09	524.72	11.31	20.11	11-VII-1	2.4
1	-338.11	2280.60	398.16	-103.40	-788.01	-13.12	11.31	20.11	10	6.6

Muro : 61 - Nodi: [74-73-173-174], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=241.126$  [11-VII-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	-1675.89	18314.09	2675.63	140.37	1066.12	523.74	11.31	20.11	11-I-3	2.4
1	-289.40	2306.07	410.89	-103.37	-787.87	-12.87	11.31	20.11	10	6.6

Muro : 62 - Nodi: [70-69-169-170], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=177.801$  [11-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	-699.63	18219.98	2624.09	135.41	1070.27	527.24	11.31	20.11	11-VII-1	2.4
1	-286.47	2387.91	-14.15	-103.01	-786.18	-10.08	11.31	20.11	10	6.7

Muro : 66 - Nodi: [71-70-170-171], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=168.406$  [11-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	-634.20	18346.40	2690.60	137.15	1069.63	526.42	11.31	20.11	11-VII-3	2.4
1	-229.96	2373.51	151.78	-103.18	-786.95	-11.28	11.31	20.11	10	6.6

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Muro : 73 - Nodi: [72-71-171-172], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=284.795$  [11-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	-1002.91	18318.59	2679.46	137.50	1067.41	525.20	11.31	20.11	11-VII-3	2.4
1	-219.81	2351.77	283.70	-103.28	-787.42	-12.03	11.31	20.11	10	6.6

Muro : 86 - Nodi: [67-66-166-167], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=49.374$  [11-VII-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	-3067.07	12001.84	833.74	-21.88	1073.71	432.04	11.31	20.11	11-I-1	2.8
1	-377.18	1554.04	1086.31	-102.87	-788.76	-4.08	11.31	20.11	10	6.6

Muro : 101 - Nodi: [69-68-168-169], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=131.526$  [11-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	-125.83	18353.72	2698.26	138.11	1071.74	529.47	11.31	20.11	11-VII-3	2.4
1	-383.82	2356.35	-155.12	-102.83	-785.40	-8.20	11.31	20.11	10	6.7

Muro : 103 - Nodi: [68-67-167-168], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=128.023$  [11-VII-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	261.72	18376.76	2781.63	137.35	1072.98	532.23	11.31	20.11	11-VII-1	2.4
1	-439.90	1991.84	65.38	-103.07	-786.60	-6.31	11.31	20.11	10	6.6

**Verifica dei Muri (Stati limite esercizio)**

Scenario di calcolo: **ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO**

**Simbologia**

P.	Numero pannello
Nx [MPa]	Sforzo normale in direzione x
Ny [MPa]	Sforzo normale in direzione y
Nxy [MPa]	Sforzo tagliante in direzione xy
Mx [daN]	Momento flettente in direzione x
My [daN]	Momento flettente in direzione y
Mxy [daN]	Momento torcente
Afx [cmq/m]	Area acciaio in direzione x per metro lineare
Afy [cmq/m]	Area acciaio in direzione y per metro lineare
$\sigma_c$ [MPa]	Tensione nel calcestruzzo compresso
$\sigma_f$ [MPa]	Tensione nell'acciaio
$\sigma_{ct}$ [MPa]	Tensione nel calcestruzzo teso
$\sigma_{sct}$ [MPa]	Tensione nel calcestruzzo teso (quando richiesto dalla verifica)
$\sigma_{sca}$ [MPa]	Tensione ammissibile nel calcestruzzo
$\sigma_{sfa}$ [MPa]	Tensione ammissibile nell'acciaio
$\sigma_{scta}$ [MPa]	Tensione ammissibile nel calcestruzzo teso
Cbc	Combinazione generatore della tensione nel cls compresso
Cbct	Combinazione generatore della tensione nel cls teso
Cbf	Combinazione generatore della tensione nell'acciaio
Cb	Combinazione
$\sigma_{fmed}$ [MPa]	Tensione media dell'acciaio
Wd [mm]	Apertura delle fessure
Wk [mm]	Apertura caratteristica delle fessure
Wamm_Freq [mm]	Apertura ammissibile delle fessure per combinazione Frequente
Wamm_Qp [mm]	Apertura ammissibile delle fessure per combinazione Quasi Permanente
Wamm_Rara [mm]	Apertura ammissibile delle fessure per combinazione Rara
Cs	Coefficiente di sicurezza definito come minimo di $\sigma_{fmed}/\sigma_f$ tra acciaio e calcestruzzo oppure Wamm/Wk

Muro [Platea]: 1 - Nodi: [79-78-62-63] Pann=16Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
10	31.42	31.42	-0.10	3.73	18	18	Si	96
8	31.42	31.42	-0.03	6.40	18	18	Si	56

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
10	31.42	31.42	-0.08	5.06	22	22	Si	71
8	31.42	31.42	-0.03	7.51	22	22	Si	48

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	-0.0	0.0	-148.98	-94.01	-46.30	7.51	0.012	0.012	22 (Qp)	Si	16
8	0.0	-0.0	0.0	-137.34	-83.13	-41.28	6.87	0.011	0.011	21 (Fr)	Si	27

Muro [Platea]: 2 - Nodi: [78-77-61-62] Pann=16Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
10	31.42	31.42	-0.11	3.74	18	18	Si	96
8	31.42	31.42	-0.04	6.05	18	18	Si	60

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
10	31.42	31.42	-0.08	5.29	22	22	Si	68
8	31.42	31.42	-0.04	7.36	22	22	Si	49

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	-0.0	0.0	-139.69	-114.27	-51.25	7.36	0.012	0.012	22 (Qp)	Si	17
8	0.0	-0.0	0.0	-126.42	-104.41	-47.71	6.61	0.011	0.011	21 (Fr)	Si	28

Muro [Platea]: 3 - Nodi: [30-29-13-14] Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.01	9.42	13	18	Si	38
8	31.42	31.42	-0.00	11.92	15	18	Si	30

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	31.42	31.42	0.00	10.28	22	22	Si	35
12	31.42	31.42	0.00	13.12	22	22	Si	27

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
16	0.1	0.0	0.0	-193.67	1.26	-49.55	12.47	0.022	0.022	22 (Qp)	Si	9.1
16	0.1	0.0	0.0	-184.45	0.67	-47.20	11.91	0.021	0.021	20 (Fr)	Si	14

Muro [Platea]: 4 - Nodi: [31-30-14-15] Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
5	31.42	31.42	-0.01	7.17	15	18	Si	50
16	31.42	31.42	-0.00	9.82	15	18	Si	37

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	31.42	31.42	0.00	7.37	22	22	Si	49
16	31.42	31.42	0.00	10.85	22	22	Si	33

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
16	0.0	0.0	0.0	-235.72	-9.01	-40.60	10.85	0.017	0.017	22 (Qp)	Si	12
16	0.0	0.0	0.0	-227.34	-9.43	-38.26	10.37	0.016	0.016	21 (Fr)	Si	19

Muro [Platea]: 5 - Nodi: [63-62-46-47] Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
11	31.42	31.42	-0.06	5.06	18	18	Si	71
5	31.42	31.42	-0.02	6.44	18	18	Si	56

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
11	31.42	31.42	-0.05	6.38	22	22	Si	56
5	31.42	31.42	-0.04	7.89	22	22	Si	46

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
5	0.0	-0.0	0.0	-157.56	-112.73	-58.97	7.89	0.013	0.013	22 (Qp)	Si	16
5	0.0	-0.0	0.0	-145.93	-103.58	-57.36	7.24	0.012	0.012	21 (Fr)	Si	26

Muro [Platea]: 6 - Nodi: [62-61-45-46] Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
11	31.42	31.42	-0.06	5.66	18	18	Si	64
12	31.42	31.42	-0.03	6.51	18	18	Si	55

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.05	7.66	22	22	Si	47
16	31.42	31.42	-0.03	8.03	22	22	Si	45

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
16	0.0	-0.0	0.0	-148.82	62.65	-85.47	8.03	0.013	0.013	22 (Qp)	Si	15
16	0.0	-0.0	0.0	-134.09	73.44	-81.44	7.27	0.012	0.012	21 (Fr)	Si	25

Muro [Platea]: 7 - Nodi: [46-45-29-30]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.06	8.78	18	18	Si	41

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.05	9.99	22	22	Si	36

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
6	0.0	0.0	0.0	-196.45	-138.35	-82.76	9.99	0.016	0.016	22 (Qp)	Si	12
6	0.0	-0.0	0.0	-184.45	-134.51	-77.50	9.33	0.015	0.015	21 (Fr)	Si	20

Muro [Platea]: 8 - Nodi: [47-46-30-31]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.06	7.73	18	18	Si	47
8	31.42	31.42	-0.03	7.91	18	18	Si	46

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.05	8.33	22	22	Si	43
8	31.42	31.42	-0.02	8.95	22	22	Si	40

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	0.0	0.0	-180.19	-85.20	-80.47	8.95	0.014	0.014	22 (Qp)	Si	14
8	0.0	0.0	0.0	-168.38	-79.30	-75.08	8.34	0.013	0.013	21 (Fr)	Si	22

Muro : 9 - Nodi: [63-62-162-163], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

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Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}[MPa]=22.41$   $\sigma_{fa}[MPa]=360.00$

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	20.11	20.11	-0.23	0.03	18	15	Si	96
8	20.11	20.11	-0.00	7.82	16	18	Si	46

Combinazione QP:  $\sigma_{ca}[MPa]=16.81$   $\sigma_{fa}[MPa]=360.00$

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	20.11	20.11	-0.15	-0.33	22	22	Si	>100
8	20.11	20.11	0.00	7.29	22	22	Si	49

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	0.0	-0.0	-6.74	-2.47	-7.45	7.29	0.020	0.020	22 (Qp)	Si	10
8	0.0	0.0	-0.0	-6.38	-2.33	-7.02	7.55	0.020	0.020	19 (Fr)	Si	15

Muro : 10 - Nodi: [62-61-161-162], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}[MPa]=22.41$   $\sigma_{fa}[MPa]=360.00$

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	20.11	-0.23	-0.31	18	18	Si	98
13	20.11	20.11	-0.16	2.15	18	15	Si	>100

Combinazione QP:  $\sigma_{ca}[MPa]=16.81$   $\sigma_{fa}[MPa]=360.00$

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	20.11	-0.11	-1.38	22	22	Si	>100
8	20.11	20.11	-0.05	0.55	22	22	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	-0.1	0.0	0.0	-5.86	-0.86	-16.13	0.55	0.001	0.001	22 (Qp)	Si	>100
8	-0.0	0.0	0.0	-5.74	-0.84	-15.35	0.44	0.001	0.001	21 (Fr)	Si	>100

Muro : 11 - Nodi: [31-131-130-30], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}[MPa]=22.41$   $\sigma_{fa}[MPa]=360.00$

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	20.11	11.31	-0.45	6.95	18	18	Si	50
14	20.11	11.31	-0.22	10.58	15	18	Si	34

Combinazione QP:  $\sigma_{ca}[MPa]=16.81$   $\sigma_{fa}[MPa]=360.00$

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
13	20.11	11.31	-0.58	8.87	22	22	Si	29

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
13	-0.1	-0.0	0.0	-205.27	8.41	83.02	8.87	0.007	0.007	22 (Qp)	Si	27
14	0.0	0.0	-0.0	-14.31	-12.28	14.26	8.24	0.013	0.013	19 (Fr)	Si	23

Muro : 12 - Nodi: [30-130-129-29], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
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Armatura a maglia doppia, Stampa elementi piu' gravosi  
Combinazione Rara:  $\sigma_{ca}[MPa]=22.41$   $\sigma_{fa}[MPa]=360.00$

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	20.11	11.31	-0.45	7.18	18	18	Si	50

Combinazione QP:  $\sigma_{ca}[MPa]=16.81$   $\sigma_{fa}[MPa]=360.00$

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
13	20.11	11.31	-0.53	4.52	22	22	Si	32

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
13	-0.1	-0.1	0.0	-203.20	-3.13	101.85	4.52	0.004	0.004	22 (Qp)	Si	57
13	-0.1	-0.1	0.0	-203.21	-3.17	101.66	4.52	0.004	0.004	19 (Fr)	Si	85

Muro [Platea]: 13 - Nodi: [64-63-47-48]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi  
Combinazione Rara:  $\sigma_{ca}[MPa]=22.41$   $\sigma_{fa}[MPa]=360.00$

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
5	31.42	31.42	-0.05	0.69	18	18	Si	>100
16	31.42	31.42	-0.02	4.09	18	18	Si	88

Combinazione QP:  $\sigma_{ca}[MPa]=16.81$   $\sigma_{fa}[MPa]=360.00$

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
5	31.42	31.42	-0.04	0.83	22	22	Si	>100
16	31.42	31.42	-0.02	4.75	22	22	Si	76

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
16	0.0	-0.0	0.0	-111.99	23.91	-59.68	4.75	0.007	0.007	22 (Qp)	Si	28
16	0.0	-0.0	0.0	-102.22	32.36	-52.91	4.40	0.007	0.007	21 (Fr)	Si	45

Muro [Platea]: 14 - Nodi: [32-31-15-16]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi  
Combinazione Rara:  $\sigma_{ca}[MPa]=22.41$   $\sigma_{fa}[MPa]=360.00$

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
14	31.42	31.42	-0.04	4.64	18	18	Si	78
16	31.42	31.42	-0.00	4.99	18	18	Si	72

Combinazione QP:  $\sigma_{ca}[MPa]=16.81$   $\sigma_{fa}[MPa]=360.00$

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
14	31.42	31.42	-0.04	5.24	22	22	Si	69
16	31.42	31.42	0.00	5.51	22	22	Si	65

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
16	0.0	0.0	0.0	-131.46	-7.84	-34.85	5.51	0.008	0.008	22 (Qp)	Si	24
16	0.0	0.0	0.0	-124.72	-8.10	-31.98	5.18	0.008	0.008	21 (Fr)	Si	39

Muro [Platea]: 15 - Nodi: [48-47-31-32]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi  
Combinazione Rara:  $\sigma_{ca}[MPa]=22.41$   $\sigma_{fa}[MPa]=360.00$



P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
5	31.42	31.42	-0.03	2.47	18	18	Si	>100
8	31.42	31.42	-0.02	4.65	18	18	Si	77

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
5	31.42	31.42	-0.02	2.71	22	22	Si	>100
8	31.42	31.42	-0.01	5.21	22	22	Si	69

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	0.0	0.0	-123.02	-55.13	-42.66	5.21	0.008	0.008	22 (Qp)	Si	26
8	0.0	0.0	0.0	-114.41	-48.13	-35.72	4.84	0.007	0.007	21 (Fr)	Si	41

Muro [Platea]: 16 - Nodi: [80-79-63-64]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
14	31.42	31.42	-0.06	3.19	18	18	Si	>100
13	31.42	31.42	-0.03	3.60	18	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
14	31.42	31.42	-0.05	4.00	22	22	Si	90
13	31.42	31.42	-0.02	4.48	22	22	Si	80

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
11	0.0	-0.0	0.0	-29.48	131.34	-27.13	1.65	0.003	0.003	22 (Qp)	Si	72
11	0.0	-0.0	0.0	-26.94	133.28	-24.83	1.52	0.003	0.003	21 (Fr)	Si	>100

Muro [Platea]: 17 - Nodi: [77-76-60-61]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
10	31.42	31.42	-0.11	3.37	18	18	Si	>100
8	31.42	31.42	-0.05	5.79	18	18	Si	62

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
10	31.42	31.42	-0.09	5.04	22	22	Si	71
8	31.42	31.42	-0.05	7.31	22	22	Si	49

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	-0.0	0.0	-147.32	-142.15	-58.86	7.31	0.012	0.012	22 (Qp)	Si	17
8	0.0	-0.0	0.0	-132.15	-131.19	-56.10	6.49	0.010	0.010	21 (Fr)	Si	29

Muro [Platea]: 18 - Nodi: [45-44-28-29]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

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P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.06	7.69	18	18	Si	47
2	31.42	31.42	-0.03	8.07	18	18	Si	45

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.05	9.05	22	22	Si	40
2	31.42	31.42	-0.02	9.40	22	22	Si	38

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
2	0.0	0.0	0.0	-186.30	-95.86	-70.61	9.40	0.015	0.015	22 (Qp)	Si	13
2	0.0	0.0	0.0	-174.00	-90.12	-65.42	8.69	0.014	0.014	21 (Fr)	Si	21

Muro [Platea]: 19 - Nodi: [29-28-12-13]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.04	10.18	18	18	Si	35
4	31.42	31.42	-0.01	10.23	18	18	Si	35

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.02	11.60	22	22	Si	31
4	31.42	31.42	-0.00	11.60	22	22	Si	31

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	0.0	0.0	0.0	-288.56	-13.33	-53.96	11.60	0.017	0.017	22 (Qp)	Si	12
4	0.0	0.0	0.0	-276.97	-13.65	-51.00	11.02	0.016	0.016	20 (Fr)	Si	19

Muro [Platea]: 20 - Nodi: [61-60-44-45]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
7	31.42	31.42	-0.06	5.28	18	18	Si	68
4	31.42	31.42	-0.04	6.24	18	18	Si	58

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.06	7.59	22	22	Si	47
4	31.42	31.42	-0.03	7.87	22	22	Si	46

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	0.0	-0.0	0.0	-146.38	62.89	-86.74	7.87	0.013	0.013	22 (Qp)	Si	15
4	0.0	-0.0	0.0	-133.03	73.57	-82.28	7.10	0.012	0.012	21 (Fr)	Si	26

Muro [Platea]: 21 - Nodi: [94-93-77-78]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

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P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.00	5.24	18	18	Si	69
4	31.42	31.42	-0.00	5.33	18	18	Si	68

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.00	6.31	22	22	Si	57
7	31.42	31.42	0.00	6.38	22	22	Si	56

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	0.0	-106.96	2.31	-0.15	6.27	0.011	0.011	22 (Qp)	Si	19
1	0.0	0.0	0.0	-95.22	2.13	-0.38	5.60	0.010	0.010	21 (Fr)	Si	31

Muro [Platea]: 22 - Nodi: [96-95-79-80]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.01	4.41	18	18	Si	82
7	31.42	31.42	-0.00	4.43	18	18	Si	81

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.01	5.20	22	22	Si	69

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	-0.0	0.0	-113.65	24.04	-96.08	5.20	0.008	0.008	22 (Qp)	Si	25
8	0.0	-0.0	0.0	-105.67	24.39	-94.13	4.80	0.007	0.007	21 (Fr)	Si	40

Muro [Platea]: 23 - Nodi: [93-92-76-77]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.00	4.86	18	18	Si	74
1	31.42	31.42	-0.00	5.19	15	18	Si	69

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.00	6.05	22	22	Si	60
1	31.42	31.42	0.00	6.31	22	22	Si	57

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	0.0	-107.20	2.70	-0.19	6.31	0.011	0.011	22 (Qp)	Si	19
1	0.0	0.0	0.0	-93.44	2.49	-0.37	5.53	0.009	0.009	21 (Fr)	Si	32

Muro [Platea]: 24 - Nodi: [95-94-78-79]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.01	8.03	18	18	Si	45

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Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.01	9.09	22	22	Si	40

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
2	0.0	-0.0	0.0	-163.70	19.88	-22.09	9.09	0.015	0.015	22 (Qp)	Si	13
2	0.0	-0.0	0.0	-152.90	20.54	-20.60	8.48	0.014	0.014	21 (Fr)	Si	21

Muro : 25 - Nodi: [78-77-177-178], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	11.31	20.11	-1.59	29.81	18	18	Si	12
16	11.31	20.11	-1.58	29.82	18	18	Si	12

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	11.31	20.11	-0.52	4.26	22	22	Si	32

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.1	-0.1	0.1	-4.35	-200.90	95.60	4.26	0.003	0.003	22 (Qp)	Si	60
4	-0.1	-0.1	0.1	-4.42	-200.90	95.69	4.26	0.003	0.003	20 (Fr)	Si	91

Muro : 26 - Nodi: [79-78-178-179], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	11.31	20.11	-1.66	36.13	18	18	Si	10.0

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	11.31	20.11	-0.58	8.98	22	22	Si	29
8	11.31	20.11	-0.05	9.55	22	22	Si	38

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.0	-0.1	0.0	7.50	-206.13	82.06	8.98	0.008	0.008	22 (Qp)	Si	27
8	0.0	0.0	-0.0	-14.52	-14.89	12.22	9.80	0.016	0.016	19 (Fr)	Si	19

Muro : 27 - Nodi: [77-76-176-177], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	11.31	20.11	-1.58	29.82	18	18	Si	12

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	11.31	20.11	-0.52	4.10	22	22	Si	33

Verifica aperture fessure:Wamm\_Freq[mm]=0.300 Wamm\_Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.1	-0.1	0.1	-8.46	-198.80	94.74	4.10	0.003	0.003	22 (Qp)	Si	63
4	-0.1	-0.1	0.1	-8.45	-198.80	94.83	4.10	0.003	0.003	19 (Fr)	Si	94

Muro : 28 - Nodi: [61-60-160-161], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	20.11	20.11	-0.23	-0.31	18	18	Si	98
1	20.11	20.11	-0.16	2.03	18	15	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	20.11	20.11	-0.11	-1.43	22	22	Si	>100
8	20.11	20.11	-0.07	0.38	22	22	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	-0.1	0.0	0.0	-2.78	-0.40	-19.94	0.38	0.001	0.001	22 (Qp)	Si	>100
12	-0.1	0.0	0.0	-2.42	-0.29	-19.67	0.37	0.001	0.001	19 (Fr)	Si	>100

Muro : 29 - Nodi: [29-129-128-28], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	20.11	11.31	-0.44	6.05	18	18	Si	51

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	11.31	-0.53	4.42	22	22	Si	32
13	20.11	11.31	-0.53	4.43	22	22	Si	32

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
13	-0.1	-0.1	0.1	-203.63	-7.11	103.92	4.43	0.003	0.003	22 (Qp)	Si	58
13	-0.1	-0.1	0.1	-203.62	-7.08	103.71	4.42	0.003	0.003	19 (Fr)	Si	87

Muro : 30 - Nodi: [60-59-159-160], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	20.11	20.11	-0.23	-0.32	18	18	Si	98
1	20.11	20.11	-0.16	1.76	18	15	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	20.11	20.11	-0.11	-1.42	22	22	Si	>100
12	20.11	20.11	-0.06	0.41	22	22	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
12	-0.1	0.0	0.0	-1.02	-0.10	-21.97	0.41	0.001	0.001	22 (Qp)	Si	>100
12	-0.1	0.0	0.0	-1.20	-0.12	-21.26	0.41	0.001	0.001	20 (Fr)	Si	>100

Muro : 31 - Nodi: [28-128-127-27], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	20.11	11.31	-0.43	5.61	18	18	Si	52

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	11.31	-0.53	4.42	22	22	Si	32

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
13	-0.1	-0.1	0.1	-203.67	-7.60	104.02	4.41	0.003	0.003	19 (Fr)	Si	87
16	-0.1	-0.1	-0.0	-203.72	-7.82	-89.69	4.42	0.003	0.003	22 (Qp)	Si	58

Muro [Platea]: 32 - Nodi: [28-27-11-12]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.04	6.26	18	18	Si	58

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.03	7.81	22	22	Si	46

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	0.0	-165.81	-89.16	-122.75	7.44	0.011	0.011	22 (Qp)	Si	17
1	0.0	0.0	0.0	-152.91	-82.92	-117.46	6.75	0.010	0.010	20 (Fr)	Si	29

Muro [Platea]: 33 - Nodi: [44-43-27-28]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.06	5.63	18	18	Si	64
2	31.42	31.42	-0.02	5.99	18	18	Si	60

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.05	7.07	22	22	Si	51
2	31.42	31.42	-0.02	7.43	22	22	Si	48

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
2	0.0	0.0	0.0	-152.13	-104.80	-79.02	7.43	0.012	0.012	22 (Qp)	Si	17
2	0.0	0.0	0.0	-138.96	-98.69	-74.41	6.70	0.011	0.011	20 (Fr)	Si	28

Muro [Platea]: 34 - Nodi: [76-75-59-60]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
10	31.42	31.42	-0.11	2.58	18	18	Si	>100
8	31.42	31.42	-0.05	5.04	18	18	Si	71

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
10	31.42	31.42	-0.09	4.29	22	22	Si	84
8	31.42	31.42	-0.06	6.64	22	22	Si	54

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	-0.0	0.0	-137.38	-161.67	-63.84	6.64	0.011	0.011	22 (Qp)	Si	19
8	0.0	-0.0	0.0	-121.38	-149.76	-61.46	5.78	0.009	0.009	19 (Fr)	Si	33

Muro [Platea]: 35 - Nodi: [60-59-43-44]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
11	31.42	31.42	-0.06	3.63	18	18	Si	99
1	31.42	31.42	-0.01	4.94	18	18	Si	73

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.07	6.65	22	22	Si	54
5	31.42	31.42	-0.06	6.96	22	22	Si	52

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
5	0.0	0.0	0.0	-142.82	-193.45	-89.86	6.96	0.011	0.011	22 (Qp)	Si	18
5	0.0	0.0	0.0	-127.27	-182.91	-87.13	6.10	0.010	0.010	19 (Fr)	Si	31

Muro [Platea]: 36 - Nodi: [92-91-75-76]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.00	4.00	18	18	Si	90
1	31.42	31.42	0.00	4.71	13	18	Si	76

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.00	5.23	22	22	Si	69
1	31.42	31.42	0.00	5.91	22	22	Si	61

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	0.0	-100.34	2.78	-1.01	5.91	0.010	0.010	22 (Qp)	Si	20
1	0.0	0.0	0.0	-85.45	2.57	-1.13	5.08	0.009	0.009	21 (Fr)	Si	34

Muro : 37 - Nodi: [76-75-175-176], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	11.31	20.11	-1.58	29.80	18	18	Si	12

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	11.31	20.11	-0.52	4.09	22	22	Si	33

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.1	-0.1	0.1	-7.81	-198.65	94.08	4.08	0.003	0.003	19 (Fr)	Si	95
16	-0.1	-0.1	-0.0	-7.64	-198.65	-95.23	4.09	0.003	0.003	22 (Qp)	Si	63

Muro : 38 - Nodi: [73-72-172-173], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	11.31	20.11	-1.58	29.78	18	18	Si	12

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	11.31	20.11	-0.52	4.08	22	22	Si	33

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.1	-0.1	0.1	-7.45	-198.58	93.82	4.07	0.003	0.003	20 (Fr)	Si	95
16	-0.1	-0.1	-0.0	-7.37	-198.60	-95.17	4.08	0.003	0.003	22 (Qp)	Si	63

Muro : 39 - Nodi: [58-57-157-158], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	20.11	20.11	-0.23	-0.32	18	18	Si	98
1	20.11	20.11	-0.16	1.54	18	15	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	20.11	20.11	-0.11	-1.01	22	22	Si	>100
12	20.11	20.11	-0.03	0.42	22	22	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
12	-0.0	0.0	0.0	0.49	0.10	-22.31	0.42	0.001	0.001	22 (Qp)	Si	>100
12	-0.0	0.0	0.0	0.29	0.07	-21.93	0.42	0.001	0.001	19 (Fr)	Si	>100

Muro : 40 - Nodi: [75-74-174-175], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	11.31	20.11	-1.58	29.79	18	18	Si	12

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

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P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	11.31	20.11	-0.52	4.09	22	22	Si	33

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.1	-0.1	0.1	-7.61	-198.60	93.86	4.08	0.003	0.003	19 (Fr)	Si	95
16	-0.1	-0.1	-0.0	-7.54	-198.63	-95.30	4.09	0.003	0.003	22 (Qp)	Si	63

Muro : 41 - Nodi: [26-126-125-25], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	20.11	11.31	-0.43	5.45	18	18	Si	52
4	20.11	11.31	-0.42	17.51	18	15	Si	21

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	11.31	-0.53	4.42	22	22	Si	32

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
13	-0.1	-0.1	0.1	-203.72	-7.87	103.91	4.41	0.003	0.003	19 (Fr)	Si	87
16	-0.1	-0.1	-0.0	-203.74	-7.91	-90.02	4.42	0.003	0.003	22 (Qp)	Si	58

Muro : 42 - Nodi: [59-58-158-159], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	20.11	20.11	-0.23	-0.32	18	18	Si	98
1	20.11	20.11	-0.16	1.63	18	15	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	20.11	20.11	-0.11	-1.24	22	22	Si	>100
12	20.11	20.11	-0.04	0.42	22	22	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
12	-0.0	0.0	0.0	-0.09	0.02	-22.47	0.42	0.001	0.001	22 (Qp)	Si	>100
12	-0.0	0.0	0.0	-0.28	-0.00	-21.92	0.42	0.001	0.001	20 (Fr)	Si	>100

Muro [Platea]: 43 - Nodi: [27-26-10-11]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.04	3.64	18	18	Si	99

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.03	5.21	22	22	Si	69
1	31.42	31.42	0.00	5.33	22	22	Si	68

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σfmed	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
5	0.0	0.0	0.0	-102.75	-112.68	-111.79	5.06	0.008	0.008	22 (Qp)	Si	25
5	0.0	0.0	0.0	-89.67	-104.31	-108.74	4.37	0.007	0.007	19 (Fr)	Si	43

Muro [Platea]: 44 - Nodi: [75-74-58-59]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σca[MPa]=22.41 σfa[MPa]=360.00

P.	Afx	Afy	σc	σf	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
10	31.42	31.42	-0.11	1.46	18	18	Si	>100
8	31.42	31.42	-0.06	3.85	18	18	Si	93

Combinazione QP: σca[MPa]=16.81 σfa[MPa]=360.00

P.	Afx	Afy	σc	σf	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
10	31.42	31.42	-0.09	3.17	22	22	Si	>100
8	31.42	31.42	-0.07	5.45	22	22	Si	66

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σfmed	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	-0.0	0.0	-116.63	-175.49	-65.79	5.45	0.009	0.009	22 (Qp)	Si	23
8	0.0	-0.0	0.0	-100.52	-162.87	-63.99	4.59	0.007	0.007	19 (Fr)	Si	42

Muro [Platea]: 45 - Nodi: [59-58-42-43]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σca[MPa]=22.41 σfa[MPa]=360.00

P.	Afx	Afy	σc	σf	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
11	31.42	31.42	-0.06	2.11	18	18	Si	>100
13	31.42	31.42	-0.02	3.78	18	17	Si	95

Combinazione QP: σca[MPa]=16.81 σfa[MPa]=360.00

P.	Afx	Afy	σc	σf	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.07	5.31	22	22	Si	68
1	31.42	31.42	-0.03	5.69	22	22	Si	63

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σfmed	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
5	0.0	0.0	0.0	-120.41	-212.43	-92.29	5.68	0.009	0.009	22 (Qp)	Si	22
5	0.0	0.0	0.0	-104.79	-201.05	-90.05	4.82	0.008	0.008	19 (Fr)	Si	40

Muro [Platea]: 46 - Nodi: [43-42-26-27]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σca[MPa]=22.41 σfa[MPa]=360.00

P.	Afx	Afy	σc	σf	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.06	3.94	18	18	Si	91
2	31.42	31.42	-0.02	4.82	18	15	Si	75

Combinazione QP: σca[MPa]=16.81 σfa[MPa]=360.00

P.	Afx	Afy	σc	σf	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.04	5.20	22	22	Si	69
2	31.42	31.42	-0.01	5.52	22	22	Si	65

Verifica aperture fessure:Wamm\_Freq[mm]=0.300 Wamm\_Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
2	0.0	0.0	0.0	-116.46	-108.04	-78.89	5.52	0.009	0.009	22 (Qp)	Si	23
2	0.0	0.0	0.0	-103.15	-101.62	-75.15	4.78	0.007	0.007	19 (Fr)	Si	40

Muro : 47 - Nodi: [57-56-156-157], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	20.11	20.11	-0.23	-0.32	18	18	Si	98
16	20.11	20.11	-0.23	1.81	18	15	Si	98

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	20.11	20.11	-0.11	-0.79	22	22	Si	>100
12	20.11	20.11	-0.01	0.41	22	22	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
12	-0.0	0.0	0.0	0.83	0.14	-21.76	0.41	0.001	0.001	22 (Qp)	Si	>100
12	-0.0	0.0	0.0	0.63	0.11	-21.55	0.41	0.001	0.001	19 (Fr)	Si	>100

Muro : 48 - Nodi: [27-127-126-26], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	20.11	11.31	-0.43	5.49	18	18	Si	52
8	20.11	11.31	-0.34	14.24	18	15	Si	25

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	11.31	-0.53	4.42	22	22	Si	32

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
13	-0.1	-0.1	0.1	-203.71	-7.80	104.03	4.41	0.003	0.003	20 (Fr)	Si	87
16	-0.1	-0.1	-0.0	-203.73	-7.91	-89.83	4.42	0.003	0.003	22 (Qp)	Si	58

Muro : 49 - Nodi: [25-125-124-24], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	20.11	11.31	-0.43	5.42	18	18	Si	52
1	20.11	11.31	-0.42	17.54	18	15	Si	21

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	11.31	-0.53	4.42	22	22	Si	32

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
13	-0.1	-0.0	0.1	-203.72	-7.86	103.76	4.41	0.003	0.003	20 (Fr)	Si	87
16	-0.1	-0.0	-0.0	-203.73	-7.88	-90.20	4.42	0.003	0.003	22 (Qp)	Si	58

Muro [Platea]: 50 - Nodi: [26-25-9-10]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.03	1.79	18	18	Si	>100
1	31.42	31.42	-0.00	3.36	18	17	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.03	3.31	22	22	Si	>100
1	31.42	31.42	0.00	3.89	22	22	Si	93

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
13	0.0	0.0	0.0	-36.95	-91.12	-79.18	3.88	0.006	0.006	22 (Qp)	Si	34
13	0.0	0.0	0.0	-25.19	-84.51	-79.43	3.61	0.005	0.005	21 (Fr)	Si	55

Muro [Platea]: 51 - Nodi: [91-90-74-75]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.00	2.87	18	18	Si	>100
1	31.42	31.42	0.00	3.77	13	18	Si	96

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.00	4.09	22	22	Si	88
1	31.42	31.42	0.00	5.00	22	22	Si	72

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	0.0	-83.80	2.82	-1.49	5.00	0.009	0.009	22 (Qp)	Si	23
1	0.0	0.0	0.0	-68.56	2.62	-1.55	4.15	0.007	0.007	21 (Fr)	Si	42

Muro [Platea]: 52 - Nodi: [25-24-8-9]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.02	0.55	18	18	Si	>100
1	31.42	31.42	-0.01	1.41	18	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.02	1.95	22	22	Si	>100
1	31.42	31.42	0.00	3.96	22	22	Si	91

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
13	0.0	0.0	0.0	-24.49	-93.62	-74.44	3.96	0.006	0.006	22 (Qp)	Si	34
13	0.0	0.0	0.0	-13.14	-86.99	-75.54	3.69	0.006	0.006	21 (Fr)	Si	54

Muro [Platea]: 53 - Nodi: [42-41-25-26]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.05	4.07	18	18	Si	89
8	31.42	31.42	-0.02	4.26	18	18	Si	85

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.04	3.81	22	22	Si	94
8	31.42	31.42	-0.01	4.03	22	22	Si	89

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
2	0.0	0.0	0.0	-83.88	-110.31	-75.86	3.83	0.006	0.006	22 (Qp)	Si	34
6	0.0	0.0	0.0	-52.85	-145.44	-91.88	3.43	0.005	0.005	19 (Fr)	Si	62

Muro [Platea]: 54 - Nodi: [74-73-57-58]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
10	31.42	31.42	-0.11	0.65	18	18	Si	>100
8	31.42	31.42	-0.06	2.56	18	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
10	31.42	31.42	-0.09	1.96	22	22	Si	>100
8	31.42	31.42	-0.07	4.12	22	22	Si	87

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	-0.0	0.0	-92.08	-185.84	-65.76	4.12	0.006	0.006	22 (Qp)	Si	32
8	0.0	-0.0	0.0	-76.23	-172.82	-64.75	3.27	0.005	0.005	21 (Fr)	Si	61

Muro [Platea]: 55 - Nodi: [58-57-41-42]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
11	31.42	31.42	-0.06	0.90	18	17	Si	>100
13	31.42	31.42	-0.02	4.24	18	17	Si	85

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
5	31.42	31.42	-0.07	5.11	22	22	Si	70
13	31.42	31.42	-0.02	5.61	22	22	Si	64

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
9	0.0	0.0	0.0	-83.96	-227.71	-79.36	5.24	0.007	0.007	22 (Qp)	Si	27
9	0.0	0.0	0.0	-68.99	-215.83	-78.26	4.57	0.006	0.006	21 (Fr)	Si	47

Muro [Platea]: 56 - Nodi: [90-89-73-74]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

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P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.00	1.77	18	18	Si	>100
1	31.42	31.42	0.00	2.61	13	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.00	2.95	22	22	Si	>100
1	31.42	31.42	0.00	3.83	22	22	Si	94

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	0.0	-62.38	2.87	-1.55	3.83	0.007	0.007	22 (Qp)	Si	30
1	0.0	0.0	0.0	-47.23	2.68	-1.58	2.99	0.005	0.005	21 (Fr)	Si	57

Muro [Platea]: 57 - Nodi: [57-56-40-41]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
7	31.42	31.42	-0.06	0.55	18	18	Si	>100
1	31.42	31.42	-0.03	4.35	18	17	Si	83

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
5	31.42	31.42	-0.07	5.57	22	22	Si	65
13	31.42	31.42	-0.02	6.08	22	22	Si	59

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
9	0.0	0.0	0.0	-64.77	-238.29	-75.64	5.69	0.008	0.008	22 (Qp)	Si	25
9	0.0	0.0	0.0	-50.38	-226.33	-74.83	5.01	0.007	0.007	19 (Fr)	Si	43

Muro [Platea]: 58 - Nodi: [41-40-24-25]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.05	4.20	18	18	Si	86
8	31.42	31.42	-0.01	4.40	18	18	Si	82

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.04	3.97	22	22	Si	91
8	31.42	31.42	-0.00	4.17	22	22	Si	86

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
6	0.0	0.0	0.0	-45.89	-152.52	-91.25	4.02	0.006	0.006	22 (Qp)	Si	35
6	0.0	0.0	0.0	-34.09	-147.55	-90.47	3.57	0.005	0.005	19 (Fr)	Si	60

Muro [Platea]: 59 - Nodi: [89-88-72-73]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				

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P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
8	31.42	31.42	-0.00	0.99	18	18	Si	>100
1	31.42	31.42	0.00	1.55	13	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.00	2.12	22	22	Si	>100
1	31.42	31.42	0.00	2.72	22	22	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	0.0	-41.82	2.95	-1.21	2.72	0.005	0.005	22 (Qp)	Si	42
1	0.0	0.0	0.0	-27.01	2.77	-1.23	1.90	0.003	0.003	21 (Fr)	Si	87

Muro [Platea]: 60 - Nodi: [73-72-56-57]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.11	0.67	18	18	Si	>100
16	31.42	31.42	-0.04	1.71	18	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
10	31.42	31.42	-0.09	0.98	22	22	Si	>100
16	31.42	31.42	-0.03	3.50	22	22	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
16	0.0	0.0	0.0	-42.23	-129.47	-131.95	3.50	0.005	0.005	22 (Qp)	Si	41
16	0.0	0.0	0.0	-27.91	-117.63	-130.33	2.91	0.004	0.004	19 (Fr)	Si	74

Muro : 61 - Nodi: [74-73-173-174], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	11.31	20.11	-1.58	29.79	18	18	Si	12

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	11.31	20.11	-0.52	4.08	22	22	Si	33

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.1	-0.1	0.1	-7.53	-198.59	93.80	4.07	0.003	0.003	19 (Fr)	Si	95
16	-0.1	-0.1	-0.0	-7.47	-198.62	-95.28	4.08	0.003	0.003	22 (Qp)	Si	63

Muro : 62 - Nodi: [70-69-169-170], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	11.31	20.11	-1.58	29.78	18	18	Si	12

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

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P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	11.31	20.11	-0.52	4.07	22	22	Si	33

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.1	-0.1	0.1	-6.89	-198.49	94.66	4.07	0.003	0.003	22 (Qp)	Si	63
4	-0.1	-0.1	0.1	-6.91	-198.49	94.64	4.07	0.003	0.003	19 (Fr)	Si	95

Muro : 63 - Nodi: [22-122-121-21], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	20.11	11.31	-0.43	5.41	18	18	Si	52
1	20.11	11.31	-0.42	17.49	18	15	Si	21

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	11.31	-0.53	4.41	22	22	Si	32
13	20.11	11.31	-0.53	4.42	22	22	Si	32

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
13	-0.1	-0.0	0.1	-203.73	-7.89	103.35	4.42	0.003	0.003	22 (Qp)	Si	58
13	-0.1	-0.0	0.1	-203.72	-7.85	103.40	4.42	0.003	0.003	20 (Fr)	Si	87

Muro : 64 - Nodi: [54-53-153-154], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	20.11	-0.23	-0.32	18	18	Si	98
13	20.11	20.11	-0.16	1.32	18	15	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	20.11	-0.11	-0.86	22	22	Si	>100
8	20.11	20.11	-0.02	0.44	22	22	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	-0.0	0.0	0.0	2.23	0.26	-18.52	0.44	0.001	0.001	22 (Qp)	Si	>100
8	-0.0	0.0	0.0	2.07	0.24	-18.83	0.35	0.001	0.001	21 (Fr)	Si	>100

Muro : 65 - Nodi: [24-124-123-23], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	20.11	11.31	-0.43	5.40	18	18	Si	52
1	20.11	11.31	-0.42	17.52	18	15	Si	21

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	11.31	-0.53	4.41	22	22	Si	32



Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
13	-0.1	-0.0	0.1	-203.71	-7.82	103.63	4.41	0.003	0.003	20 (Fr)	Si	87
16	-0.1	-0.0	-0.0	-203.73	-7.85	-90.34	4.41	0.003	0.003	22 (Qp)	Si	58

Muro : 66 - Nodi: [71-70-170-171], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	11.31	20.11	-1.58	29.77	18	18	Si	12

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	11.31	20.11	-0.52	4.07	22	22	Si	33

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.1	-0.1	0.1	-7.15	-198.53	94.18	4.07	0.003	0.003	22 (Qp)	Si	63
4	-0.0	-0.1	0.1	-7.17	-198.53	94.18	4.07	0.003	0.003	19 (Fr)	Si	95

Muro [Platea]: 67 - Nodi: [23-22-6-7]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
15	31.42	31.42	-0.01	0.59	18	18	Si	>100
4	31.42	31.42	-0.01	4.63	18	13	Si	78

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.02	3.95	22	22	Si	91
1	31.42	31.42	0.00	4.09	22	22	Si	88

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	0.0	-28.55	-97.42	-107.73	4.09	0.006	0.006	22 (Qp)	Si	33
1	0.0	0.0	0.0	-17.50	-90.77	-106.58	3.82	0.006	0.006	19 (Fr)	Si	53

Muro [Platea]: 68 - Nodi: [24-23-7-8]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
15	31.42	31.42	-0.02	0.79	18	18	Si	>100
13	31.42	31.42	-0.00	1.49	15	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
5	31.42	31.42	-0.02	3.92	22	22	Si	92
1	31.42	31.42	0.00	4.04	22	22	Si	89

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
13	0.0	0.0	0.0	-21.98	-95.87	-70.59	4.03	0.006	0.006	22 (Qp)	Si	33
13	0.0	0.0	0.0	-11.02	-89.27	-72.50	3.77	0.006	0.006	21 (Fr)	Si	53

Muro [Platea]: 69 - Nodi: [56-55-39-40]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
7	31.42	31.42	-0.06	0.62	18	18	Si	>100
13	31.42	31.42	-0.03	1.98	18	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.07	6.19	22	22	Si	58
13	31.42	31.42	-0.02	6.63	22	22	Si	54

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
9	0.0	0.0	0.0	-55.49	-250.19	-70.77	6.19	0.009	0.009	22 (Qp)	Si	23
9	0.0	0.0	0.0	-41.70	-238.35	-70.59	5.52	0.008	0.008	19 (Fr)	Si	39

Muro [Platea]: 70 - Nodi: [40-39-23-24]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.05	4.35	18	18	Si	83
8	31.42	31.42	-0.01	4.55	18	18	Si	79

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.04	4.12	22	22	Si	87
8	31.42	31.42	-0.00	4.32	22	22	Si	83

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
6	0.0	0.0	0.0	-36.18	-154.47	-90.53	4.16	0.006	0.006	22 (Qp)	Si	34
6	0.0	0.0	0.0	-24.92	-149.50	-90.56	3.71	0.005	0.005	19 (Fr)	Si	58

Muro [Platea]: 71 - Nodi: [72-71-55-56]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.11	0.70	18	18	Si	>100
16	31.42	31.42	-0.04	2.22	18	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.09	0.97	22	22	Si	>100
16	31.42	31.42	-0.03	4.00	22	22	Si	90

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	0.0	0.0	0.0	-42.74	-132.47	-13.10	3.59	0.005	0.005	22 (Qp)	Si	40
16	0.0	0.0	0.0	-27.93	-128.67	-128.72	3.41	0.005	0.005	19 (Fr)	Si	63

Muro : 72 - Nodi: [55-54-154-155], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	20.11	-0.23	1.81	18	15	Si	98
8	20.11	20.11	-0.01	2.20	18	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	20.11	-0.11	-0.63	22	22	Si	>100
8	20.11	20.11	-0.01	0.38	22	22	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	-0.0	0.0	0.0	1.40	0.15	-20.11	0.38	0.001	0.001	22 (Qp)	Si	>100
8	0.0	0.0	0.0	1.21	0.13	-20.20	0.39	0.001	0.001	19 (Fr)	Si	>100

Muro : 73 - Nodi: [72-71-171-172], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	11.31	20.11	-1.58	29.77	18	18	Si	12

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	11.31	20.11	-0.52	4.07	22	22	Si	33

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.0	-0.1	0.1	-7.34	-198.56	93.93	4.07	0.003	0.003	19 (Fr)	Si	95
16	-0.1	-0.1	-0.0	-7.22	-198.58	-94.94	4.07	0.003	0.003	22 (Qp)	Si	63

Muro : 74 - Nodi: [23-123-122-22], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	20.11	11.31	-0.43	5.38	18	18	Si	52
1	20.11	11.31	-0.42	17.50	18	15	Si	21

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	11.31	-0.53	4.41	22	22	Si	32
13	20.11	11.31	-0.53	4.41	22	22	Si	32

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
13	-0.1	-0.0	0.1	-203.72	-7.84	103.51	4.41	0.003	0.003	22 (Qp)	Si	58
13	-0.1	-0.0	0.1	-203.71	-7.80	103.52	4.41	0.003	0.003	19 (Fr)	Si	87

Muro : 75 - Nodi: [56-55-155-156], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	20.11	20.11	-0.23	1.81	18	15	Si	98
12	20.11	20.11	-0.01	2.31	18	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	20.11	-0.11	-0.58	22	22	Si	>100
12	20.11	20.11	-0.01	0.38	22	22	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
12	-0.0	0.0	0.0	1.12	0.18	-20.93	0.38	0.001	0.001	22 (Qp)	Si	>100
12	0.0	0.0	0.0	0.93	0.15	-20.90	0.38	0.001	0.001	19 (Fr)	Si	>100

Muro [Platea]: 76 - Nodi: [87-86-70-71]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
7	31.42	31.42	-0.00	1.50	17	18	Si	>100
8	31.42	31.42	-0.00	1.54	18	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.00	2.52	22	22	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	0.0	0.0	-56.16	-7.51	-32.07	2.52	0.004	0.004	22 (Qp)	Si	52
8	0.0	0.0	0.0	-43.16	-7.18	-32.61	1.80	0.003	0.003	21 (Fr)	Si	>100

Muro [Platea]: 77 - Nodi: [88-87-71-72]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.00	0.82	18	18	Si	>100
1	31.42	31.42	0.00	0.86	13	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.00	1.88	22	22	Si	>100
1	31.42	31.42	0.00	1.97	22	22	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	0.0	-27.71	3.05	-0.52	1.97	0.004	0.004	22 (Qp)	Si	56
1	0.0	0.0	0.0	-13.32	2.88	-0.53	1.18	0.002	0.002	21 (Fr)	Si	>100

Muro [Platea]: 78 - Nodi: [71-70-54-55]Pann=16Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.11	0.74	18	18	Si	>100

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

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P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
16	31.42	31.42	-0.04	2.95	18	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.09	1.03	22	22	Si	>100
16	31.42	31.42	-0.03	4.70	22	22	Si	77

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
12	0.0	0.0	0.0	-59.43	-220.88	-78.06	4.04	0.005	0.005	22 (Qp)	Si	36
12	0.0	0.0	0.0	-45.85	-208.09	-78.43	3.48	0.005	0.005	19 (Fr)	Si	64

Muro [Platea]: 79 - Nodi: [70-69-53-54]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.11	0.96	18	18	Si	>100
16	31.42	31.42	-0.04	3.93	18	18	Si	92

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.09	1.55	22	22	Si	>100
16	31.42	31.42	-0.03	5.59	22	22	Si	64

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
12	0.0	0.0	0.0	-85.21	-236.52	-77.26	4.86	0.007	0.007	22 (Qp)	Si	30
12	0.0	0.0	0.0	-72.57	-224.25	-78.15	4.32	0.006	0.006	19 (Fr)	Si	51

Muro [Platea]: 80 - Nodi: [55-54-38-39]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.06	2.37	18	18	Si	>100
13	31.42	31.42	-0.03	2.76	18	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.07	6.86	22	22	Si	52
13	31.42	31.42	-0.01	7.37	22	22	Si	49

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
9	0.0	0.0	0.0	-60.27	-266.27	-64.33	6.86	0.010	0.010	22 (Qp)	Si	21
9	0.0	0.0	0.0	-47.15	-254.78	-64.73	6.19	0.009	0.009	19 (Fr)	Si	35

Muro [Platea]: 81 - Nodi: [22-21-5-6]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.02	1.35	18	18	Si	>100

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
1	31.42	31.42	-0.00	1.53	15	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.02	3.84	22	22	Si	94
1	31.42	31.42	0.00	4.06	22	22	Si	89

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	0.0	-30.78	-97.62	-105.54	4.06	0.006	0.006	22 (Qp)	Si	33
1	0.0	0.0	0.0	-20.24	-91.05	-105.21	3.80	0.006	0.006	19 (Fr)	Si	53

Muro [Platea]: 82 - Nodi: [39-38-22-23]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.05	4.50	18	18	Si	80
8	31.42	31.42	-0.01	4.69	18	18	Si	77

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.04	4.25	22	22	Si	85
8	31.42	31.42	0.00	4.43	22	22	Si	81

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
6	0.0	0.0	0.0	-26.69	-149.97	-92.03	3.83	0.005	0.005	19 (Fr)	Si	56
8	0.0	0.0	0.0	-36.91	-117.22	-106.75	4.43	0.006	0.006	22 (Qp)	Si	32

Muro [Platea]: 83 - Nodi: [86-85-69-70]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.00	3.50	18	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.00	4.37	22	22	Si	82

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	0.0	0.0	-90.06	-8.02	-27.77	4.37	0.007	0.007	22 (Qp)	Si	29
8	0.0	0.0	0.0	-78.27	-7.71	-28.57	3.72	0.006	0.006	21 (Fr)	Si	51

Muro [Platea]: 84 - Nodi: [54-53-37-38]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.06	3.27	18	18	Si	>100
13	31.42	31.42	-0.03	3.77	18	18	Si	95

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.08	7.71	22	22	Si	47
13	31.42	31.42	-0.00	8.29	22	22	Si	43

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
9	0.0	0.0	0.0	-84.19	-286.55	-54.09	7.71	0.011	0.011	22 (Qp)	Si	19
9	0.0	0.0	0.0	-71.97	-275.72	-54.98	7.07	0.010	0.010	19 (Fr)	Si	30

Muro [Platea]: 85 - Nodi: [38-37-21-22]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.05	4.61	18	18	Si	78
8	31.42	31.42	-0.01	4.72	18	18	Si	76

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.04	4.33	22	22	Si	83
2	31.42	31.42	0.00	4.43	22	22	Si	81

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
2	0.0	0.0	0.0	-30.78	-115.20	-69.74	4.43	0.006	0.006	22 (Qp)	Si	32
4	0.0	0.0	0.0	-32.76	-146.84	-91.00	3.88	0.005	0.005	19 (Fr)	Si	55

Muro : 86 - Nodi: [67-66-166-167], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	11.31	20.11	-1.64	35.48	18	18	Si	10

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	11.31	20.11	-0.57	8.37	22	22	Si	30

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
12	0.0	0.0	0.0	-10.87	-13.75	-9.67	7.50	0.012	0.012	22 (Qp)	Si	17
12	0.0	0.0	0.0	-9.71	-13.54	-8.78	6.88	0.011	0.011	21 (Fr)	Si	27

Muro [Platea]: 87 - Nodi: [20-19-3-4]Pann=16Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
5	31.42	31.42	-0.02	2.94	18	18	Si	>100
13	31.42	31.42	-0.01	3.14	18	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.03	4.20	22	22	Si	86

Verifica aperture fessure:Wamm\_Freq[mm]=0.300 Wamm\_Qp[mm]=0.200

P.	Nx MPa	Ny MPa	Nxy MPa	Mx daN	My daN	Mxy daN	$\sigma_{fmed}$ MPa	Wd mm	Wk mm	Cb	Ver	Cs
9	0.0	0.0	0.0	-82.73	-111.79	-49.39	4.20	0.007	0.007	22 (Qp)	Si	29
9	0.0	0.0	0.0	-75.54	-104.23	-52.75	3.81	0.006	0.006	21 (Fr)	Si	49

Muro [Platea]: 88 - Nodi: [85-84-68-69]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx cmq/m	Afy cmq/m	$\sigma_c$ MPa	$\sigma_f$ MPa	Cbc	Cbf	Ver	Cs
8	31.42	31.42	-0.00	7.24	18	18	Si	50

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx cmq/m	Afy cmq/m	$\sigma_c$ MPa	$\sigma_f$ MPa	Cbc	Cbf	Ver	Cs
8	31.42	31.42	-0.00	7.97	22	22	Si	45

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx MPa	Ny MPa	Nxy MPa	Mx daN	My daN	Mxy daN	$\sigma_{fmed}$ MPa	Wd mm	Wk mm	Cb	Ver	Cs
8	0.0	0.0	0.0	-155.25	-8.09	-19.21	7.97	0.013	0.013	22 (Qp)	Si	15
8	0.0	0.0	0.0	-145.33	-7.83	-20.18	7.41	0.012	0.012	21 (Fr)	Si	25

Muro [Platea]: 89 - Nodi: [21-20-4-5]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx cmq/m	Afy cmq/m	$\sigma_c$ MPa	$\sigma_f$ MPa	Cbc	Cbf	Ver	Cs
9	31.42	31.42	-0.02	2.91	18	17	Si	>100
1	31.42	31.42	-0.00	3.31	18	17	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx cmq/m	Afy cmq/m	$\sigma_c$ MPa	$\sigma_f$ MPa	Cbc	Cbf	Ver	Cs
9	31.42	31.42	-0.03	3.40	22	22	Si	>100
1	31.42	31.42	0.00	3.82	22	22	Si	94

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx MPa	Ny MPa	Nxy MPa	Mx daN	My daN	Mxy daN	$\sigma_{fmed}$ MPa	Wd mm	Wk mm	Cb	Ver	Cs
1	0.0	0.0	0.0	-46.76	-95.05	-101.82	3.82	0.006	0.006	22 (Qp)	Si	36
1	0.0	0.0	0.0	-36.88	-88.62	-102.32	3.56	0.005	0.005	19 (Fr)	Si	58

Muro [Platea]: 90 - Nodi: [52-51-35-36]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx cmq/m	Afy cmq/m	$\sigma_c$ MPa	$\sigma_f$ MPa	Cbc	Cbf	Ver	Cs
9	31.42	31.42	-0.06	8.42	18	18	Si	43
13	31.42	31.42	-0.01	8.53	18	18	Si	42

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx cmq/m	Afy cmq/m	$\sigma_c$ MPa	$\sigma_f$ MPa	Cbc	Cbf	Ver	Cs
5	31.42	31.42	-0.06	9.12	22	22	Si	39
9	31.42	31.42	-0.06	9.72	22	22	Si	37

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx MPa	Ny MPa	Nxy MPa	Mx daN	My daN	Mxy daN	$\sigma_{fmed}$ MPa	Wd mm	Wk mm	Cb	Ver	Cs
9	0.0	0.0	0.0	-203.71	-294.32	-22.24	9.72	0.015	0.015	22 (Qp)	Si	13
9	0.0	0.0	0.0	-195.16	-286.25	-23.90	9.22	0.015	0.015	21 (Fr)	Si	21



Muro [Platea]: 91 - Nodi: [53-52-36-37]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.06	7.33	18	17	Si	49
13	31.42	31.42	-0.03	7.90	18	17	Si	46

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.07	8.51	22	22	Si	42
13	31.42	31.42	0.00	9.02	22	22	Si	40

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	0.0	-36.83	-207.01	-103.74	7.84	0.011	0.011	19 (Fr)	Si	27
13	0.0	0.0	0.0	-177.11	-235.00	-0.84	9.02	0.013	0.013	22 (Qp)	Si	16

Muro [Platea]: 92 - Nodi: [68-67-51-52]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.08	7.48	18	18	Si	48
12	31.42	31.42	-0.07	9.17	18	18	Si	39

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
12	31.42	31.42	-0.06	10.06	22	22	Si	36
13	31.42	31.42	-0.01	10.10	22	22	Si	36

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
13	0.0	-0.0	0.0	-215.09	18.31	2.55	10.10	0.016	0.016	22 (Qp)	Si	13
13	0.0	-0.0	0.0	-209.24	17.82	3.15	9.66	0.015	0.015	21 (Fr)	Si	20

Muro [Platea]: 93 - Nodi: [37-36-20-21]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.04	4.48	18	18	Si	80
2	31.42	31.42	-0.00	4.65	17	18	Si	77

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.03	4.15	22	22	Si	87
2	31.42	31.42	0.00	4.33	22	22	Si	83

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
7	0.0	0.0	0.0	-85.57	1.03	-88.78	4.26	0.007	0.007	22 (Qp)	Si	29
7	0.0	0.0	0.0	-76.08	12.38	-92.15	3.73	0.006	0.006	21 (Fr)	Si	50

Muro [Platea]: 94 - Nodi: [69-68-52-53]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.10	2.62	18	18	Si	>100
13	31.42	31.42	-0.04	5.99	18	18	Si	60

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.08	3.92	22	22	Si	92
13	31.42	31.42	-0.02	7.20	22	22	Si	50

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
9	0.0	-0.0	0.0	-120.60	3.44	2.46	5.63	0.009	0.009	21 (Fr)	Si	34
13	0.0	-0.0	0.0	-189.03	17.88	8.39	7.20	0.010	0.010	22 (Qp)	Si	20

Muro [Platea]: 95 - Nodi: [84-83-67-68]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	8.87	18	18	Si	41
8	31.42	31.42	-0.00	9.95	18	18	Si	36

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	9.55	22	22	Si	38
8	31.42	31.42	-0.00	10.54	22	22	Si	34

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	0.0	0.0	-197.10	-8.08	-9.11	10.54	0.017	0.017	22 (Qp)	Si	11
8	0.0	0.0	0.0	-189.80	-7.87	-9.84	10.12	0.017	0.017	19 (Fr)	Si	18

Muro [Platea]: 96 - Nodi: [67-66-50-51]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.07	9.91	18	18	Si	36

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.07	10.60	22	22	Si	34

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	0.0	0.0	-221.91	-247.84	-2.69	10.60	0.017	0.017	22 (Qp)	Si	12
8	0.0	0.0	0.0	-213.13	-236.97	-5.95	10.19	0.016	0.016	19 (Fr)	Si	19

Muro : 97 - Nodi: [21-121-120-20], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	20.11	11.31	-0.43	5.63	18	18	Si	52
8	20.11	11.31	-0.34	14.45	18	15	Si	25

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	11.31	-0.53	4.43	22	22	Si	32

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
13	-0.1	-0.0	0.1	-203.77	-8.14	103.10	4.42	0.003	0.003	19 (Fr)	Si	87
16	-0.1	-0.1	-0.1	-203.85	-8.61	-91.39	4.43	0.003	0.003	22 (Qp)	Si	58

Muro : 98 - Nodi: [20-120-119-19], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	20.11	11.31	-0.44	6.28	18	18	Si	51
8	20.11	11.31	-0.34	15.14	18	15	Si	24

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	11.31	-0.53	4.46	22	22	Si	32

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
13	-0.1	-0.1	0.1	-203.84	-8.69	102.40	4.44	0.003	0.003	19 (Fr)	Si	87
16	-0.1	-0.1	-0.0	-203.74	-8.06	-92.00	4.46	0.003	0.003	22 (Qp)	Si	57

Muro : 99 - Nodi: [19-119-118-18], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	20.11	11.31	-0.45	6.67	18	18	Si	50
5	20.11	11.31	-0.35	15.46	18	15	Si	23

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	11.31	-0.58	8.91	22	22	Si	29
15	20.11	11.31	-0.05	10.33	22	22	Si	35

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
15	0.0	0.0	0.0	-14.46	-12.44	-8.82	10.33	0.018	0.018	22 (Qp)	Si	11
15	0.0	0.0	0.0	-14.26	-11.33	-7.82	9.69	0.017	0.017	21 (Fr)	Si	17

Muro : 100 - Nodi: [52-51-151-152], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	20.11	20.11	-0.23	-0.32	18	18	Si	98
1	20.11	20.11	-0.15	2.09	18	15	Si	>100

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

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Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	20.11	20.11	-0.11	-1.34	22	22	Si	>100
12	20.11	20.11	-0.06	0.46	22	22	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
12	-0.1	0.0	0.0	6.49	0.88	-10.24	0.46	0.001	0.001	22 (Qp)	Si	>100
12	-0.1	0.0	0.0	6.52	0.89	-10.66	0.45	0.001	0.001	19 (Fr)	Si	>100

Muro : 101 - Nodi: [69-68-168-169], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	11.31	20.11	-1.58	29.78	18	18	Si	12
4	11.31	20.11	-1.58	29.78	18	18	Si	12

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	11.31	20.11	-0.52	4.08	22	22	Si	33
4	11.31	20.11	-0.52	4.08	22	22	Si	33

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.1	-0.1	0.1	-6.69	-198.47	95.35	4.08	0.003	0.003	22 (Qp)	Si	63
4	-0.1	-0.1	0.1	-6.70	-198.47	95.32	4.08	0.003	0.003	19 (Fr)	Si	95

Muro : 102 - Nodi: [51-50-150-151], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
13	20.11	20.11	-0.24	-0.36	18	18	Si	95
12	20.11	20.11	0.00	7.02	13	18	Si	51

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
13	20.11	20.11	-0.17	-0.45	22	22	Si	>100
12	20.11	20.11	0.00	6.71	22	22	Si	54

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
12	0.0	0.0	0.0	4.14	1.33	-3.97	6.71	0.018	0.018	22 (Qp)	Si	11
12	0.0	0.0	0.0	4.35	1.42	-4.22	6.28	0.017	0.017	21 (Fr)	Si	18

Muro : 103 - Nodi: [68-67-167-168], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	11.31	20.11	-1.58	29.88	18	18	Si	12

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				

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P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
16	11.31	20.11	-0.52	4.14	22	22	Si	33

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.1	-0.1	0.1	-6.81	-198.46	96.06	4.10	0.003	0.003	19 (Fr)	Si	95
16	-0.1	-0.1	-0.0	-5.92	-198.33	-91.99	4.14	0.003	0.003	22 (Qp)	Si	62

Muro : 104 - Nodi: [53-52-152-153], Pann.X=4, Pann.Y=4Spess.=40 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	20.11	20.11	-0.23	-0.32	18	18	Si	98
13	20.11	20.11	-0.15	1.80	18	15	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	20.11	-0.11	-1.26	22	22	Si	>100
8	20.11	20.11	-0.04	0.49	22	22	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	-0.0	0.0	0.0	3.80	0.47	-15.88	0.49	0.001	0.001	22 (Qp)	Si	>100
8	-0.0	0.0	0.0	3.68	0.45	-16.32	0.40	0.001	0.001	21 (Fr)	Si	>100

Muro [Platea]: 105 - Nodi: [19-18-2-3]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
5	31.42	31.42	-0.01	3.33	18	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
5	31.42	31.42	-0.03	4.12	22	22	Si	87

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
5	0.0	0.0	0.0	-88.04	-105.32	-37.38	4.12	0.006	0.006	22 (Qp)	Si	31
9	0.0	0.0	0.0	-72.64	-88.20	-28.40	3.70	0.006	0.006	21 (Fr)	Si	50

Muro [Platea]: 106 - Nodi: [35-34-18-19]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.02	4.65	18	18	Si	77
1	31.42	31.42	-0.01	5.06	13	18	Si	71

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	5.12	22	22	Si	70
1	31.42	31.42	0.00	5.74	22	22	Si	63

Verifica aperture fessure:Wamm\_Freq[mm]=0.300 Wamm\_Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	0.0	-109.73	-14.17	-32.21	5.74	0.009	0.009	22 (Qp)	Si	21
1	0.0	0.0	0.0	-101.23	-3.79	-34.89	5.35	0.009	0.009	21 (Fr)	Si	34

Muro [Platea]: 107 - Nodi: [83-82-66-67]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.01	10.28	18	18	Si	35

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.01	10.81	22	22	Si	33

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
6	0.0	0.0	-0.0	-205.97	-21.18	18.05	10.81	0.018	0.018	22 (Qp)	Si	11
6	0.0	0.0	-0.0	-200.13	-20.60	17.12	10.50	0.017	0.017	20 (Fr)	Si	17

Muro [Platea]: 108 - Nodi: [51-50-34-35]Pann=16Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.06	9.43	18	18	Si	38

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
9	31.42	31.42	-0.07	10.36	22	22	Si	35
5	31.42	31.42	-0.07	10.39	22	22	Si	35

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
9	0.0	0.0	0.0	-210.48	-308.59	-31.12	10.36	0.017	0.017	22 (Qp)	Si	12
9	0.0	0.0	0.0	-204.19	-299.70	-31.75	9.99	0.016	0.016	20 (Fr)	Si	19

Muro [Platea]: 109 - Nodi: [36-35-19-20]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.02	4.70	18	15	Si	77
7	31.42	31.42	-0.01	5.09	13	18	Si	71

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.01	4.91	22	22	Si	73
7	31.42	31.42	0.00	5.81	22	22	Si	62

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			

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P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
7	0.0	0.0	0.0	-107.85	-12.88	-53.59	5.81	0.010	0.010	22 (Qp)	Si	21
7	0.0	0.0	0.0	-100.75	-2.24	-57.63	5.39	0.009	0.009	21 (Fr)	Si	34

Muro [Platea]: 110 - Nodi: [34-33-17-18]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42		-0.01	0.62	13	18	Si >100
1	31.42	31.42		-0.01	2.15	13	18	Si >100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	31.42	31.42		0.00	2.29	22	22	Si >100
2	31.42	31.42		0.00	2.54	22	22	Si >100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
2	0.0	0.0	0.0	-50.05	-49.04	-15.63	2.54	0.004	0.004	22 (Qp)	Si	48
2	0.0	0.0	0.0	-47.16	-41.47	-19.71	2.14	0.003	0.003	19 (Fr)	Si	86

Muro [Platea]: 111 - Nodi: [66-65-49-50]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42		-0.04	2.06	18	18	Si >100
3	31.42	31.42		-0.03	3.92	18	18	Si 92

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42		-0.04	4.19	22	22	Si 86
4	31.42	31.42		-0.02	5.61	22	22	Si 64

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
7	0.0	0.0	-0.0	64.05	32.69	-45.05	2.42	0.003	0.003	20 (Fr)	Si	88
8	0.0	0.0	0.0	31.79	-121.57	-22.55	4.57	0.006	0.006	22 (Qp)	Si	31

Muro [Platea]: 112 - Nodi: [82-81-65-66]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42		-0.00	0.43	18	18	Si >100
1	31.42	31.42		-0.00	4.82	18	18	Si 75

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42		-0.00	0.42	22	22	Si >100
1	31.42	31.42		-0.00	4.85	22	22	Si 74

Verifica aperture fessure:Wamm\_Freq[mm]=0.300 Wamm\_Qp[mm]=0.200

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P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	-0.0	-97.74	-2.79	-19.03	4.85	0.008	0.008	22 (Qp)	Si	26
1	0.0	0.0	-0.0	-95.07	-2.78	-18.52	4.71	0.008	0.008	19 (Fr)	Si	40

Muro [Platea]: 113 - Nodi: [50-49-33-34] Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.03	3.60	18	17	Si	>100
1	31.42	31.42	-0.02	4.69	18	18	Si	77

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.04	4.49	22	22	Si	80
1	31.42	31.42	-0.02	7.42	22	22	Si	48

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	-0.0	-120.62	-177.74	19.74	7.42	0.011	0.011	22 (Qp)	Si	18
1	0.0	0.0	-0.0	-116.49	-170.27	16.89	6.96	0.010	0.010	19 (Fr)	Si	29

Muro [Platea]: 114 - Nodi: [18-17-1-2] Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.01	0.85	18	18	Si	>100
1	31.42	31.42	-0.01	1.15	18	18	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

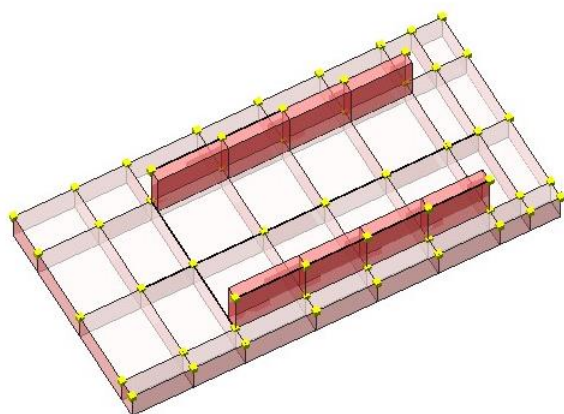
P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.01	1.07	22	22	Si	>100
1	31.42	31.42	-0.01	1.59	22	22	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	-0.0	-42.27	-48.10	7.04	0.85	0.001	0.001	22 (Qp)	Si	>100
2	0.0	-0.0	-0.0	-35.84	7.27	-6.17	0.97	0.001	0.001	21 (Fr)	Si	>100



#### 4. BASAMENTO PER BIOFILTRO BTK 2



##### Validazione del calcolo

Di seguito si riportano alcuni dati significativi del calcolo in base ai quali si ritiene che il codice di calcolo è affidabile ed i risultati accettati dal progettista.

##### Taglianti di piano

Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

I taglianti sono dati per combinazioni di calcolo C-S-Pm con C=Combinazione(1,2,...) S=Sisma(I,II) Pm=posizione masse(1,2,...). Le azioni, complessive, sono riferite al sistema di riferimento globale.

$\Theta = F_z \cdot dr / (F_h \cdot H)$  con:

Fz Forza verticale  
dr Spostamento medio del piano rispetto al piano inferiore  
Fh Tagliante  
H Altezza del piano

dx spostamento medio di piano in direzione X

dy spostamento medio di piano in direzione Y

dr  $((dx_s - dx_i)^2 + (dy_s - dy_i)^2)^{0.5}$  s=impalcato superiore i=impalcato inferiore

Nel caso di combinazioni sismiche l'aliquota dovuta al sisma di dx e dy è valutata secondo le indicazioni in 7.3.3, moltiplicando lo spostamento per  $\mu_d$

**Combinazione: 12-I-1 (SISMAxSLV)**

Piano	Fx	Fy	Fz	dx	dy	$\Theta$
	daN	daN	daN	mm	mm	
0	-5459.24	10.53	18783.88	0.00	0.00	--
1	5674.52	-89.14	-15701.10	0.03	-0.01	0.000104

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	-5459.24	10.53	-5459.24	10.53
1	0.00	0.00	0.00	0.00	5674.52	-89.14	5674.52	-89.14

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 12-I-2 (SISMAxSLV)**

Piano	Fx daN	Fy daN	Fz daN	dx mm	dy mm	Θ
0	-6874.07	10.35	18992.65	0.00	0.00	--
1	6691.01	2.62	-15839.64	0.03	-0.01	0.000084

Piano	FxPil/Isol. daN	FyPil/Isol. daN	FxPar daN	FyPar daN	FxShell daN	FyShell daN	FxTot daN	FyTot daN
0	0.00	0.00	0.00	0.00	-6874.07	10.35	-6874.07	10.35
1	0.00	0.00	0.00	0.00	6691.01	2.62	6691.01	2.62

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	--	--	--

**Combinazione: 12-I-3 (SISMAxSLV)**

Piano	Fx daN	Fy daN	Fz daN	dx mm	dy mm	Θ
0	-5780.57	88.25	19260.98	0.00	0.00	--
1	5888.58	-52.09	-15924.11	0.03	-0.01	0.000101

Piano	FxPil/Isol. daN	FyPil/Isol. daN	FxPar daN	FyPar daN	FxShell daN	FyShell daN	FxTot daN	FyTot daN
0	0.00	0.00	0.00	0.00	-5780.57	88.25	-5780.57	88.25
1	0.00	0.00	0.00	0.00	5888.58	-52.09	5888.58	-52.09

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 12-I-4 (SISMAxSLV)**

Piano	Fx daN	Fy daN	Fz daN	dx mm	dy mm	Θ
0	-5299.68	-2.78	18878.12	0.00	0.00	--
1	5339.31	1.12	-15512.35	0.03	-0.01	0.000110

Piano	FxPil/Isol. daN	FyPil/Isol. daN	FxPar daN	FyPar daN	FxShell daN	FyShell daN	FxTot daN	FyTot daN
0	0.00	0.00	0.00	0.00	-5299.68	-2.78	-5299.68	-2.78
1	0.00	0.00	0.00	0.00	5339.31	1.12	5339.31	1.12

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

**Combinazione: 13-I-1 (SISMAySLV)**

Piano	Fx daN	Fy daN	Fz daN	dx mm	dy mm	Θ
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**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
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Piano	Fx	Fy	Fz	dx	dy	Θ
0	16.04	-5060.77	18628.37	0.00	0.00	--
1	-1.76	5066.81	-15398.91	0.01	0.12	0.000442

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	16.04	-5060.77	16.04	-5060.77
1	0.00	0.00	0.00	0.00	-1.76	5066.81	-1.76	5066.81

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 13-I-2 (SISMAYSLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	6.66	-6796.98	19060.97	0.00	0.00	--
1	-14.83	6740.44	-15711.82	0.01	0.10	0.000302

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	6.66	-6796.98	6.66	-6796.98
1	0.00	0.00	0.00	0.00	-14.83	6740.44	-14.83	6740.44

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 13-I-3 (SISMAYSLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	-13.71	-5002.76	18938.03	0.00	0.00	--
1	-5.36	5026.54	-15687.28	0.01	0.12	0.000455

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	-13.71	-5002.76	-13.71	-5002.76
1	0.00	0.00	0.00	0.00	-5.36	5026.54	-5.36	5026.54

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 13-I-4 (SISMAYSLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	12.73	-6997.12	19010.94	0.00	0.00	--
1	-20.51	6773.96	-15760.65	0.01	0.10	0.000299

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
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Piano	FxPil/Isol. daN	FyPil/Isol. daN	FxPar daN	FyPar daN	FxShell daN	FyShell daN	FxTot daN	FyTot daN
0	0.00	0.00	0.00	0.00	12.73	-6997.12	12.73	-6997.12
1	0.00	0.00	0.00	0.00	-20.51	6773.96	-20.51	6773.96

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 14-I-1 (SISMAx1SLV)**

Piano	Fx daN	Fy daN	Fz daN	dx mm	dy mm	Θ
0	-5459.24	10.53	18783.88	0.00	0.00	--
1	5674.52	-89.14	-15701.10	0.03	-0.02	0.000124

Piano	FxPil/Isol. daN	FyPil/Isol. daN	FxPar daN	FyPar daN	FxShell daN	FyShell daN	FxTot daN	FyTot daN
0	0.00	0.00	0.00	0.00	-5459.24	10.53	-5459.24	10.53
1	0.00	0.00	0.00	0.00	5674.52	-89.14	5674.52	-89.14

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 14-I-2 (SISMAx1SLV)**

Piano	Fx daN	Fy daN	Fz daN	dx mm	dy mm	Θ
0	-6874.07	10.35	18992.65	0.00	0.00	--
1	6691.01	2.62	-15839.64	0.03	-0.02	0.000102

Piano	FxPil/Isol. daN	FyPil/Isol. daN	FxPar daN	FyPar daN	FxShell daN	FyShell daN	FxTot daN	FyTot daN
0	0.00	0.00	0.00	0.00	-6874.07	10.35	-6874.07	10.35
1	0.00	0.00	0.00	0.00	6691.01	2.62	6691.01	2.62

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	--	--	--

**Combinazione: 14-I-3 (SISMAx1SLV)**

Piano	Fx daN	Fy daN	Fz daN	dx mm	dy mm	Θ
0	-5780.57	88.25	19260.98	0.00	0.00	--
1	5888.58	-52.09	-15924.11	0.03	-0.02	0.000121

Piano	FxPil/Isol. daN	FyPil/Isol. daN	FxPar daN	FyPar daN	FxShell daN	FyShell daN	FxTot daN	FyTot daN
0	0.00	0.00	0.00	0.00	-5780.57	88.25	-5780.57	88.25
1	0.00	0.00	0.00	0.00	5888.58	-52.09	5888.58	-52.09

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Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 14-I-4 (SISMAx1SLV)**

Piano	Fx daN	Fy daN	Fz daN	dx mm	dy mm	Θ
0	-5299.68	-2.78	18878.12	0.00	0.00	--
1	5339.31	1.12	-15512.35	0.03	-0.02	0.000132

Piano	FxPil/Isol. daN	FyPil/Isol. daN	FxPar daN	FyPar daN	FxShell daN	FyShell daN	FxTot daN	FyTot daN
0	0.00	0.00	0.00	0.00	-5299.68	-2.78	-5299.68	-2.78
1	0.00	0.00	0.00	0.00	5339.31	1.12	5339.31	1.12

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

**Combinazione: 15-I-1 (SISMAy1SLV)**

Piano	Fx daN	Fy daN	Fz daN	dx mm	dy mm	Θ
0	16.04	-5060.77	18628.37	0.00	0.00	--
1	-1.76	5066.81	-15398.91	0.01	0.11	0.000421

Piano	FxPil/Isol. daN	FyPil/Isol. daN	FxPar daN	FyPar daN	FxShell daN	FyShell daN	FxTot daN	FyTot daN
0	0.00	0.00	0.00	0.00	16.04	-5060.77	16.04	-5060.77
1	0.00	0.00	0.00	0.00	-1.76	5066.81	-1.76	5066.81

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 15-I-2 (SISMAy1SLV)**

Piano	Fx daN	Fy daN	Fz daN	dx mm	dy mm	Θ
0	6.66	-6796.98	19060.97	0.00	0.00	--
1	-14.83	6740.44	-15711.82	0.01	0.10	0.000285

Piano	FxPil/Isol. daN	FyPil/Isol. daN	FxPar daN	FyPar daN	FxShell daN	FyShell daN	FxTot daN	FyTot daN
0	0.00	0.00	0.00	0.00	6.66	-6796.98	6.66	-6796.98
1	0.00	0.00	0.00	0.00	-14.83	6740.44	-14.83	6740.44

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 15-I-3 (SISMAy1SLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	-13.71	-5002.76	18938.03	0.00	0.00	--
1	-5.36	5026.54	-15687.28	0.01	0.11	0.000432

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	-13.71	-5002.76	-13.71	-5002.76
1	0.00	0.00	0.00	0.00	-5.36	5026.54	-5.36	5026.54

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 15-I-4 (SISMAy1SLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	12.73	-6997.12	19010.94	0.00	0.00	--
1	-20.51	6773.96	-15760.65	0.01	0.10	0.000282

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	12.73	-6997.12	12.73	-6997.12
1	0.00	0.00	0.00	0.00	-20.51	6773.96	-20.51	6773.96

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Risultati Analisi Dinamica - Statistiche matrice di rigidità**

Scenario di calcolo: ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO

Minimo della diagonale	1.809725e+06
Massimo della diagonale	7.897278e+09
Rapporto Max/Min	4.363801e+03
Media della diagonale	8.769509e+08
Densità	2.024191e+00

Dati generali

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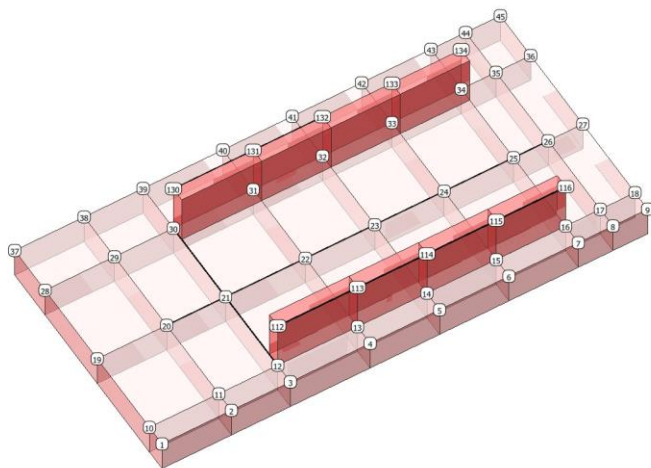
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Nome struttura	
Numero di frequenze	90
% Filtro masse libere	0.1
% Coefficiente di smorzamento viscoso	5
Spostamenti modali con segno	Si
Deformabilità a taglio delle aste	Si
Spostamento ammissibile impalcato	0.0050*h

**Nodi - Geometria e vincoli**

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
		Coordinate [m]								
1	-7.000	0.000	0.000	1	1	0	0	0	1	0
2	-6.000	0.000	0.000	1	1	0	0	0	1	0
3	-5.150	0.000	0.000	1	1	0	0	0	1	0
4	-4.000	0.000	0.000	1	1	0	0	0	1	0
5	-3.000	0.000	0.000	1	1	0	0	0	1	0
6	-2.000	0.000	0.000	1	1	0	0	0	1	0
7	-1.000	0.000	0.000	1	1	0	0	0	1	0
8	-0.500	0.000	0.000	1	1	0	0	0	1	0
9	0.000	0.000	0.000	1	1	0	0	0	1	0
10	-7.000	0.300	0.000	1	1	0	0	0	1	0
11	-6.000	0.300	0.000	1	1	0	0	0	1	0
12	-5.150	0.300	0.000	1	1	0	0	0	1	0
13	-4.000	0.300	0.000	1	1	0	0	0	1	0
14	-3.000	0.300	0.000	1	1	0	0	0	1	0
15	-2.000	0.300	0.000	1	1	0	0	0	1	0
16	-1.000	0.300	0.000	1	1	0	0	0	1	0
17	-0.500	0.300	0.000	1	1	0	0	0	1	0
18	0.000	0.300	0.000	1	1	0	0	0	1	0
19	-7.000	1.540	0.000	1	1	0	0	0	1	0
20	-6.000	1.540	0.000	1	1	0	0	0	1	0
21	-5.150	1.540	0.000	1	1	0	0	0	1	0
22	-4.000	1.540	0.000	1	1	0	0	0	1	0
23	-3.000	1.540	0.000	1	1	0	0	0	1	0
24	-2.000	1.540	0.000	1	1	0	0	0	1	0
25	-1.000	1.540	0.000	1	1	0	0	0	1	0
26	-0.500	1.540	0.000	1	1	0	0	0	1	0
27	0.000	1.540	0.000	1	1	0	0	0	1	0
28	-7.000	2.780	0.000	1	1	0	0	0	1	0
29	-6.000	2.780	0.000	1	1	0	0	0	1	0
30	-5.150	2.780	0.000	1	1	0	0	0	1	0
31	-4.000	2.780	0.000	1	1	0	0	0	1	0
32	-3.000	2.780	0.000	1	1	0	0	0	1	0
33	-2.000	2.780	0.000	1	1	0	0	0	1	0
34	-1.000	2.780	0.000	1	1	0	0	0	1	0
35	-0.500	2.780	0.000	1	1	0	0	0	1	0
36	0.000	2.780	0.000	1	1	0	0	0	1	0
37	-7.000	3.500	0.000	1	1	0	0	0	1	0
38	-6.000	3.500	0.000	1	1	0	0	0	1	0
39	-5.150	3.500	0.000	1	1	0	0	0	1	0
40	-4.000	3.500	0.000	1	1	0	0	0	1	0
41	-3.000	3.500	0.000	1	1	0	0	0	1	0
42	-2.000	3.500	0.000	1	1	0	0	0	1	0
43	-1.000	3.500	0.000	1	1	0	0	0	1	0
44	-0.500	3.500	0.000	1	1	0	0	0	1	0
45	0.000	3.500	0.000	1	1	0	0	0	1	0
112	-5.150	0.300	0.800	0	0	0	0	0	0	1
113	-4.000	0.300	0.800	0	0	0	0	0	0	1
114	-3.000	0.300	0.800	0	0	0	0	0	0	1
115	-2.000	0.300	0.800	0	0	0	0	0	0	1
116	-1.000	0.300	0.800	0	0	0	0	0	0	1
130	-5.150	2.780	0.800	0	0	0	0	0	0	1
131	-4.000	2.780	0.800	0	0	0	0	0	0	1
132	-3.000	2.780	0.800	0	0	0	0	0	0	1
133	-2.000	2.780	0.800	0	0	0	0	0	0	1
134	-1.000	2.780	0.800	0	0	0	0	0	0	1



**Nodi - Carichi**

N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
		daN			daN*m			cm			°			°C
112	biofiltro	0.00	0.00	975.00	0.00	0.00	0.00							
112	vento y	0.00	-85.00	0.00	140.00	0.00	0.00							
112	vento x	85.00	0.00	0.00	0.00	140.00	0.00							
112	azione sismica SLV y	0.00	-	380.00	705.00	0.00	0.00							
112	azione sismica SLV x	380.00	0.00	0.00	0.00	705.00	0.00							
112	azione sismica SLD y	0.00	-	150.00	280.00	0.00	0.00							
112	azione sismica SLD x	150.00	0.00	0.00	0.00	275.00	0.00							
113	biofiltro	0.00	0.00	1950.00	0.00	0.00	0.00							
113	vento y	0.00	-	170.00	280.00	0.00	0.00							
113	vento x	85.00	0.00	0.00	0.00	140.00	0.00							
113	azione sismica SLV y	0.00	-	760.00	1255.00	0.00	0.00							
113	azione sismica SLV x	760.00	0.00	0.00	0.00	1255.00	0.00							
113	azione sismica SLD y	0.00	-	300.00	1005.00	0.00	0.00							
113	azione sismica SLD x	150.00	0.00	0.00	0.00	275.00	0.00							
114	biofiltro	0.00	0.00	1950.00	0.00	0.00	0.00							
114	vento y	0.00	-	170.00	280.00	0.00	0.00							
114	vento x	85.00	0.00	0.00	0.00	140.00	0.00							
114	azione sismica SLV y	0.00	-	760.00	1255.00	0.00	0.00							
114	azione sismica SLV x	760.00	0.00	0.00	0.00	1255.00	0.00							
114	azione sismica SLD y	0.00	-	300.00	1005.00	0.00	0.00							
114	azione sismica SLD x	150.00	0.00	0.00	0.00	275.00	0.00							
115	biofiltro	0.00	0.00	1950.00	0.00	0.00	0.00							



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N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
115	vento y	0.00	-170.00	0.00	280.00	0.00	0.00							
115	vento x	85.00	0.00	0.00	0.00	140.00	0.00							
115	azione sismica SLV y	0.00	-760.00	0.00	1255.00	0.00	0.00							
115	azione sismica SLV x	-760.00	0.00	0.00	0.00	1255.00	0.00							
115	azione sismica SLD y	0.00	-300.00	0.00	1005.00	0.00	0.00							
115	azione sismica SLD x	-150.00	0.00	0.00	0.00	275.00	0.00							
116	biofiltro	0.00	0.00	975.00	0.00	0.00	0.00							
116	vento y	0.00	-85.00	0.00	140.00	0.00	0.00							
116	vento x	85.00	0.00	0.00	0.00	140.00	0.00							
116	azione sismica SLV y	0.00	-380.00	0.00	705.00	0.00	0.00							
116	azione sismica SLV x	-380.00	0.00	0.00	0.00	705.00	0.00							
116	azione sismica SLD y	0.00	-150.00	0.00	280.00	0.00	0.00							
116	azione sismica SLD x	-150.00	0.00	0.00	0.00	275.00	0.00							
130	biofiltro	0.00	0.00	975.00	0.00	0.00	0.00							
130	vento y	0.00	-85.00	0.00	140.00	0.00	0.00							
130	vento x	85.00	0.00	0.00	0.00	140.00	0.00							
130	azione sismica SLV y	0.00	-380.00	0.00	705.00	0.00	0.00							
130	azione sismica SLV x	-380.00	0.00	0.00	0.00	705.00	0.00							
130	azione sismica SLD y	0.00	-150.00	0.00	280.00	0.00	0.00							
130	azione sismica SLD x	-150.00	0.00	0.00	0.00	275.00	0.00							
131	biofiltro	0.00	0.00	1950.00	0.00	0.00	0.00							
131	vento y	0.00	-170.00	0.00	280.00	0.00	0.00							
131	vento x	85.00	0.00	0.00	0.00	140.00	0.00							
131	azione sismica SLV y	0.00	-760.00	0.00	1255.00	0.00	0.00							
131	azione sismica SLV x	-760.00	0.00	0.00	0.00	1255.00	0.00							
131	azione sismica SLD y	0.00	-300.00	0.00	1005.00	0.00	0.00							
131	azione sismica SLD x	-150.00	0.00	0.00	0.00	275.00	0.00							
132	biofiltro	0.00	0.00	1950.00	0.00	0.00	0.00							
132	vento y	0.00	-170.00	0.00	280.00	0.00	0.00							
132	vento x	85.00	0.00	0.00	0.00	140.00	0.00							
132	azione sismica SLV y	0.00	-760.00	0.00	1255.00	0.00	0.00							
132	azione sismica SLV x	-760.00	0.00	0.00	0.00	1255.00	0.00							
132	azione sismica SLD y	0.00	-300.00	0.00	1005.00	0.00	0.00							
132	azione sismica SLD x	-150.00	0.00	0.00	0.00	275.00	0.00							
133	biofiltro	0.00	0.00	1950.00	0.00	0.00	0.00							
133	vento y	0.00	-170.00	0.00	280.00	0.00	0.00							
133	vento x	85.00	0.00	0.00	0.00	140.00	0.00							
133	azione sismica SLV y	0.00	-760.00	0.00	1255.00	0.00	0.00							
133	azione sismica SLV x	-760.00	0.00	0.00	0.00	1255.00	0.00							
133	azione sismica SLD y	0.00	-300.00	0.00	1005.00	0.00	0.00							
133	azione sismica SLD x	-150.00	0.00	0.00	0.00	275.00	0.00							
134	biofiltro	0.00	0.00	975.00	0.00	0.00	0.00							

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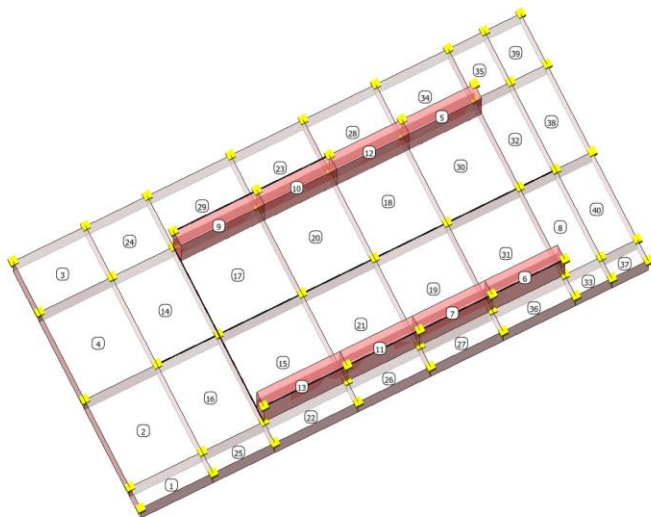
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N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
134	vento y	0.00	-85.00	0.00	140.00	0.00	0.00							
134	vento x	85.00	0.00	0.00	0.00	140.00	0.00							
134	azione sismica SLV y	0.00	-	0.00	705.00	0.00	0.00							
134	azione sismica SLV x	380.00	0.00	0.00	0.00	705.00	0.00							
134	azione sismica SLD y	0.00	-	0.00	280.00	0.00	0.00							
134	azione sismica SLD x	150.00	0.00	0.00	0.00	275.00	0.00							

**Pareti - geometria e vincoli**

Parete	Nodi	Tipo	Materiale	Criterio	N.P.	N.P.X	N.P.Y	Spess.
								m
1	1-2-11-10	Platea	C35/45	CLS Platee ND	4			0.50
2	11-20-19-10	Platea	C35/45	CLS Platee ND	4			0.50
3	29-38-37-28	Platea	C35/45	CLS Platee ND	4			0.50
4	20-29-28-19	Platea	C35/45	CLS Platee ND	4			0.50
5	34-33-133-134	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
6	16-116-115-15	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
7	15-115-114-14	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
8	26-25-16-17	Platea	C35/45	CLS Platee ND	4			0.50
9	31-30-130-131	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
10	32-31-131-132	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
11	14-114-113-13	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
12	33-32-132-133	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
13	13-113-112-12	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
14	30-29-20-21	Platea	C35/45	CLS Platee ND	4			0.50
15	22-21-12-13	Platea	C35/45	CLS Platee ND	8			0.50
16	21-20-11-12	Platea	C35/45	CLS Platee ND	4			0.50
17	31-30-21-22	Platea	C35/45	CLS Platee ND	8			0.50
18	33-32-23-24	Platea	C35/45	CLS Platee ND	8			0.50
19	24-23-14-15	Platea	C35/45	CLS Platee ND	8			0.50
20	32-31-22-23	Platea	C35/45	CLS Platee ND	8			0.50
21	23-22-13-14	Platea	C35/45	CLS Platee ND	8			0.50
22	3-4-13-12	Platea	C35/45	CLS Platee ND	8			0.50
23	41-40-31-32	Platea	C35/45	CLS Platee ND	8			0.50
24	39-38-29-30	Platea	C35/45	CLS Platee ND	4			0.50
25	2-3-12-11	Platea	C35/45	CLS Platee ND	4			0.50
26	4-5-14-13	Platea	C35/45	CLS Platee ND	8			0.50
27	5-6-15-14	Platea	C35/45	CLS Platee ND	8			0.50
28	33-42-41-32	Platea	C35/45	CLS Platee ND	8			0.50
29	40-39-30-31	Platea	C35/45	CLS Platee ND	8			0.50
30	34-33-24-25	Platea	C35/45	CLS Platee ND	8			0.50
31	25-24-15-16	Platea	C35/45	CLS Platee ND	8			0.50
32	35-34-25-26	Platea	C35/45	CLS Platee ND	4			0.50
33	7-8-17-16	Platea	C35/45	CLS Platee ND	4			0.50
34	34-43-42-33	Platea	C35/45	CLS Platee ND	8			0.50
35	35-44-43-34	Platea	C35/45	CLS Platee ND	4			0.50
36	6-7-16-15	Platea	C35/45	CLS Platee ND	8			0.50
37	8-9-18-17	Platea	C35/45	CLS Platee ND	4			0.50
38	36-35-26-27	Platea	C35/45	CLS Platee ND	4			0.50
39	36-45-44-35	Platea	C35/45	CLS Platee ND	4			0.50
40	27-26-17-18	Platea	C35/45	CLS Platee ND	4			0.50



#### Muri - Carichi

Shell Indice dello shell  
Cond. Condizione di carico  
Tipo Tipologia di spinta  
 $\gamma$  Peso specifico: terreno o acqua  
Ht Quota del piano di campagna  
 $\emptyset$  Angolo di attrito interno  
c Coesione  
 $\delta$  Angolo di attrito terreno paramento shell  
 $\beta$  Angolo di inclinazione del piano di campagna  
 $k_0$  Coefficiente di spinta a riposo (quando richiesto)  
 $\beta_m$  Coefficiente di riduzione dell'accelerazione massima attesa al sito (quando richiesto)  
Ag Accelerazione del sito a meno di 'g': quando richiesto, rappresenta il valore della accelerazione dello spettro per  $T=0$ , quindi comprensiva dei coefficienti di amplificazione topografica ( $S_T$ ) e stratigrafica ( $S_S$ )  
Q Valore del carico uniforme  
Vert.1 Valore del carico nel primo vertice<sup>(1)</sup>  
Vert.2 Valore del carico nel secondo vertice<sup>(1)</sup>  
Vert.3 Valore del carico nel terzo vertice<sup>(1)</sup>  
Vert.4 Valore del carico nel quarto vertice<sup>(1)</sup>  
Hw Altezza del pelo libero dell'acqua  
<sup>(1)</sup>: Per shell con numero di vertici maggiori 4, per carichi trapezoidali, il valore del carico nei vertici e' stampato a gruppi di 4 secondo l'ordine con cui i vertici sono stati definiti

Shell	Cond.	Tipo	Ht	$\gamma$	$\emptyset$	c	$\delta$	$\beta$	$k_0$	$\beta_m$	Ag
1			m	daN/m <sup>3</sup>	°	daN/cm <sup>2</sup>	°	°			
8	serbatoio	Sisma terreno - Riposo - Dir.Neg.	0.00	1900.00	--	--	--	--	0.50	1.00	0.00
32	serbatoio	Sisma terreno - Riposo - Dir.Neg.	0.00	1900.00	--	--	--	--	0.50	1.00	0.00
38	serbatoio	Sisma terreno - Riposo - Dir.Neg.	0.00	1900.00	--	--	--	--	0.50	1.00	0.00
40	serbatoio	Sisma terreno - Riposo - Dir.Neg.	0.00	1900.00	--	--	--	--	0.50	1.00	0.00

Shell	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	$\gamma$
1			daN/m <sup>2</sup>	daN/m <sup>2</sup>	daN/m <sup>2</sup>	daN/m <sup>2</sup>	daN/m <sup>2</sup>	m	daN/m <sup>3</sup>
1	Peso Proprio	Peso Proprio daN	375.00						
1	NEVE	Uniforme GLOBZ	60.00						
1	accidentali	Uniforme GLOBZ	600.00						
1	4100	Uniforme_GLOBZ	4100.00						

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She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
2	Peso Proprio	Peso Proprio daN	1550.0 0						
2	NEVE	Uniforme GLOBZ	60.00						
2	accidentali	Uniforme GLOBZ	600.00						
2	4100	Uniforme GLOBZ	4100.0 0						
3	Peso Proprio	Peso Proprio daN	900.00						
3	NEVE	Uniforme GLOBZ	60.00						
3	accidentali	Uniforme GLOBZ	600.00						
3	4100	Uniforme GLOBZ	4100.0 0						
4	Peso Proprio	Peso Proprio daN	1550.0 0						
4	NEVE	Uniforme GLOBZ	60.00						
4	accidentali	Uniforme GLOBZ	600.00						
4	4100	Uniforme GLOBZ	4100.0 0						
5	Peso Proprio	Peso Proprio daN	400.00						
6	Peso Proprio	Peso Proprio daN	400.00						
6	vento y	Uniforme GLOBY	- 100.00						
7	Peso Proprio	Peso Proprio daN	400.00						
7	vento y	Uniforme GLOBY	- 100.00						
8	Peso Proprio	Peso Proprio daN	775.00						
8	NEVE	Uniforme GLOBZ	60.00						
8	serbatoio	Uniforme GLOBZ	1500.0 0						
8	4100	Uniforme GLOBZ	4100.0 0						
9	Peso Proprio	Peso Proprio daN	460.00						
10	Peso Proprio	Peso Proprio daN	400.00						
11	Peso Proprio	Peso Proprio daN	400.00						
11	vento y	Uniforme GLOBY	- 100.00						
12	Peso Proprio	Peso Proprio daN	400.00						
13	Peso Proprio	Peso Proprio daN	460.00						
13	vento y	Uniforme GLOBY	- 100.00						
14	Peso Proprio	Peso Proprio daN	1317.5 0						
14	NEVE	Uniforme GLOBZ	60.00						
14	ventilatore	Uniforme GLOBZ	500.00						
14	4100	Uniforme GLOBZ	4100.0 0						
15	Peso Proprio	Peso Proprio daN	1782.5 0						
15	NEVE	Uniforme GLOBZ	60.00						
15	4100	Uniforme GLOBZ	4100.0 0						
16	Peso Proprio	Peso Proprio daN	1317.5 0						
16	NEVE	Uniforme GLOBZ	60.00						
16	ventilatore	Uniforme GLOBZ	500.00						
16	4100	Uniforme GLOBZ	4100.0 0						
17	Peso Proprio	Peso Proprio daN	1782.5 0						
17	NEVE	Uniforme GLOBZ	60.00						
17	4100	Uniforme GLOBZ	4100.0 0						
18	Peso Proprio	Peso Proprio daN	1550.0 0						
18	NEVE	Uniforme GLOBZ	60.00						
18	4100	Uniforme GLOBZ	4100.0 0						
19	Peso Proprio	Peso Proprio daN	1550.0 0						
19	NEVE	Uniforme GLOBZ	60.00						
19	4100	Uniforme GLOBZ	4100.0 0						
20	Peso Proprio	Peso Proprio daN	1550.0 0						
20	NEVE	Uniforme GLOBZ	60.00						

She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
20	4100	Uniforme_GLOBZ	4100.0 0						
21	Peso Proprio	Peso Proprio daN	1550.0 0						
21	NEVE	Uniforme_GLOBZ	60.00						
21	4100	Uniforme_GLOBZ	4100.0 0						
22	Peso Proprio	Peso Proprio daN	431.25						
22	NEVE	Uniforme_GLOBZ	60.00						
22	accidentali	Uniforme_GLOBZ	600.00						
22	4100	Uniforme_GLOBZ	4100.0 0						
23	Peso Proprio	Peso Proprio daN	900.00						
23	NEVE	Uniforme_GLOBZ	60.00						
23	accidentali	Uniforme_GLOBZ	600.00						
23	4100	Uniforme_GLOBZ	4100.0 0						
24	Peso Proprio	Peso Proprio daN	765.00						
24	NEVE	Uniforme_GLOBZ	60.00						
24	accidentali	Uniforme_GLOBZ	600.00						
24	4100	Uniforme_GLOBZ	4100.0 0						
25	Peso Proprio	Peso Proprio daN	318.75						
25	NEVE	Uniforme_GLOBZ	60.00						
25	accidentali	Uniforme_GLOBZ	600.00						
25	4100	Uniforme_GLOBZ	4100.0 0						
26	Peso Proprio	Peso Proprio daN	375.00						
26	NEVE	Uniforme_GLOBZ	60.00						
26	accidentali	Uniforme_GLOBZ	600.00						
26	4100	Uniforme_GLOBZ	4100.0 0						
27	Peso Proprio	Peso Proprio daN	375.00						
27	NEVE	Uniforme_GLOBZ	60.00						
27	accidentali	Uniforme_GLOBZ	600.00						
27	4100	Uniforme_GLOBZ	4100.0 0						
28	Peso Proprio	Peso Proprio daN	900.00						
28	NEVE	Uniforme_GLOBZ	60.00						
28	accidentali	Uniforme_GLOBZ	600.00						
28	4100	Uniforme_GLOBZ	4100.0 0						
29	Peso Proprio	Peso Proprio daN	1035.0 0						
29	NEVE	Uniforme_GLOBZ	60.00						
29	accidentali	Uniforme_GLOBZ	600.00						
29	4100	Uniforme_GLOBZ	4100.0 0						
30	Peso Proprio	Peso Proprio daN	1550.0 0						
30	NEVE	Uniforme_GLOBZ	60.00						
30	4100	Uniforme_GLOBZ	4100.0 0						
31	Peso Proprio	Peso Proprio daN	1550.0 0						
31	NEVE	Uniforme_GLOBZ	60.00						
31	4100	Uniforme_GLOBZ	4100.0 0						
32	Peso Proprio	Peso Proprio daN	775.00						
32	NEVE	Uniforme_GLOBZ	60.00						
32	serbatoio	Uniforme_GLOBZ	1500.0 0						
32	4100	Uniforme_GLOBZ	4100.0 0						
33	Peso Proprio	Peso Proprio daN	187.50						
33	NEVE	Uniforme_GLOBZ	60.00						
33	accidentali	Uniforme_GLOBZ	600.00						
33	4100	Uniforme_GLOBZ	4100.0 0						
34	Peso Proprio	Peso Proprio daN	900.00						
34	NEVE	Uniforme_GLOBZ	60.00						
34	accidentali	Uniforme_GLOBZ	600.00						
34	4100	Uniforme_GLOBZ	4100.0 0						
35	Peso Proprio	Peso Proprio daN	450.00						

She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
35	NEVE	Uniforme GLOBZ	60.00						
35	accidentali	Uniforme GLOBZ	600.00						
35	4100	Uniforme_GLOBZ	4100.0 0						
36	Peso Proprio	Peso Proprio daN	375.00						
36	NEVE	Uniforme GLOBZ	60.00						
36	accidentali	Uniforme GLOBZ	600.00						
36	4100	Uniforme_GLOBZ	4100.0 0						
37	Peso Proprio	Peso Proprio daN	187.50						
37	NEVE	Uniforme GLOBZ	60.00						
37	accidentali	Uniforme GLOBZ	600.00						
37	4100	Uniforme_GLOBZ	4100.0 0						
38	Peso Proprio	Peso Proprio daN	775.00						
38	NEVE	Uniforme GLOBZ	60.00						
38	4100	Uniforme_GLOBZ	4100.0 0						
39	Peso Proprio	Peso Proprio daN	450.00						
39	NEVE	Uniforme GLOBZ	60.00						
39	accidentali	Uniforme GLOBZ	600.00						
39	4100	Uniforme_GLOBZ	4100.0 0						
40	Peso Proprio	Peso Proprio daN	775.00						
40	NEVE	Uniforme GLOBZ	60.00						
40	4100	Uniforme_GLOBZ	4100.0 0						

#### Tabulati di verifica

L'esito di ogni elaborazione viene sintetizzato nei disegni e schemi grafici allegati, che evidenziano i valori numerici nei punti e/o nelle sezioni significative, ai fini della valutazione del comportamento complessivo della struttura, e quelli necessari ai fini delle verifiche di misura della sicurezza.

Di seguito si riportano le tabelle relative a:

- Forze sismiche e masse
- Spostamenti Relativi dei nodi (SLD)
- Massime tensioni terreno platee per combinazione
- Massimi spostamenti dei nodi
- Massime reazioni vincolari
- Massimi spostamenti degli impalcati
- Massimi spostamenti degli impalcati (SLD)
- Massime sollecitazioni muri Discretizzati
- Massime tensioni terreno platee per combinazione (SLE)
- Massimi spostamenti dei nodi (SLE)
- Massime reazioni vincolari (SLE)
- Massime sollecitazioni muri Discretizzati (SLE)

#### Risultati Analisi Dinamica - Baricentri masse e masse

Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

Piano	Rigido	Massa daN	X m	Y m	Z m
0	No	0.00	0.00	0.00	0.00
1	Si	17040.00	-3.03	1.40	0.79

Piano	Rigido	Massa daN	X m	Y m	Z m
0	No	0.00	0.00	0.00	0.00
1	Si	17040.00	-2.82	1.53	0.79

Piano	Rigido	Massa daN	X m	Y m	Z m
0	No	0.00	0.00	0.00	0.00
1	Si	17040.00	-3.03	1.65	0.79

Piano	Rigido	Massa daN	X m	Y m	Z m
0	No	0.00	0.00	0.00	0.00

Piano	Rigido	Massa	X	Y	Z
1	Si	17040.00	-3.23	1.53	0.79

**Verifica Degli Spostamenti Relativi**

Scenario di calcolo: ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO

Interp	Comb.	$\eta_{Xv}$	$\eta_{Xh}$	$\eta_{Yv}$	$\eta_{Yh}$	Nodo1	Nodo2	$\eta$	$\eta_{Amm}$	Cs
		mm	mm	mm	mm			mm	mm	
0-1	(31+32)-IV-4	0.08	0.00	0.11	0.02	12	112	0.12	4.00	33
0-1	(31+32)-IV-3	0.07	0.00	0.11	0.01	13	113	0.12	4.00	33
0-1	(31+32)-II-3	0.07	0.00	0.11	0.02	14	114	0.12	4.00	32
0-1	(31+32)-II-4	0.06	0.00	0.11	0.02	15	115	0.12	4.00	32
0-1	(31+32)-II-3	0.08	0.00	0.11	0.02	16	116	0.12	4.00	33
0-1	(31+32)-VII-3	0.08	0.00	0.04	0.01	30	130	0.08	4.00	50
0-1	(31+32)-V-4	0.07	0.00	0.04	0.00	31	131	0.07	4.00	56
0-1	(31+32)-V-3	0.06	0.00	0.04	0.00	32	132	0.07	4.00	59
0-1	(31+32)-V-4	0.06	0.00	0.04	0.00	33	133	0.06	4.00	62
0-1	(31+32)-V-4	0.08	0.00	0.05	0.00	34	134	0.08	4.00	47
<b>Minimo</b>										
0-1	(31+32)-II-4	0.06	0.00	0.11	0.02	15	115	0.12	4.00	32

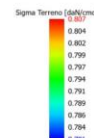
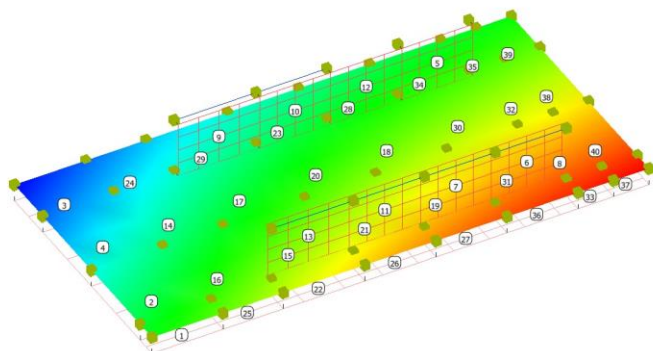
**Risultati Analisi Dinamica - Sollecitazioni massime per combinazione - Sigma terreno platea**

Scenario di calcolo: ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO

Combinazione	Muro	Nodi	SigmaMax daN/cm <sup>2</sup>	SigmaMin daN/cm <sup>2</sup>
1	37	8-9-18-17	0.19	0.17
2	37	8-9-18-17	0.40	0.18
3	37	8-9-18-17	0.81	0.78
4	37	8-9-18-17	0.39	0.26
5	37	8-9-18-17	0.37	0.29
6	37	8-9-18-17	0.39	0.27
7	37	8-9-18-17	0.38	0.29
8	37	8-9-18-17	0.39	0.27
9	37	8-9-18-17	0.38	0.27
10	39	36-45-44-35	0.37	0.28
11	37	8-9-18-17	0.36	0.22
12-I-1	37	8-9-18-17	0.33	0.13
12-II-1	37	8-9-18-17	0.34	0.12
12-I-2	37	8-9-18-17	0.34	0.13
12-II-2	37	8-9-18-17	0.33	0.12
12-I-3	37	8-9-18-17	0.33	0.13
12-II-3	37	8-9-18-17	0.34	0.12
12-I-4	37	8-9-18-17	0.33	0.12
12-II-4	37	8-9-18-17	0.34	0.13
13-I-1	39	36-45-44-35	0.33	0.13
13-II-1	39	36-45-44-35	0.35	0.11
13-I-2	39	36-45-44-35	0.35	0.11
13-II-2	39	36-45-44-35	0.33	0.13
13-I-3	39	36-45-44-35	0.33	0.13
13-II-3	39	36-45-44-35	0.35	0.11
13-I-4	39	36-45-44-35	0.35	0.11
13-II-4	39	36-45-44-35	0.33	0.13
14-I-1	37	8-9-18-17	0.34	0.09
14-II-1	37	8-9-18-17	0.34	0.08
14-I-2	37	8-9-18-17	0.34	0.09
14-II-2	37	8-9-18-17	0.34	0.08
14-I-3	37	8-9-18-17	0.34	0.09
14-II-3	37	8-9-18-17	0.34	0.08
14-I-4	37	8-9-18-17	0.33	0.08
14-II-4	37	8-9-18-17	0.34	0.09
15-I-1	39	36-45-44-35	0.32	0.11
15-II-1	39	36-45-44-35	0.34	0.08
15-I-2	39	36-45-44-35	0.34	0.09
15-II-2	39	36-45-44-35	0.32	0.11
15-I-3	39	36-45-44-35	0.32	0.11
15-II-3	39	36-45-44-35	0.34	0.09
15-I-4	39	36-45-44-35	0.34	0.08
15-II-4	39	36-45-44-35	0.32	0.11
Assoluti				

Combinazione	Muro	Nodi	SigmaMax	SigmaMin
3	37	8-9-18-17	0.81	
14-II-3	37	8-9-18-17		0.08

Tipo diagramma: Tensioni medie terreno  
Combinazione corrente : Scenario ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO - C 3  
Tensioni medie terreno aste  
Tensioni medie terreno platee



**Risultati Analisi Dinamica - Spostamenti massimi - Nodi**  
Scenario di calcolo: ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO

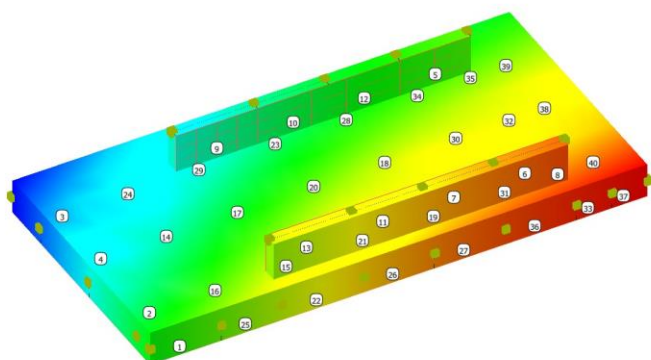
la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Nodo	Trasl. X mm	Trasl. Y mm	Trasl. Z mm	Rotaz. X °	Rotaz. Y °	Rotaz. Z °
1	0.00 (1)	0.00 (1)	-3.97 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)
2	0.00 (1)	0.00 (1)	-3.98 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)
3	0.00 (1)	0.00 (1)	-3.99 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)
4	0.00 (1)	0.00 (1)	-4.01 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
5	0.00 (1)	0.00 (1)	-4.02 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
6	0.00 (1)	0.00 (1)	-4.02 (3)	-0.02 (13-I-2)	0.01 (14-I-4)	0.00 (1)
7	0.00 (1)	0.00 (1)	-4.03 (3)	-0.02 (13-I-2)	0.01 (14-II-4)	0.00 (1)
8	0.00 (1)	0.00 (1)	-4.03 (3)	-0.02 (13-I-2)	0.01 (14-II-4)	0.00 (1)
9	0.00 (1)	0.00 (1)	-4.03 (3)	-0.02 (13-I-2)	0.01 (14-II-4)	0.00 (1)
10	0.00 (1)	0.00 (1)	-3.96 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)
11	0.00 (1)	0.00 (1)	-3.98 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)
12	0.00 (1)	0.00 (1)	-3.99 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)
13	0.00 (1)	0.00 (1)	-4.00 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
14	0.00 (1)	0.00 (1)	-4.01 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
15	0.00 (1)	0.00 (1)	-4.02 (3)	-0.02 (13-I-2)	0.01 (14-II-4)	0.00 (1)
16	0.00 (1)	0.00 (1)	-4.02 (3)	-0.02 (13-I-2)	0.01 (14-II-4)	0.00 (1)
17	0.00 (1)	0.00 (1)	-4.03 (3)	-0.02 (13-I-2)	0.01 (14-II-4)	0.00 (1)
18	0.00 (1)	0.00 (1)	-4.03 (3)	-0.02 (13-I-2)	0.01 (14-II-4)	0.00 (1)
19	0.00 (1)	0.00 (1)	-3.94 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)
20	0.00 (1)	0.00 (1)	-3.95 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)
21	0.00 (1)	0.00 (1)	-3.96 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)
22	0.00 (1)	0.00 (1)	-3.98 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
23	0.00 (1)	0.00 (1)	-3.99 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
24	0.00 (1)	0.00 (1)	-3.99 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
25	0.00 (1)	0.00 (1)	-4.00 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
26	0.00 (1)	0.00 (1)	-4.00 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
27	0.00 (1)	0.00 (1)	-4.00 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
28	0.00 (1)	0.00 (1)	-3.92 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)
29	0.00 (1)	0.00 (1)	-3.93 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)
30	0.00 (1)	0.00 (1)	-3.94 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)
31	0.00 (1)	0.00 (1)	-3.96 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
32	0.00 (1)	0.00 (1)	-3.97 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
33	0.00 (1)	0.00 (1)	-3.97 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)



Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
34	0.00 (1)	0.00 (1)	-3.98 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
35	0.00 (1)	0.00 (1)	-3.98 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
36	0.00 (1)	0.00 (1)	-3.98 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
37	0.00 (1)	0.00 (1)	-3.91 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)
38	0.00 (1)	0.00 (1)	-3.92 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)
39	0.00 (1)	0.00 (1)	-3.93 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)
40	0.00 (1)	0.00 (1)	-3.94 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
41	0.00 (1)	0.00 (1)	-3.95 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
42	0.00 (1)	0.00 (1)	-3.96 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)
43	0.00 (1)	0.00 (1)	-3.96 (3)	-0.02 (13-II-3)	0.01 (14-I-4)	0.00 (1)
44	0.00 (1)	0.00 (1)	-3.97 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
45	0.00 (1)	0.00 (1)	-3.97 (3)	-0.02 (13-II-3)	0.01 (14-II-4)	0.00 (1)
112	0.16 (14-I-4)	0.46 (13-I-4)	-3.99 (3)	-0.06 (13-I-4)	0.04 (14-II-4)	0.00 (12-I-4)
113	0.14 (14-I-4)	0.45 (13-I-4)	-4.00 (3)	-0.06 (13-II-4)	0.03 (14-I-4)	0.00 (12-II-1)
114	0.13 (14-I-4)	0.46 (13-II-2)	-4.01 (3)	-0.06 (13-II-4)	0.03 (14-I-4)	0.00 (12-I-1)
115	0.13 (14-I-4)	0.46 (13-II-2)	-4.02 (3)	-0.06 (13-II-2)	0.03 (14-I-4)	0.00 (12-II-2)
116	0.17 (14-II-4)	0.48 (13-I-2)	-4.02 (3)	-0.07 (13-I-2)	0.05 (14-II-1)	0.00 (12-I-2)
130	0.15 (14-I-4)	0.51 (13-I-4)	-3.94 (3)	-0.08 (13-I-4)	0.04 (14-II-4)	0.00 (13-II-4)
131	0.13 (14-I-4)	0.51 (13-I-3)	-3.96 (3)	-0.07 (13-II-4)	0.03 (14-I-4)	-0.00 (14-I-4)
132	0.13 (14-I-4)	0.53 (13-I-3)	-3.97 (3)	-0.08 (13-I-3)	0.03 (14-I-4)	-0.00 (14-II-3)
133	0.13 (14-I-4)	0.53 (13-II-2)	-3.97 (3)	-0.08 (13-II-2)	0.03 (14-I-4)	-0.00 (14-II-2)
134	0.16 (14-II-4)	0.54 (13-I-2)	-3.98 (3)	-0.08 (13-I-2)	0.05 (14-II-3)	-0.00 (15-II-2)

Tipo diagramma: Deformata  
Combinazione corrente : Scenario ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO - C 3



Risultati Analisi Dinamica - Reazioni massime - Nodi  
Scenario di calcolo: ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO

Nodo	Rx	Ry	Rz	Mx	My	Mz
	daN	daN	daN	daN*m	daN*m	daN*m
1	-28.21 (2)	-8.62 (2)	0	0	0	0
2	-217.97 (2)	-17.17 (15-I-3)	0	0	0	-2.69 (13-I-3)
3	-247.54 (2)	-8.52 (2)	0	0	0	1.84 (2)
4	-140.85 (12-II-4)	-13.50 (2)	0	0	0	0
5	-79.28 (12-II-1)	-14.41 (2)	0	0	0	0
6	-80.12 (12-II-2)	-15.83 (2)	0	0	0	0
7	153.66 (2)	-14.20 (2)	0	0	0	-3.08 (15-I-2)
8	115.44 (2)	-12.39 (14-I-1)	0	0	0	0
9	14.76 (2)	-5.07 (2)	0	0	0	0
10	-87.15 (2)	111.35 (13-II-4)	0	0	0	11.87 (2)
11	-663.46 (2)	217.51 (9)	0	0	0	41.58 (11)
12	-628.96 (9)	-378.75 (15-I-3)	0	0	0	16.32 (15-II-4)
13	-454.68 (12-I-4)	-890.77 (15-I-3)	0	0	0	-34.36 (9)
14	-443.59 (12-I-1)	-880.13 (15-I-3)	0	0	0	33.91 (12-I-1)
15	-627.65 (12-I-1)	-889.81 (15-I-3)	0	0	0	49.98 (12-I-1)

Nodo	Rx	Ry	Rz	Mx	My	Mz
16	350.55(14-II-2)	-419.56(15-I-2)	0	0	0	14.00(13-I-2)
17	455.86(14-II-2)	215.39(12-II-2)	0	0	0	-34.45(14-II-2)
18	58.97(2)	52.37(4)	0	0	0	-8.89(12-II-2)
19	-131.07(2)	404.20(13-II-4)	0	0	0	5.15(13-I-1)
20	-652.27(11)	488.03(13-II-4)	0	0	0	-14.44(13-II-4)
21	-275.45(11)	669.73(13-II-4)	0	0	0	-9.10(13-II-4)
22	-172.66(12-II-4)	873.15(13-II-4)	0	0	0	-5.48(15-II-2)
23	138.41(11)	870.09(13-II-4)	0	0	0	-3.36(14-II-1)
24	177.20(11)	832.18(13-I-1)	0	0	0	2.36(13-II-4)
25	144.28(11)	512.13(13-I-1)	0	0	0	0
26	417.46(11)	364.15(13-II-2)	0	0	0	11.12(15-II-2)
27	100.11(12-II-2)	186.33(13-II-2)	0	0	0	1.16(14-I-1)
28	-97.72(11)	167.61(13-II-4)	0	0	0	-13.20(9)
29	-657.95(11)	-298.03(9)	0	0	0	-26.82(2)
30	-601.99(9)	-483.62(13-I-4)	0	0	0	26.63(13-II-4)
31	-369.69(12-I-4)	-1323.63(13-I-1)	0	0	0	35.09(9)
32	-344.70(12-II-3)	-1314.82(13-I-1)	0	0	0	-28.53(12-II-3)
33	-539.95(12-II-3)	-1350.23(13-I-1)	0	0	0	-39.70(12-II-3)
34	497.79(14-II-2)	-489.08(13-I-2)	0	0	0	15.85(15-I-2)
35	492.55(14-II-2)	-219.36(4)	0	0	0	21.07(14-II-2)
36	64.49(11)	-97.49(9)	0	0	0	7.40(10)
37	-49.48(15-I-1)	15.96(15-II-4)	0	0	0	-2.36(9)
38	-432.68(15-I-1)	22.45(15-I-3)	0	0	0	-9.14(11)
39	-585.51(13-II-4)	67.62(15-I-1)	0	0	0	-11.74(11)
40	-262.10(13-II-4)	112.26(15-II-4)	0	0	0	-6.73(13-II-4)
41	90.08(2)	111.39(15-II-4)	0	0	0	3.19(2)
42	185.95(15-II-2)	123.32(15-II-2)	0	0	0	6.22(15-II-2)
43	347.19(15-I-1)	86.99(15-II-2)	0	0	0	11.79(11)
44	218.56(15-I-1)	32.48(14-II-3)	0	0	0	9.41(11)
45	27.95(15-I-1)	9.32(14-II-3)	0	0	0	1.73(13-I-1)

**Risultati Analisi Dinamica - Spostamenti massimi - Impalcati**

Scenario di calcolo: **ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Piano	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	mm	mm	mm	°	°	°
1	0.10(14-I-4)	0.36(13-I-3)	-3.99(3-1)	0.00(1-1)	0.00(1-1)	0.00(13-I-2)

**Risultati Analisi Dinamica - Spostamenti massimi - Impalcati (SLD)**

Scenario di calcolo: **ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Piano	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	mm	mm	mm	°	°	°
1	0.06(31-I-4)	0.20(30-I-3)	-1.27(20-1)	0.00(16-1)	0.00(16-1)	0.00(30-I-2)

**Risultati Analisi Dinamica - Sollecitazioni Massime - Muri discretizzati**

Scenario di calcolo: **ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO**

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
		MPa	MPa	MPa	daN*m/m	daN*m/m	daN*m/m
1	1	0.0(15-I-2)	-0.0(13-II-4)	0.0(2)	13.57(2)	-4.34(13-II-4)	14.39(2)
1	2	0.0(15-II-2)	-0.0(9)	-0.0(15-II-4)	16.42(2)	12.50(9)	-30.76(2)
1	3	0.0(15-II-4)	-0.0(9)	0.0(2)	-46.55(11)	-6.04(9)	11.26(15-II-4)
1	4	0.0(15-II-4)	-0.0(9)	0.0(9)	-48.81(15-II-4)	19.22(9)	-58.36(2)
2	1	-0.0(9)	0.0(15-II-4)	-0.0(2)	44.50(9)	-78.69(15-II-4)	60.29(9)
2	2	-0.0(9)	0.0(15-II-4)	-0.0(2)	45.87(2)	27.81(2)	28.49(9)
2	3	-0.0(9)	0.0(11)	0.0(13-II-4)	118.09(9)	-89.61(11)	-64.61(13-II-4)
2	4	-0.0(9)	0.0(11)	0.0(13-II-4)	107.91(9)	21.53(11)	36.34(2)
3	1	-0.0(13-I-1)	0.0(2)	0.0(13-I-1)	37.30(13-I-1)	-72.38(2)	-83.55(13-II-4)
3	2	-0.0(13-I-1)	0.0(2)	0.0(13-II-4)	35.39(10)	29.78(15-II-4)	-43.94(13-II-4)
3	3	-0.0(13-I-1)	0.0(2)	0.0(13-II-4)	-10.58(9)	-74.97(2)	-35.02(13-II-4)
3	4	-0.0(10)	0.0(2)	0.0(13-II-4)	10.37(15-II-4)	27.72(15-II-4)	8.91(2)
4	1	-0.0(9)	0.0(2)	0.0(13-II-4)	127.52(9)	-88.71(11)	-89.90(13-II-4)
4	2	-0.0(9)	0.0(11)	0.0(13-II-4)	121.23(9)	22.35(2)	-42.65(13-II-4)
4	3	-0.0(10)	0.0(2)	0.0(13-II-4)	87.53(13-II-4)	-89.31(2)	-94.07(13-II-4)
4	4	-0.0(9)	0.0(2)	0.0(13-II-4)	83.39(13-II-4)	21.50(11)	-41.58(13-II-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
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BTK3**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
5	1	-0.1 (14-II-2)	-0.5 (14-II-3)	-0.1 (11)	-173.04 (15-I-2)	-2144.45 (15-I-2)	-117.21 (15-II-2)
5	2	-0.1 (14-II-2)	-0.5 (14-II-3)	0.1 (12-I-2)	-92.05 (15-I-2)	-2036.74 (15-I-2)	-36.00 (14-I-2)
5	3	-0.4 (14-II-3)	-0.6 (14-II-2)	0.3 (12-I-2)	-223.52 (15-I-2)	-2195.85 (15-I-2)	379.30 (13-I-2)
5	4	-0.3 (14-II-2)	1.2 (12-I-2)	0.1 (9)	172.48 (12-I-2)	-3116.59 (15-I-2)	1363.26 (13-I-2)
5	5	-0.1 (14-II-2)	-0.2 (14-II-2)	-0.0 (11)	-247.92 (15-I-2)	-2159.61 (15-II-2)	-36.56 (15-II-2)
5	6	-0.2 (14-II-2)	-0.1 (11)	-0.1 (14-II-2)	-184.75 (15-I-2)	-1934.46 (15-II-2)	-31.57 (15-II-2)
5	7	-0.1 (14-II-2)	0.1 (12-I-2)	-0.2 (14-II-2)	-259.67 (15-I-2)	-1468.01 (15-II-2)	201.13 (13-I-2)
5	8	0.4 (12-II-3)	0.0 (9)	-0.2 (14-II-3)	-334.89 (15-I-2)	-255.74 (15-II-2)	304.15 (13-I-2)
5	9	-0.0 (11)	-0.2 (14-II-2)	-0.1 (14-II-2)	-254.92 (15-I-1)	-2145.02 (15-I-1)	23.87 (13-I-2)
5	10	-0.1 (11)	-0.2 (14-II-2)	-0.2 (14-II-2)	-196.16 (15-I-2)	-1903.61 (15-I-1)	37.34 (13-I-2)
5	11	-0.1 (14-II-2)	-0.1 (14-II-2)	-0.3 (14-II-2)	-277.22 (15-I-2)	-1434.19 (15-I-1)	-137.42 (15-II-2)
5	12	0.1 (12-I-2)	0.1 (12-I-2)	-0.1 (14-II-2)	-354.46 (15-I-2)	-283.73 (15-I-1)	-224.61 (15-II-2)
5	13	-0.0 (9)	-0.2 (12-II-2)	-0.1 (11)	-274.29 (15-I-1)	-2107.29 (15-I-1)	25.30 (13-I-2)
5	14	-0.0 (9)	-0.2 (12-II-2)	-0.1 (11)	-281.48 (15-I-1)	-1966.22 (15-I-1)	42.09 (13-I-2)
5	15	0.3 (12-I-2)	-0.5 (12-II-2)	-0.1 (9)	-163.37 (15-I-2)	-2050.26 (15-I-1)	-189.88 (15-II-2)
5	16	-0.1 (9)	-2.0 (14-II-2)	-0.5 (14-II-2)	-137.36 (14-II-2)	-2813.33 (15-II-2)	-1340.31 (15-II-2)
6	1	-0.5 (14-I-1)	-0.1 (14-II-2)	-0.1 (2)	1770.71 (15-I-2)	145.55 (15-I-2)	86.91 (15-II-2)
6	2	-0.2 (14-II-2)	-0.1 (14-I-1)	-0.1 (2)	1765.55 (15-II-2)	206.63 (15-I-2)	24.96 (15-II-2)
6	3	-0.2 (12-II-2)	-0.1 (2)	-0.1 (14-II-2)	1745.27 (15-I-3)	209.82 (15-I-3)	-21.88 (13-I-2)
6	4	-0.2 (12-II-2)	-0.0 (9)	-0.1 (2)	1715.39 (15-I-3)	221.98 (15-I-3)	-22.07 (13-I-2)
6	5	-0.5 (14-I-1)	-0.1 (14-I-1)	0.1 (12-I-2)	1640.22 (15-I-2)	77.69 (15-I-2)	-36.46 (13-I-2)
6	6	-0.1 (2)	-0.2 (14-I-1)	-0.1 (14-II-2)	1553.48 (15-II-2)	160.49 (15-I-2)	-29.22 (13-I-2)
6	7	-0.1 (12-II-2)	-0.1 (2)	-0.2 (14-II-2)	1521.74 (15-I-3)	165.33 (15-I-2)	-35.99 (13-I-2)
6	8	-0.2 (12-II-2)	-0.1 (9)	-0.1 (2)	1566.20 (15-I-3)	220.06 (15-I-3)	-37.12 (13-I-2)
6	9	-0.6 (14-II-2)	-0.4 (14-II-2)	0.3 (12-I-2)	1723.19 (15-I-2)	180.52 (15-I-2)	-320.72 (13-I-2)
6	10	0.1 (12-I-2)	-0.1 (14-II-2)	-0.2 (14-II-2)	1159.52 (15-II-2)	223.15 (15-I-2)	-178.21 (13-I-2)
6	11	-0.1 (14-II-2)	-0.1 (14-II-2)	-0.3 (14-II-2)	1124.37 (15-I-3)	230.17 (15-I-2)	102.64 (15-II-2)
6	12	-0.5 (12-II-2)	0.3 (12-I-2)	-0.1 (9)	1581.71 (15-I-3)	123.09 (15-I-2)	145.82 (15-II-2)
6	13	1.2 (12-I-2)	-0.3 (14-II-2)	0.1 (9)	2390.14 (15-I-2)	172.90 (14-I-2)	-1070.17 (13-I-2)
6	14	0.0 (9)	0.4 (12-I-2)	-0.2 (14-I-1)	204.08 (15-II-2)	286.80 (15-I-2)	-256.14 (13-I-2)
6	15	0.1 (12-I-2)	0.1 (12-I-2)	-0.1 (14-II-2)	225.95 (15-I-3)	293.71 (15-I-2)	167.72 (15-II-2)
6	16	-2.0 (14-II-2)	-0.2 (9)	-0.5 (14-II-2)	2093.85 (15-II-2)	-132.20 (12-II-2)	996.03 (15-II-2)
7	1	-0.2 (9)	-0.0 (14-II-2)	-0.1 (14-I-1)	1700.07 (15-I-3)	220.45 (15-I-3)	10.69 (15-II-2)
7	2	-0.1 (9)	-0.0 (2)	-0.1 (14-I-1)	1699.45 (15-I-3)	205.18 (15-I-3)	11.40 (15-II-2)
7	3	-0.1 (12-I-2)	-0.1 (9)	-0.1 (14-I-1)	1690.53 (15-I-3)	203.67 (15-I-3)	-20.87 (13-I-2)
7	4	-0.2 (12-I-2)	-0.0 (9)	-0.0 (14-I-1)	1671.64 (13-I-3)	215.85 (13-I-3)	-20.02 (13-I-2)
7	5	-0.2 (9)	-0.1 (14-II-2)	-0.0 (2)	1553.49 (15-I-3)	218.97 (15-I-3)	-20.78 (13-I-2)
7	6	-0.1 (9)	-0.1 (14-I-2)	-0.1 (14-I-1)	1483.08 (15-I-3)	164.11 (15-I-3)	-22.61 (13-I-2)
7	7	-0.2 (12-I-2)	-0.1 (9)	-0.2 (14-I-1)	1475.90 (15-I-3)	161.60 (15-I-3)	-26.25 (13-I-2)
7	8	-0.3 (12-I-2)	-0.1 (9)	-0.0 (2)	1530.62 (13-I-3)	211.88 (13-I-3)	-27.86 (13-I-2)
7	9	-0.3 (9)	-0.3 (14-II-2)	0.1 (12-II-1)	1573.51 (15-I-3)	120.68 (15-I-2)	-187.55 (13-I-2)
7	10	0.1 (14-I-1)	-0.2 (9)	-0.2 (14-I-1)	1096.02 (15-I-3)	226.36 (15-I-3)	-145.04 (13-I-2)
7	11	-0.2 (12-I-2)	-0.2 (2)	-0.3 (14-I-1)	1091.84 (15-I-3)	222.62 (15-I-3)	115.17 (15-II-2)
7	12	-0.5 (12-I-2)	0.2 (12-II-2)	-0.1 (9)	1560.23 (13-I-3)	115.45 (13-I-2)	150.13 (15-II-2)
7	13	1.6 (14-I-1)	-0.2 (9)	-0.3 (14-I-1)	2092.77 (15-II-2)	132.00 (14-I-1)	-1033.59 (13-I-2)
7	14	-0.0 (12-II-1)	-0.1 (9)	-0.1 (14-I-1)	213.27 (15-I-3)	286.19 (15-I-3)	-211.91 (13-I-2)
7	15	0.0 (12-II-1)	-0.2 (2)	-0.1 (14-I-1)	212.00 (15-I-3)	281.10 (15-I-3)	185.23 (15-II-2)
7	16	-2.0 (12-II-2)	-0.3 (2)	-0.4 (14-II-2)	2088.88 (15-II-2)	-142.26 (14-I-1)	1003.98 (15-II-2)
8	1	0.0 (11)	-0.0 (4)	0.0 (15-II-2)	-53.74 (2)	229.40 (4)	73.65 (4)
8	2	0.0 (14-II-2)	-0.0 (4)	-0.0 (2)	-44.08 (14-II-2)	-87.83 (15-I-3)	88.58 (4)
8	3	0.0 (11)	-0.0 (4)	-0.0 (9)	-192.59 (11)	233.13 (4)	-59.62 (13-II-2)
8	4	0.0 (14-II-2)	0.0 (15-I-3)	-0.0 (9)	-238.26 (14-II-2)	-175.97 (15-I-3)	-82.85 (13-I-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
9	1	-0.0 (14-I-2)	-0.1 (9)	0.1 (9)	-256.89 (13-I-1)	-1947.23 (13-I-1)	-9.33 (14-II-4)
9	2	-0.1 (14-I-3)	-0.2 (9)	0.1 (11)	-265.00 (13-I-1)	-1829.07 (13-I-1)	39.50 (13-II-4)
9	3	-0.3 (14-II-3)	-0.3 (9)	0.2 (14-II-4)	-159.57 (13-I-4)	-1921.19 (13-I-1)	276.92 (13-II-4)
9	4	-0.2 (11)	1.5 (14-I-3)	-0.2 (12-I-4)	101.75 (14-I-4)	-2614.27 (13-I-1)	1285.40 (13-II-4)
9	5	-0.0 (9)	-0.1 (9)	0.1 (9)	-235.17 (13-I-1)	-1947.83 (13-I-1)	-9.87 (15-I-4)
9	6	-0.1 (11)	-0.1 (9)	0.1 (9)	-199.91 (13-I-1)	-1693.57 (13-I-1)	33.34 (13-II-4)
9	7	-0.1 (11)	-0.0 (9)	-0.2 (12-I-4)	-301.32 (13-I-1)	-1205.39 (13-I-1)	191.02 (13-II-4)
9	8	-0.1 (14-II-4)	-0.0 (14-II-4)	-0.0 (12-I-4)	-410.28 (13-I-1)	-185.19 (13-I-1)	244.78 (13-II-4)
9	9	-0.1 (9)	-0.1 (9)	0.1 (11)	-231.48 (13-I-1)	-1951.70 (13-I-1)	36.18 (13-II-4)
9	10	-0.1 (9)	-0.1 (10)	0.1 (11)	-194.71 (13-I-1)	-1709.47 (13-I-1)	18.34 (13-II-4)
9	11	-0.1 (11)	-0.1 (14-I-4)	-0.2 (12-I-4)	-286.76 (13-I-1)	-1221.57 (13-I-1)	-194.91 (15-I-4)
9	12	-0.2 (14-I-4)	0.0 (14-II-4)	-0.1 (12-I-4)	-401.50 (13-I-1)	-165.02 (13-I-1)	-264.03 (15-I-4)
9	13	-0.1 (9)	-0.4 (9)	0.1 (11)	-174.81 (13-I-1)	-1941.63 (13-I-1)	86.21 (13-II-4)
9	14	-0.0 (9)	-0.4 (9)	0.1 (14-II-4)	-114.08 (13-I-1)	-1862.22 (13-I-1)	-29.32 (15-I-4)
9	15	0.3 (12-II-4)	-0.3 (9)	0.2 (14-II-4)	-212.64 (13-I-1)	-2035.28 (13-I-1)	-398.21 (15-I-4)
9	16	0.0 (9)	-1.4 (14-I-4)	-0.2 (12-I-4)	-144.68 (12-I-4)	-2782.81 (13-I-4)	-1247.02 (15-I-4)
10	1	-0.0 (14-I-2)	-0.2 (9)	-0.0 (14-II-3)	-265.07 (15-I-1)	-2041.83 (15-I-1)	-10.22 (15-I-2)
10	2	-0.1 (14-I-2)	-0.2 (9)	0.0 (12-I-3)	-269.99 (15-I-1)	-1915.98 (15-I-1)	-12.95 (14-I-3)
10	3	-0.3 (14-I-2)	-0.3 (9)	0.2 (12-II-4)	-150.45 (15-I-2)	-2021.02 (15-I-1)	225.88 (13-II-2)
10	4	-0.3 (11)	1.6 (14-I-4)	-0.2 (14-I-4)	118.90 (12-I-4)	-2808.57 (15-II-4)	1373.79 (13-II-4)
10	5	-0.1 (14-I-2)	-0.1 (9)	-0.1 (14-II-3)	-242.27 (15-I-1)	-2044.10 (15-I-1)	-7.71 (15-I-4)
10	6	-0.1 (14-I-2)	-0.1 (9)	-0.1 (14-I-4)	-186.23 (15-I-1)	-1825.13 (15-I-1)	23.14 (13-II-4)
10	7	-0.2 (11)	-0.1 (9)	-0.2 (14-I-4)	-261.55 (15-I-1)	-1383.52 (15-I-1)	183.38 (13-II-4)
10	8	-0.2 (11)	-0.0 (12-I-3)	-0.1 (14-I-3)	-331.40 (15-I-1)	-263.34 (15-I-1)	273.11 (13-II-4)
10	9	-0.0 (11)	-0.2 (12-II-3)	-0.1 (12-I-4)	-239.20 (15-I-1)	-2022.98 (15-I-1)	33.89 (13-II-4)
10	10	-0.1 (11)	-0.2 (12-II-3)	-0.1 (12-I-4)	-181.99 (15-I-1)	-1810.95 (15-I-1)	44.00 (13-II-4)
10	11	-0.2 (11)	-0.2 (12-II-3)	-0.3 (12-II-3)	-255.67 (15-I-1)	-1369.67 (13-I-1)	-116.61 (15-I-4)
10	12	-0.2 (14-I-2)	0.0 (12-II-4)	-0.1 (14-II-3)	-327.72 (15-I-1)	-269.62 (13-I-1)	-211.41 (15-I-4)
10	13	-0.0 (9)	-0.2 (12-II-3)	0.0 (9)	-257.94 (15-I-1)	-1977.05 (13-I-1)	36.83 (13-II-4)
10	14	-0.1 (11)	-0.3 (12-II-3)	0.0 (14-II-4)	-265.54 (15-I-1)	-1872.90 (13-I-1)	58.32 (13-II-4)
10	15	0.2 (12-II-2)	-0.6 (12-II-3)	0.1 (14-I-3)	-138.17 (13-I-2)	-2000.47 (13-I-1)	-159.51 (15-I-4)
10	16	-0.3 (14-II-3)	-1.9 (12-II-3)	-0.4 (12-II-3)	-144.14 (12-II-3)	-2701.25 (13-I-1)	-1291.51 (15-I-4)
11	1	-0.2 (9)	-0.1 (14-I-2)	-0.0 (14-I-1)	1662.65 (13-I-3)	214.34 (13-I-3)	6.92 (15-I-2)
11	2	-0.1 (9)	-0.1 (14-I-2)	-0.1 (14-I-1)	1661.79 (13-I-3)	198.69 (13-I-3)	5.79 (14-I-4)
11	3	-0.2 (12-II-1)	-0.0 (2)	-0.1 (12-I-4)	1645.40 (13-I-3)	196.28 (13-I-3)	-26.25 (13-II-4)
11	4	-0.2 (12-I-1)	-0.0 (9)	0.0 (9)	1612.52 (13-I-3)	208.75 (13-I-3)	-28.29 (13-II-4)
11	5	-0.2 (9)	-0.1 (14-I-2)	0.0 (12-II-1)	1523.17 (13-I-3)	209.42 (13-I-3)	-15.17 (13-II-2)
11	6	-0.1 (9)	-0.1 (14-I-2)	-0.1 (14-I-4)	1452.59 (13-I-3)	154.08 (13-I-3)	-23.49 (13-II-4)
11	7	-0.2 (12-II-1)	-0.1 (2)	-0.1 (12-I-4)	1441.91 (13-I-3)	150.83 (13-I-3)	-33.72 (13-II-4)
11	8	-0.3 (12-I-1)	-0.1 (2)	0.0 (14-II-4)	1490.87 (13-I-3)	206.02 (13-I-3)	-44.07 (13-II-4)
11	9	-0.3 (9)	-0.3 (14-I-2)	0.2 (12-II-4)	1555.58 (13-I-3)	110.65 (13-I-2)	-178.70 (13-II-2)
11	10	-0.1 (9)	-0.2 (2)	-0.2 (14-I-4)	1077.87 (13-I-3)	211.17 (13-I-3)	-146.49 (13-II-4)
11	11	-0.2 (12-II-1)	-0.2 (2)	-0.2 (12-I-1)	1067.68 (13-I-3)	206.76 (13-I-3)	94.01 (15-I-4)
11	12	-0.6 (12-I-1)	0.2 (12-II-2)	0.1 (14-II-1)	1540.82 (13-I-3)	101.02 (13-I-2)	127.33 (15-I-4)
11	13	1.6 (14-I-4)	-0.3 (2)	-0.2 (14-I-4)	2088.14 (13-II-2)	119.43 (12-I-4)	-1027.15 (13-II-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
11	14	-0.0 (12-II-1)	-0.2 (2)	-0.1 (14-I-1)	207.33 (13-I-3)	266.53 (13-I-3)	-213.64 (13-II-4)
11	15	0.0 (12-II-4)	-0.2 (14-I-2)	-0.1 (12-I-1)	211.97 (13-I-3)	263.75 (13-I-3)	165.20 (15-I-4)
11	16	-1.9 (12-I-1)	-0.3 (14-II-1)	-0.4 (12-I-1)	2008.74 (13-I-3)	-145.43 (14-I-1)	964.19 (15-I-4)
12	1	-0.0 (14-II-2)	-0.2 (9)	-0.1 (14-II-3)	-272.68 (15-I-1)	-2089.47 (15-I-1)	-15.75 (15-II-2)
12	2	-0.1 (14-II-2)	-0.2 (9)	-0.0 (11)	-281.12 (15-I-1)	-1952.96 (15-I-1)	-18.73 (14-II-2)
12	3	-0.3 (14-II-2)	-0.3 (9)	0.1 (12-II-3)	-162.50 (15-I-2)	-2042.31 (15-I-1)	231.01 (13-I-2)
12	4	-0.2 (9)	1.6 (14-II-2)	-0.3 (14-I-3)	131.91 (12-II-2)	-2812.59 (15-II-2)	1377.01 (13-I-2)
12	5	-0.0 (11)	-0.1 (9)	-0.1 (14-I-3)	-250.56 (15-I-1)	-2093.00 (15-I-1)	-16.15 (15-II-2)
12	6	-0.1 (14-I-2)	-0.1 (9)	-0.1 (14-I-3)	-198.57 (15-I-1)	-1863.98 (15-I-1)	18.81 (13-I-2)
12	7	-0.1 (9)	0.1 (14-II-2)	-0.2 (14-I-3)	-279.93 (15-I-1)	-1406.34 (15-I-1)	177.17 (13-I-2)
12	8	-0.1 (9)	-0.0 (12-I-2)	-0.1 (14-II-3)	-355.07 (15-I-1)	-270.83 (15-I-1)	266.96 (13-I-2)
12	9	-0.1 (9)	-0.1 (12-I-2)	-0.1 (14-I-3)	-248.70 (15-I-1)	-2081.73 (15-I-1)	25.11 (13-I-2)
12	10	-0.1 (9)	-0.2 (12-I-2)	-0.2 (14-I-3)	-195.70 (15-I-1)	-1855.30 (15-I-1)	31.37 (13-I-2)
12	11	-0.2 (11)	-0.2 (12-I-2)	-0.3 (14-II-3)	-275.80 (15-I-1)	-1401.47 (15-I-1)	-144.36 (15-II-2)
12	12	-0.1 (11)	0.0 (12-II-3)	-0.1 (14-II-3)	-349.56 (15-I-1)	-269.42 (15-I-1)	-237.60 (15-II-2)
12	13	-0.0 (9)	-0.2 (12-II-4)	-0.0 (14-I-3)	-267.04 (15-I-1)	-2053.70 (15-I-1)	24.79 (13-I-2)
12	14	-0.1 (9)	-0.3 (12-I-2)	-0.0 (11)	-273.09 (15-I-1)	-1925.64 (15-I-1)	35.03 (13-I-2)
12	15	0.2 (12-II-2)	-0.5 (12-II-2)	-0.1 (9)	-156.22 (15-I-2)	-2027.01 (15-I-1)	-190.30 (15-II-2)
12	16	-0.2 (11)	-2.0 (12-II-2)	-0.4 (14-II-2)	-142.92 (14-I-3)	-2809.65 (15-II-4)	-1345.18 (15-II-2)
13	1	-0.1 (9)	-0.0 (14-I-2)	0.1 (9)	1588.90 (13-I-3)	208.06 (13-I-3)	-7.82 (13-II-4)
13	2	-0.1 (9)	-0.0 (9)	0.1 (9)	1587.03 (13-I-3)	194.22 (15-I-3)	8.37 (15-I-4)
13	3	-0.1 (9)	-0.1 (9)	0.1 (2)	1598.32 (13-I-3)	193.74 (13-I-3)	-24.06 (13-II-4)
13	4	-0.4 (9)	-0.1 (9)	0.1 (2)	1609.67 (13-I-3)	147.12 (13-I-3)	-62.30 (13-II-4)
13	5	-0.2 (9)	-0.1 (14-I-2)	0.1 (2)	1458.74 (13-I-3)	206.88 (13-I-3)	-34.85 (13-II-4)
13	6	-0.1 (9)	-0.1 (2)	0.1 (9)	1357.86 (13-I-3)	169.17 (13-I-3)	-27.57 (13-II-4)
13	7	-0.1 (12-I-4)	-0.1 (9)	0.1 (2)	1377.53 (13-I-3)	169.56 (13-I-3)	27.90 (15-I-4)
13	8	-0.4 (9)	-0.0 (9)	0.1 (14-II-4)	1504.12 (13-I-3)	95.81 (13-I-3)	43.02 (15-I-4)
13	9	-0.3 (9)	-0.3 (14-I-2)	0.2 (14-II-4)	1482.77 (13-I-3)	118.88 (13-I-4)	-215.08 (13-II-4)
13	10	-0.0 (9)	-0.1 (2)	-0.2 (12-I-4)	949.89 (13-I-3)	250.90 (13-I-3)	-144.83 (13-II-4)
13	11	-0.1 (14-I-4)	-0.1 (2)	-0.2 (12-I-4)	970.12 (13-I-3)	246.24 (13-I-3)	168.94 (15-I-4)
13	12	-0.3 (9)	0.3 (12-II-4)	0.2 (14-II-4)	1598.61 (13-I-3)	174.32 (13-I-3)	334.49 (15-I-4)
13	13	1.5 (14-II-1)	-0.2 (2)	-0.2 (12-II-1)	1944.79 (13-I-3)	100.01 (12-I-4)	-959.78 (13-II-4)
13	14	-0.0 (14-II-4)	-0.1 (14-I-1)	-0.0 (12-I-4)	151.91 (13-I-3)	338.44 (13-I-3)	-184.94 (13-II-4)
13	15	0.0 (14-II-4)	-0.2 (14-I-4)	-0.1 (12-I-4)	134.58 (13-I-3)	339.64 (13-I-3)	220.96 (15-I-4)
13	16	-1.4 (14-I-4)	0.0 (9)	-0.2 (12-I-4)	2133.92 (13-I-4)	-142.65 (14-I-4)	980.00 (15-I-4)
14	1	0.0 (2)	-0.0 (13-I-1)	-0.0 (13-II-4)	-290.72 (2)	118.31 (13-I-1)	172.52 (13-II-4)
14	2	0.1 (2)	-0.0 (9)	-0.0 (13-II-4)	-276.24 (2)	203.02 (9)	120.27 (13-II-4)
14	3	0.0 (2)	-0.0 (10)	-0.0 (13-II-4)	-78.06 (2)	84.43 (13-I-1)	115.94 (13-II-4)
14	4	0.0 (2)	-0.0 (9)	-0.0 (13-II-4)	-84.75 (11)	183.36 (9)	93.93 (13-II-4)
15	1	0.1 (11)	-0.1 (9)	0.0 (14-I-1)	-320.94 (2)	322.93 (9)	163.09 (13-II-4)
15	2	0.1 (2)	0.1 (15-I-3)	0.0 (12-I-1)	-365.91 (11)	-417.52 (15-I-3)	141.74 (13-II-4)
15	3	0.1 (2)	-0.0 (9)	-0.0 (13-II-4)	-301.02 (2)	384.76 (9)	-97.10 (14-I-1)
15	4	0.1 (11)	0.1 (15-I-3)	0.0 (14-I-1)	-371.93 (11)	-513.85 (15-I-3)	86.99 (13-II-4)
15	5	0.1 (2)	-0.0 (9)	-0.0 (13-II-4)	-276.70 (2)	367.45 (9)	-91.41 (14-I-1)
15	6	0.1 (11)	0.0 (15-I-3)	-0.0 (13-II-4)	-368.50 (11)	-482.36 (15-I-3)	-88.49 (12-I-1)
15	7	0.1 (11)	-0.0 (9)	-0.0 (13-II-4)	-232.68 (2)	273.13 (9)	-119.88 (9)
15	8	0.1 (11)	0.0 (15-I-3)	-0.0 (13-II-4)	-313.54 (11)	-310.54 (15-I-3)	-146.88 (9)
16	1	0.1 (11)	-0.0 (9)	-0.0 (13-II-4)	-290.51 (11)	206.97 (9)	96.92 (13-II-4)
16	2	0.0 (11)	0.0 (15-I-3)	0.0 (2)	-307.70 (11)	-159.86 (15-I-3)	-118.17 (2)
16	3	0.0 (11)	-0.0 (9)	-0.0 (13-II-4)	-72.97 (11)	185.34 (9)	-97.20 (2)
16	4	0.0 (11)	-0.0 (9)	0.0 (2)	-66.40 (15-II-4)	-65.00 (15-I-3)	-104.95 (9)
17	1	0.1 (11)	-0.1 (13-I-1)	-0.0 (13-II-4)	-344.00 (2)	314.68 (13-I-1)	115.01 (13-II-4)
17	2	0.1 (2)	-0.1 (10)	-0.0 (13-II-4)	-311.17 (11)	311.54 (9)	103.31 (13-II-4)
17	3	0.1 (2)	-0.1 (13-I-1)	-0.0 (13-II-4)	-349.21 (2)	325.80 (13-I-1)	113.15 (13-II-4)
17	4	0.1 (11)	-0.0 (13-I-1)	-0.0 (13-II-4)	-297.29 (11)	377.47 (9)	87.16 (13-II-4)
17	5	0.1 (2)	-0.1 (13-I-1)	-0.0 (13-II-4)	-348.72 (2)	289.95 (13-I-1)	127.87 (13-II-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
17	6	0.1 (11)	-0.0 (13-I-1)	-0.0 (13-II-4)	-278.04 (11)	359.42 (9)	98.38 (13-II-4)
17	7	0.1 (2)	-0.0 (13-I-1)	-0.0 (13-II-4)	-306.18 (2)	203.61 (13-I-1)	154.58 (13-II-4)
17	8	0.1 (2)	-0.0 (10)	-0.0 (13-II-4)	-243.21 (11)	262.95 (9)	97.63 (13-II-4)
18	1	0.1 (11)	-0.1 (13-I-1)	0.0 (15-II-2)	-249.92 (2)	338.57 (13-I-1)	-84.14 (4)
18	2	0.1 (2)	-0.1 (10)	0.0 (15-II-2)	-215.84 (11)	325.77 (4)	-86.28 (2)
18	3	0.1 (2)	-0.1 (13-I-1)	0.0 (14-II-1)	-296.81 (2)	374.53 (13-I-1)	-46.99 (14-II-1)
18	4	0.1 (11)	-0.1 (13-I-1)	0.0 (14-II-1)	-245.51 (11)	404.70 (4)	-41.01 (14-II-1)
18	5	0.1 (2)	-0.1 (13-I-1)	0.0 (14-II-1)	-331.11 (2)	375.87 (13-I-1)	-34.77 (14-II-1)
18	6	0.1 (11)	-0.1 (13-I-1)	0.0 (14-II-1)	-281.21 (11)	406.67 (4)	-31.98 (14-II-1)
18	7	0.1 (11)	-0.1 (13-I-1)	0.0 (14-II-1)	-356.28 (2)	342.43 (13-I-1)	50.82 (9)
18	8	0.1 (2)	-0.1 (10)	0.0 (14-II-1)	-318.44 (11)	330.62 (4)	58.86 (9)
19	1	0.1 (11)	-0.1 (4)	0.0 (14-II-1)	-223.96 (2)	338.14 (4)	120.55 (13-I-2)
19	2	0.1 (2)	0.1 (15-I-3)	0.0 (12-II-1)	-273.40 (11)	-436.82 (15-I-3)	103.48 (13-I-2)
19	3	0.1 (2)	-0.1 (4)	0.0 (14-II-1)	-248.26 (2)	412.68 (4)	-57.20 (14-II-1)
19	4	0.1 (11)	0.1 (15-I-3)	0.0 (14-II-1)	-317.22 (11)	-552.92 (15-I-3)	-40.19 (14-II-1)
19	5	0.1 (2)	-0.1 (4)	0.0 (14-II-1)	-280.67 (2)	414.66 (4)	-71.27 (14-II-1)
19	6	0.1 (11)	0.1 (15-I-3)	0.0 (14-II-1)	-347.26 (11)	-554.96 (15-I-3)	-54.69 (14-II-1)
19	7	0.1 (11)	-0.1 (4)	-0.0 (13-I-2)	-316.58 (2)	343.74 (4)	-101.86 (12-II-1)
19	8	0.1 (2)	0.1 (15-I-3)	-0.0 (13-I-2)	-367.11 (11)	-442.92 (15-I-3)	-94.99 (12-II-1)
20	1	0.1 (11)	-0.1 (13-I-1)	-0.0 (13-I-2)	-322.80 (2)	343.22 (13-I-1)	-72.69 (2)
20	2	0.1 (2)	-0.1 (10)	-0.0 (13-I-2)	-288.03 (11)	331.25 (4)	-87.27 (14-II-1)
20	3	0.1 (2)	-0.1 (13-I-1)	-0.0 (13-I-2)	-350.53 (2)	372.35 (13-I-1)	64.20 (13-II-4)
20	4	0.1 (11)	-0.1 (13-I-1)	-0.0 (13-I-2)	-300.96 (11)	402.08 (4)	57.29 (13-II-4)
20	5	0.1 (2)	-0.1 (13-I-1)	-0.0 (13-II-4)	-360.57 (2)	366.42 (13-I-1)	70.53 (13-II-4)
20	6	0.1 (11)	-0.1 (13-I-1)	-0.0 (13-II-4)	-313.02 (11)	395.47 (9)	61.80 (13-II-4)
20	7	0.1 (11)	-0.1 (13-I-1)	-0.0 (13-II-4)	-357.14 (2)	326.28 (13-I-1)	65.00 (10)
20	8	0.1 (2)	-0.1 (10)	-0.0 (13-II-4)	-323.50 (11)	314.86 (9)	57.66 (9)
21	1	0.1 (11)	-0.1 (4)	0.0 (14-II-1)	-295.41 (2)	342.61 (4)	150.91 (13-II-4)
21	2	0.1 (2)	0.1 (15-I-3)	0.0 (12-II-1)	-340.52 (11)	-435.07 (15-I-3)	129.24 (13-II-4)
21	3	0.1 (2)	-0.1 (9)	0.0 (14-II-1)	-302.51 (2)	407.94 (4)	-72.19 (14-II-1)
21	4	0.1 (11)	0.1 (15-I-3)	0.0 (14-II-1)	-366.06 (11)	-543.12 (15-I-3)	-58.46 (14-II-1)
21	5	0.1 (2)	-0.1 (9)	-0.0 (13-II-4)	-310.73 (2)	401.92 (9)	-89.47 (14-II-1)
21	6	0.1 (11)	0.1 (15-I-3)	0.0 (14-II-1)	-372.61 (11)	-537.77 (15-I-3)	-74.75 (14-II-1)
21	7	0.1 (11)	-0.1 (9)	-0.0 (13-II-4)	-319.08 (2)	327.23 (9)	-111.36 (12-I-1)
21	8	0.1 (2)	0.1 (15-I-3)	-0.0 (13-II-4)	-364.47 (11)	-422.72 (15-I-3)	-115.30 (12-I-1)
22	1	0.1 (2)	0.0 (15-II-4)	-0.0 (13-II-4)	-344.94 (11)	21.52 (2)	30.27 (13-I-3)
22	2	0.1 (2)	-0.0 (13-I-3)	-0.0 (13-I-3)	-355.54 (11)	-43.53 (2)	142.64 (13-II-4)
22	3	0.1 (2)	-0.0 (13-I-3)	-0.0 (13-II-4)	-376.61 (2)	23.08 (2)	36.97 (12-II-4)
22	4	0.1 (2)	-0.0 (13-I-4)	0.0 (2)	-385.18 (2)	-55.47 (2)	-112.61 (2)
22	5	0.1 (2)	0.0 (2)	0.0 (12-I-1)	-351.99 (2)	13.42 (2)	47.99 (12-II-4)
22	6	0.1 (2)	0.0 (2)	0.0 (2)	-360.60 (2)	-38.62 (2)	-119.21 (12-I-1)
22	7	0.1 (2)	0.0 (2)	0.0 (12-I-1)	-374.59 (2)	-4.99 (12-II-4)	18.75 (12-II-4)
22	8	0.1 (2)	0.0 (2)	-0.0 (13-II-4)	-382.59 (2)	-30.38 (2)	-76.90 (14-I-1)
23	1	0.1 (11)	0.0 (15-II-2)	0.0 (2)	-348.64 (11)	28.35 (15-II-2)	39.43 (15-I-2)
23	2	0.1 (11)	0.0 (15-II-2)	0.0 (14-II-1)	-363.35 (11)	-167.63 (15-II-4)	70.21 (13-I-2)
23	3	0.1 (11)	0.0 (15-II-4)	-0.0 (13-II-4)	-354.88 (11)	81.71 (15-II-2)	-16.59 (12-II-4)
23	4	0.1 (11)	0.0 (15-II-2)	-0.0 (13-II-4)	-384.03 (11)	-218.97 (15-II-4)	72.33 (13-II-4)
23	5	0.1 (11)	0.0 (15-II-2)	-0.0 (13-II-4)	-357.47 (11)	83.63 (15-II-4)	-19.68 (12-II-4)
23	6	0.1 (11)	0.0 (15-II-2)	-0.0 (13-II-4)	-385.79 (11)	-215.44 (15-II-2)	92.98 (13-II-4)
23	7	0.1 (11)	0.0 (15-II-4)	-0.0 (13-II-4)	-357.85 (2)	34.86 (15-II-4)	-30.49 (14-II-1)
23	8	0.1 (11)	0.0 (15-II-2)	-0.0 (13-II-4)	-371.15 (11)	-159.23 (15-II-2)	68.58 (13-II-4)
24	1	0.1 (2)	0.0 (15-I-4)	-0.0 (13-II-4)	-303.76 (11)	-8.51 (4)	51.83 (13-II-4)
24	2	0.0 (2)	-0.0 (13-II-4)	-0.0 (13-II-4)	-297.59 (11)	-41.27 (11)	179.14 (13-II-4)
24	3	0.0 (11)	-0.0 (13-I-1)	-0.0 (13-II-4)	-66.40 (2)	27.13 (15-I-1)	-36.12 (2)
24	4	0.0 (2)	-0.0 (13-I-1)	-0.0 (13-II-4)	-65.60 (2)	42.19 (13-I-1)	136.75 (13-II-4)
25	1	0.0 (2)	0.0 (15-I-3)	0.0 (2)	-72.46 (15-II-4)	5.00 (15-I-3)	30.76 (2)
25	2	0.0 (11)	0.0 (2)	0.0 (4)	-95.80 (15-II-4)	-27.49 (15-I-3)	-117.41 (2)
25	3	0.1 (11)	-0.0 (13-I-3)	-0.0 (13-I-3)	-289.24 (2)	-8.62 (9)	53.67 (15-II-4)
25	4	0.1 (11)	0.0 (15-I-3)	-0.0 (15-I-3)	-280.33 (2)	-28.33 (15-II-4)	111.21 (13-I-3)
26	1	0.1 (2)	0.0 (2)	0.0 (14-I-1)	-347.64 (2)	16.47 (14-II-4)	8.16 (12-II-4)
26	2	0.1 (2)	0.0 (2)	0.0 (14-I-1)	-355.91 (2)	-28.01 (2)	-66.59 (12-II-1)
26	3	0.1 (2)	0.0 (2)	0.0 (14-II-1)	-360.50 (2)	16.97 (14-II-4)	19.90 (12-II-4)
26	4	0.1 (2)	0.0 (2)	0.0 (14-I-1)	-370.50 (2)	-37.24 (2)	-98.83 (14-II-1)
26	5	0.1 (2)	0.0 (2)	0.0 (14-II-1)	-361.46 (2)	17.17 (2)	17.96 (12-II-4)
26	6	0.1 (2)	0.0 (2)	0.0 (14-II-1)	-371.69 (2)	-39.35 (2)	-90.12 (12-II-1)
26	7	0.1 (2)	0.0 (2)	0.0 (14-II-1)	-367.04 (2)	9.00 (2)	4.07 (12-II-4)
26	8	0.1 (2)	0.0 (2)	0.0 (14-II-1)	-373.70 (2)	-33.07 (2)	-54.00 (14-II-1)
27	1	0.1 (2)	0.0 (2)	0.0 (14-II-1)	-356.15 (2)	12.66 (14-I-1)	-6.14 (2)
27	2	0.1 (2)	0.0 (2)	0.0 (14-II-1)	-363.33 (2)	-32.70 (2)	-45.70 (14-II-1)
27	3	0.1 (2)	0.0 (2)	0.0 (14-II-1)	-333.78 (2)	17.70 (2)	-13.53 (11)

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
27	4	0.1 (2)	0.0 (2)	0.0 (14-II-1)	-343.79 (2)	-39.45 (2)	-69.35 (14-II-1)
27	5	0.1 (2)	0.0 (2)	0.0 (14-II-1)	-315.18 (2)	17.38 (2)	13.39 (12-II-2)
27	6	0.1 (2)	0.0 (2)	0.0 (14-II-1)	-326.74 (2)	-39.43 (2)	-69.09 (12-II-1)
27	7	0.1 (2)	0.0 (2)	0.0 (14-II-1)	-295.03 (2)	10.56 (2)	9.71 (12-II-2)
27	8	0.1 (2)	0.0 (2)	0.0 (14-II-1)	-304.05 (2)	-31.85 (2)	-35.52 (14-II-1)
28	1	0.0 (15-II-4)	0.1 (11)	-0.0 (14-II-1)	-176.91 (15-II-2)	-269.38 (11)	46.30 (14-II-1)
28	2	0.0 (15-II-4)	0.1 (11)	-0.0 (14-II-1)	-229.82 (15-II-4)	-327.28 (11)	52.21 (2)
28	3	0.0 (15-II-4)	0.1 (11)	-0.0 (14-II-1)	-225.72 (15-II-4)	-362.06 (11)	47.53 (2)
28	4	0.0 (15-II-4)	0.1 (11)	0.0 (13-I-2)	-168.82 (15-II-2)	-393.21 (11)	46.38 (14-II-1)
28	5	0.0 (15-II-4)	0.1 (11)	-0.0 (15-II-2)	34.89 (15-II-2)	-256.01 (11)	21.16 (12-II-2)
28	6	0.0 (15-II-4)	0.1 (11)	-0.0 (2)	87.33 (15-II-2)	-297.56 (11)	20.63 (12-II-2)
28	7	0.0 (15-II-4)	0.1 (11)	-0.0 (2)	84.55 (15-II-4)	-333.36 (11)	13.51 (12-II-2)
28	8	0.0 (15-II-4)	0.1 (11)	0.0 (13-I-2)	29.79 (15-II-2)	-378.13 (11)	25.36 (14-II-1)
29	1	0.1 (11)	0.0 (15-II-2)	-0.0 (13-II-4)	-385.18 (11)	22.16 (15-I-4)	61.79 (13-II-4)
29	2	0.1 (11)	0.0 (15-II-2)	-0.0 (13-II-4)	-396.35 (11)	-180.74 (15-II-4)	138.14 (13-II-4)
29	3	0.1 (11)	0.0 (15-I-1)	-0.0 (13-II-4)	-353.74 (11)	82.75 (15-II-4)	-38.84 (12-II-4)
29	4	0.1 (11)	0.0 (15-II-4)	-0.0 (13-II-4)	-378.83 (11)	-241.48 (15-II-4)	172.63 (13-II-4)
29	5	0.1 (11)	0.0 (15-I-1)	-0.0 (13-II-4)	-332.37 (2)	90.95 (15-II-4)	-28.13 (14-II-4)
29	6	0.1 (11)	0.0 (15-I-4)	-0.0 (13-II-4)	-366.20 (11)	-235.15 (15-I-4)	208.81 (13-II-4)
29	7	0.1 (11)	0.0 (15-I-4)	-0.0 (13-II-4)	-273.91 (2)	56.64 (15-II-4)	42.60 (13-II-4)
29	8	0.1 (11)	0.0 (15-I-4)	-0.0 (13-II-4)	-310.42 (2)	-124.00 (15-I-4)	172.65 (13-II-4)
30	1	0.0 (2)	-0.0 (13-I-1)	0.0 (15-II-2)	-216.97 (14-II-2)	225.88 (13-I-1)	-117.65 (12-II-3)
30	2	0.0 (2)	-0.0 (10)	0.0 (15-II-2)	-129.72 (14-II-2)	273.56 (4)	-102.16 (14-II-3)
30	3	0.1 (2)	-0.1 (13-I-1)	0.0 (15-II-2)	-256.54 (14-II-2)	304.79 (13-I-1)	-72.58 (15-II-2)
30	4	0.0 (11)	-0.0 (13-I-1)	0.0 (15-II-2)	-162.74 (11)	359.01 (4)	-50.53 (11)
30	5	0.1 (2)	-0.1 (13-I-1)	0.0 (11)	-261.73 (2)	333.80 (13-I-1)	-55.41 (15-II-2)
30	6	0.0 (11)	-0.1 (13-I-1)	0.0 (14-II-1)	-204.04 (11)	376.95 (4)	-33.60 (15-II-2)
30	7	0.1 (11)	-0.1 (13-I-1)	0.0 (2)	-289.37 (2)	323.67 (13-I-1)	-59.94 (15-II-2)
30	8	0.1 (2)	-0.1 (10)	0.0 (14-II-1)	-249.03 (2)	313.66 (4)	52.26 (4)
31	1	0.0 (11)	-0.0 (4)	0.0 (15-II-2)	-149.57 (14-II-2)	284.27 (4)	100.20 (10)
31	2	0.1 (14-II-2)	0.1 (15-I-3)	0.0 (13-I-3)	-272.18 (14-II-2)	-319.38 (15-I-3)	127.96 (4)
31	3	0.0 (2)	-0.0 (4)	0.0 (15-II-2)	-175.27 (14-II-2)	371.29 (4)	58.28 (9)
31	4	0.1 (14-II-2)	0.1 (15-I-3)	-0.0 (9)	-305.91 (14-II-2)	-494.97 (15-I-3)	64.28 (9)
31	5	0.0 (2)	-0.0 (4)	-0.0 (9)	-209.51 (2)	389.90 (4)	-56.21 (14-II-1)
31	6	0.1 (11)	0.1 (15-I-3)	-0.0 (9)	-294.82 (11)	-531.30 (15-I-3)	-47.51 (15-II-2)
31	7	0.1 (11)	-0.1 (4)	-0.0 (13-I-2)	-256.05 (11)	328.61 (4)	-112.15 (13-II-2)
31	8	0.1 (2)	0.1 (15-I-3)	-0.0 (9)	-315.35 (11)	-437.39 (15-I-3)	-103.28 (13-II-2)
32	1	0.0 (2)	-0.0 (13-I-1)	0.0 (15-II-2)	-36.44 (11)	109.17 (13-I-1)	-76.84 (14-II-3)
32	2	0.0 (2)	-0.0 (10)	0.0 (15-II-2)	-55.94 (11)	222.79 (4)	-75.47 (14-II-3)
32	3	0.0 (11)	-0.0 (13-I-1)	0.0 (15-I-1)	-199.22 (14-II-2)	140.29 (13-I-1)	-121.30 (15-I-1)
32	4	0.0 (2)	-0.0 (10)	0.0 (15-II-2)	-177.97 (2)	224.63 (4)	-63.40 (15-II-2)
33	1	0.0 (14-II-2)	0.0 (15-I-3)	0.0 (15-I-3)	-276.03 (14-II-2)	-8.34 (4)	-55.64 (15-I-3)
33	2	0.0 (14-II-2)	0.0 (15-I-3)	0.0 (15-I-3)	-267.20 (14-II-2)	-41.98 (15-I-3)	-101.39 (13-I-3)
33	3	0.0 (14-II-2)	0.0 (15-I-3)	-0.0 (2)	-28.70 (14-II-3)	10.35 (2)	-42.65 (14-II-2)
33	4	0.0 (14-II-2)	0.0 (15-I-3)	0.0 (15-I-3)	-38.42 (15-II-2)	-46.30 (15-I-3)	69.33 (4)
34	1	0.0 (15-I-2)	0.1 (11)	-0.0 (15-I-1)	-140.88 (15-I-2)	-203.58 (14-II-2)	102.93 (15-II-2)
34	2	0.0 (15-I-2)	0.1 (11)	-0.0 (15-II-2)	-264.53 (15-I-2)	-268.79 (14-II-2)	144.71 (15-II-2)
34	3	0.0 (15-II-2)	0.1 (11)	-0.0 (14-II-1)	-269.84 (15-II-2)	-300.77 (11)	118.68 (15-II-2)
34	4	0.0 (15-II-2)	0.1 (11)	-0.0 (14-II-1)	-201.71 (15-II-2)	-351.57 (11)	100.47 (15-II-2)
34	5	0.0 (15-I-2)	0.1 (11)	-0.0 (15-I-1)	59.88 (15-I-3)	-152.54 (12-II-2)	-26.84 (14-I-1)
34	6	0.0 (15-I-2)	0.1 (11)	-0.0 (15-II-2)	102.69 (15-II-2)	-220.61 (14-II-2)	-18.27 (9)
34	7	0.0 (15-II-2)	0.1 (11)	-0.0 (15-II-2)	93.28 (15-II-2)	-268.38 (11)	39.51 (12-II-2)



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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
34	8	0.0 (15-II-2)	0.1 (11)	-0.0 (15-II-2)	25.50 (15-I-2)	-338.21 (11)	53.38 (14-II-2)
35	1	-0.0 (13-I-1)	0.0 (11)	-0.0 (15-II-2)	41.41 (13-I-1)	21.36 (15-II-2)	62.69 (13-I-1)
35	2	0.0 (14-II-2)	0.0 (14-II-2)	-0.0 (15-I-1)	-63.20 (14-II-3)	-210.91 (11)	107.23 (15-I-1)
35	3	0.0 (14-II-3)	0.0 (11)	-0.0 (15-I-1)	34.13 (15-I-1)	-13.76 (12-I-1)	-40.25 (14-II-2)
35	4	-0.0 (13-II-2)	0.0 (14-II-2)	-0.0 (15-I-1)	10.33 (14-II-3)	-206.81 (11)	40.85 (15-I-1)
36	1	0.1 (2)	0.0 (14-I-1)	-0.0 (9)	-307.25 (2)	12.32 (14-II-2)	21.27 (12-II-2)
36	2	0.1 (2)	0.0 (2)	-0.0 (9)	-316.91 (2)	-37.17 (2)	37.37 (9)
36	3	0.1 (2)	0.0 (14-I-1)	-0.0 (9)	-285.96 (2)	20.59 (14-II-2)	42.87 (12-II-2)
36	4	0.1 (2)	0.0 (14-I-1)	-0.0 (4)	-296.14 (2)	-57.26 (14-I-1)	70.24 (9)
36	5	0.1 (14-II-2)	0.0 (14-I-1)	-0.0 (9)	-345.20 (14-II-2)	39.59 (14-I-1)	29.10 (12-II-2)
36	6	0.1 (14-II-2)	-0.0 (13-I-2)	-0.0 (4)	-355.98 (14-II-2)	-85.98 (14-I-1)	93.80 (9)
36	7	0.1 (14-II-2)	0.0 (14-II-2)	0.0 (13-I-3)	-306.49 (14-II-2)	32.18 (14-I-1)	-37.65 (15-I-3)
36	8	0.1 (14-II-2)	-0.0 (13-I-2)	0.0 (15-I-3)	-325.90 (14-II-2)	-61.23 (14-II-2)	-96.93 (15-I-3)
37	1	0.0 (2)	-0.0 (9)	-0.0 (2)	-48.77 (2)	-7.03 (4)	-7.74 (12-II-3)
37	2	0.0 (14-II-3)	-0.0 (9)	-0.0 (4)	-45.99 (14-II-2)	21.32 (4)	33.83 (2)
37	3	0.0 (2)	-0.0 (4)	-0.0 (14-I-1)	16.04 (14-I-1)	2.80 (15-I-2)	-11.36 (2)
37	4	0.0 (2)	-0.0 (4)	-0.0 (15-I-2)	18.13 (2)	22.60 (4)	21.80 (4)
38	1	0.0 (2)	-0.0 (10)	0.0 (15-II-2)	22.83 (2)	107.79 (13-I-1)	-24.67 (12-II-3)
38	2	0.0 (11)	-0.0 (4)	0.0 (15-II-2)	22.82 (2)	200.40 (4)	-29.53 (12-II-3)
38	3	0.0 (11)	-0.0 (10)	0.0 (15-II-2)	-59.91 (2)	106.95 (13-I-1)	-58.35 (15-II-2)
38	4	0.0 (2)	-0.0 (4)	0.0 (15-II-2)	-68.35 (2)	193.28 (4)	-52.65 (15-II-2)
39	1	-0.0 (13-I-1)	0.0 (11)	-0.0 (15-II-2)	50.92 (13-I-1)	22.46 (11)	19.84 (13-I-1)
39	2	-0.0 (13-I-1)	0.0 (4)	-0.0 (15-II-2)	50.66 (13-I-1)	-45.38 (11)	38.71 (15-II-2)
39	3	-0.0 (13-I-1)	0.0 (11)	-0.0 (15-II-2)	9.82 (15-II-2)	20.69 (11)	-8.90 (14-II-2)
39	4	-0.0 (13-I-1)	0.0 (14-II-2)	-0.0 (13-I-1)	-10.12 (4)	-55.43 (11)	-13.63 (12-I-1)
40	1	0.0 (11)	-0.0 (4)	0.0 (13-II-2)	25.22 (11)	199.27 (4)	30.22 (4)
40	2	0.0 (14-II-2)	-0.0 (4)	-0.0 (2)	25.20 (11)	78.11 (4)	27.46 (4)
40	3	0.0 (11)	-0.0 (4)	-0.0 (9)	-73.90 (11)	193.01 (4)	-29.92 (13-II-2)
40	4	0.0 (14-II-2)	-0.0 (4)	-0.0 (4)	-67.81 (14-II-2)	68.00 (4)	35.54 (2)

**Risultati Analisi Dinamica - Sollecitazioni massime per combinazione - Sigma terreno platea - S.L.E**  
Scenario di calcolo: ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO

Combinazione	Muro	Nodi	SigmaMax daN/cm <sup>2</sup>	SigmaMin daN/cm <sup>2</sup>
16	37	8-9-18-17	0.27	0.21
17	37	8-9-18-17	0.28	0.20
18	39	36-45-44-35	0.27	0.21
19	37	8-9-18-17	0.27	0.20
20	37	8-9-18-17	0.28	0.20
21	37	8-9-18-17	0.27	0.21
22	37	8-9-18-17	0.26	0.16
23	37	8-9-18-17	0.28	0.18
24	37	8-9-18-17	0.28	0.19
25	37	8-9-18-17	0.28	0.19
26	37	8-9-18-17	0.27	0.19
27	37	8-9-18-17	0.28	0.14
28	37	8-9-18-17	0.28	0.18
29-I-1	37	8-9-18-17	0.29	0.17
29-II-1	37	8-9-18-17	0.30	0.16
29-I-2	37	8-9-18-17	0.30	0.17
29-II-2	37	8-9-18-17	0.29	0.16
29-I-3	37	8-9-18-17	0.29	0.17
29-II-3	37	8-9-18-17	0.30	0.16
29-I-4	37	8-9-18-17	0.29	0.16
29-II-4	37	8-9-18-17	0.30	0.17
30-I-1	39	36-45-44-35	0.30	0.17
30-II-1	39	36-45-44-35	0.31	0.15
30-I-2	39	36-45-44-35	0.31	0.15
30-II-2	39	36-45-44-35	0.30	0.17
30-I-3	39	36-45-44-35	0.30	0.17
30-II-3	39	36-45-44-35	0.31	0.15
30-I-4	39	36-45-44-35	0.31	0.15
30-II-4	39	36-45-44-35	0.30	0.17
31-I-1	37	8-9-18-17	0.30	0.13
31-II-1	37	8-9-18-17	0.30	0.12
31-I-2	37	8-9-18-17	0.30	0.13
31-II-2	37	8-9-18-17	0.30	0.12
31-I-3	37	8-9-18-17	0.30	0.13



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Combinazione	Muro	Nodi	SigmaMax	SigmaMin
31-II-3	37	8-9-18-17	0.30	0.12
31-I-4	37	8-9-18-17	0.30	0.12
31-II-4	37	8-9-18-17	0.30	0.13
32-I-1	39	36-45-44-35	0.28	0.14
32-II-1	39	36-45-44-35	0.29	0.13
32-I-2	39	36-45-44-35	0.29	0.13
32-II-2	39	36-45-44-35	0.28	0.14
32-I-3	39	36-45-44-35	0.28	0.14
32-II-3	39	36-45-44-35	0.29	0.13
32-I-4	39	36-45-44-35	0.29	0.13
32-II-4	39	36-45-44-35	0.28	0.14
Assoluti				
30-II-3	39	36-45-44-35	0.31	
31-II-3	37	8-9-18-17		0.12

**Risultati Analisi Dinamica - Spostamenti massimi - Nodi - S.I.E.**

Scenario di calcolo: **ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Nodo	Trasl. X mm	Trasl. Y mm	Trasl. Z mm	Rotaz. X °	Rotaz. Y °	Rotaz. Z °
1	0.00 (16)	0.00 (16)	-1.19 (20)	-0.01 (30-II-3)	0.01 (31-I-4)	0.00 (16)
2	0.00 (16)	0.00 (16)	-1.23 (20)	-0.01 (30-II-3)	0.01 (31-I-4)	0.00 (16)
3	0.00 (16)	0.00 (16)	-1.27 (20)	-0.01 (30-II-3)	0.01 (31-I-4)	0.00 (16)
4	0.00 (16)	0.00 (16)	-1.31 (20)	-0.01 (30-II-3)	0.00 (31-II-4)	0.00 (16)
5	0.00 (16)	0.00 (16)	-1.35 (20)	-0.01 (30-II-3)	0.00 (31-II-4)	0.00 (16)
6	0.00 (16)	0.00 (16)	-1.38 (29-II-4)	-0.01 (30-I-2)	0.00 (31-I-4)	0.00 (16)
7	0.00 (16)	0.00 (16)	-1.44 (31-II-4)	-0.01 (30-I-2)	0.00 (31-II-4)	0.00 (16)
8	0.00 (16)	0.00 (16)	-1.47 (31-II-4)	-0.01 (30-I-2)	0.00 (31-II-4)	0.00 (16)
9	0.00 (16)	0.00 (16)	-1.50 (31-II-4)	-0.01 (30-I-2)	0.00 (31-II-4)	0.00 (16)
10	0.00 (16)	0.00 (16)	-1.17 (20)	-0.01 (30-II-3)	0.01 (31-I-4)	0.00 (16)
11	0.00 (16)	0.00 (16)	-1.21 (20)	-0.01 (30-II-3)	0.01 (31-I-4)	0.00 (16)
12	0.00 (16)	0.00 (16)	-1.25 (20)	-0.01 (30-II-3)	0.01 (31-I-4)	0.00 (16)
13	0.00 (16)	0.00 (16)	-1.30 (20)	-0.01 (30-II-3)	0.00 (31-II-4)	0.00 (16)
14	0.00 (16)	0.00 (16)	-1.33 (20)	-0.01 (30-II-3)	0.00 (31-II-4)	0.00 (16)
15	0.00 (16)	0.00 (16)	-1.36 (29-II-4)	-0.01 (30-I-2)	0.00 (31-II-4)	0.00 (16)
16	0.00 (16)	0.00 (16)	-1.42 (29-II-4)	-0.01 (30-I-2)	0.00 (31-II-4)	0.00 (16)
17	0.00 (16)	0.00 (16)	-1.44 (31-II-4)	-0.01 (30-I-2)	0.00 (31-II-4)	0.00 (16)
18	0.00 (16)	0.00 (16)	-1.47 (31-II-4)	-0.01 (30-I-2)	0.00 (31-II-4)	0.00 (16)
19	0.00 (16)	0.00 (16)	-1.10 (20)	-0.01 (30-II-3)	0.01 (31-I-4)	0.00 (16)
20	0.00 (16)	0.00 (16)	-1.14 (20)	-0.01 (30-II-3)	0.01 (31-I-4)	0.00 (16)
21	0.00 (16)	0.00 (16)	-1.18 (20)	-0.01 (30-II-3)	0.01 (31-I-4)	0.00 (16)
22	0.00 (16)	0.00 (16)	-1.22 (20)	-0.01 (30-II-3)	0.00 (31-II-4)	0.00 (16)
23	0.00 (16)	0.00 (16)	-1.25 (20)	-0.01 (30-II-3)	0.00 (31-II-4)	0.00 (16)
24	0.00 (16)	0.00 (16)	-1.28 (21)	-0.01 (30-II-3)	0.00 (31-II-4)	0.00 (16)
25	0.00 (16)	0.00 (16)	-1.33 (29-II-4)	-0.01 (30-I-2)	0.00 (31-II-4)	0.00 (16)
26	0.00 (16)	0.00 (16)	-1.36 (29-II-4)	-0.01 (30-I-2)	0.00 (31-II-4)	0.00 (16)
27	0.00 (16)	0.00 (16)	-1.38 (29-II-4)	-0.01 (30-I-2)	0.00 (31-II-4)	0.00 (16)
28	0.00 (16)	0.00 (16)	-1.14 (30-II-3)	-0.01 (30-II-3)	0.01 (31-I-4)	0.00 (16)
29	0.00 (16)	0.00 (16)	-1.19 (30-II-3)	-0.01 (30-II-3)	0.01 (31-I-4)	0.00 (16)
30	0.00 (16)	0.00 (16)	-1.24 (30-II-3)	-0.01 (30-II-3)	0.01 (31-I-4)	0.00 (16)
31	0.00 (16)	0.00 (16)	-1.29 (30-II-3)	-0.01 (30-II-3)	0.00 (31-II-4)	0.00 (16)
32	0.00 (16)	0.00 (16)	-1.34 (30-II-3)	-0.01 (30-II-3)	0.00 (31-II-4)	0.00 (16)
33	0.00 (16)	0.00 (16)	-1.37 (30-II-3)	-0.01 (30-II-3)	0.00 (31-I-4)	0.00 (16)
34	0.00 (16)	0.00 (16)	-1.40 (30-II-3)	-0.01 (30-II-3)	0.00 (31-II-4)	0.00 (16)
35	0.00 (16)	0.00 (16)	-1.42 (30-II-3)	-0.01 (30-II-3)	0.00 (31-II-4)	0.00 (16)
36	0.00 (16)	0.00 (16)	-1.43 (30-II-3)	-0.01 (30-II-3)	0.00 (31-II-4)	0.00 (16)
37	0.00 (16)	0.00 (16)	-1.23 (30-II-3)	-0.01 (30-II-3)	0.01 (31-I-4)	0.00 (16)
38	0.00 (16)	0.00 (16)	-1.29 (30-II-3)	-0.01 (30-II-3)	0.01 (31-I-4)	0.00 (16)
39	0.00 (16)	0.00 (16)	-1.34 (30-II-3)	-0.01 (30-II-3)	0.01 (31-I-4)	0.00 (16)
40	0.00 (16)	0.00 (16)	-1.40 (30-II-3)	-0.01 (30-II-3)	0.00 (31-II-4)	0.00 (16)
41	0.00 (16)	0.00 (16)	-1.44 (30-II-3)	-0.01 (30-II-3)	0.00 (31-II-4)	0.00 (16)
42	0.00 (16)	0.00 (16)	-1.47 (30-II-3)	-0.01 (30-II-3)	0.00 (31-I-4)	0.00 (16)
43	0.00 (16)	0.00 (16)	-1.50 (30-II-3)	-0.01 (30-II-3)	0.00 (31-I-4)	0.00 (16)
44	0.00 (16)	0.00 (16)	-1.52 (30-II-3)	-0.01 (30-II-3)	0.00 (31-II-4)	0.00 (16)
45	0.00 (16)	0.00 (16)	-1.53 (30-II-3)	-0.01 (30-II-3)	0.00 (31-II-4)	0.00 (16)
112	0.08 (31-I-4)	0.20 (30-I-4)	-1.28 (20)	-0.02 (30-I-4)	0.02 (31-II-4)	0.00 (30-II-4)
113	0.07 (31-I-4)	0.25 (30-II-4)	-1.31 (20)	-0.04 (30-II-4)	0.01 (31-I-4)	0.00 (30-II-4)
114	0.07 (31-I-4)	0.26 (30-II-2)	-1.34 (20)	-0.04 (30-II-2)	0.01 (31-I-4)	0.00 (29-I-1)
115	0.07 (31-I-4)	0.26 (30-II-2)	-1.38 (29-II-4)	-0.04 (30-II-2)	0.01 (31-I-4)	-0.00 (32-II-2)
116	0.08 (31-II-4)	0.22 (30-I-2)	-1.46 (29-II-4)	-0.03 (30-I-2)	0.02 (31-II-1)	-0.00 (32-II-2)
130	0.08 (31-I-4)	0.26 (30-I-4)	-1.30 (30-I-3)	-0.04 (30-I-4)	0.02 (31-II-4)	0.00 (30-II-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

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Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
131	0.07 (31-I-4)	0.31 (30-I-3)	-1.38 (30-II-3)	-0.05 (30-II-4)	0.01 (31-I-4)	0.00 (30-II-4)
132	0.07 (31-I-4)	0.33 (30-I-3)	-1.42 (30-II-3)	-0.05 (30-I-3)	0.01 (31-I-4)	-0.00 (31-II-3)
133	0.06 (31-I-4)	0.32 (30-II-2)	-1.46 (30-II-3)	-0.05 (30-II-2)	0.01 (31-I-4)	-0.00 (32-II-2)
134	0.08 (31-II-4)	0.28 (30-I-2)	-1.47 (30-II-3)	-0.04 (30-I-2)	0.02 (31-II-3)	-0.00 (32-II-2)

**Risultati Analisi Dinamica - Reazioni massime - Nodi - S.L.E**  
Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

Nodo	Rx daN	Ry daN	Rz daN	Mx daN*m	My daN*m	Mz daN*m
1	-18.45 (27)	-5.46 (27)	0	0	0	0
2	-141.41 (27)	-10.72 (32-I-3)	0	0	0	-1.62 (30-I-3)
3	-162.95 (19)	-5.99 (31-I-2)	0	0	0	1.26 (27)
4	-68.61 (29-II-4)	-8.96 (31-I-2)	0	0	0	0
5	25.18 (32-I-2)	-9.97 (31-I-2)	0	0	0	0
6	36.15 (19)	-11.27 (31-I-3)	0	0	0	0
7	108.56 (31-I-1)	-10.50 (31-I-1)	0	0	0	-1.93 (32-I-2)
8	87.75 (31-I-1)	-9.23 (31-I-1)	0	0	0	0
9	11.13 (31-II-2)	-3.86 (31-I-1)	0	0	0	0
10	-58.45 (27)	69.97 (30-II-4)	0	0	0	8.07 (27)
11	-444.39 (27)	147.27 (19)	0	0	0	28.88 (32-II-4)
12	-429.84 (19)	244.46 (17)	0	0	0	10.71 (32-II-4)
13	213.30 (32-II-4)	401.01 (19)	0	0	0	-23.24 (19)
14	-123.57 (29-I-1)	394.50 (17)	0	0	0	9.15 (29-I-1)
15	-274.41 (29-I-1)	414.89 (29-I-2)	0	0	0	25.56 (29-I-1)
16	283.75 (31-II-2)	198.37 (19)	0	0	0	-8.42 (31-I-2)
17	339.76 (31-II-2)	152.37 (29-II-2)	0	0	0	-25.23 (32-II-2)
18	44.98 (31-II-2)	35.00 (29-II-1)	0	0	0	-6.74 (29-II-2)
19	-89.39 (27)	203.07 (30-II-4)	0	0	0	3.09 (30-I-1)
20	-456.06 (32-I-1)	254.51 (30-II-4)	0	0	0	-7.61 (30-II-4)
21	-204.38 (32-I-3)	360.94 (30-II-4)	0	0	0	-5.28 (30-II-4)
22	-50.22 (29-II-4)	503.97 (30-II-4)	0	0	0	-3.84 (32-II-2)
23	98.98 (32-II-1)	520.85 (30-II-4)	0	0	0	-1.60 (31-II-1)
24	134.25 (32-II-1)	482.56 (30-I-1)	0	0	0	1.50 (30-II-4)
25	117.33 (32-I-1)	284.33 (30-I-1)	0	0	0	0
26	306.96 (31-II-2)	197.72 (30-I-1)	0	0	0	6.41 (32-II-2)
27	76.73 (29-II-2)	98.58 (30-II-2)	0	0	0	0
28	-75.78 (32-I-1)	-91.51 (31-I-1)	0	0	0	-9.00 (19)
29	-480.61 (32-I-1)	-202.43 (19)	0	0	0	-18.24 (27)
30	-453.27 (32-II-4)	-241.76 (30-I-4)	0	0	0	19.04 (30-II-4)
31	205.86 (19)	-855.74 (30-I-1)	0	0	0	25.25 (32-I-1)
32	71.79 (19)	-899.72 (30-I-1)	0	0	0	-8.11 (29-II-3)
33	-210.88 (29-II-3)	-865.60 (30-I-1)	0	0	0	-23.13 (29-II-3)
34	376.15 (31-II-2)	-243.03 (30-I-2)	0	0	0	7.57 (32-I-2)
35	364.45 (31-II-2)	-149.70 (29-I-1)	0	0	0	16.14 (31-II-2)
36	48.78 (32-I-1)	-65.99 (19)	0	0	0	5.26 (29-II-2)
37	-38.05 (32-I-1)	9.08 (32-II-4)	0	0	0	-1.63 (30-I-1)
38	-313.67 (32-I-1)	16.26 (32-I-3)	0	0	0	-6.29 (32-II-2)
39	-409.38 (30-II-4)	47.68 (32-II-4)	0	0	0	-9.17 (32-II-4)
40	-177.71 (30-II-4)	82.28 (32-II-4)	0	0	0	-4.64 (30-II-4)
41	64.84 (31-II-1)	85.48 (32-II-4)	0	0	0	2.12 (27)
42	164.24 (32-II-2)	90.94 (32-II-2)	0	0	0	5.40 (32-II-2)
43	268.94 (32-I-1)	65.55 (32-II-2)	0	0	0	9.08 (32-I-1)
44	169.59 (32-I-1)	20.88 (31-II-3)	0	0	0	7.24 (32-I-2)
45	22.58 (32-I-1)	5.24 (31-II-3)	0	0	0	1.38 (30-I-1)

**Risultati Analisi Dinamica - Sollecitazioni Massime - Muri discretizzati - S.L.E**  
Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

Muro	Pann.	Sxx MPa	Syy MPa	Sxy MPa	Mxx daN*m/m	Myy daN*m/m	Mxy daN*m/m
1	1	0.0 (32-I-2)	-0.0 (30-II-4)	0.0 (27)	8.79 (19)	-2.08 (30-II-4)	9.55 (27)
1	2	0.0 (32-II-2)	-0.0 (19)	0.0 (29-I-1)	10.64 (19)	8.51 (19)	-19.89 (27)
1	3	0.0 (32-II-4)	-0.0 (19)	0.0 (19)	-36.26 (32-I-2)	-4.10 (19)	7.20 (32-II-4)
1	4	0.0 (32-II-4)	-0.0 (19)	0.0 (19)	-39.80 (32-II-4)	13.06 (19)	-38.17 (19)
2	1	-0.0 (19)	0.0 (32-II-4)	-0.0 (19)	30.30 (19)	-65.25 (32-II-4)	41.10 (19)
2	2	-0.0 (19)	0.0 (32-II-4)	-0.0 (31-I-1)	29.32 (19)	18.58 (27)	19.37 (19)
2	3	-0.0 (19)	0.0 (32-II-4)	-0.0 (31-I-1)	80.03 (19)	-65.69 (32-II-4)	39.31 (31-I-1)
2	4	-0.0 (19)	0.0 (32-II-4)	0.0 (30-II-4)	73.22 (19)	15.87 (32-II-4)	23.69 (31-I-1)
3	1	-0.0 (30-I-1)	0.0 (27)	0.0 (30-II-4)	27.48 (30-I-1)	-48.65 (27)	-52.27 (30-II-4)
3	2	-0.0 (30-I-1)	0.0 (27)	0.0 (30-II-4)	28.20 (30-I-1)	21.61 (32-II-4)	-29.13 (30-II-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
3	3	-0.0 (30-I-1)	0.0 (27)	0.0 (30-II-4)	-7.23 (19)	-50.68 (27)	-19.04 (30-II-4)
3	4	-0.0 (30-II-3)	0.0 (27)	0.0 (30-II-4)	5.42 (32-II-4)	19.76 (32-II-4)	5.73 (27)
4	1	-0.0 (19)	0.0 (27)	0.0 (30-II-4)	86.50 (19)	-60.85 (32-I-1)	-48.96 (30-II-4)
4	2	-0.0 (30-I-1)	0.0 (32-I-1)	0.0 (30-II-4)	82.36 (19)	14.95 (27)	-25.65 (30-II-4)
4	3	-0.0 (30-I-1)	0.0 (27)	0.0 (30-II-4)	58.17 (30-II-4)	-59.90 (27)	-56.08 (30-II-4)
4	4	-0.0 (19)	0.0 (27)	0.0 (30-II-4)	57.53 (30-II-4)	17.71 (32-II-4)	-25.91 (30-II-4)
5	1	-0.0 (31-II-2)	-0.3 (31-II-3)	-0.0 (32-II-4)	-93.39 (32-I-2)	-1215.21 (32-II-2)	-95.66 (32-II-2)
5	2	-0.0 (31-II-2)	-0.3 (31-II-3)	0.0 (29-I-2)	-42.95 (32-I-2)	-1149.23 (32-I-2)	-65.78 (32-II-2)
5	3	-0.2 (31-II-3)	-0.3 (31-II-2)	0.2 (29-I-2)	-112.98 (32-I-2)	-1157.87 (32-I-2)	115.32 (30-I-2)
5	4	-0.1 (31-II-2)	0.4 (29-I-2)	0.1 (19)	77.33 (29-I-2)	-1495.54 (32-I-2)	597.80 (30-I-2)
5	5	-0.1 (31-II-2)	-0.1 (31-II-2)	-0.0 (32-II-4)	-140.03 (32-I-2)	-1272.71 (32-II-2)	-42.47 (32-II-2)
5	6	-0.1 (31-II-2)	-0.1 (32-I-2)	-0.0 (32-II-2)	-97.22 (32-I-2)	-1142.05 (32-II-2)	-78.42 (32-II-2)
5	7	-0.1 (31-II-2)	-0.1 (19)	-0.1 (31-II-2)	-145.74 (32-I-2)	-850.14 (32-II-2)	-45.40 (32-II-2)
5	8	0.2 (29-II-3)	0.0 (19)	-0.1 (31-II-3)	-203.25 (32-I-2)	-171.87 (32-II-2)	68.46 (18)
5	9	-0.0 (31-II-2)	-0.1 (31-II-2)	-0.1 (31-II-2)	-154.48 (32-I-1)	-1314.37 (32-I-1)	-9.78 (32-II-2)
5	10	-0.1 (32-I-2)	-0.1 (31-II-2)	-0.1 (31-II-2)	-113.62 (32-I-2)	-1205.00 (32-I-1)	-52.29 (32-II-2)
5	11	-0.1 (31-II-2)	-0.1 (31-II-2)	-0.2 (31-II-2)	-159.89 (32-I-2)	-951.60 (32-I-1)	-217.28 (32-II-2)
5	12	0.1 (29-I-2)	0.0 (29-I-2)	-0.1 (31-II-2)	-195.27 (32-I-2)	-165.05 (32-I-1)	-290.66 (32-II-2)
5	13	-0.0 (19)	-0.1 (29-II-2)	-0.1 (31-II-2)	-175.64 (32-I-1)	-1332.82 (32-I-1)	-7.92 (32-II-2)
5	14	-0.0 (19)	-0.1 (29-II-2)	-0.1 (31-II-3)	-189.78 (32-I-1)	-1312.99 (32-I-1)	-35.39 (32-II-2)
5	15	-0.1 (19)	-0.2 (29-II-2)	-0.1 (32-II-3)	-96.41 (32-I-2)	-1495.89 (32-I-1)	-220.56 (32-II-2)
5	16	-0.1 (19)	-0.6 (31-II-2)	-0.2 (31-II-2)	-40.57 (31-II-2)	-2257.72 (32-II-2)	-1146.14 (32-II-2)
6	1	-0.3 (31-I-1)	-0.0 (31-II-2)	-0.0 (27)	840.31 (32-I-2)	65.75 (32-I-2)	64.54 (32-II-2)
6	2	-0.1 (31-II-2)	-0.1 (31-I-1)	-0.0 (19)	879.33 (32-II-2)	98.93 (32-I-2)	30.18 (32-II-2)
6	3	-0.1 (29-II-2)	-0.0 (31-II-2)	-0.1 (31-II-2)	916.09 (32-I-3)	109.69 (32-I-3)	11.17 (32-II-2)
6	4	-0.1 (29-II-2)	-0.0 (19)	-0.1 (31-II-2)	942.37 (32-I-3)	123.61 (32-I-3)	11.02 (32-II-2)
6	5	-0.3 (31-I-1)	-0.0 (31-I-1)	0.0 (29-I-2)	752.50 (32-I-2)	28.58 (32-I-2)	48.79 (32-II-2)
6	6	-0.1 (27)	-0.1 (31-I-1)	-0.0 (27)	761.22 (32-II-2)	73.22 (32-I-2)	64.12 (32-II-2)
6	7	-0.1 (29-II-2)	-0.1 (27)	-0.1 (31-II-2)	823.84 (32-I-3)	83.20 (32-I-2)	53.05 (32-II-2)
6	8	-0.1 (29-II-2)	-0.0 (19)	-0.1 (31-I-1)	913.78 (32-I-3)	128.73 (32-I-3)	40.05 (32-II-2)
6	9	-0.3 (31-II-2)	-0.2 (31-II-2)	0.2 (29-I-2)	685.02 (32-I-2)	70.04 (32-I-2)	-57.13 (30-I-2)
6	10	-0.1 (19)	-0.1 (31-II-2)	-0.1 (31-II-2)	541.66 (32-II-2)	109.52 (32-I-2)	67.52 (32-II-2)
6	11	-0.0 (31-II-2)	-0.1 (31-II-2)	-0.2 (31-II-2)	642.12 (32-I-3)	113.26 (32-I-3)	182.50 (32-II-2)
6	12	-0.2 (29-II-2)	-0.1 (19)	-0.1 (19)	1027.77 (32-I-3)	56.53 (32-I-2)	176.42 (32-II-2)
6	13	0.4 (29-I-2)	-0.1 (31-II-2)	0.1 (19)	767.91 (32-I-2)	77.49 (31-I-2)	-304.88 (30-I-2)
6	14	0.0 (19)	0.2 (29-I-2)	-0.1 (31-II-2)	120.24 (32-II-2)	155.51 (32-I-2)	40.90 (32-II-2)
6	15	0.0 (29-I-2)	0.1 (29-I-2)	-0.1 (31-II-2)	107.34 (32-I-3)	134.95 (32-I-2)	233.81 (32-II-2)
6	16	-0.6 (31-II-2)	-0.1 (19)	-0.2 (31-II-2)	1537.36 (32-II-2)	-38.14 (29-II-2)	801.75 (32-II-2)
7	1	-0.1 (19)	-0.0 (31-II-2)	-0.0 (31-I-1)	974.67 (32-I-3)	126.19 (32-I-3)	23.46 (32-II-2)
7	2	-0.1 (19)	-0.0 (31-II-2)	-0.0 (31-I-1)	1008.61 (32-I-3)	117.07 (32-I-3)	19.15 (32-II-2)
7	3	-0.1 (29-I-2)	-0.0 (19)	-0.0 (31-I-1)	1021.93 (32-I-3)	118.89 (32-I-3)	-7.75 (30-I-2)
7	4	-0.1 (29-I-2)	-0.0 (19)	-0.0 (31-I-1)	1015.54 (30-I-3)	131.41 (30-I-3)	-11.02 (30-I-2)
7	5	-0.1 (19)	-0.0 (31-II-2)	-0.0 (31-I-1)	943.34 (32-I-3)	129.76 (32-I-3)	43.60 (32-II-2)
7	6	-0.1 (19)	-0.1 (31-I-2)	-0.0 (31-I-1)	919.62 (32-I-3)	84.04 (32-I-3)	29.77 (32-II-2)
7	7	-0.1 (29-I-2)	-0.1 (19)	-0.1 (31-I-1)	929.72 (32-I-3)	86.16 (32-I-3)	9.16 (32-II-2)
7	8	-0.2 (29-I-2)	-0.1 (19)	-0.0 (31-I-1)	974.92 (30-I-3)	135.15 (30-I-3)	-13.52 (30-I-2)
7	9	-0.2 (19)	-0.1 (31-II-2)	0.0 (29-II-1)	1048.78 (32-I-3)	59.81 (32-I-2)	-68.79 (30-I-2)
7	10	-0.1 (19)	-0.1 (19)	-0.0 (31-I-1)	714.28 (32-I-3)	118.95 (32-I-3)	-58.36 (30-I-2)
7	11	-0.1 (29-I-2)	-0.1 (31-I-2)	-0.1 (31-I-1)	720.17 (32-I-3)	121.78 (32-I-3)	95.37 (32-II-2)
7	12	-0.2 (29-I-2)	-0.1 (19)	-0.1 (19)	1067.95 (30-I-3)	70.22 (30-I-2)	108.82 (32-II-2)
7	13	-0.4 (19)	-0.1 (19)	0.1 (19)	1540.62 (32-II-2)	-25.74 (19)	-713.65 (30-I-2)
7	14	0.0 (19)	-0.1 (19)	-0.0 (31-I-1)	133.92 (32-I-3)	150.27 (32-I-3)	-110.29 (30-I-2)
7	15	0.0 (29-II-1)	-0.1 (31-I-2)	-0.0 (31-I-1)	135.58 (32-I-3)	154.30 (32-I-3)	144.16 (32-II-2)
7	16	-0.6 (29-II-2)	-0.2 (31-I-2)	-0.2 (31-II-2)	1545.69 (32-II-2)	-41.90 (31-I-1)	746.77 (32-II-2)
8	1	0.0 (31-II-2)	-0.0 (29-II-2)	0.0 (32-II-2)	-38.15 (31-II-3)	165.44 (29-II-2)	54.26 (29-I-1)
8	2	0.0 (31-II-2)	-0.0 (17)	-0.0 (19)	-33.00 (31-II-1)	-40.03 (32-I-3)	65.12 (29-I-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
8	3	0.0 (31-II-2)	-0.0 (29-II-2)	-0.0 (19)	-142.79 (31-II-2)	166.30 (29-II-2)	-32.66 (30-II-2)
8	4	0.0 (31-II-2)	-0.0 (19)	-0.0 (19)	-170.39 (31-II-2)	-94.40 (32-I-3)	39.88 (19)
9	1	-0.0 (31-I-2)	-0.1 (19)	0.1 (32-II-3)	-165.20 (30-I-1)	-1242.62 (30-I-1)	17.25 (30-II-4)
9	2	-0.0 (31-I-3)	-0.1 (19)	0.1 (32-II-3)	-177.70 (30-I-1)	-1234.47 (30-I-1)	63.81 (30-II-4)
9	3	-0.1 (31-II-3)	-0.2 (19)	0.1 (31-II-4)	-95.56 (30-I-4)	-1412.42 (30-I-1)	269.17 (30-II-4)
9	4	-0.1 (32-I-1)	-0.4 (19)	0.1 (19)	-20.63 (19)	-2100.96 (30-I-1)	1080.64 (30-II-4)
9	5	-0.0 (32-I-4)	-0.1 (19)	0.1 (32-II-3)	-141.67 (30-I-1)	-1195.59 (30-I-1)	16.60 (30-II-4)
9	6	-0.1 (31-II-3)	-0.1 (19)	0.1 (19)	-113.06 (30-I-1)	-1074.04 (30-I-1)	74.81 (30-II-4)
9	7	-0.1 (32-I-1)	-0.0 (19)	0.1 (19)	-170.58 (30-I-1)	-798.08 (30-I-1)	242.79 (30-II-4)
9	8	-0.1 (31-II-4)	-0.0 (19)	0.0 (19)	-233.96 (30-I-1)	-92.06 (30-I-1)	284.65 (30-II-4)
9	9	-0.1 (19)	-0.1 (30-I-4)	0.0 (32-I-1)	-130.14 (30-I-1)	-1136.07 (30-I-1)	43.59 (30-II-4)
9	10	-0.1 (19)	-0.1 (29-I-4)	0.0 (32-II-2)	-106.01 (30-I-1)	-993.72 (30-I-1)	72.79 (30-II-4)
9	11	-0.1 (31-I-4)	-0.1 (31-I-4)	0.1 (19)	-165.30 (30-I-1)	-698.60 (30-I-1)	-39.39 (22)
9	12	0.1 (19)	0.0 (31-II-4)	0.1 (19)	-237.45 (30-I-1)	-121.39 (30-I-1)	-60.68 (22)
9	13	-0.0 (19)	-0.3 (19)	0.0 (31-II-3)	-93.04 (30-I-1)	-1071.67 (30-I-1)	73.87 (30-II-4)
9	14	-0.0 (19)	-0.3 (19)	0.0 (31-II-4)	-56.67 (30-I-1)	-1022.11 (30-I-1)	56.09 (30-II-4)
9	15	-0.1 (19)	-0.2 (19)	-0.1 (19)	-109.68 (30-I-1)	-1051.90 (30-I-1)	-128.85 (32-I-4)
9	16	0.0 (19)	-0.6 (31-I-4)	-0.1 (29-I-4)	-51.83 (29-I-4)	-1329.70 (30-I-4)	-546.65 (32-I-4)
10	1	-0.0 (31-I-2)	-0.1 (19)	0.0 (19)	-181.57 (32-I-1)	-1391.35 (32-I-1)	-8.88 (32-I-2)
10	2	-0.1 (31-I-2)	-0.1 (19)	0.0 (29-I-3)	-194.67 (32-I-1)	-1364.68 (32-I-1)	-5.54 (32-I-2)
10	3	-0.1 (31-I-2)	-0.2 (19)	0.1 (29-II-4)	-107.99 (32-I-2)	-1531.35 (32-I-1)	168.08 (30-II-2)
10	4	-0.2 (32-I-1)	-0.4 (19)	0.1 (19)	-37.00 (32-I-2)	-2266.18 (32-II-4)	1103.37 (30-II-4)
10	5	-0.0 (31-I-2)	-0.1 (19)	0.0 (19)	-160.37 (32-I-1)	-1392.74 (32-I-1)	-3.64 (32-I-4)
10	6	-0.1 (31-I-2)	-0.1 (19)	0.0 (19)	-115.04 (32-I-1)	-1292.48 (32-I-1)	18.38 (30-II-4)
10	7	-0.1 (32-I-1)	-0.1 (19)	0.1 (19)	-167.16 (32-I-1)	-1019.85 (32-I-1)	145.71 (30-II-4)
10	8	-0.1 (32-I-1)	0.0 (19)	0.0 (19)	-212.70 (32-I-1)	-189.14 (32-I-1)	215.95 (30-II-4)
10	9	-0.0 (32-II-3)	-0.1 (29-II-3)	0.0 (19)	-156.04 (32-I-1)	-1363.76 (32-I-1)	33.31 (30-II-4)
10	10	-0.1 (32-I-1)	-0.1 (29-II-3)	-0.0 (29-I-4)	-108.92 (32-I-1)	-1271.60 (32-I-1)	51.83 (30-II-4)
10	11	-0.1 (31-I-2)	-0.1 (29-II-3)	-0.1 (29-II-3)	-158.58 (32-I-1)	-1003.07 (30-I-1)	-59.21 (32-I-4)
10	12	-0.1 (31-I-2)	0.0 (29-II-4)	-0.0 (31-II-3)	-204.57 (32-I-1)	-192.79 (30-I-1)	-136.62 (32-I-4)
10	13	-0.0 (32-I-1)	-0.1 (29-II-3)	0.0 (19)	-170.21 (32-I-1)	-1301.90 (30-I-1)	39.96 (30-II-4)
10	14	-0.0 (32-I-1)	-0.2 (29-II-3)	0.0 (32-II-4)	-183.36 (32-I-1)	-1300.17 (30-I-1)	73.81 (30-II-4)
10	15	-0.1 (19)	-0.2 (29-II-3)	-0.0 (19)	-87.72 (30-I-2)	-1496.91 (30-I-1)	-76.31 (32-I-4)
10	16	-0.2 (31-II-3)	-0.6 (29-II-3)	-0.2 (29-II-3)	-40.26 (29-II-3)	-2173.82 (30-I-1)	-1006.88 (32-I-4)
11	1	-0.1 (19)	-0.0 (31-I-2)	0.0 (19)	1011.82 (30-I-3)	130.79 (30-I-3)	5.59 (32-I-2)
11	2	-0.1 (19)	-0.0 (31-I-2)	0.0 (19)	1009.97 (30-I-3)	116.73 (30-I-3)	-3.12 (30-II-4)
11	3	-0.1 (29-II-1)	-0.0 (27)	0.0 (19)	985.77 (30-I-3)	113.10 (30-I-3)	-25.53 (30-II-4)
11	4	-0.1 (29-I-1)	-0.0 (19)	0.0 (19)	937.12 (30-I-3)	121.04 (30-I-3)	-31.28 (30-II-4)
11	5	-0.1 (19)	-0.1 (31-I-2)	0.0 (29-II-1)	971.75 (30-I-3)	134.10 (30-I-3)	-5.26 (30-II-2)
11	6	-0.1 (19)	-0.1 (31-I-2)	0.0 (19)	919.76 (30-I-3)	82.86 (30-I-3)	-18.42 (30-II-4)
11	7	-0.1 (29-II-1)	-0.1 (27)	-0.0 (29-I-4)	902.35 (30-I-3)	77.79 (30-I-3)	-41.31 (30-II-4)
11	8	-0.2 (29-I-1)	-0.0 (27)	0.0 (19)	917.94 (30-I-3)	123.99 (30-I-3)	-59.39 (30-II-4)
11	9	-0.2 (19)	-0.1 (31-I-2)	0.1 (29-II-4)	1065.91 (30-I-3)	68.11 (30-I-2)	-120.80 (30-II-2)
11	10	-0.1 (19)	-0.1 (27)	0.1 (19)	714.16 (30-I-3)	116.80 (30-I-3)	-108.44 (30-II-4)
11	11	-0.1 (29-II-1)	-0.1 (31-I-2)	-0.1 (29-I-1)	701.00 (30-I-3)	109.75 (30-I-3)	36.67 (32-I-4)
11	12	-0.2 (29-I-1)	-0.1 (19)	-0.0 (19)	1037.14 (30-I-3)	50.62 (30-I-2)	44.37 (32-I-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
11	13	-0.4 (19)	-0.2 (27)	0.1 (19)	1545.44 (30-II-2)	-23.64 (19)	-756.50 (30-II-4)
11	14	0.0 (19)	-0.1 (27)	0.0 (19)	133.13 (30-I-3)	147.87 (30-I-3)	-156.15 (30-II-4)
11	15	0.0 (29-II-4)	-0.1 (31-I-2)	-0.0 (29-I-1)	135.12 (30-I-3)	140.71 (30-I-3)	90.46 (32-I-4)
11	16	-0.6 (29-I-1)	-0.2 (31-II-1)	-0.2 (29-I-1)	1480.99 (30-I-3)	-40.49 (31-I-1)	679.44 (32-I-4)
12	1	-0.0 (31-II-2)	-0.1 (19)	-0.0 (31-II-3)	-178.23 (32-I-1)	-1363.02 (32-I-1)	-28.59 (32-II-2)
12	2	-0.0 (32-I-1)	-0.1 (19)	-0.0 (31-I-3)	-191.66 (32-I-1)	-1342.14 (32-I-1)	-49.13 (32-II-2)
12	3	-0.1 (31-II-2)	-0.2 (19)	0.0 (29-II-3)	-101.38 (32-I-2)	-1517.19 (32-I-1)	112.17 (30-I-2)
12	4	-0.1 (19)	-0.4 (19)	0.1 (19)	-26.41 (19)	-2261.30 (32-II-2)	1057.25 (30-I-2)
12	5	-0.0 (32-II-3)	-0.1 (19)	-0.0 (31-I-3)	-162.35 (32-I-1)	-1401.60 (32-I-1)	-23.88 (32-II-2)
12	6	-0.1 (31-I-2)	-0.1 (19)	-0.0 (31-I-3)	-118.37 (32-I-1)	-1300.08 (32-I-1)	-33.46 (32-II-2)
12	7	-0.1 (32-I-1)	-0.1 (19)	-0.0 (31-I-3)	-172.33 (32-I-1)	-1024.33 (32-I-1)	90.55 (30-I-2)
12	8	-0.1 (32-I-1)	0.0 (19)	-0.0 (31-II-3)	-218.94 (32-I-1)	-191.42 (32-I-1)	165.40 (30-I-2)
12	9	-0.0 (19)	-0.1 (29-I-2)	-0.0 (31-I-3)	-163.90 (32-I-1)	-1412.98 (32-I-1)	12.26 (30-I-2)
12	10	-0.1 (19)	-0.1 (29-I-2)	-0.1 (31-I-3)	-120.21 (32-I-1)	-1308.93 (32-I-1)	8.57 (30-I-2)
12	11	-0.1 (32-I-1)	-0.1 (29-I-2)	-0.1 (31-II-3)	-174.85 (32-I-1)	-1029.65 (32-I-1)	-124.73 (32-II-2)
12	12	-0.1 (32-I-1)	0.0 (29-II-3)	-0.0 (31-II-3)	-222.61 (32-I-1)	-192.96 (32-I-1)	-196.68 (32-II-2)
12	13	-0.0 (19)	-0.1 (29-II-4)	-0.0 (31-I-3)	-182.61 (32-I-1)	-1397.74 (32-I-1)	16.03 (30-I-2)
12	14	-0.1 (32-I-1)	-0.2 (29-I-2)	-0.0 (32-II-2)	-196.35 (32-I-1)	-1369.95 (32-I-1)	20.91 (30-I-2)
12	15	-0.1 (19)	-0.2 (29-II-2)	-0.1 (19)	-111.05 (32-I-2)	-1534.67 (32-I-1)	-149.09 (32-II-2)
12	16	-0.2 (32-I-1)	-0.6 (29-II-2)	-0.2 (31-II-2)	-42.59 (31-I-3)	-2266.67 (32-II-4)	-1088.10 (32-II-2)
13	1	-0.1 (19)	-0.0 (31-I-2)	0.1 (19)	884.17 (30-I-3)	116.43 (30-I-3)	-18.07 (30-II-4)
13	2	-0.1 (19)	-0.0 (19)	0.1 (19)	834.66 (30-I-3)	100.79 (32-I-3)	-16.95 (30-II-4)
13	3	-0.1 (19)	-0.1 (19)	0.0 (31-II-4)	781.80 (30-I-3)	92.34 (30-I-3)	-30.89 (30-II-4)
13	4	-0.3 (19)	-0.0 (19)	0.0 (31-II-1)	736.66 (30-I-3)	65.00 (30-I-3)	-49.14 (30-II-4)
13	5	-0.1 (19)	-0.0 (31-I-2)	0.1 (19)	863.94 (30-I-3)	119.79 (30-I-3)	-59.11 (30-II-4)
13	6	-0.1 (19)	-0.1 (31-I-1)	0.1 (19)	737.98 (30-I-3)	82.45 (30-I-3)	-69.06 (30-II-4)
13	7	-0.1 (29-I-4)	-0.1 (19)	0.0 (27)	660.99 (30-I-3)	80.79 (30-I-3)	-60.92 (30-II-4)
13	8	-0.3 (19)	-0.0 (19)	0.0 (31-II-4)	662.57 (30-I-3)	38.24 (30-I-3)	-41.21 (30-II-4)
13	9	-0.2 (19)	-0.1 (31-I-2)	0.1 (31-I-1)	973.84 (30-I-3)	55.33 (30-I-4)	-207.51 (30-II-4)
13	10	-0.0 (19)	-0.1 (27)	0.1 (19)	542.34 (30-I-3)	120.26 (30-I-3)	-196.96 (30-II-4)
13	11	-0.1 (31-I-4)	-0.1 (31-I-4)	0.1 (19)	446.73 (30-I-3)	124.62 (30-I-3)	-58.28 (30-II-4)
13	12	-0.2 (19)	-0.1 (19)	-0.1 (19)	614.66 (30-I-3)	71.22 (30-I-3)	65.56 (32-I-4)
13	13	-0.4 (19)	-0.1 (27)	0.1 (19)	1431.17 (30-I-3)	-20.47 (19)	-755.39 (30-II-4)
13	14	-0.0 (19)	-0.1 (31-I-1)	0.0 (19)	58.71 (30-I-3)	162.17 (30-I-3)	-225.20 (30-II-4)
13	15	0.0 (31-II-4)	0.1 (19)	0.1 (19)	90.83 (30-I-3)	175.35 (30-I-3)	-36.13 (30-II-4)
13	16	-0.6 (31-I-4)	0.0 (19)	-0.1 (29-I-4)	679.89 (30-I-4)	51.80 (30-I-3)	279.88 (32-I-4)
14	1	0.0 (27)	-0.0 (30-I-1)	-0.0 (30-II-4)	-197.81 (27)	59.97 (30-I-1)	110.90 (30-II-4)
14	2	0.0 (27)	-0.0 (30-I-1)	-0.0 (30-II-4)	-188.77 (27)	137.44 (19)	66.34 (30-II-4)
14	3	0.0 (27)	-0.0 (30-I-1)	-0.0 (30-II-4)	-52.16 (27)	51.08 (30-I-1)	78.58 (30-II-4)
14	4	0.0 (27)	-0.0 (30-I-1)	-0.0 (30-II-4)	-59.54 (32-I-1)	124.41 (19)	63.70 (30-II-4)
15	1	0.1 (32-I-1)	-0.0 (19)	0.0 (31-I-1)	-221.11 (32-I-1)	218.55 (19)	101.91 (30-II-4)
15	2	0.1 (27)	0.0 (32-I-3)	0.0 (29-I-1)	-259.80 (32-I-1)	-240.26 (32-I-3)	87.31 (30-II-4)
15	3	0.0 (27)	-0.0 (19)	0.0 (31-I-1)	-206.85 (27)	260.78 (19)	-52.35 (31-I-1)
15	4	0.1 (32-II-4)	-0.0 (19)	0.0 (31-I-1)	-269.28 (32-II-4)	-307.90 (32-I-3)	-50.46 (31-I-1)
15	5	0.0 (32-II-4)	-0.0 (19)	-0.0 (30-II-4)	-189.53 (27)	249.19 (19)	-66.20 (31-I-1)
15	6	0.1 (32-II-4)	-0.0 (19)	0.0 (31-I-1)	-266.88 (32-II-4)	-287.47 (32-I-3)	-63.09 (29-I-1)
15	7	0.1 (32-II-4)	-0.0 (19)	-0.0 (30-II-4)	-158.37 (27)	185.23 (19)	-81.85 (19)
15	8	0.1 (32-II-4)	0.0 (32-I-3)	-0.0 (30-II-4)	-223.87 (32-II-4)	-174.83 (32-I-3)	-99.81 (19)
16	1	0.0 (32-II-4)	-0.0 (19)	0.0 (31-I-1)	-205.78 (32-II-4)	140.16 (19)	-52.45 (31-I-1)
16	2	0.0 (32-II-4)	-0.0 (17)	0.0 (19)	-222.93 (32-II-4)	-88.27 (32-I-3)	-79.97 (19)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
16	3	0.0 (32-II-4)	-0.0 (19)	-0.0 (30-II-4)	-54.45 (32-II-4)	125.80 (19)	-64.38 (19)
16	4	0.0 (32-II-4)	-0.0 (19)	0.0 (31-I-1)	-55.09 (32-II-4)	-29.64 (32-I-3)	-71.35 (19)
17	1	0.1 (32-I-1)	-0.0 (30-I-1)	-0.0 (30-II-4)	-236.07 (27)	179.04 (30-I-1)	58.01 (30-II-4)
17	2	0.1 (27)	-0.0 (30-I-1)	-0.0 (30-II-4)	-214.86 (32-I-1)	210.72 (19)	-56.43 (31-I-1)
17	3	0.1 (27)	-0.0 (30-I-1)	-0.0 (30-II-4)	-238.56 (27)	158.21 (30-I-1)	69.61 (30-II-4)
17	4	0.0 (32-I-1)	-0.0 (30-I-1)	-0.0 (30-II-4)	-209.45 (32-I-1)	255.76 (19)	46.45 (30-II-4)
17	5	0.1 (27)	-0.0 (30-I-1)	-0.0 (30-II-4)	-237.46 (27)	129.86 (30-I-1)	83.52 (30-II-4)
17	6	0.0 (32-I-1)	-0.0 (30-I-1)	-0.0 (30-II-4)	-197.57 (32-I-1)	243.67 (19)	60.84 (30-II-4)
17	7	0.0 (27)	-0.0 (30-I-1)	-0.0 (30-II-4)	-208.26 (27)	97.34 (30-I-1)	114.59 (30-II-4)
17	8	0.0 (27)	-0.0 (30-I-1)	-0.0 (30-II-4)	-173.34 (32-I-1)	178.22 (19)	74.28 (30-II-4)
18	1	0.0 (32-I-1)	-0.0 (30-I-1)	0.0 (32-II-2)	-171.14 (31-II-2)	200.13 (30-I-1)	-61.39 (29-II-1)
18	2	0.0 (27)	-0.0 (30-I-1)	-0.0 (19)	-154.10 (32-I-1)	219.13 (17)	-64.92 (31-II-1)
18	3	0.0 (27)	-0.1 (30-I-1)	0.0 (32-II-2)	-203.22 (27)	206.57 (30-I-1)	-27.83 (31-II-1)
18	4	0.0 (32-I-1)	-0.0 (30-I-1)	0.0 (31-II-1)	-177.43 (32-I-1)	272.82 (17)	-32.54 (31-II-1)
18	5	0.1 (27)	-0.1 (30-I-1)	0.0 (31-II-1)	-226.90 (27)	209.97 (30-I-1)	-14.45 (31-II-1)
18	6	0.0 (32-I-1)	-0.0 (30-I-1)	0.0 (31-II-1)	-201.57 (32-I-1)	274.44 (17)	-21.10 (31-II-1)
18	7	0.1 (32-I-1)	-0.1 (30-I-1)	0.0 (31-II-1)	-244.58 (27)	209.35 (30-I-1)	34.59 (19)
18	8	0.0 (27)	-0.0 (30-I-1)	0.0 (31-II-1)	-222.64 (32-I-1)	222.87 (17)	39.93 (19)
19	1	0.0 (32-I-1)	-0.0 (29-II-2)	0.0 (32-II-2)	-159.69 (31-II-2)	227.49 (17)	87.36 (30-I-2)
19	2	0.0 (27)	0.0 (32-I-3)	0.0 (30-II-2)	-189.81 (32-II-2)	-254.32 (32-I-3)	72.56 (30-I-2)
19	3	0.0 (27)	-0.0 (17)	0.0 (31-II-1)	-170.25 (27)	278.18 (17)	24.72 (30-I-2)
19	4	0.1 (32-I-1)	-0.0 (29-II-2)	0.0 (31-II-1)	-225.28 (32-I-1)	-346.57 (32-I-3)	14.53 (30-I-2)
19	5	0.0 (27)	-0.0 (17)	-0.0 (30-I-2)	-192.77 (27)	279.82 (17)	-26.60 (31-II-1)
19	6	0.1 (32-I-1)	0.0 (32-I-3)	-0.0 (30-I-2)	-247.26 (32-I-1)	-352.64 (32-I-3)	-26.86 (31-II-1)
19	7	0.1 (32-I-1)	-0.0 (17)	-0.0 (30-I-2)	-217.97 (27)	231.77 (17)	-75.98 (30-II-2)
19	8	0.1 (27)	0.0 (32-I-3)	-0.0 (30-I-2)	-258.56 (32-I-1)	-270.56 (32-I-3)	-67.50 (30-II-2)
20	1	0.1 (32-I-1)	-0.1 (30-I-1)	-0.0 (30-I-2)	-221.76 (27)	210.95 (30-I-1)	-56.40 (31-II-1)
20	2	0.1 (27)	-0.0 (30-I-1)	-0.0 (30-I-2)	-202.72 (32-I-1)	223.67 (17)	-67.66 (31-II-1)
20	3	0.1 (27)	-0.1 (30-I-1)	-0.0 (30-I-2)	-240.23 (27)	208.96 (30-I-1)	34.39 (30-II-4)
20	4	0.1 (32-I-1)	-0.0 (30-I-1)	-0.0 (30-I-2)	-215.56 (32-I-1)	271.92 (17)	-32.43 (31-II-1)
20	5	0.1 (27)	-0.0 (30-I-1)	-0.0 (30-II-4)	-246.87 (27)	202.82 (30-I-1)	45.60 (30-II-4)
20	6	0.1 (32-I-1)	-0.0 (30-I-1)	-0.0 (30-II-4)	-223.77 (32-I-1)	267.74 (19)	34.54 (30-II-4)
20	7	0.1 (32-I-1)	-0.0 (30-I-1)	-0.0 (30-II-4)	-244.50 (27)	193.24 (30-I-1)	55.54 (30-I-2)
20	8	0.1 (27)	-0.0 (30-I-1)	0.0 (31-II-1)	-227.23 (32-I-1)	212.95 (19)	42.44 (30-I-2)
21	1	0.1 (32-I-1)	-0.0 (17)	0.0 (31-II-1)	-202.96 (27)	231.56 (17)	102.26 (30-II-4)
21	2	0.1 (27)	0.0 (32-I-3)	0.0 (29-II-1)	-236.48 (32-I-1)	-264.61 (32-I-3)	87.08 (30-II-4)
21	3	0.1 (27)	-0.0 (19)	0.0 (31-II-1)	-207.57 (27)	276.05 (17)	34.53 (30-II-4)
21	4	0.1 (32-I-1)	0.0 (32-I-3)	0.0 (31-II-1)	-259.17 (32-I-1)	-345.36 (32-I-3)	30.42 (30-II-4)
21	5	0.1 (27)	-0.0 (19)	-0.0 (30-II-4)	-213.31 (27)	272.20 (19)	-45.12 (31-II-1)
21	6	0.1 (32-I-1)	-0.0 (19)	-0.0 (30-II-4)	-264.85 (32-I-1)	-338.54 (32-I-3)	-45.09 (31-I-1)
21	7	0.1 (32-I-1)	-0.0 (19)	-0.0 (30-II-4)	-219.43 (27)	221.45 (19)	-78.35 (29-I-1)
21	8	0.1 (27)	0.0 (32-I-3)	-0.0 (30-II-4)	-257.46 (32-II-4)	-248.69 (32-I-3)	-79.20 (29-I-1)
22	1	0.1 (27)	0.0 (32-II-4)	0.0 (31-I-1)	-250.67 (32-II-4)	14.14 (27)	16.72 (30-I-3)
22	2	0.1 (27)	0.0 (31-I-1)	-0.0 (30-I-3)	-260.26 (32-II-4)	-28.31 (27)	-67.06 (31-I-1)
22	3	0.1 (27)	0.0 (31-I-1)	0.0 (31-I-1)	-258.19 (27)	15.19 (27)	17.20 (29-II-4)
22	4	0.1 (27)	0.0 (27)	0.0 (19)	-262.84 (27)	-34.91 (27)	-87.09 (31-I-1)
22	5	0.1 (27)	0.0 (27)	0.0 (29-I-1)	-240.92 (27)	9.09 (31-I-4)	21.25 (29-II-4)
22	6	0.1 (27)	0.0 (27)	0.0 (31-I-1)	-245.78 (27)	-24.23 (27)	-73.77 (29-I-1)
22	7	0.1 (27)	0.0 (31-II-1)	0.0 (29-I-1)	-254.36 (27)	2.85 (27)	5.88 (29-II-4)
22	8	0.1 (27)	0.0 (31-II-1)	0.0 (31-I-1)	-259.12 (27)	-22.24 (31-I-1)	-46.32 (31-I-1)
23	1	0.1 (32-I-1)	0.0 (32-II-2)	0.0 (31-II-1)	-276.45 (32-II-4)	22.79 (32-II-2)	25.40 (32-I-2)
23	2	0.1 (32-I-1)	0.0 (32-II-2)	0.0 (31-II-1)	-291.53 (32-II-4)	-129.26 (32-II-4)	40.81 (30-I-2)
23	3	0.1 (32-I-1)	0.0 (32-II-4)	-0.0 (30-I-2)	-268.99 (32-I-1)	63.18 (32-II-4)	7.57 (32-I-2)
23	4	0.1 (32-I-1)	0.0 (32-II-2)	-0.0 (30-I-2)	-299.37 (32-I-1)	-169.03 (32-II-4)	41.66 (30-II-4)
23	5	0.1 (32-I-1)	0.0 (32-II-4)	-0.0 (30-II-4)	-261.42 (32-I-1)	63.32 (32-II-4)	8.66 (32-II-4)
23	6	0.1 (32-I-1)	0.0 (32-II-2)	-0.0 (30-II-4)	-291.57 (32-I-1)	-164.75 (32-II-2)	57.59 (30-II-4)
23	7	0.1 (32-I-1)	0.0 (32-II-4)	-0.0 (30-II-4)	-246.92 (32-II-2)	25.79 (32-II-4)	-15.86 (31-II-1)
23	8	0.1 (32-I-1)	0.0 (32-II-2)	-0.0 (30-II-4)	-261.93 (32-II-2)	-120.05 (32-II-2)	43.00 (30-II-4)
24	1	0.0 (27)	0.0 (32-I-4)	-0.0 (30-II-4)	-222.39 (32-I-1)	-5.67 (17)	-22.72 (27)
24	2	0.0 (27)	0.0 (27)	-0.0 (30-II-4)	-216.15 (32-I-1)	-28.20 (22)	109.15 (30-II-4)
24	3	0.0 (32-II-2)	-0.0 (30-I-1)	-0.0 (30-II-4)	-42.50 (27)	19.25 (32-I-3)	-22.84 (27)
24	4	0.0 (27)	-0.0 (30-I-1)	-0.0 (30-II-4)	-41.77 (27)	26.16 (30-I-1)	88.05 (30-II-4)
25	1	0.0 (32-II-4)	0.0 (32-I-3)	0.0 (19)	-58.05 (32-II-4)	3.90 (32-I-3)	20.91 (27)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
25	2	0.0 (32-II-4)	0.0 (27)	0.0 (29-I-1)	-71.07 (32-II-4)	13.19 (17)	-79.17 (19)
25	3	0.0 (32-II-4)	0.0 (31-I-1)	0.0 (31-I-1)	-196.17 (27)	-6.22 (30-I-1)	41.32 (32-II-4)
25	4	0.0 (32-II-4)	0.0 (32-I-3)	-0.0 (32-I-3)	-190.64 (27)	-21.99 (32-II-4)	-74.69 (31-I-1)
26	1	0.1 (27)	0.0 (31-II-4)	0.0 (31-I-1)	-238.32 (27)	9.92 (31-II-4)	2.09 (30-II-4)
26	2	0.1 (27)	0.0 (31-II-4)	0.0 (31-I-1)	-243.48 (27)	-20.74 (31-I-1)	-35.78 (29-II-1)
26	3	0.1 (27)	0.0 (31-II-4)	0.0 (31-II-1)	-245.54 (27)	13.04 (31-II-4)	7.68 (29-II-4)
26	4	0.1 (27)	0.0 (31-I-1)	0.0 (31-I-1)	-251.86 (27)	-28.20 (31-II-1)	-44.14 (31-II-1)
26	5	0.1 (27)	0.0 (31-I-2)	0.0 (31-II-1)	-245.92 (27)	11.42 (31-II-4)	7.74 (29-II-4)
26	6	0.1 (27)	0.0 (31-I-2)	0.0 (31-II-1)	-252.41 (27)	-27.58 (31-II-4)	-37.15 (29-II-1)
26	7	0.1 (27)	0.0 (31-I-2)	0.0 (31-II-1)	-248.97 (27)	5.94 (27)	1.82 (30-I-2)
26	8	0.1 (27)	0.0 (31-I-2)	0.0 (31-II-1)	-253.09 (27)	-23.07 (31-II-4)	-22.54 (31-II-1)
27	1	0.1 (27)	0.0 (31-II-4)	0.0 (31-II-1)	-242.69 (27)	7.78 (31-I-1)	-4.11 (27)
27	2	0.1 (27)	0.0 (31-II-4)	0.0 (31-II-1)	-247.17 (27)	-22.05 (31-II-2)	-13.61 (31-II-1)
27	3	0.1 (27)	0.0 (31-I-2)	-0.0 (30-I-2)	-226.95 (27)	12.56 (31-I-2)	-9.93 (32-I-2)
27	4	0.1 (27)	0.0 (27)	0.0 (31-II-1)	-233.26 (27)	-26.32 (31-I-2)	18.85 (30-I-2)
27	5	0.1 (27)	0.0 (31-I-1)	-0.0 (19)	-214.31 (27)	11.23 (27)	-7.26 (32-I-2)
27	6	0.1 (27)	0.0 (31-I-1)	0.0 (31-II-1)	-221.61 (27)	-25.17 (27)	17.00 (19)
27	7	0.1 (27)	0.0 (27)	-0.0 (19)	-200.92 (27)	6.86 (27)	-3.60 (32-II-2)
27	8	0.1 (27)	0.0 (31-I-1)	-0.0 (19)	-206.43 (27)	-20.83 (31-I-1)	16.17 (19)
28	1	0.0 (32-II-2)	0.1 (32-I-1)	-0.0 (32-II-2)	-129.72 (32-II-2)	-207.70 (32-I-2)	28.21 (31-II-1)
28	2	0.0 (32-II-4)	0.1 (32-II-4)	-0.0 (32-II-2)	-173.71 (32-II-4)	-256.28 (32-II-4)	44.06 (32-II-2)
28	3	0.0 (32-II-4)	0.1 (32-II-4)	-0.0 (31-II-1)	-173.85 (32-II-4)	-281.54 (32-I-1)	33.68 (31-II-1)
28	4	0.0 (32-II-4)	0.1 (32-II-4)	0.0 (30-I-2)	-131.99 (32-II-2)	-297.50 (32-II-2)	33.88 (31-II-1)
28	5	0.0 (32-II-4)	0.1 (32-I-1)	-0.0 (32-II-2)	28.28 (32-II-2)	-193.12 (32-I-2)	-7.16 (32-I-2)
28	6	0.0 (32-II-4)	0.1 (32-I-1)	-0.0 (32-II-2)	66.95 (32-II-2)	-224.93 (32-II-4)	-4.19 (32-I-2)
28	7	0.0 (32-II-4)	0.1 (32-II-4)	-0.0 (31-II-1)	64.48 (32-II-4)	-251.10 (32-I-1)	-6.56 (32-I-2)
28	8	0.0 (32-II-4)	0.1 (32-II-4)	0.0 (30-I-2)	21.66 (32-II-2)	-281.97 (32-II-2)	17.00 (32-II-2)
29	1	0.1 (32-II-2)	0.0 (32-II-4)	-0.0 (30-II-4)	-304.59 (32-II-4)	16.19 (32-I-4)	41.26 (30-II-4)
29	2	0.1 (32-II-2)	0.0 (32-II-2)	-0.0 (30-II-4)	-317.64 (32-I-1)	-129.90 (32-II-4)	91.86 (30-II-4)
29	3	0.1 (32-I-1)	0.0 (32-II-4)	-0.0 (30-II-4)	-257.56 (32-I-1)	60.52 (32-II-4)	15.74 (32-II-4)
29	4	0.1 (32-I-1)	0.0 (32-II-4)	-0.0 (30-II-4)	-284.52 (32-I-1)	-169.59 (32-II-4)	117.35 (30-II-4)
29	5	0.1 (32-I-1)	0.0 (32-II-4)	-0.0 (30-II-4)	-227.59 (27)	68.00 (32-II-4)	14.12 (30-II-4)
29	6	0.1 (32-I-1)	0.0 (32-I-4)	-0.0 (30-II-4)	-257.07 (32-I-4)	-160.95 (32-I-4)	141.70 (30-II-4)
29	7	0.1 (32-I-1)	0.0 (32-I-4)	-0.0 (30-II-4)	-184.14 (27)	42.99 (32-II-4)	21.52 (30-II-4)
29	8	0.1 (32-I-1)	0.0 (32-I-4)	-0.0 (30-II-4)	-209.83 (27)	-83.25 (32-I-4)	105.19 (30-II-4)
30	1	0.0 (31-II-2)	-0.0 (30-I-1)	0.0 (32-II-2)	-149.88 (31-II-2)	116.67 (30-I-1)	-91.48 (30-II-2)
30	2	0.0 (31-II-2)	-0.0 (30-I-1)	0.0 (32-II-2)	-95.91 (32-I-1)	192.68 (29-II-2)	-68.82 (31-II-3)
30	3	0.0 (31-II-2)	-0.0 (30-I-1)	0.0 (32-II-2)	-185.63 (31-II-2)	143.57 (30-I-1)	-58.98 (32-II-2)
30	4	0.0 (31-II-2)	-0.0 (30-I-1)	0.0 (32-II-2)	-120.20 (31-II-2)	255.66 (29-II-2)	-38.98 (32-II-2)
30	5	0.0 (31-II-2)	-0.0 (30-I-1)	0.0 (32-II-2)	-189.59 (31-II-2)	164.74 (30-I-1)	-41.63 (32-II-2)
30	6	0.0 (32-I-1)	-0.0 (30-I-1)	0.0 (32-II-2)	-143.79 (32-I-1)	264.75 (29-II-2)	-26.18 (32-II-2)
30	7	0.0 (32-II-4)	-0.0 (30-I-1)	0.0 (31-II-1)	-198.42 (27)	184.09 (30-I-1)	-32.39 (32-II-2)
30	8	0.0 (31-II-2)	-0.0 (30-I-1)	0.0 (31-II-1)	-171.91 (27)	215.23 (29-II-2)	36.74 (29-I-1)
31	1	0.0 (32-I-1)	-0.0 (29-II-2)	0.0 (32-II-2)	-104.68 (31-II-2)	202.71 (29-II-2)	70.12 (30-I-2)
31	2	0.0 (31-II-2)	0.0 (32-I-3)	0.0 (30-I-3)	-179.22 (31-II-2)	-178.35 (32-I-3)	88.79 (29-I-1)
31	3	0.0 (31-II-2)	-0.0 (17)	0.0 (32-II-2)	-130.42 (31-II-2)	267.29 (29-II-2)	39.89 (19)
31	4	0.0 (31-II-2)	-0.0 (19)	-0.0 (19)	-212.42 (31-II-2)	-295.41 (32-I-3)	43.14 (19)
31	5	0.0 (31-II-2)	-0.0 (17)	-0.0 (19)	-149.07 (31-II-2)	276.61 (29-II-2)	17.85 (19)
31	6	0.0 (31-II-2)	-0.0 (29-I-2)	-0.0 (19)	-214.44 (32-II-2)	-319.38 (32-I-3)	-28.64 (32-II-2)
31	7	0.0 (31-II-2)	-0.0 (17)	-0.0 (30-I-2)	-181.86 (32-I-1)	228.01 (29-II-2)	-82.72 (30-II-2)
31	8	0.0 (31-II-2)	0.0 (32-I-3)	-0.0 (19)	-229.23 (32-I-1)	-251.44 (32-I-3)	-75.36 (30-II-2)
32	1	0.0 (31-II-2)	-0.0 (30-I-1)	0.0 (32-II-2)	-25.65 (32-I-2)	70.82 (30-I-1)	-58.88 (32-II-2)
32	2	0.0 (31-II-2)	-0.0 (30-I-1)	0.0 (32-II-2)	-40.37 (32-I-1)	157.93 (29-II-2)	-47.93 (31-II-3)
32	3	0.0 (31-II-2)	-0.0 (30-I-1)	0.0 (32-I-1)	-149.18 (31-II-2)	78.36 (30-I-1)	-79.68 (32-I-1)
32	4	0.0 (31-II-2)	-0.0 (30-I-1)	0.0 (32-II-2)	-135.39 (31-II-2)	157.56 (29-II-2)	-37.19 (32-II-2)



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DEL RECAPITO FINALE DI SQUINZANO (LE)  
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BTK3**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
33	1	0.0 (31-II-2)	0.0 (32-I-3)	0.0 (32-I-3)	-196.53 (31-II-2)	-5.89 (29-II-2)	-40.88 (32-I-3)
33	2	0.0 (31-II-2)	0.0 (32-I-3)	0.0 (32-I-3)	-189.39 (31-II-2)	-31.50 (32-I-3)	-41.90 (30-I-3)
33	3	0.0 (31-II-2)	0.0 (32-I-3)	-0.0 (31-I-1)	-19.41 (31-II-3)	7.57 (31-I-1)	-28.46 (31-II-2)
33	4	0.0 (31-II-2)	0.0 (32-I-3)	0.0 (32-I-3)	-26.62 (32-II-2)	-24.52 (32-I-3)	49.76 (29-I-1)
34	1	0.0 (32-I-2)	0.0 (32-I-2)	-0.0 (32-I-1)	-91.64 (32-I-2)	-133.81 (31-II-2)	67.45 (32-II-2)
34	2	0.0 (32-I-2)	0.0 (32-I-2)	-0.0 (32-II-2)	-180.56 (32-I-2)	-194.96 (31-II-2)	113.60 (32-II-2)
34	3	0.0 (32-II-2)	0.0 (32-I-2)	-0.0 (32-II-2)	-189.88 (32-II-2)	-233.18 (32-II-2)	98.00 (32-II-2)
34	4	0.0 (32-II-2)	0.0 (32-I-2)	-0.0 (32-II-2)	-145.47 (32-II-2)	-276.32 (32-I-1)	82.46 (32-II-2)
34	5	0.0 (32-I-2)	0.0 (32-II-4)	-0.0 (32-I-1)	48.22 (32-I-3)	-99.66 (29-II-2)	-19.07 (31-I-1)
34	6	0.0 (32-I-2)	0.0 (31-II-2)	-0.0 (32-II-2)	79.35 (32-II-2)	-163.04 (31-II-2)	-12.81 (19)
34	7	0.0 (32-II-2)	0.0 (32-II-4)	-0.0 (32-II-2)	69.79 (32-II-2)	-199.43 (32-II-4)	12.02 (29-II-2)
34	8	0.0 (32-II-2)	0.0 (32-I-2)	-0.0 (32-II-2)	18.10 (32-I-2)	-261.32 (32-I-1)	39.78 (32-II-2)
35	1	-0.0 (30-I-1)	0.0 (32-I-2)	-0.0 (32-II-2)	23.09 (30-I-1)	12.11 (32-II-2)	38.94 (30-I-1)
35	2	0.0 (31-II-2)	0.0 (31-II-2)	-0.0 (32-I-1)	-40.20 (31-II-3)	-159.75 (32-I-2)	62.32 (32-I-1)
35	3	0.0 (31-II-3)	0.0 (32-I-2)	-0.0 (32-I-1)	25.75 (32-I-3)	-10.54 (29-I-1)	-25.82 (31-II-2)
35	4	-0.0 (30-II-2)	0.0 (31-II-2)	-0.0 (32-I-1)	7.84 (32-II-2)	-158.84 (32-I-2)	22.01 (32-I-1)
36	1	0.0 (31-II-2)	0.0 (31-I-1)	-0.0 (19)	-208.85 (27)	6.12 (31-II-2)	5.51 (29-II-2)
36	2	0.0 (31-II-2)	0.0 (31-I-1)	-0.0 (19)	-214.51 (27)	-24.87 (31-I-1)	25.47 (19)
36	3	0.1 (31-II-2)	0.0 (31-I-1)	-0.0 (19)	-213.27 (31-II-2)	13.93 (31-II-2)	-12.40 (19)
36	4	0.1 (31-II-2)	0.0 (31-I-1)	-0.0 (29-I-1)	-220.36 (31-II-2)	-39.80 (31-I-1)	47.85 (19)
36	5	0.1 (31-II-2)	0.0 (31-I-1)	-0.0 (19)	-239.45 (31-II-2)	26.41 (31-I-1)	-11.83 (19)
36	6	0.1 (31-II-2)	0.0 (31-II-2)	-0.0 (29-I-1)	-248.67 (31-II-2)	-57.59 (31-I-1)	63.88 (19)
36	7	0.1 (31-II-2)	0.0 (31-II-2)	0.0 (30-I-3)	-199.73 (31-II-2)	22.84 (31-I-1)	-24.12 (32-I-3)
36	8	0.1 (31-II-2)	0.0 (31-II-2)	0.0 (32-I-3)	-213.14 (31-II-2)	-39.49 (31-II-2)	44.02 (19)
37	1	0.0 (31-II-2)	-0.0 (19)	-0.0 (31-I-1)	-37.05 (31-II-2)	-4.87 (29-II-2)	-5.34 (29-II-1)
37	2	0.0 (32-II-2)	-0.0 (19)	-0.0 (29-I-1)	-33.44 (31-II-2)	14.42 (17)	24.62 (31-I-1)
37	3	0.0 (31-II-2)	-0.0 (17)	-0.0 (31-I-1)	12.28 (31-I-1)	1.90 (32-I-2)	-8.52 (31-II-2)
37	4	0.0 (31-II-2)	-0.0 (20)	-0.0 (32-I-2)	13.76 (31-II-2)	15.08 (29-II-2)	16.67 (29-I-1)
38	1	0.0 (31-II-2)	-0.0 (30-I-1)	0.0 (32-II-2)	17.33 (31-II-2)	80.67 (30-I-1)	-17.18 (29-II-3)
38	2	0.0 (31-II-3)	-0.0 (29-II-2)	0.0 (32-II-2)	17.37 (31-II-2)	139.16 (29-I-1)	-20.24 (29-II-3)
38	3	0.0 (31-II-2)	-0.0 (30-I-1)	0.0 (32-II-2)	-44.97 (31-II-2)	76.09 (30-I-1)	-38.21 (32-II-2)
38	4	0.0 (31-II-2)	-0.0 (29-II-2)	0.0 (32-II-2)	-51.41 (31-II-2)	133.42 (29-I-1)	-33.03 (32-II-2)
39	1	-0.0 (30-I-1)	0.0 (31-II-2)	-0.0 (32-II-2)	35.48 (30-I-1)	18.37 (32-I-1)	14.35 (30-I-1)
39	2	-0.0 (30-I-1)	0.0 (29-I-1)	-0.0 (32-II-2)	32.91 (30-I-1)	-33.85 (31-II-2)	24.31 (32-II-2)
39	3	-0.0 (30-I-1)	0.0 (32-I-2)	-0.0 (32-II-2)	6.37 (32-I-4)	16.96 (32-I-3)	-5.98 (31-II-2)
39	4	-0.0 (30-I-1)	0.0 (31-II-2)	-0.0 (30-I-1)	-6.92 (29-I-1)	-43.31 (32-I-2)	-9.82 (29-I-1)
40	1	0.0 (31-II-2)	-0.0 (29-II-2)	0.0 (30-II-2)	19.08 (32-II-2)	141.58 (29-II-2)	21.82 (29-I-1)
40	2	0.0 (32-II-2)	-0.0 (29-II-2)	-0.0 (31-I-1)	18.45 (31-II-2)	53.52 (29-I-1)	20.48 (29-I-1)
40	3	0.0 (31-II-2)	-0.0 (29-II-2)	-0.0 (19)	-54.43 (31-II-2)	136.17 (29-II-2)	15.43 (31-I-1)
40	4	0.0 (31-II-2)	-0.0 (29-II-2)	-0.0 (29-I-1)	-50.90 (32-II-2)	45.93 (17)	24.71 (31-I-1)

Verifiche stato limite ultimo

Verifica dei Muri in calcestruzzo

Scenario di calcolo: **ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO**

Simbologia:

Muro	Indice del muro in verifica
Nodi	[n1-n2-n3-n4...] Indici dei nodi di attacco del muro
Pann.X	Numero di pannelli in direzione locale X del muro(per muri a pannelli)
Pann.Y	Numero di pannelli in direzione locale Y del muro(per muri a pannelli)
Pann	Numero totale di pannelli (per muri a mesh)
Spess [cm]	Spessore del muro
Criterio	Criterio di verifica adottato per la verifica
Pannello	Indice del pannello
Nx [daN]	Sforzo in direzione x locale per metro lineare (Nx=sxx*spessore)
Ny [daN]	Sforzo in direzione y locale per metro lineare (Ny=syy*spessore)
Nxy [daN]	Sforzo tagliante locale per metro lineare (Nxy=sxy*spessore)
Mx [daN*m]	Momento in direzione x locale per metro lineare



My [daN*m]	Momento in direzione y locale per metro lineare
Mxy [daN*m]	Momento torcente locale per metro lineare
Ax [m <sup>2</sup> ]	Armatura totale pannello in direzione x locale <sup>(1)</sup>
Ay [m <sup>2</sup> ]	Armatura totale pannello in direzione y locale <sup>(1)</sup>
εc	Deformazione nel cls <sup>(2)</sup>
εf	Deformazione nell'acciaio <sup>(2)</sup>
Massimi	Armature massime riscontrate nel muro
Massimo	massima sigma ideale riscontrata nel muro
σid+,σid- [MPa]	$(\sigma_x^2 + \sigma_y^2 - \sigma_x \sigma_y + 3 \tau_{xy}^2)^{1/2}$ Tensioni ideali ai lembi della lastra (Acciaio)
σid+,σid- [MPa]	$(\sigma_x^2 + \sigma_y^2 - \sigma_x \sigma_y + 3 \tau_{xy}^2)^{1/2}$ Tensioni ideali ai lembi della lastra (Legno)
Fatt.Ampl.Sisma	Fattore moltiplicativo di gruppo per le azioni sismiche (solo se diverso da 1.0)
Cs	Coefficiente di sicurezza definito dal rapporto  Mr(N) / Md  (Mr(N)=Momento resistente corrispondente allo sforzo normale N,Md=momento agente), quando richiesto dal criterio di verifica
ζs	Livello di sicurezza sismico definito come rapporto tra l'accelerazione sopportabile e l'accelerazione di progetto, quando richiesto dal criterio di verifica

Note Verifica muri:

<sup>(1)</sup>: Le armature Ax ed Ay vanno intese come a metro lineare di pannello.

<sup>(2)</sup>:Le deformazioni sono stampate a meno del fattore 10<sup>-3</sup>; esse si riferiscono alla verifica considerando quali sollecitazioni di progetto Mx,d=Mx +/- |Mxy|,My,d=My +/- |Mxy| scegliendo il segno in modo tale da rendere massimo in valore assoluto il relativo momento flettente,le sollecitazioni stampate si riferiscono alle sollecitazioni in una data combinazione riferite al sistema locale del pannello

Muro [Platea]: 1 - Nodi: [1-2-11-10] Pann=4 Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,  $\zeta_e=1546.267$  [(14+15)-VIII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	231.38	-114.34	381.86	-37.00	15.35	-58.36	31.42	31.42	2	>100
1	53.73	9.91	114.80	13.57	2.63	14.39	31.42	31.42	2	>100

Muro [Platea]: 2 - Nodi: [11-20-19-10] Pann=4 Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,  $\zeta_e=306.660$  [(14+15)-III-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
3	-	455.62	-497.55	118.09	-58.54	43.65	31.42	31.42	9	>100
1	-509.89	325.91	-751.39	39.57	-66.63	58.22	31.42	31.42	2	>100

Muro [Platea]: 3 - Nodi: [29-38-37-28] Pann=4 Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,  $\zeta_e=1486.527$  [(14+15)-IV-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
3	-33.59	536.13	51.71	-10.34	-74.97	15.24	31.42	31.42	2	>100
1	-157.30	413.41	107.72	16.61	-66.54	-23.48	31.42	31.42	11	>100

Muro [Platea]: 4 - Nodi: [20-29-28-19] Pann=4 Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,  $\zeta_e=415.408$  [(14+15)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
1	-	519.57	-51.44	127.52	-61.25	10.91	31.42	31.42	9	>100
	1249.91									

Muro : 5 - Nodi: [34-33-133-134], Pann.X=4, Pann.Y=4 Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45,  $\zeta_e=25.797$  [(12+13)-VI-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	2832.66	6119.53	3328.92	-25.17	1353.81	-650.05	11.31	20.11	11	2.8
1	-957.45	6614.43	-893.49	-68.12	-872.92	-53.50	11.31	20.11	10	6.0

Muro : 6 - Nodi: [16-116-115-15], Pann.X=4, Pann.Y=4 Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45,  $\zeta_e=26.700$  [(12+13)-VI-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
13	23875.4	6397.05	1593.97	-406.31	128.70	121.66	20.11	11.31	(12+13)-II-4	6.5
1	6661.27	-994.43	-948.30	345.35	29.79	6.99	20.11	11.31	10	16

Muro : 7 - Nodi: [15-115-114-14], Pann.X=4, Pann.Y=4 Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45,  $\zeta_e=26.936$  [(12+13)-VI-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		

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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
13	32418.9 0	-199.10	5003.57	-368.66	112.80	132.23	20.11	11.31	(14+15)-IV-3	5.5
1	3123.70	-506.95	-841.38	342.21	43.39	0.10	20.11	11.31	11	16

Muro [Platea]: 8 - Nodi: [26-25-16-17] Pann=4 Spess.=50 cm, Terreno=Terreno1, , Criterio=CLS\_Platee\_ND, Materiale=C35/45,  $\zeta_e=958.049$  [(14+15)-II-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
1	1199.26	2152.86	-223.61	-50.48	229.40	73.65	31.42	31.42	4	84

Muro : 9 - Nodi: [31-30-130-131], Pann.X=4, Pann.Y=4 Spess.=20 cm, Terreno=--, Criterio=CLS\_Muri\_ND, Materiale=C35/45,  $\zeta_e=38.373$  [(12+13)-VIII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	3132.23	5213.53	2947.38	-22.39	1257.90	618.54	11.31	20.11	10	2.9
1	-494.17	2699.08	1450.15	-109.05	-819.25	0.14	11.31	20.11	11	6.5

Muro : 10 - Nodi: [32-31-131-132], Pann.X=4, Pann.Y=4 Spess.=20 cm, Terreno=--, Criterio=CLS\_Muri\_ND, Materiale=C35/45,  $\zeta_e=50.227$  [(12+13)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	4499.25	6135.10	2856.49	-21.54	1352.91	656.45	11.31	20.11	10	2.8
1	-675.72	3260.95	110.20	-114.14	-871.14	-5.07	11.31	20.11	11	6.1

Muro : 11 - Nodi: [14-114-113-13], Pann.X=4, Pann.Y=4 Spess.=20 cm, Terreno=--, Criterio=CLS\_Muri\_ND, Materiale=C35/45,  $\zeta_e=48.856$  [(14+15)-IV-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
13	32408.4 0	1750.03	4671.68	-370.25	112.17	142.97	20.11	11.31	(14+15)-IV-3	5.4
1	3271.57	-670.36	141.46	339.16	42.73	0.24	20.11	11.31	11	16

Muro : 12 - Nodi: [33-32-132-133], Pann.X=4, Pann.Y=4 Spess.=20 cm, Terreno=--, Criterio=CLS\_Muri\_ND, Materiale=C35/45,  $\zeta_e=28.627$  [(12+13)-VI-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	3398.82	6112.22	2585.48	-27.12	1354.16	649.68	11.31	20.11	10	2.8
1	-507.60	3150.69	-901.66	-116.57	-886.49	-8.55	11.31	20.11	11	6.0

Muro : 13 - Nodi: [13-113-112-12], Pann.X=4, Pann.Y=4 Spess.=20 cm, Terreno=--, Criterio=CLS\_Muri\_ND, Materiale=C35/45,  $\zeta_e=37.034$  [(12+13)-IV-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
13	29563.1 2	-40.74	4466.25	-347.52	89.86	130.86	20.11	11.31	(14+15)-IV-1	6.3
1	2695.60	-489.67	1432.41	318.15	40.55	-0.95	20.11	11.31	11	17

Muro [Platea]: 14 - Nodi: [30-29-20-21]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=430.336$  [(12+13)-VII-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
1	2324.68	-392.93	-749.22	-280.95	-8.05	65.43	31.42	31.42	11	71

Muro [Platea]: 15 - Nodi: [22-21-12-13]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=113.284$  [(12+13)-I-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
8	3804.58	-587.28	885.66	-307.94	-21.35	-139.76	31.42	31.42	2	54
1	3957.35	1338.28	550.05	-319.98	211.58	48.33	31.42	31.42	11	66

Muro [Platea]: 16 - Nodi: [21-20-11-12]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=140.400$  [(14+15)-III-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
2	2327.53	-485.87	1316.77	-297.48	-5.67	-118.17	31.42	31.42	2	59
1	2477.73	1441.22	821.27	-284.15	143.61	-71.46	31.42	31.42	2	69

Muro [Platea]: 17 - Nodi: [31-30-21-22]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=220.162$  [(12+13)-VIII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
1	3846.86	-464.16	-174.57	-344.00	-45.86	-54.33	31.42	31.42	2	61

Muro [Platea]: 18 - Nodi: [33-32-23-24]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=434.503$  [(14+15)-VI-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	2549.50	2320.85	13.18	-193.16	404.70	-31.16	31.42	31.42	4	59
1	3208.86	-490.38	80.89	-249.92	-38.19	-83.12	31.42	31.42	2	73

Muro [Platea]: 19 - Nodi: [24-23-14-15]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=98.715$  [(14+15)-II-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
8	3638.43	263.60	-375.99	-367.11	-129.16	-74.88	31.42	31.42	11	55
1	2864.23	2918.24	263.34	-190.36	334.28	78.42	31.42	31.42	9	62

Muro [Platea]: 20 - Nodi: [32-31-22-23]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=222.231$  [(12+13)-II-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	2798.73	-	52.80	-221.74	402.08	-25.77	31.42	31.42	4	60
1	3839.18	-527.59	-50.18	-322.80	-36.01	-72.69	31.42	31.42	2	61

Muro [Platea]: 21 - Nodi: [23-22-13-14]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=92.049$  [(14+15)-IV-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
8	4017.89	-	250.42	-358.14	28.17	-91.90	31.42	31.42	2	54
1	3322.29	-	506.60	-249.42	341.93	52.64	31.42	31.42	9	65

Muro [Platea]: 22 - Nodi: [3-4-13-12]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=89.618$  [(12+13)-I-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	4431.69	145.24	579.43	-385.18	-55.47	-112.61	31.42	31.42	2	49
1	4385.65	88.49	122.34	-344.94	17.36	8.91	31.42	31.42	11	68

Muro [Platea]: 23 - Nodi: [41-40-31-32]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=533.407$  [(14+15)-I-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
6	4393.38	631.47	-101.75	-385.79	-153.62	6.73	31.42	31.42	11	62
1	4342.73	311.72	183.77	-348.64	25.86	15.89	31.42	31.42	11	66

Muro [Platea]: 24 - Nodi: [39-38-29-30]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=655.730$  [(14+15)-VII-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
2	2407.65	115.32	-77.75	-297.59	-41.27	62.63	31.42	31.42	11	68
1	2529.27	69.54	-19.56	-292.11	-1.87	-37.29	31.42	31.42	2	75

Muro [Platea]: 25 - Nodi: [2-3-12-11]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=145.928$  [(14+15)-I-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	2575.92	-76.08	354.00	-280.33	-18.39	-110.90	31.42	31.42	2	63
1	1352.94	-0.08	372.95	-60.80	4.59	29.62	31.42	31.42	11	>100

Muro [Platea]: 26 - Nodi: [4-5-14-13]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=544.967$  [(14+15)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	4374.45	139.67	188.44	-370.50	-37.24	-39.39	31.42	31.42	2	59
1	4389.31	92.84	185.59	-347.64	11.28	-1.40	31.42	31.42	2	69

Muro [Platea]: 27 - Nodi: [5-6-15-14]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=640.049$  [(14+15)-VII-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
2	4246.70	161.04	151.56	-363.33	-32.70	-5.04	31.42	31.42	2	66
1	4199.13	93.16	48.94	-356.15	9.56	-6.14	31.42	31.42	2	67

Muro [Platea]: 28 - Nodi: [33-42-41-32]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=541.554$  [(14+15)-I-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	796.31	4107.28	32.20	-123.72	-393.21	38.96	31.42	31.42	11	56
1	904.86	3806.55	-494.49	-121.65	-269.38	28.17	31.42	31.42	11	82

Muro [Platea]: 29 - Nodi: [40-39-30-31]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=344.548$  [(12+13)-VI-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
6	4197.62	576.56	-448.69	-366.20	-163.95	89.69	31.42	31.42	11	53
1	4202.10	329.31	-117.41	-385.18	18.96	25.92	31.42	31.42	11	59

Muro [Platea]: 30 - Nodi: [34-33-24-25]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=453.710$  [(14+15)-VI-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	1851.18	1945.37	56.96	-135.47	359.01	-43.22	31.42	31.42	4	63
1	2331.94	236.99	271.58	-215.67	-105.70	-118.40	31.42	31.42	(14+15)-V-4	74

Muro [Platea]: 31 - Nodi: [25-24-15-16]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=99.157$  [(12+13)-II-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
3	1954.05	2115.30	-171.46	-145.00	371.29	50.10	31.42	31.42	4	60
1	2003.00	2356.78	-15.87	-118.38	284.27	98.21	31.42	31.42	4	67

Muro [Platea]: 32 - Nodi: [35-34-25-26]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=158.634$  [(12+13)-VI-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
2	1163.62	2076.53	0.40	-50.96	222.79	-54.00	31.42	31.42	4	92
1	1082.04	1109.36	486.14	-35.81	66.39	-69.95	31.42	31.42	10	>100

Muro [Platea]: 33 - Nodi: [7-8-17-16]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=218.913$  [(12+13)-I-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
1	2323.28	52.25	-52.50	-278.12	-5.48	-54.60	31.42	31.42	(14+15)-II-2	74

Muro [Platea]: 34 - Nodi: [34-43-42-33]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,ζ<sub>e</sub>=650.148 [(12+13)-I-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	886.28	3163.24	-281.37	-142.88	-351.57	81.72	31.42	31.42	11	56
1	351.82	2844.94	-232.34	-86.81	-205.60	-8.74	31.42	31.42	(14+15)-II-1	>100

Muro [Platea]: 35 - Nodi: [35-44-43-34]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,ζ<sub>e</sub>=1060.008 [(14+15)-I-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
2	162.70	1350.43	-227.26	-46.38	-210.91	37.52	31.42	31.42	11	100
1	308.42	1023.22	120.05	-41.33	-1.00	-5.36	31.42	31.42	(14+15)-II-1	>100

Muro [Platea]: 36 - Nodi: [6-7-16-15]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,ζ<sub>e</sub>=590.743 [(14+15)-VI-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
6	3410.38	224.23	-334.82	-307.57	-68.76	87.46	31.42	31.42	2	62
1	3447.15	97.67	-106.33	-307.25	6.83	-1.44	31.42	31.42	2	79

Muro [Platea]: 37 - Nodi: [8-9-18-17]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,ζ<sub>e</sub>=2461.979 [(14+15)-I-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
2	251.97	-101.23	-158.79	-46.31	9.43	29.69	31.42	31.42	(14+15)-IV-1	>100
1	270.68	-27.07	-132.71	-48.88	-4.62	-7.59	31.42	31.42	(14+15)-II-2	>100

Muro [Platea]: 38 - Nodi: [36-35-26-27]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,ζ<sub>e</sub>=1721.222 [(14+15)-VI-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
2	165.01	2088.39	-39.09	21.79	200.40	-24.90	31.42	31.42	4	>100
1	145.55	1214.17	132.15	20.50	92.43	-19.97	31.42	31.42	10	>100

Muro [Platea]: 39 - Nodi: [36-45-44-35]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,ζ<sub>e</sub>=2477.430 [(14+15)-II-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	20.77	252.82	28.45	-9.21	-52.36	-14.40	31.42	31.42	(12+13)-II-1	>100
1	-269.30	110.98	26.06	38.43	22.06	14.15	31.42	31.42	10	>100

Muro [Platea]: 40 - Nodi: [27-26-17-18]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,ζ<sub>e</sub>=1063.203 [(14+15)-II-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
1	189.29	2148.62	-72.73	22.35	199.27	30.22	31.42	31.42	4	>100

#### Verifiche stato limite di esercizio

##### Verifica dei Muri (Stati limite esercizio)

Scenario di calcolo: **ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO**

#### Simbologia

P.	Numero pannello
Nx [MPa]	Sforzo normale in direzione x
Ny [MPa]	Sforzo normale in direzione y
Nxy [MPa]	Sforzo tagliante in direzione xy
Mx [daN]	Momento flettente in direzione x
My [daN]	Momento flettente in direzione y
Mxy [daN]	Momento torcente
Afx [cmq/m]	Area acciaio in direzione x per metro lineare
Afy [cmq/m]	Area acciaio in direzione y per metro lineare
$\sigma_c$ [MPa]	Tensione nel calcestruzzo compresso
$\sigma_f$ [MPa]	Tensione nell'acciaio
$\sigma_{ct}$ [MPa]	Tensione nel calcestruzzo teso
$\sigma_{sct}$ [MPa]	Tensione nel calcestruzzo teso (quando richiesto dalla verifica)
$\sigma_{sca}$ [MPa]	Tensione ammissibile nel calcestruzzo
$\sigma_{sfa}$ [MPa]	Tensione ammissibile nell'acciaio
$\sigma_{scta}$ [MPa]	Tensione ammissibile nel calcestruzzo teso
Cbc	Combinazione generatore della tensione nel cls compresso
Cbct	Combinazione generatore della tensione nel cls teso
Cbf	Combinazione generatore della tensione nell'acciaio
Cb	Combinazione
$\sigma_{fmed}$ [MPa]	Tensione media dell'acciaio
Wd [mm]	Apertura delle fessure
Wk [mm]	Apertura caratteristica delle fessure
Wamm_Freq [mm]	Apertura ammissibile delle fessure per combinazione Frequente
Wamm_Qp [mm]	Apertura ammissibile delle fessure per combinazione Quasi Permanente
Wamm_Rara [mm]	Apertura ammissibile delle fessure per combinazione Rara
Cs	Coefficiente di sicurezza definito come minimo di $\sigma_{Am}/\sigma$ tra acciaio e calcestruzzo oppure Wamm/Wk



Muro [Platea]: 1 - Nodi: [1-2-11-10]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.00	0.24	20	22	Si	>100
3	31.42	31.42	-0.00	1.33	21	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	0.27	28	28	Si	>100
3	31.42	31.42	-0.00	0.51	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	0.0	-0.0	0.0	-11.60	12.13	-36.45	0.27	0.000	0.000	28 (Qp)	Si	>100
4	0.0	-0.0	0.0	-9.90	12.34	-36.03	0.19	0.000	0.000	24 (Fr)	Si	>100

Muro [Platea]: 2 - Nodi: [11-20-19-10]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.02	2.33	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.03	1.51	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
3	-0.0	0.0	-0.0	71.15	-37.32	31.30	1.51	0.002	0.002	28 (Qp)	Si	91
3	-0.0	0.0	-0.0	51.77	-59.03	35.23	1.24	0.001	0.001	27 (Fr)	Si	>100

Muro [Platea]: 3 - Nodi: [29-38-37-28]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	31.42	31.42	-0.01	1.65	21	22	Si	>100
3	31.42	31.42	-0.00	1.77	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.01	0.41	28	28	Si	>100
3	31.42	31.42	-0.00	1.25	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	-0.0	0.0	0.0	14.93	-31.78	-7.81	1.20	0.002	0.002	28 (Qp)	Si	>100
3	-0.0	0.0	0.0	-6.31	-31.56	1.29	0.60	0.001	0.001	26 (Fr)	Si	>100

Muro [Platea]: 4 - Nodi: [20-29-28-19]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	31.42	31.42	-0.02	2.36	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	31.42	31.42	-0.03	1.71	28	28	Si	>100

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Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	-0.0	0.0	-0.0	78.46	-39.54	10.94	1.71	0.003	0.003	28 (Qp)	Si	77
1	-0.0	0.0	-0.0	78.55	-36.93	6.04	1.61	0.002	0.002	26 (Fr)	Si	>100

Muro : 5 - Nodi: [34-33-133-134], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	11.31	20.11	-2.71	58.28	22	22	Si	6.2

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	11.31	20.11	-1.03	16.09	28	28	Si	16
8	11.31	20.11	-0.08	17.12	28	28	Si	21

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	0.0	-0.2	0.1	7.78	-364.25	149.35	11.11	0.009	0.009	25 (Fr)	Si	33
8	0.1	0.0	-0.0	-23.93	-25.86	23.60	17.12	0.028	0.028	28 (Qp)	Si	7.1

Muro : 6 - Nodi: [16-116-115-15], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	20.11	11.31	-0.64	9.11	22	22	Si	35
14	20.11	11.31	-0.13	18.73	22	22	Si	19

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
13	20.11	11.31	-1.03	16.06	28	28	Si	16
14	20.11	11.31	-0.08	16.58	28	28	Si	22

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
14	0.0	0.1	-0.0	-25.82	-23.67	23.71	16.58	0.027	0.027	28 (Qp)	Si	7.4
14	0.0	0.1	-0.0	-26.19	-25.68	24.22	9.37	0.008	0.008	25 (Fr)	Si	38

Muro : 7 - Nodi: [15-115-114-14], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	20.11	11.31	-0.64	8.82	22	22	Si	35

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
13	20.11	11.31	-0.94	8.06	28	28	Si	18

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
10	-0.0	-0.1	0.0	-99.86	-15.51	10.52	2.95	0.002	0.002	26 (Fr)	Si	>100
13	-0.2	-0.1	0.1	-360.87	-11.97	172.03	8.06	0.006	0.006	28 (Qp)	Si	32

Muro [Platea]: 8 - Nodi: [26-25-16-17]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.04	5.82	22	22	Si	62
4	31.42	31.42	-0.01	5.91	22	22	Si	61

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.06	5.35	28	28	Si	67
4	31.42	31.42	-0.01	5.44	28	28	Si	66

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
3	0.0	-0.0	-0.0	-117.43	150.24	6.59	5.35	0.008	0.008	28 (Qp)	Si	24
3	0.0	-0.0	-0.0	-114.80	152.67	7.19	5.24	0.008	0.008	25 (Fr)	Si	37

Muro : 9 - Nodi: [31-30-130-131], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	11.31	20.11	-2.45	46.85	22	22	Si	7.7
16	11.31	20.11	-2.43	54.41	22	22	Si	6.6

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	11.31	20.11	-0.94	16.60	28	28	Si	18

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
16	0.0	-0.1	-0.0	10.08	-325.36	-133.45	16.60	0.014	0.014	28 (Qp)	Si	14
16	0.0	-0.1	-0.0	10.07	-325.37	-133.45	16.60	0.014	0.014	23 (Fr)	Si	21

Muro : 10 - Nodi: [32-31-131-132], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	11.31	20.11	-2.62	48.58	22	22	Si	7.4

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	11.31	20.11	-0.94	7.98	28	28	Si	18

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.2	-0.2	0.1	-11.77	-360.71	173.08	7.98	0.006	0.006	28 (Qp)	Si	32
11	-0.1	-0.0	-0.0	-24.39	-151.12	-11.81	6.68	0.006	0.006	23 (Fr)	Si	54

Muro : 11 - Nodi: [14-114-113-13], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	20.11	11.31	-0.62	8.50	22	22	Si	36
3	20.11	11.31	-0.62	8.60	22	22	Si	36

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
13	20.11	11.31	-0.94	7.97	28	28	Si	18

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
10	-0.0	-0.1	0.0	-98.64	-14.75	12.82	2.74	0.002	0.002	26 (Fr)	Si	>100
13	-0.2	-0.2	0.1	-360.62	-11.12	174.19	7.97	0.006	0.006	28 (Qp)	Si	32

Muro : 12 - Nodi: [33-32-132-133], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

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Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	11.31	20.11	-2.63	48.73	22	22	Si	7.4

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	11.31	20.11	-0.94	8.06	28	28	Si	18

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.1	-0.2	0.1	-12.81	-360.98	171.61	8.06	0.006	0.006	28 (Qp)	Si	32
16	-0.1	-0.2	-0.1	-12.36	-360.81	-171.15	7.98	0.006	0.006	23 (Fr)	Si	48

Muro : 13 - Nodi: [13-113-112-12], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	20.11	11.31	-0.59	10.13	22	22	Si	36
16	20.11	11.31	-0.43	33.48	22	20	Si	11

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	20.11	11.31	-0.94	16.61	28	28	Si	18

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
15	0.0	0.1	0.0	-15.49	-31.61	-20.40	10.53	0.009	0.009	23 (Fr)	Si	34
16	-0.1	0.0	-0.0	-325.71	9.71	-133.04	16.61	0.014	0.014	28 (Qp)	Si	14

Muro [Platea]: 14 - Nodi: [30-29-20-21]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.03	8.50	22	22	Si	42

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.05	6.12	28	28	Si	59

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
2	0.0	-0.0	0.0	-132.72	124.21	-12.40	6.12	0.010	0.010	28 (Qp)	Si	21
2	0.0	-0.0	-0.0	-125.27	126.46	-6.34	5.79	0.009	0.009	26 (Fr)	Si	33

Muro [Platea]: 15 - Nodi: [22-21-12-13]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.07	11.13	22	22	Si	32
4	31.42	31.42	-0.05	13.33	22	22	Si	27

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.09	8.42	28	28	Si	43
4	31.42	31.42	-0.03	10.55	28	28	Si	34

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

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P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
4	0.0	-0.0	0.0	-201.84	-32.17	-35.01	10.55	0.017	0.017	28 (Op)	Si	12
4	0.0	-0.0	0.0	-196.08	-32.04	-34.86	10.23	0.017	0.017	23 (Fr)	Si	18

Muro [Platea]: 16 - Nodi: [21-20-11-12]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	31.42	31.42	-0.03	8.75	22	22	Si	41

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	31.42	31.42	-0.05	6.12	28	28	Si	59

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	-0.0	0.0	-137.31	126.27	-39.44	6.12	0.009	0.009	28 (Op)	Si	21
1	0.0	-0.0	0.0	-130.15	129.81	-38.28	5.81	0.009	0.009	23 (Fr)	Si	34

Muro [Platea]: 17 - Nodi: [31-30-21-22]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.06	11.12	22	22	Si	32
3	31.42	31.42	-0.02	12.43	22	22	Si	29

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.08	8.26	28	28	Si	44
3	31.42	31.42	-0.03	10.19	28	28	Si	35

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
3	0.0	-0.0	-0.0	-194.17	-67.65	-2.34	10.19	0.017	0.017	28 (Op)	Si	12
3	0.0	-0.0	-0.0	-186.83	-49.72	3.42	9.82	0.016	0.016	26 (Fr)	Si	19

Muro [Platea]: 18 - Nodi: [33-32-23-24]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.07	10.40	22	22	Si	35
7	31.42	31.42	-0.03	11.83	22	22	Si	30

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.09	8.63	28	28	Si	42
5	31.42	31.42	-0.03	10.41	28	28	Si	35

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
5	0.0	-0.0	0.0	-200.19	-58.01	-3.76	10.41	0.017	0.017	28 (Op)	Si	12
5	0.0	-0.0	0.0	-195.80	-37.97	-2.80	10.20	0.017	0.017	26 (Fr)	Si	18

Muro [Platea]: 19 - Nodi: [24-23-14-15]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.08	9.77	22	22	Si	37
6	31.42	31.42	-0.05	12.42	22	22	Si	29

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
5	31.42	31.42	-0.09	8.87	28	28	Si	41
6	31.42	31.42	-0.03	10.85	28	28	Si	33

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
6	0.0	-0.0	-0.0	-207.47	-18.42	-12.67	10.85	0.018	0.018	28 (Qp)	Si	11
6	0.0	-0.0	-0.0	-204.06	-18.12	-12.10	10.67	0.018	0.018	23 (Fr)	Si	17

Muro [Platea]: 20 - Nodi: [32-31-22-23]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.07	11.59	22	22	Si	31
5	31.42	31.42	-0.02	12.91	22	22	Si	28

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.09	9.27	28	28	Si	39
3	31.42	31.42	-0.03	11.01	28	28	Si	33

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
3	0.0	-0.0	0.0	-207.62	-57.04	-11.76	11.01	0.018	0.018	28 (Qp)	Si	11
3	0.0	-0.0	-0.0	-202.55	-37.44	-8.39	10.74	0.018	0.018	26 (Fr)	Si	17

Muro [Platea]: 21 - Nodi: [23-22-13-14]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.08	11.52	22	22	Si	31
6	31.42	31.42	-0.05	13.52	22	22	Si	27

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.09	9.47	28	28	Si	38
4	31.42	31.42	-0.03	11.36	28	28	Si	32

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	0.0	-0.0	0.0	-214.90	-17.24	-14.38	11.36	0.019	0.019	28 (Qp)	Si	11
4	0.0	-0.0	0.0	-210.74	-17.16	-13.68	11.12	0.018	0.018	23 (Fr)	Si	16

Muro [Platea]: 22 - Nodi: [3-4-13-12]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.01	13.65	22	22	Si	26
3	31.42	31.42	-0.00	13.87	22	22	Si	26

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.01	11.38	28	28	Si	32

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
2	0.0	0.0	0.0	-184.52	-23.47	-56.79	10.95	0.019	0.019	28 (Qp)	Si	11
2	0.0	0.0	0.0	-179.21	-21.32	-47.84	10.58	0.018	0.018	26 (Fr)	Si	17

Muro [Platea]: 23 - Nodi: [41-40-31-32]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.02	13.88	22	22	Si	26
6	31.42	31.42	-0.02	13.94	22	22	Si	26

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.01	11.37	28	28	Si	32

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
2	0.0	0.0	0.0	-205.59	-44.13	-4.46	11.31	0.019	0.019	28 (Qp)	Si	11
2	0.0	0.0	0.0	-202.64	-42.74	-3.86	11.11	0.019	0.019	23 (Fr)	Si	16

Muro [Platea]: 24 - Nodi: [39-38-29-30]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.01	8.59	22	22	Si	42
1	31.42	31.42	-0.00	8.69	21	22	Si	41

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.00	6.39	28	28	Si	56
1	31.42	31.42	-0.00	6.62	28	28	Si	54

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	-0.0	-157.33	-4.89	-19.08	6.62	0.010	0.010	28 (Qp)	Si	20
1	0.0	0.0	-0.0	-153.55	-5.15	-15.32	6.33	0.009	0.009	26 (Fr)	Si	32

Muro [Platea]: 25 - Nodi: [2-3-12-11]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	8.80	22	22	Si	41
3	31.42	31.42	-0.00	9.00	18	22	Si	40

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	6.31	28	28	Si	57
3	31.42	31.42	0.00	6.64	28	28	Si	54

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
3	0.0	0.0	0.0	-149.58	-4.88	23.86	6.64	0.010	0.010	28 (Qp)	Si	20
3	0.0	0.0	0.0	-143.55	-5.07	23.33	6.33	0.010	0.010	23 (Fr)	Si	31

Muro [Platea]: 26 - Nodi: [4-5-14-13]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.00	13.01	22	22	Si	28
2	31.42	31.42	-0.00	13.15	22	22	Si	27

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
6	31.42	31.42	-0.00	11.85	28	28	Si	30
8	31.42	31.42	-0.00	11.97	28	28	Si	30

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.1	0.0	0.0	-225.61	-17.90	-11.43	11.97	0.020	0.020	28 (Qp)	Si	10
8	0.1	0.0	0.0	-218.16	-16.25	-9.47	11.60	0.019	0.019	26 (Fr)	Si	16

Muro [Platea]: 27 - Nodi: [5-6-15-14]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	11.97	22	22	Si	30
2	31.42	31.42	-0.00	12.62	22	22	Si	29

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	11.33	28	28	Si	32
2	31.42	31.42	-0.00	11.80	28	28	Si	31

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
2	0.1	0.0	0.0	-219.49	-17.42	-3.27	11.80	0.020	0.020	28 (Qp)	Si	10
2	0.0	0.0	0.0	-213.20	-15.85	-2.27	11.44	0.019	0.019	26 (Fr)	Si	16

Muro [Platea]: 28 - Nodi: [33-42-41-32]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.03	12.76	22	22	Si	28
4	31.42	31.42	-0.00	13.39	22	22	Si	27

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.01	10.74	28	28	Si	34
4	31.42	31.42	-0.00	11.17	28	28	Si	32

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	0.0	0.0	-0.0	-47.20	-222.71	20.12	11.17	0.018	0.018	28 (Qp)	Si	11
4	0.0	0.0	-0.0	-45.54	-218.32	18.96	10.98	0.018	0.018	23 (Fr)	Si	17

Muro [Platea]: 29 - Nodi: [40-39-30-31]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.03	13.27	22	22	Si	27
2	31.42	31.42	-0.00	13.70	22	22	Si	26

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.02	10.49	28	28	Si	34
2	31.42	31.42	-0.00	10.93	28	28	Si	33

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	-0.0	-210.64	6.39	6.13	10.90	0.018	0.018	28 (Qp)	Si	11
1	0.0	0.0	-0.0	-206.43	5.86	6.16	10.63	0.017	0.017	23 (Fr)	Si	17

Muro [Platea]: 30 - Nodi: [34-33-24-25]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45



Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.06	7.48	22	22	Si	48
7	31.42	31.42	-0.02	9.30	22	22	Si	39

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.09	6.48	28	28	Si	56
5	31.42	31.42	-0.03	8.57	28	28	Si	42

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
5	0.0	-0.0	0.0	-165.28	-62.86	-13.49	8.57	0.014	0.014	28 (Qp)	Si	14
5	0.0	-0.0	0.0	-162.90	-59.02	-13.23	8.44	0.014	0.014	25 (Fr)	Si	22

Muro [Platea]: 31 - Nodi: [25-24-15-16]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
5	31.42	31.42	-0.08	7.58	22	22	Si	48
6	31.42	31.42	-0.05	10.36	22	22	Si	35

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
5	31.42	31.42	-0.09	6.79	28	28	Si	53
6	31.42	31.42	-0.03	9.42	28	28	Si	38

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
6	0.0	-0.0	-0.0	-180.68	-31.76	13.69	9.42	0.015	0.015	28 (Qp)	Si	13
6	0.0	-0.0	-0.0	-177.77	-29.68	15.46	9.26	0.015	0.015	25 (Fr)	Si	20

Muro [Platea]: 32 - Nodi: [35-34-25-26]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.04	5.39	22	22	Si	67

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.06	5.15	28	28	Si	70

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	0.0	-0.0	0.0	-112.16	143.48	5.55	5.15	0.008	0.008	28 (Qp)	Si	25
4	0.0	-0.0	0.0	-109.79	146.56	6.30	5.06	0.008	0.008	25 (Fr)	Si	38

Muro [Platea]: 33 - Nodi: [7-8-17-16]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	2.55	20	22	Si	>100
1	31.42	31.42	-0.00	6.33	21	22	Si	57

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.00	6.19	28	28	Si	58
1	31.42	31.42	-0.00	6.54	28	28	Si	55

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	-0.0	-157.54	-5.22	-23.61	6.54	0.010	0.010	28 (Qp)	Si	21
1	0.0	-0.0	-0.0	-153.60	-5.40	-22.69	6.36	0.009	0.009	25 (Fr)	Si	32

Muro [Platea]: 34 - Nodi: [34-43-42-33]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.03	9.36	22	22	Si	38
4	31.42	31.42	-0.01	10.86	22	22	Si	33

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.02	8.48	28	28	Si	42
4	31.42	31.42	-0.01	9.46	28	28	Si	38

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	0.0	-0.0	7.15	-199.25	16.59	9.41	0.015	0.015	28 (Qp)	Si	14
8	0.0	0.0	-0.0	6.78	-196.89	16.13	9.32	0.015	0.015	23 (Fr)	Si	20

Muro [Platea]: 35 - Nodi: [35-44-43-34]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.01	5.29	22	22	Si	68
4	31.42	31.42	-0.00	5.38	22	22	Si	67

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.01	4.90	28	28	Si	73
4	31.42	31.42	-0.00	4.96	28	28	Si	73

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.0	0.0	-0.0	1.92	-126.23	-6.83	4.96	0.007	0.007	28 (Qp)	Si	28
4	-0.0	0.0	-0.0	1.36	-123.68	-6.98	4.86	0.007	0.007	25 (Fr)	Si	43

Muro [Platea]: 36 - Nodi: [6-7-16-15]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.01	10.39	22	22	Si	35
5	31.42	31.42	-0.00	10.71	22	22	Si	34

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.01	10.26	28	28	Si	35
2	31.42	31.42	-0.00	10.38	28	28	Si	35

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
2	0.0	0.0	-0.0	-200.24	-20.11	19.04	10.38	0.017	0.017	28 (Qp)	Si	12
2	0.0	0.0	-0.0	-195.00	-17.98	17.56	10.15	0.017	0.017	26 (Fr)	Si	18

Muro [Platea]: 37 - Nodi: [8-9-18-17]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

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P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.01	0.88	20	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.01	0.83	28	28	Si	>100
1	31.42	31.42	-0.00	1.07	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
3	0.0	-0.0	-0.0	10.19	-1.04	-6.75	0.40	0.001	0.001	28 (Qp)	Si	>100
3	0.0	-0.0	-0.0	9.83	-1.22	-6.33	0.38	0.001	0.001	26 (Fr)	Si	>100

Muro [Platea]: 38 - Nodi: [36-35-26-27]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.03	0.65	22	22	Si	>100
4	31.42	31.42	-0.03	1.57	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.05	0.61	28	28	Si	>100
4	31.42	31.42	-0.05	1.55	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
2	0.0	-0.0	-0.0	14.95	127.24	-16.60	0.61	0.001	0.001	28 (Qp)	Si	>100
2	0.0	-0.0	-0.0	14.71	130.48	-16.41	0.60	0.001	0.001	25 (Fr)	Si	>100

Muro [Platea]: 39 - Nodi: [36-45-44-35]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.01	0.85	22	22	Si	>100
4	31.42	31.42	-0.01	1.15	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.01	1.06	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
3	-0.0	0.0	0.0	-1.96	11.07	-2.52	0.48	0.001	0.001	28 (Qp)	Si	>100
3	-0.0	0.0	0.0	-2.38	10.73	-2.13	0.47	0.001	0.001	25 (Fr)	Si	>100

Muro [Platea]: 40 - Nodi: [27-26-17-18]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	31.42	31.42	-0.03	0.73	22	22	Si	>100
3	31.42	31.42	-0.03	1.70	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	31.42	31.42	-0.05	0.67	28	28	Si	>100
3	31.42	31.42	-0.05	1.55	28	28	Si	>100

Verifica aperture fessure:Wamm\_Freq[mm]=0.300 Wamm\_Qp[mm]=0.200

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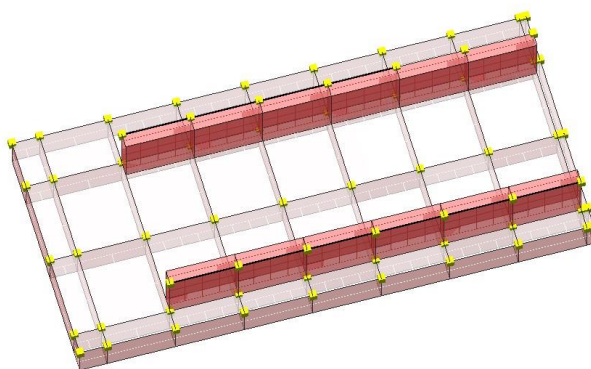
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P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{med}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	-0.0	-0.0	15.30	127.49	19.80	0.67	0.001	0.001	28 (Qp)	Si	>100
1	0.0	-0.0	-0.0	15.03	130.02	20.00	0.66	0.001	0.001	25 (Fr)	Si	>100

## 5. BASAMENTO PER BIOFILTRO BTK 3



### Taglianti di piano

Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

I taglianti sono dati per combinazioni di calcolo C-S-Pm con C=Combinazione(1,2,...) S=Sisma(I,II) Pm=posizione masse(1,2,...). Le azioni, complessive, sono riferite al sistema di riferimento globale.

$\Theta = F_z \cdot dr / (F_h \cdot H)$  con:

$F_z$  Forza verticale

$dr$  Spostamento medio del piano rispetto al piano inferiore

$F_h$  Tagliante

$H$  Altezza del piano

$dx$  spostamento medio di piano in direzione X

$dy$  spostamento medio di piano in direzione Y

$dr = ((dx_s - dx_i)^2 + (dy_s - dy_i)^2)^{0.5}$   $s$ =impalcato superiore  $i$ =impalcato inferiore

Nel caso di combinazioni sismiche l'aliquota dovuta al sisma di  $dx$  e  $dy$  è valutata secondo le indicazioni in 7.3.3, moltiplicando lo spostamento per  $\mu_d$

**Combinazione: 12-I-1 (SISMAxSLV)**

Piano	Fx	Fy	Fz	dx	dy	$\Theta$
	daN	daN	daN	mm	mm	
0	-5628.73	7.58	20340.58	0.00	0.00	--
1	5717.05	-6.46	-15478.24	0.01	-0.01	0.000043

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	-5628.73	7.58	-5628.73	7.58
1	0.00	0.00	0.00	0.00	5717.05	-6.46	5717.05	-6.46

Percentuali assorbite in direzione X

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Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

**Combinazione: 12-I-2 (SISMAxSLV)**

Piano	Fx daN	Fy daN	Fz daN	dx mm	dy mm	Θ
0	-5310.46	-4.79	20304.20	0.00	0.00	--
1	5406.79	31.03	-15392.30	0.01	-0.01	0.000046

Piano	FxPil/Isol. daN	FyPil/Isol. daN	FxPar daN	FyPar daN	FxShell daN	FyShell daN	FxTot daN	FyTot daN
0	0.00	0.00	0.00	0.00	-5310.46	-4.79	-5310.46	-4.79
1	0.00	0.00	0.00	0.00	5406.79	31.03	5406.79	31.03

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	0.00	0.00	100.00

**Combinazione: 12-I-3 (SISMAxSLV)**

Piano	Fx daN	Fy daN	Fz daN	dx mm	dy mm	Θ
0	-5796.10	-14.12	20330.34	0.00	0.00	--
1	5739.45	10.46	-15480.33	0.01	-0.01	0.000043

Piano	FxPil/Isol. daN	FyPil/Isol. daN	FxPar daN	FyPar daN	FxShell daN	FyShell daN	FxTot daN	FyTot daN
0	0.00	0.00	0.00	0.00	-5796.10	-14.12	-5796.10	-14.12
1	0.00	0.00	0.00	0.00	5739.45	10.46	5739.45	10.46

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 12-I-4 (SISMAxSLV)**

Piano	Fx daN	Fy daN	Fz daN	dx mm	dy mm	Θ
0	-6901.67	-6.00	20180.75	0.00	0.00	--
1	6569.15	-1.30	-15496.02	0.01	-0.01	0.000036

Piano	FxPil/Isol. daN	FyPil/Isol. daN	FxPar daN	FyPar daN	FxShell daN	FyShell daN	FxTot daN	FyTot daN
0	0.00	0.00	0.00	0.00	-6901.67	-6.00	-6901.67	-6.00
1	0.00	0.00	0.00	0.00	6569.15	-1.30	6569.15	-1.30

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

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Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

**Combinazione: 13-I-1 (SISMAYSLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	-13.92	-6747.45	20465.92	0.00	0.00	--
1	2.93	6703.22	-15632.23	-0.00	0.05	0.000156

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	-13.92	-6747.45	-13.92	-6747.45
1	0.00	0.00	0.00	0.00	2.93	6703.22	2.93	6703.22

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 13-I-2 (SISMAYSLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	40.18	-5194.00	20158.86	0.00	0.00	--
1	-8.60	5244.31	-15360.38	-0.00	0.06	0.000220

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	40.18	-5194.00	40.18	-5194.00
1	0.00	0.00	0.00	0.00	-8.60	5244.31	-8.60	5244.31

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 13-I-3 (SISMAYSLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	-7.17	-5163.06	20352.56	0.00	0.00	--
1	29.48	5174.29	-15532.03	-0.00	0.06	0.000226

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	-7.17	-5163.06	-7.17	-5163.06
1	0.00	0.00	0.00	0.00	29.48	5174.29	29.48	5174.29

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 13-I-4 (SISMAySLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	0.77	-5183.83	20144.56	0.00	0.00	--
1	-6.51	5215.25	-15370.38	-0.00	0.06	0.000222

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	0.77	-5183.83	0.77	-5183.83
1	0.00	0.00	0.00	0.00	-6.51	5215.25	-6.51	5215.25

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 14-I-1 (SISMAx1SLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	-5628.73	7.58	20340.58	0.00	0.00	--
1	5717.05	-6.46	-15478.24	0.01	-0.01	0.000058

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	-5628.73	7.58	-5628.73	7.58
1	0.00	0.00	0.00	0.00	5717.05	-6.46	5717.05	-6.46

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

**Combinazione: 14-I-2 (SISMAx1SLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	-5310.46	-4.79	20304.20	0.00	0.00	--
1	5406.79	31.03	-15392.30	0.01	-0.01	0.000062

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	-5310.46	-4.79	-5310.46	-4.79
1	0.00	0.00	0.00	0.00	5406.79	31.03	5406.79	31.03

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	0.00	0.00	100.00

**Combinazione: 14-I-3 (SISMAx1SLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	



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Piano	Fx	Fy	Fz	dx	dy	Θ
0	-5796.10	-14.12	20330.34	0.00	0.00	--
1	5739.45	10.46	-15480.33	0.01	-0.01	0.000058

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	-5796.10	-14.12	-5796.10	-14.12
1	0.00	0.00	0.00	0.00	5739.45	10.46	5739.45	10.46

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 14-I-4 (SISMAx1SLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	-6901.67	-6.00	20180.75	0.00	0.00	--
1	6569.15	-1.30	-15496.02	0.01	-0.01	0.000050

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	-6901.67	-6.00	-6901.67	-6.00
1	0.00	0.00	0.00	0.00	6569.15	-1.30	6569.15	-1.30

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--

**Combinazione: 15-I-1 (SISMAy1SLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	-13.92	-6747.45	20465.92	0.00	0.00	--
1	2.93	6703.22	-15632.23	0.00	0.05	0.000145

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	daN	daN	daN	daN	daN	daN	daN	daN
0	0.00	0.00	0.00	0.00	-13.92	-6747.45	-13.92	-6747.45
1	0.00	0.00	0.00	0.00	2.93	6703.22	2.93	6703.22

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 15-I-2 (SISMAy1SLV)**

Piano	Fx	Fy	Fz	dx	dy	Θ
	daN	daN	daN	mm	mm	
0	40.18	-5194.00	20158.86	0.00	0.00	--
1	-8.60	5244.31	-15360.38	0.00	0.06	0.000206

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Piano	FxPil/Isol. daN	FyPil/Isol. daN	FxPar daN	FyPar daN	FxShell daN	FyShell daN	FxTot daN	FyTot daN
0	0.00	0.00	0.00	0.00	40.18	-5194.00	40.18	-5194.00
1	0.00	0.00	0.00	0.00	-8.60	5244.31	-8.60	5244.31

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	0.00	0.00	100.00
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 15-I-3 (SISMAY1SLV)**

Piano	Fx daN	Fy daN	Fz daN	dx mm	dy mm	Θ
0	-7.17	-5163.06	20352.56	0.00	0.00	--
1	29.48	5174.29	-15532.03	0.00	0.06	0.000212

Piano	FxPil/Isol. daN	FyPil/Isol. daN	FxPar daN	FyPar daN	FxShell daN	FyShell daN	FxTot daN	FyTot daN
0	0.00	0.00	0.00	0.00	-7.17	-5163.06	-7.17	-5163.06
1	0.00	0.00	0.00	0.00	29.48	5174.29	29.48	5174.29

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Combinazione: 15-I-4 (SISMAY1SLV)**

Piano	Fx daN	Fy daN	Fz daN	dx mm	dy mm	Θ
0	0.77	-5183.83	20144.56	0.00	0.00	--
1	-6.51	5215.25	-15370.38	0.00	0.06	0.000208

Piano	FxPil/Isol. daN	FyPil/Isol. daN	FxPar daN	FyPar daN	FxShell daN	FyShell daN	FxTot daN	FyTot daN
0	0.00	0.00	0.00	0.00	0.77	-5183.83	0.77	-5183.83
1	0.00	0.00	0.00	0.00	-6.51	5215.25	-6.51	5215.25

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	0.00	0.00	100.00
1	0.00	0.00	100.00

**Risultati Analisi Dinamica - Statistiche matrice di rigidezza**

Scenario di calcolo: ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO

Minimo della diagonale	1.809725e+06
Massimo della diagonale	2.868508e+10
Rapporto Max/Min	1.585052e+04
Media della diagonale	9.458013e+08
Densità	1.526647e+00

Periodi di vibrazione e Masse modali

Scenario di calcolo: ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO

Posizione masse 1

Numero di Frequenze calcolate =45, filtrate=26

N	T s	Coeff. Partecipazione		Masse Modali kgm*g		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1 (1)	0.0583	-1.083	23.127	11.50	5245.25	0.07	29.86
2 (2)	0.0404	-9.569	-9.778	897.93	937.52	5.11	5.34
3 (3)	0.0310	-13.296	5.330	1733.71	278.55	9.87	1.59
4 (4)	0.0229	-4.604	0.383	207.91	1.44	1.18	0.01
5 (5)	0.0219	-0.813	6.712	6.47	441.85	0.04	2.52
6 (6)	0.0205	-5.360	0.597	281.72	3.49	1.60	0.02
7 (8)	0.0183	0.070	-2.595	0.05	66.02	0.00	0.38
8 (11)	0.0160	-0.235	-20.054	0.54	3943.84	0.00	22.45
9 (12)	0.0156	-0.319	-24.710	1.00	5987.80	0.01	34.08
10 (13)	0.0142	0.011	5.183	0.00	263.45	0.00	1.50
11 (20)	0.0089	0.214	-1.548	0.45	23.50	0.00	0.13
12 (21)	0.0084	-6.709	-0.033	441.36	0.01	2.51	0.00
13 (22)	0.0074	-3.860	0.035	146.09	0.01	0.83	0.00
14 (24)	0.0065	10.256	0.029	1031.43	0.01	5.87	0.00
15 (27)	0.0061	9.847	0.002	950.94	0.00	5.41	0.00
16 (28)	0.0060	21.026	0.027	4335.32	0.01	24.68	0.00
17 (29)	0.0058	-10.194	-0.022	1019.08	0.00	5.80	0.00
18 (32)	0.0055	8.477	0.002	704.74	0.00	4.01	0.00
19 (33)	0.0055	3.586	0.013	126.08	0.00	0.72	0.00
20 (35)	0.0054	-18.709	0.010	3432.68	0.00	19.54	0.00
21 (37)	0.0050	-6.322	-0.286	392.00	0.80	2.23	0.00
22 (38)	0.0050	-5.617	0.230	309.45	0.52	1.76	0.00
23 (39)	0.0050	1.683	-0.004	27.78	0.00	0.16	0.00
24 (41)	0.0045	5.594	0.204	306.91	0.41	1.75	0.00
25 (42)	0.0045	4.710	-0.256	217.57	0.64	1.24	0.00
26 (43)	0.0024	-0.331	2.629	1.08	67.78	0.01	0.39
Somma delle Masse Modali [kgm*g]				16583.80	17262.91		
Masse strutturali libere [kgm*g]				17567.50	17567.50		
Percentuale				94.40	98.27	94.40	98.27

Masse e coefficienti di partecipazione rotazionali:

Masse e coefficienti di partecipazione modali				
N	T (s)	Coeff. Partecipazione	Masse Modali	Percentuali
			kgm*g	
1 (1)	0.0583	1.269	15.80	0.02
2 (2)	0.0404	0.455	2.03	0.00
3 (3)	0.0310	3.901	149.23	0.18
4 (4)	0.0229	-45.991	20742.64	25.32
5 (5)	0.0219	-5.858	336.54	0.41
6 (6)	0.0205	25.457	6355.04	7.76
7 (8)	0.0183	-0.011	0.00	0.00
8 (11)	0.0160	-0.757	5.62	0.01
9 (12)	0.0156	-2.674	70.11	0.09
10 (13)	0.0142	0.370	1.34	0.00
11 (20)	0.0089	-2.730	73.07	0.09
12 (21)	0.0084	8.708	743.68	0.91
13 (22)	0.0074	-11.605	1320.66	1.61
14 (24)	0.0065	8.408	693.29	0.85
15 (27)	0.0061	2.296	51.69	0.06
16 (28)	0.0060	-0.449	1.98	0.00
17 (29)	0.0058	10.049	990.22	1.21
18 (32)	0.0055	-3.083	93.24	0.11
19 (33)	0.0055	-0.609	3.64	0.00
20 (35)	0.0054	1.118	12.26	0.01
21 (37)	0.0050	7.910	613.53	0.75
22 (38)	0.0050	4.561	203.98	0.25
23 (39)	0.0050	1.280	16.06	0.02
24 (41)	0.0045	6.431	405.60	0.50
25 (42)	0.0045	5.250	270.34	0.33
26 (43)	0.0024	-11.207	1231.69	1.50

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**Posizione masse 2**

Numero di Frequenze calcolate =45, filtrate=36

N	T s	Coeff. Partecipazione		Masse Modali kgm*g		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.0573	1.303	-23.929	16.64	5615.33	0.09	31.96
2(2)	0.0439	-9.141	-7.998	819.44	627.39	4.66	3.57
3(3)	0.0290	-14.062	3.710	1939.30	134.96	11.04	0.77
4(4)	0.0237	-3.972	-0.931	154.74	8.50	0.88	0.05
5(5)	0.0230	-0.496	-4.682	2.42	214.94	0.01	1.22
6(6)	0.0204	-4.451	1.089	194.30	11.62	1.11	0.07
7(7)	0.0193	0.703	1.347	4.85	17.78	0.03	0.10
8(8)	0.0187	-3.549	0.916	123.48	8.23	0.70	0.05
9(9)	0.0170	-0.668	-8.291	4.38	674.09	0.02	3.84
10(10)	0.0168	-1.804	2.881	31.92	81.39	0.18	0.46
11(11)	0.0159	-0.294	-30.709	0.85	9247.88	0.00	52.64
12(12)	0.0149	-0.409	-3.200	1.64	100.42	0.01	0.57
13(13)	0.0148	-0.148	5.425	0.22	288.58	0.00	1.64
14(18)	0.0112	1.985	-1.508	38.62	22.29	0.22	0.13
15(19)	0.0111	1.020	4.269	10.21	178.74	0.06	1.02
16(21)	0.0082	-5.424	-0.010	288.52	0.00	1.64	0.00
17(23)	0.0069	9.236	0.201	836.48	0.39	4.76	0.00
18(24)	0.0067	-2.105	0.867	43.47	7.36	0.25	0.04
19(25)	0.0063	7.117	-0.045	496.76	0.02	2.83	0.00
20(26)	0.0062	1.676	0.204	27.53	0.41	0.16	0.00
21(27)	0.0059	25.182	-0.013	6218.56	0.00	35.40	0.00
22(28)	0.0059	-12.298	-0.084	1483.21	0.07	8.44	0.00
23(29)	0.0059	-5.247	0.052	270.03	0.03	1.54	0.00
24(31)	0.0055	-9.476	0.018	880.65	0.00	5.01	0.00
25(32)	0.0055	3.719	-0.027	135.62	0.01	0.77	0.00
26(33)	0.0055	4.547	0.065	202.79	0.04	1.15	0.00
27(35)	0.0053	-6.592	0.051	426.19	0.03	2.43	0.00
28(36)	0.0053	-1.715	-0.306	28.83	0.92	0.16	0.01
29(37)	0.0052	9.030	0.052	799.72	0.03	4.55	0.00
30(38)	0.0052	-3.049	0.151	91.20	0.22	0.52	0.00
31(39)	0.0049	6.168	0.031	373.12	0.01	2.12	0.00
32(40)	0.0049	3.543	-0.059	123.10	0.03	0.70	0.00
33(41)	0.0041	-7.188	-0.132	506.65	0.17	2.88	0.00
34(42)	0.0041	-2.384	0.345	55.75	1.17	0.32	0.01
35(43)	0.0024	-0.902	-1.914	7.99	35.94	0.05	0.20
36(44)	0.0022	0.839	-1.537	6.90	23.17	0.04	0.13
Somma delle Masse Modali [kgm*g]				16646.08	17302.18		
Masse strutturali libere [kgm*g]				17567.50	17567.50		
Percentuale				94.75	98.49	94.75	98.49

**Masse e coefficienti di partecipazione rotazionali:**

N	T(s)	Coeff. Partecipazione	Masse Modali kgm*g		Percentuali
1(1)	0.0573	-8.604	725.96		0.88
2(2)	0.0439	-1.566	24.05		0.03
3(3)	0.0290	5.859	336.59		0.41
4(4)	0.0237	-5.358	281.56		0.34
5(5)	0.0230	-45.985	20737.40		25.02
6(6)	0.0204	1.262	15.61		0.02
7(7)	0.0193	22.833	5112.70		6.17
8(8)	0.0187	0.016	0.00		0.00
9(9)	0.0170	-13.338	1744.62		2.10
10(10)	0.0168	3.642	130.07		0.16
11(11)	0.0159	2.655	69.13		0.08
12(12)	0.0149	-4.805	226.44		0.27
13(13)	0.0148	6.741	445.59		0.54
14(18)	0.0112	6.252	383.37		0.46
15(19)	0.0111	-22.518	4972.63		6.00
16(21)	0.0082	0.828	6.72		0.01
17(23)	0.0069	0.664	4.33		0.01
18(24)	0.0067	4.326	183.55		0.22
19(25)	0.0063	1.810	32.13		0.04
20(26)	0.0062	-7.154	501.84		0.61
21(27)	0.0059	-1.097	11.79		0.01
22(28)	0.0059	1.937	36.80		0.04
23(29)	0.0059	2.390	56.03		0.07
24(31)	0.0055	-1.177	13.58		0.02

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N	T(s)	Coeff. Partecipazione	Masse Modali	Percentuali
25 (32)	0.0055	-5.204	265.63	0.32
26 (33)	0.0055	-1.918	36.09	0.04
27 (35)	0.0053	1.635	26.21	0.03
28 (36)	0.0053	-6.630	431.02	0.52
29 (37)	0.0052	-1.476	21.37	0.03
30 (38)	0.0052	-0.961	9.06	0.01
31 (39)	0.0049	-0.543	2.89	0.00
32 (40)	0.0049	-0.815	6.51	0.01
33 (41)	0.0041	5.915	343.06	0.41
34 (42)	0.0041	-9.856	952.67	1.15
35 (43)	0.0024	-61.131	36647.06	44.22
36 (44)	0.0022	-52.007	26524.81	32.00

**Posizione masse 3**

Numero di Frequenze calcolate =45, filtrate=25

N	T	Coeff. Partecipazione		Masse Modali		Percentuali	
	s			kgm*g			
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1 (1)	0.0560	-0.379	25.107	1.41	6181.95	0.01	35.19
2 (2)	0.0416	-8.769	-3.532	754.01	122.37	4.29	0.70
3 (3)	0.0312	-14.009	2.003	1924.50	39.33	10.95	0.22
4 (4)	0.0229	3.458	0.044	117.30	0.02	0.67	0.00
5 (5)	0.0219	0.569	4.752	3.17	221.49	0.02	1.26
6 (6)	0.0206	6.034	0.052	357.10	0.03	2.03	0.00
7 (8)	0.0185	0.135	2.360	0.18	54.64	0.00	0.31
8 (11)	0.0160	0.065	24.652	0.04	5959.94	0.00	33.93
9 (12)	0.0156	-0.030	-21.078	0.01	4357.12	0.00	24.80
10 (13)	0.0143	-0.064	-5.078	0.04	252.91	0.00	1.44
11 (20)	0.0090	-0.035	1.604	0.01	25.23	0.00	0.14
12 (21)	0.0083	6.563	-0.017	422.46	0.00	2.40	0.00
13 (22)	0.0076	-3.977	-0.030	155.12	0.01	0.88	0.00
14 (24)	0.0065	-10.673	0.058	1117.03	0.03	6.36	0.00
15 (27)	0.0061	9.393	0.002	865.29	0.00	4.93	0.00
16 (28)	0.0060	-20.387	0.009	4076.09	0.00	23.20	0.00
17 (29)	0.0059	10.916	-0.005	1168.49	0.00	6.65	0.00
18 (32)	0.0056	-8.832	-0.007	764.96	0.00	4.35	0.00
19 (33)	0.0055	-3.851	0.002	145.42	0.00	0.83	0.00
20 (35)	0.0054	-18.811	-0.025	3470.23	0.01	19.75	0.00
21 (37)	0.0050	-8.025	-0.053	631.60	0.03	3.60	0.00
22 (39)	0.0050	3.110	-0.092	94.86	0.08	0.54	0.00
23 (41)	0.0045	5.258	0.269	271.15	0.71	1.54	0.00
24 (42)	0.0045	-5.154	0.193	260.54	0.37	1.48	0.00
25 (43)	0.0022	0.283	-2.842	0.78	79.24	0.00	0.45
Somma delle Masse Modali [kgm*g]				16601.80	17295.50		
Masse strutturali libere [kgm*g]				17567.50	17567.50		
Percentuale				94.50	98.45	94.50	98.45

**Masse e coefficienti di partecipazione rotazionali:**

N	T(s)	Coeff. Partecipazione	Masse Modali	Percentuali
			kgm*g	
1 (1)	0.0560	1.433	20.13	0.02
2 (2)	0.0416	1.943	37.02	0.04
3 (3)	0.0312	3.166	98.28	0.12
4 (4)	0.0229	-46.806	21484.00	25.86
5 (5)	0.0219	-4.575	205.30	0.25
6 (6)	0.0206	26.962	7128.70	8.58
7 (8)	0.0185	-1.312	16.87	0.02
8 (11)	0.0160	1.610	25.42	0.03
9 (12)	0.0156	-1.331	17.37	0.02
10 (13)	0.0143	-1.494	21.89	0.03
11 (20)	0.0090	2.743	73.78	0.09
12 (21)	0.0083	7.022	483.53	0.58
13 (22)	0.0076	12.984	1653.18	1.99
14 (24)	0.0065	9.091	810.56	0.98
15 (27)	0.0061	-3.626	128.94	0.16
16 (28)	0.0060	3.501	120.23	0.14
17 (29)	0.0059	8.761	752.65	0.91
18 (32)	0.0056	-1.654	26.82	0.03
19 (33)	0.0055	0.030	0.01	0.00

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N	T(s)	Coeff. Partecipazione	Masse Modali	Percentuali
20 (35)	0.0054	2.743	73.81	0.09
21 (37)	0.0050	-4.914	236.78	0.28
22 (39)	0.0050	4.917	237.12	0.29
23 (41)	0.0045	-9.190	828.18	1.00
24 (42)	0.0045	6.131	368.60	0.44
25 (43)	0.0022	-1.168	13.38	0.02

**Posizione masse 4**

Numero di Frequenze calcolate =45, filtrate=35

N	T	Coeff. Partecipazione		Masse Modali		Percentuali	
	s			kgm*g			
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1 (1)	0.0569	0.363	-24.390	1.29	5833.61	0.01	33.21
2 (2)	0.0385	7.187	6.912	506.54	468.51	2.88	2.67
3 (3)	0.0327	-15.031	2.759	2215.61	74.65	12.61	0.42
4 (4)	0.0234	-5.287	1.873	274.08	34.41	1.56	0.20
5 (5)	0.0230	-0.396	-5.419	1.54	288.02	0.01	1.64
6 (6)	0.0205	-3.256	-0.765	103.99	5.74	0.59	0.03
7 (7)	0.0193	0.492	-1.939	2.37	36.86	0.01	0.21
8 (8)	0.0187	3.042	0.338	90.76	1.12	0.52	0.01
9 (9)	0.0170	-0.528	7.534	2.73	556.71	0.02	3.17
10 (10)	0.0169	-1.967	-2.527	37.92	62.64	0.22	0.36
11 (11)	0.0158	-0.167	-30.839	0.27	9326.35	0.00	53.09
12 (12)	0.0149	0.290	-2.571	0.83	64.83	0.00	0.37
13 (13)	0.0148	0.168	5.920	0.28	343.64	0.00	1.96
14 (18)	0.0113	-3.562	-0.468	124.43	2.15	0.71	0.01
15 (19)	0.0109	0.721	-3.545	5.09	123.24	0.03	0.70
16 (21)	0.0082	-5.061	0.024	251.15	0.01	1.43	0.00
17 (23)	0.0069	9.444	-0.161	874.72	0.25	4.98	0.00
18 (24)	0.0067	-1.943	-0.860	37.01	7.25	0.21	0.04
19 (25)	0.0063	-7.127	-0.049	498.13	0.02	2.84	0.00
20 (26)	0.0062	-1.382	0.197	18.74	0.38	0.11	0.00
21 (27)	0.0059	-20.510	-0.066	4125.18	0.04	23.48	0.00
22 (28)	0.0059	19.413	-0.043	3695.75	0.02	21.04	0.00
23 (29)	0.0059	-3.594	-0.001	126.65	0.00	0.72	0.00
24 (31)	0.0055	9.252	0.025	839.38	0.01	4.78	0.00
25 (32)	0.0055	3.477	0.004	118.59	0.00	0.68	0.00
26 (33)	0.0055	5.042	-0.065	249.34	0.04	1.42	0.00
27 (35)	0.0054	-6.078	-0.198	362.24	0.38	2.06	0.00
28 (36)	0.0053	-3.077	0.326	92.83	1.04	0.53	0.01
29 (37)	0.0052	-9.385	0.017	863.70	0.00	4.92	0.00
30 (38)	0.0052	1.784	0.136	31.21	0.18	0.18	0.00
31 (39)	0.0049	-6.563	0.009	422.46	0.00	2.40	0.00
32 (40)	0.0049	2.714	0.052	72.23	0.03	0.41	0.00
33 (41)	0.0041	7.603	0.026	566.91	0.01	3.23	0.00
34 (43)	0.0024	1.052	-1.884	10.85	34.80	0.06	0.20
35 (44)	0.0022	-0.739	-1.602	5.36	25.17	0.03	0.14
Somma delle Masse Modali [kgm*g]				16630.17	17292.11		
Masse strutturali libere [kgm*g]				17567.50	17567.50		
Percentuale				94.66	98.43	94.66	98.43

**Masse e coefficienti di partecipazione rotazionali:**

N	T(s)	Coeff. Partecipazione	Masse Modali	Percentuali
			kgm*g	
1 (1)	0.0569	5.990	351.86	0.43
2 (2)	0.0385	-3.324	108.35	0.13
3 (3)	0.0327	2.291	51.49	0.06
4 (4)	0.0234	-9.173	825.13	1.00
5 (5)	0.0230	46.314	21035.28	25.62
6 (6)	0.0205	0.590	3.41	0.00
7 (7)	0.0193	20.704	4203.88	5.12
8 (8)	0.0187	-1.845	33.37	0.04
9 (9)	0.0170	-11.961	1402.88	1.71
10 (10)	0.0169	3.374	111.65	0.14
11 (11)	0.0158	-6.562	422.31	0.51
12 (12)	0.0149	1.774	30.86	0.04
13 (13)	0.0148	-5.658	313.96	0.38
14 (18)	0.0113	-2.423	57.58	0.07
15 (19)	0.0109	-25.263	6258.90	7.62

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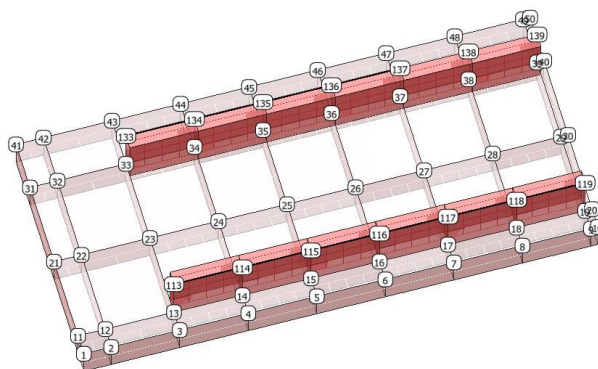
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N	T(s)	Coeff. Partecipazione	Masse Modali	Percentuali
16 (21)	0.0082	1.066	11.15	0.01
17 (23)	0.0069	-0.033	0.01	0.00
18 (24)	0.0067	3.981	155.40	0.19
19 (25)	0.0063	-1.754	30.18	0.04
20 (26)	0.0062	7.353	530.19	0.65
21 (27)	0.0059	0.950	8.86	0.01
22 (28)	0.0059	-2.919	83.58	0.10
23 (29)	0.0059	1.792	31.51	0.04
24 (31)	0.0055	1.889	34.98	0.04
25 (32)	0.0055	-6.035	357.19	0.43
26 (33)	0.0055	-1.293	16.40	0.02
27 (35)	0.0054	5.473	293.71	0.36
28 (36)	0.0053	-6.723	443.28	0.54
29 (37)	0.0052	1.182	13.71	0.02
30 (38)	0.0052	0.998	9.77	0.01
31 (39)	0.0049	0.249	0.61	0.00
32 (40)	0.0049	-0.888	7.74	0.01
33 (41)	0.0041	-0.417	1.71	0.00
34 (43)	0.0024	55.788	30521.71	37.17
35 (44)	0.0022	49.165	23704.59	28.87

**Nodi - Geometria e vincoli**

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
		Coordinate [m]		Vincoli						
1	-7.500	0.000	0.000	1	1	0	0	0	1	0
2	-7.100	0.000	0.000	1	1	0	0	0	1	0
3	-6.100	0.000	0.000	1	1	0	0	0	1	0
4	-5.100	0.000	0.000	1	1	0	0	0	1	0
5	-4.100	0.000	0.000	1	1	0	0	0	1	0
6	-3.100	0.000	0.000	1	1	0	0	0	1	0
7	-2.100	0.000	0.000	1	1	0	0	0	1	0
8	-1.100	0.000	0.000	1	1	0	0	0	1	0
9	-0.100	0.000	0.000	1	1	0	0	0	1	0
10	0.000	0.000	0.000	1	1	0	0	0	1	0
11	-7.500	0.300	0.000	1	1	0	0	0	1	0
12	-7.100	0.300	0.000	1	1	0	0	0	1	0
13	-6.100	0.300	0.000	1	1	0	0	0	1	0
14	-5.100	0.300	0.000	1	1	0	0	0	1	0
15	-4.100	0.300	0.000	1	1	0	0	0	1	0
16	-3.100	0.300	0.000	1	1	0	0	0	1	0
17	-2.100	0.300	0.000	1	1	0	0	0	1	0
18	-1.100	0.300	0.000	1	1	0	0	0	1	0
19	-0.100	0.300	0.000	1	1	0	0	0	1	0
20	0.000	0.300	0.000	1	1	0	0	0	1	0
21	-7.500	1.540	0.000	1	1	0	0	0	1	0
22	-7.100	1.540	0.000	1	1	0	0	0	1	0
23	-6.100	1.540	0.000	1	1	0	0	0	1	0
24	-5.100	1.540	0.000	1	1	0	0	0	1	0
25	-4.100	1.540	0.000	1	1	0	0	0	1	0
26	-3.100	1.540	0.000	1	1	0	0	0	1	0
27	-2.100	1.540	0.000	1	1	0	0	0	1	0
28	-1.100	1.540	0.000	1	1	0	0	0	1	0
29	-0.100	1.540	0.000	1	1	0	0	0	1	0
30	0.000	1.540	0.000	1	1	0	0	0	1	0
31	-7.500	2.780	0.000	1	1	0	0	0	1	0
32	-7.100	2.780	0.000	1	1	0	0	0	1	0
33	-6.100	2.780	0.000	1	1	0	0	0	1	0
34	-5.100	2.780	0.000	1	1	0	0	0	1	0
35	-4.100	2.780	0.000	1	1	0	0	0	1	0
36	-3.100	2.780	0.000	1	1	0	0	0	1	0
37	-2.100	2.780	0.000	1	1	0	0	0	1	0
38	-1.100	2.780	0.000	1	1	0	0	0	1	0
39	-0.100	2.780	0.000	1	1	0	0	0	1	0
40	0.000	2.780	0.000	1	1	0	0	0	1	0
41	-7.500	3.500	0.000	1	1	0	0	0	1	0
42	-7.100	3.500	0.000	1	1	0	0	0	1	0
43	-6.100	3.500	0.000	1	1	0	0	0	1	0
44	-5.100	3.500	0.000	1	1	0	0	0	1	0
45	-4.100	3.500	0.000	1	1	0	0	0	1	0
46	-3.100	3.500	0.000	1	1	0	0	0	1	0

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
47	-2.100	3.500	0.000	1	1	0	0	0	1	0
48	-1.100	3.500	0.000	1	1	0	0	0	1	0
49	-0.100	3.500	0.000	1	1	0	0	0	1	0
50	0.000	3.500	0.000	1	1	0	0	0	1	0
113	-6.100	0.300	0.800	0	0	0	0	0	0	1
114	-5.100	0.300	0.800	0	0	0	0	0	0	1
115	-4.100	0.300	0.800	0	0	0	0	0	0	1
116	-3.100	0.300	0.800	0	0	0	0	0	0	1
117	-2.100	0.300	0.800	0	0	0	0	0	0	1
118	-1.100	0.300	0.800	0	0	0	0	0	0	1
119	-0.100	0.300	0.800	0	0	0	0	0	0	1
133	-6.100	2.780	0.800	0	0	0	0	0	0	1
134	-5.100	2.780	0.800	0	0	0	0	0	0	1
135	-4.100	2.780	0.800	0	0	0	0	0	0	1
136	-3.100	2.780	0.800	0	0	0	0	0	0	1
137	-2.100	2.780	0.800	0	0	0	0	0	0	1
138	-1.100	2.780	0.800	0	0	0	0	0	0	1
139	-0.100	2.780	0.800	0	0	0	0	0	0	1



**Nodi - Carichi**

N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
		daN			daN*m			cm			°			°C
113	biofiltro	0.00	0.00	645.00	0.00	0.00	0.00							
113	vento y	0.00	-85.00	0.00	140.00	0.00	0.00							
113	vento x	60.00	0.00	0.00	0.00	100.00	0.00							
113	azione sismica SLV y	0.00	-255.00	0.00	470.00	0.00	0.00							
113	azione sismica SLV x	255.00	0.00	0.00	0.00	420.00	0.00							
113	azione sismica SLD y	0.00	-100.00	0.00	185.00	0.00	0.00							
113	azione sismica SLD x	100.00	0.00	0.00	0.00	185.00	0.00							
114	biofiltro	0.00	0.00	1290.00	0.00	0.00	0.00							



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N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
114	vento y	0.00	-165.00	0.00	275.00	0.00	0.00							
114	vento x	60.00	0.00	0.00	0.00	100.00	0.00							
114	azione sismica SLV y	0.00	-510.00	0.00	840.00	0.00	0.00							
114	azione sismica SLV x	510.00	0.00	0.00	0.00	-840.00	0.00							
114	azione sismica SLD y	0.00	-200.00	0.00	370.00	0.00	0.00							
114	azione sismica SLD x	200.00	0.00	0.00	0.00	-370.00	0.00							
115	biofiltro	0.00	0.00	1290.00	0.00	0.00	0.00							
115	vento y	0.00	-165.00	0.00	275.00	0.00	0.00							
115	vento x	60.00	0.00	0.00	0.00	100.00	0.00							
115	azione sismica SLV y	0.00	-510.00	0.00	840.00	0.00	0.00							
115	azione sismica SLV x	510.00	0.00	0.00	0.00	-840.00	0.00							
115	azione sismica SLD y	0.00	-200.00	0.00	370.00	0.00	0.00							
115	azione sismica SLD x	200.00	0.00	0.00	0.00	-370.00	0.00							
116	biofiltro	0.00	0.00	1290.00	0.00	0.00	0.00							
116	vento y	0.00	-165.00	0.00	275.00	0.00	0.00							
116	vento x	60.00	0.00	0.00	0.00	100.00	0.00							
116	azione sismica SLV y	0.00	-510.00	0.00	840.00	0.00	0.00							
116	azione sismica SLV x	510.00	0.00	0.00	0.00	-840.00	0.00							
116	azione sismica SLD y	0.00	-200.00	0.00	370.00	0.00	0.00							
116	azione sismica SLD x	200.00	0.00	0.00	0.00	-370.00	0.00							
117	biofiltro	0.00	0.00	1290.00	0.00	0.00	0.00							
117	vento y	0.00	-165.00	0.00	275.00	0.00	0.00							
117	vento x	60.00	0.00	0.00	0.00	100.00	0.00							
117	azione sismica SLV y	0.00	-510.00	0.00	840.00	0.00	0.00							
117	azione sismica SLV x	510.00	0.00	0.00	0.00	-840.00	0.00							
117	azione sismica SLD y	0.00	-200.00	0.00	370.00	0.00	0.00							
117	azione sismica SLD x	200.00	0.00	0.00	0.00	-370.00	0.00							
118	biofiltro	0.00	0.00	1290.00	0.00	0.00	0.00							
118	vento y	0.00	-165.00	0.00	275.00	0.00	0.00							
118	vento x	60.00	0.00	0.00	0.00	100.00	0.00							
118	azione sismica SLV y	0.00	-510.00	0.00	840.00	0.00	0.00							
118	azione sismica SLV x	510.00	0.00	0.00	0.00	-840.00	0.00							
118	azione sismica SLD y	0.00	-200.00	0.00	370.00	0.00	0.00							
118	azione sismica SLD x	200.00	0.00	0.00	0.00	-370.00	0.00							
119	biofiltro	0.00	0.00	645.00	0.00	0.00	0.00							
119	vento y	0.00	-85.00	0.00	140.00	0.00	0.00							
119	vento x	60.00	0.00	0.00	0.00	100.00	0.00							
119	azione sismica SLV y	0.00	-255.00	0.00	470.00	0.00	0.00							
119	azione sismica SLV x	255.00	0.00	0.00	0.00	-420.00	0.00							
119	azione sismica SLD y	0.00	-100.00	0.00	185.00	0.00	0.00							
119	azione sismica SLD x	100.00	0.00	0.00	0.00	-185.00	0.00							
133	biofiltro	0.00	0.00	645.00	0.00	0.00	0.00							
133	vento y	0.00	-85.00	0.00	140.00	0.00	0.00							

N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
133	vento x	60.00	0.00	0.00	0.00	100.00	0.00							
133	azione sismica SLV y	0.00	255.00	0.00	470.00	0.00	0.00							
133	azione sismica SLV x	255.00	0.00	0.00	0.00	420.00	0.00							
133	azione sismica SLD y	0.00	100.00	0.00	185.00	0.00	0.00							
133	azione sismica SLD x	100.00	0.00	0.00	0.00	185.00	0.00							
134	biofiltro	0.00	0.00	1290.0 0	0.00	0.00	0.00							
134	vento y	0.00	165.00	0.00	275.00	0.00	0.00							
134	vento x	60.00	0.00	0.00	0.00	100.00	0.00							
134	azione sismica SLV y	0.00	510.00	0.00	840.00	0.00	0.00							
134	azione sismica SLV x	510.00	0.00	0.00	0.00	840.00	0.00							
134	azione sismica SLD y	0.00	200.00	0.00	370.00	0.00	0.00							
134	azione sismica SLD x	200.00	0.00	0.00	0.00	370.00	0.00							
135	biofiltro	0.00	0.00	1290.0 0	0.00	0.00	0.00							
135	vento y	0.00	165.00	0.00	275.00	0.00	0.00							
135	vento x	60.00	0.00	0.00	0.00	100.00	0.00							
135	azione sismica SLV y	0.00	510.00	0.00	840.00	0.00	0.00							
135	azione sismica SLV x	510.00	0.00	0.00	0.00	840.00	0.00							
135	azione sismica SLD y	0.00	200.00	0.00	370.00	0.00	0.00							
135	azione sismica SLD x	200.00	0.00	0.00	0.00	370.00	0.00							
136	biofiltro	0.00	0.00	1290.0 0	0.00	0.00	0.00							
136	vento y	0.00	165.00	0.00	275.00	0.00	0.00							
136	vento x	60.00	0.00	0.00	0.00	100.00	0.00							
136	azione sismica SLV y	0.00	510.00	0.00	840.00	0.00	0.00							
136	azione sismica SLV x	510.00	0.00	0.00	0.00	840.00	0.00							
136	azione sismica SLD y	0.00	200.00	0.00	370.00	0.00	0.00							
136	azione sismica SLD x	200.00	0.00	0.00	0.00	370.00	0.00							
137	biofiltro	0.00	0.00	1290.0 0	0.00	0.00	0.00							
137	vento y	0.00	165.00	0.00	275.00	0.00	0.00							
137	vento x	60.00	0.00	0.00	0.00	100.00	0.00							
137	azione sismica SLV y	0.00	510.00	0.00	840.00	0.00	0.00							
137	azione sismica SLV x	510.00	0.00	0.00	0.00	840.00	0.00							
137	azione sismica SLD y	0.00	200.00	0.00	370.00	0.00	0.00							
137	azione sismica SLD x	200.00	0.00	0.00	0.00	370.00	0.00							
138	biofiltro	0.00	0.00	1290.0 0	0.00	0.00	0.00							
138	vento y	0.00	165.00	0.00	275.00	0.00	0.00							
138	vento x	60.00	0.00	0.00	0.00	100.00	0.00							
138	azione sismica SLV y	0.00	510.00	0.00	840.00	0.00	0.00							
138	azione sismica SLV x	510.00	0.00	0.00	0.00	840.00	0.00							
138	azione sismica SLD y	0.00	200.00	0.00	370.00	0.00	0.00							
138	azione sismica SLD x	200.00	0.00	0.00	0.00	370.00	0.00							
139	biofiltro	0.00	0.00	645.00	0.00	0.00	0.00							
139	vento y	0.00	-85.00	0.00	140.00	0.00	0.00							

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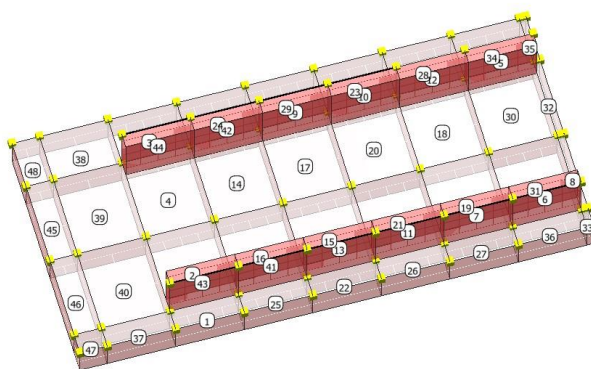
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N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
139	vento x	60.00	0.00	0.00	0.00	100.00	0.00							
139	azione sismica SLV y	0.00	255.00	0.00	470.00	0.00	0.00							
139	azione sismica SLV x	255.00	0.00	0.00	0.00	420.00	0.00							
139	azione sismica SLD y	0.00	100.00	0.00	185.00	0.00	0.00							
139	azione sismica SLD x	100.00	0.00	0.00	0.00	185.00	0.00							

**Pareti - geometria e vincoli**

Parete	Nodi	Tipo	Materiale	Criterio	N.P.	N.P.X	N.P.Y	Spess.
								m
1	3-4-14-13	Platea	C35/45	CLS Platee ND	8			0.50
2	14-24-23-13	Platea	C35/45	CLS Platee ND	8			0.50
3	34-44-43-33	Platea	C35/45	CLS Platee ND	8			0.50
4	24-34-33-23	Platea	C35/45	CLS Platee ND	8			0.50
5	39-38-138-139	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
6	19-119-118-18	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
7	18-118-117-17	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
8	30-29-19-20	Platea	C35/45	CLS Platee ND	4			0.50
9	36-35-135-136	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
10	37-36-136-137	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
11	17-117-116-16	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
12	38-37-137-138	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
13	16-116-115-15	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
14	35-34-24-25	Platea	C35/45	CLS Platee ND	8			0.50
15	26-25-15-16	Platea	C35/45	CLS Platee ND	8			0.50
16	25-24-14-15	Platea	C35/45	CLS Platee ND	8			0.50
17	36-35-25-26	Platea	C35/45	CLS Platee ND	8			0.50
18	38-37-27-28	Platea	C35/45	CLS Platee ND	8			0.50
19	28-27-17-18	Platea	C35/45	CLS Platee ND	8			0.50
20	37-36-26-27	Platea	C35/45	CLS Platee ND	8			0.50
21	27-26-16-17	Platea	C35/45	CLS Platee ND	8			0.50
22	5-6-16-15	Platea	C35/45	CLS Platee ND	8			0.50
23	47-46-36-37	Platea	C35/45	CLS Platee ND	8			0.50
24	45-44-34-35	Platea	C35/45	CLS Platee ND	8			0.50
25	4-5-15-14	Platea	C35/45	CLS Platee ND	8			0.50
26	6-7-17-16	Platea	C35/45	CLS Platee ND	8			0.50
27	7-8-18-17	Platea	C35/45	CLS Platee ND	8			0.50
28	38-48-47-37	Platea	C35/45	CLS Platee ND	8			0.50
29	46-45-35-36	Platea	C35/45	CLS Platee ND	8			0.50
30	39-38-28-29	Platea	C35/45	CLS Platee ND	8			0.50
31	29-28-18-19	Platea	C35/45	CLS Platee ND	8			0.50
32	40-39-29-30	Platea	C35/45	CLS Platee ND	4			0.50
33	9-10-20-19	Platea	C35/45	CLS Platee ND	4			0.50
34	39-49-48-38	Platea	C35/45	CLS Platee ND	8			0.50
35	40-50-49-39	Platea	C35/45	CLS Platee ND	4			0.50
36	8-9-19-18	Platea	C35/45	CLS Platee ND	8			0.50
37	2-3-13-12	Platea	C35/45	CLS Platee ND	4			0.50
38	33-43-42-32	Platea	C35/45	CLS Platee ND	4			0.50
39	23-33-32-22	Platea	C35/45	CLS Platee ND	4			0.50
40	13-23-22-12	Platea	C35/45	CLS Platee ND	4			0.50
41	15-115-114-14	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
42	35-34-134-135	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
43	14-114-113-13	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
44	34-33-133-134	Discreto	C35/45	CLS Muri ND	16	4	4	0.20
45	22-32-31-21	Platea	C35/45	CLS Platee ND	4			0.50
46	12-22-21-11	Platea	C35/45	CLS Platee ND	4			0.50
47	1-2-12-11	Platea	C35/45	CLS Platee ND	4			0.50
48	32-42-41-31	Platea	C35/45	CLS Platee ND	4			0.50



#### Muri - Carichi

Shell	Indice dello shell
Cond.	Condizione di carico
Tipo	Tipologia di spinta
$\gamma$	Peso specifico: terreno o acqua
Ht	Quota del piano di campagna
$\phi$	Angolo di attrito interno
c	Coesione
$\delta$	Angolo di attrito terreno paramento shell
$\beta$	Angolo di inclinazione del piano di campagna
k0	Coefficiente di spinta a riposo (quando richiesto)
$\beta_m$	Coefficiente di riduzione dell'accelerazione massima attesa al sito (quando richiesto)
Ag	Accelerazione del sito a meno di 'g': quando richiesto, rappresenta il valore della accelerazione dello spettro per T=0, quindi comprensiva dei coefficienti di amplificazione topografica ( $S_T$ ) e stratigrafica ( $S_S$ )
Q	Valore del carico uniforme
Vert.1	Valore del carico nel primo vertice <sup>(1)</sup>
Vert.2	Valore del carico nel secondo vertice <sup>(1)</sup>
Vert.3	Valore del carico nel terzo vertice <sup>(1)</sup>
Vert.4	Valore del carico nel quarto vertice <sup>(1)</sup>
Hw	Altezza del pelo libero dell'acqua

<sup>(1)</sup>: Per shell con numero di vertici maggiori 4, per carichi trapezoidali, il valore del carico nei vertici e' stampato a gruppi di 4 secondo l'ordine con cui i vertici sono stati definiti

Shell	Cond.	Tipo	Ht	$\gamma$	$\phi$	c	$\delta$	$\beta$	k0	$\beta_m$	Ag
			m	daN/ m <sup>3</sup>	°	daN/ cmq	°	°			
8	serbatoio	Sisma terreno - Riposo - Dir.Neg.	0.00	1900 .00	--	--	--	--	0.50	1.00	0.00
32	serbatoio	Sisma terreno - Riposo - Dir.Neg.	0.00	1900 .00	--	--	--	--	0.50	1.00	0.00

Shell	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	$\gamma$
			daN/m <sup>2</sup>	daN/m <sup>2</sup>	daN/m <sup>2</sup>	daN/m <sup>2</sup>	daN/m <sup>2</sup>	m	daN/m <sup>3</sup>
1	Peso Proprio	Peso Proprio daN	375.00						
1	NEVE	Uniforme GLOBZ	60.00						

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She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
1	accidentali	Uniforme_GLOBZ	600.00						
1	4100	Uniforme_GLOBZ	4100.00						
2	Peso Proprio	Peso Proprio daN	1550.00						
2	NEVE	Uniforme_GLOBZ	60.00						
2	serbatoio	Uniforme_GLOBZ	1500.00						
2	4100	Uniforme_GLOBZ	4100.00						
3	Peso Proprio	Peso Proprio daN	900.00						
3	NEVE	Uniforme_GLOBZ	60.00						
3	accidentali	Uniforme_GLOBZ	600.00						
3	4100	Uniforme_GLOBZ	4100.00						
4	Peso Proprio	Peso Proprio daN	1550.00						
4	NEVE	Uniforme_GLOBZ	60.00						
4	serbatoio	Uniforme_GLOBZ	1500.00						
4	4100	Uniforme_GLOBZ	4100.00						
5	Peso Proprio	Peso Proprio daN	400.00						
6	Peso Proprio	Peso Proprio daN	400.00						
6	vento y	Uniforme_GLOBY	100.00						
7	Peso Proprio	Peso Proprio daN	400.00						
7	vento y	Uniforme_GLOBY	100.00						
8	Peso Proprio	Peso Proprio daN	155.00						
8	NEVE	Uniforme_GLOBZ	60.00						
8	4100	Uniforme_GLOBZ	4100.00						
9	Peso Proprio	Peso Proprio daN	400.00						
10	Peso Proprio	Peso Proprio daN	400.00						
11	Peso Proprio	Peso Proprio daN	400.00						
11	vento y	Uniforme_GLOBY	100.00						
12	Peso Proprio	Peso Proprio daN	400.00						
13	Peso Proprio	Peso Proprio daN	400.00						
13	vento y	Uniforme_GLOBY	100.00						
14	Peso Proprio	Peso Proprio daN	1550.00						
14	NEVE	Uniforme_GLOBZ	60.00						
14	4100	Uniforme_GLOBZ	4100.00						
15	Peso Proprio	Peso Proprio daN	1550.00						
15	NEVE	Uniforme_GLOBZ	60.00						
15	4100	Uniforme_GLOBZ	4100.00						
16	Peso Proprio	Peso Proprio daN	1550.00						
16	NEVE	Uniforme_GLOBZ	60.00						
16	4100	Uniforme_GLOBZ	4100.00						
17	Peso Proprio	Peso Proprio daN	1550.00						
17	NEVE	Uniforme_GLOBZ	60.00						
17	4100	Uniforme_GLOBZ	4100.00						
18	Peso Proprio	Peso Proprio daN	1550.00						
18	NEVE	Uniforme_GLOBZ	60.00						
18	4100	Uniforme_GLOBZ	4100.00						
19	Peso Proprio	Peso Proprio daN	1550.00						
19	NEVE	Uniforme_GLOBZ	60.00						
19	4100	Uniforme_GLOBZ	4100.00						
20	Peso Proprio	Peso Proprio daN	1550.00						
20	NEVE	Uniforme_GLOBZ	60.00						

She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
20	4100	Uniforme_GLOBZ	4100.0 0						
21	Peso Proprio	Peso Proprio daN	1550.0 0						
21	NEVE	Uniforme_GLOBZ	60.00						
21	4100	Uniforme_GLOBZ	4100.0 0						
22	Peso Proprio	Peso Proprio daN	375.00						
22	NEVE	Uniforme_GLOBZ	60.00						
22	accidentali	Uniforme_GLOBZ	600.00						
22	4100	Uniforme_GLOBZ	4100.0 0						
23	Peso Proprio	Peso Proprio daN	900.00						
23	NEVE	Uniforme_GLOBZ	60.00						
23	accidentali	Uniforme_GLOBZ	600.00						
23	4100	Uniforme_GLOBZ	4100.0 0						
24	Peso Proprio	Peso Proprio daN	900.00						
24	NEVE	Uniforme_GLOBZ	60.00						
24	accidentali	Uniforme_GLOBZ	600.00						
24	4100	Uniforme_GLOBZ	4100.0 0						
25	Peso Proprio	Peso Proprio daN	375.00						
25	NEVE	Uniforme_GLOBZ	60.00						
25	accidentali	Uniforme_GLOBZ	600.00						
25	4100	Uniforme_GLOBZ	4100.0 0						
26	Peso Proprio	Peso Proprio daN	375.00						
26	NEVE	Uniforme_GLOBZ	60.00						
26	accidentali	Uniforme_GLOBZ	600.00						
26	4100	Uniforme_GLOBZ	4100.0 0						
27	Peso Proprio	Peso Proprio daN	375.00						
27	NEVE	Uniforme_GLOBZ	60.00						
27	accidentali	Uniforme_GLOBZ	600.00						
27	4100	Uniforme_GLOBZ	4100.0 0						
28	Peso Proprio	Peso Proprio daN	900.00						
28	NEVE	Uniforme_GLOBZ	60.00						
28	accidentali	Uniforme_GLOBZ	600.00						
28	4100	Uniforme_GLOBZ	4100.0 0						
29	Peso Proprio	Peso Proprio daN	900.00						
29	NEVE	Uniforme_GLOBZ	60.00						
29	accidentali	Uniforme_GLOBZ	600.00						
29	4100	Uniforme_GLOBZ	4100.0 0						
30	Peso Proprio	Peso Proprio daN	1550.0 0						
30	NEVE	Uniforme_GLOBZ	60.00						
30	4100	Uniforme_GLOBZ	4100.0 0						
31	Peso Proprio	Peso Proprio daN	1550.0 0						
31	NEVE	Uniforme_GLOBZ	60.00						
31	4100	Uniforme_GLOBZ	4100.0 0						
32	Peso Proprio	Peso Proprio daN	155.00						
32	NEVE	Uniforme_GLOBZ	60.00						
32	4100	Uniforme_GLOBZ	4100.0 0						
33	Peso Proprio	Peso Proprio daN	37.50						
33	NEVE	Uniforme_GLOBZ	60.00						
33	accidentali	Uniforme_GLOBZ	600.00						
33	4100	Uniforme_GLOBZ	4100.0 0						
34	Peso Proprio	Peso Proprio daN	900.00						
34	NEVE	Uniforme_GLOBZ	60.00						
34	accidentali	Uniforme_GLOBZ	600.00						
34	4100	Uniforme_GLOBZ	4100.0 0						
35	Peso Proprio	Peso Proprio daN	90.00						
35	NEVE	Uniforme_GLOBZ	60.00						
35	accidentali	Uniforme_GLOBZ	600.00						

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

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She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
35	4100	Uniforme_GLOBZ	4100.0 0						
36	Peso Proprio	Peso Proprio daN	375.00						
36	NEVE	Uniforme_GLOBZ	60.00						
36	accidentali	Uniforme_GLOBZ	600.00						
36	4100	Uniforme_GLOBZ	4100.0 0						
37	Peso Proprio	Peso Proprio daN	375.00						
37	NEVE	Uniforme_GLOBZ	60.00						
37	accidentali	Uniforme_GLOBZ	600.00						
37	4100	Uniforme_GLOBZ	4100.0 0						
38	Peso Proprio	Peso Proprio daN	900.00						
38	NEVE	Uniforme_GLOBZ	60.00						
38	accidentali	Uniforme_GLOBZ	600.00						
38	4100	Uniforme_GLOBZ	4100.0 0						
39	Peso Proprio	Peso Proprio daN	1550.0 0						
39	NEVE	Uniforme_GLOBZ	60.00						
39	accidentali	Uniforme_GLOBZ	600.00						
39	ventilatore	Uniforme_GLOBZ	500.00						
39	4100	Uniforme_GLOBZ	4100.0 0						
40	Peso Proprio	Peso Proprio daN	1550.0 0						
40	NEVE	Uniforme_GLOBZ	60.00						
40	accidentali	Uniforme_GLOBZ	600.00						
40	ventilatore	Uniforme_GLOBZ	500.00						
40	4100	Uniforme_GLOBZ	4100.0 0						
41	Peso Proprio	Peso Proprio daN	400.00						
41	vento y	Uniforme_GLOBY	- 100.00						
42	Peso Proprio	Peso Proprio daN	400.00						
43	Peso Proprio	Peso Proprio daN	400.00						
43	vento y	Uniforme_GLOBY	- 100.00						
44	Peso Proprio	Peso Proprio daN	400.00						
45	Peso Proprio	Peso Proprio daN	620.00						
45	NEVE	Uniforme_GLOBZ	60.00						
45	accidentali	Uniforme_GLOBZ	600.00						
45	4100	Uniforme_GLOBZ	4100.0 0						
46	Peso Proprio	Peso Proprio daN	620.00						
46	NEVE	Uniforme_GLOBZ	60.00						
46	accidentali	Uniforme_GLOBZ	600.00						
46	4100	Uniforme_GLOBZ	4100.0 0						
47	Peso Proprio	Peso Proprio daN	150.00						
47	NEVE	Uniforme_GLOBZ	60.00						
47	accidentali	Uniforme_GLOBZ	600.00						
47	4100	Uniforme_GLOBZ	4100.0 0						
48	Peso Proprio	Peso Proprio daN	360.00						
48	NEVE	Uniforme_GLOBZ	60.00						
48	accidentali	Uniforme_GLOBZ	600.00						
48	4100	Uniforme_GLOBZ	4100.0 0						

Risultati Analisi Dinamica - Baricentri masse e masse  
Scenario di calcolo: ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO

Piano	Rigido	Massa	X	Y	Z
		daN	m	m	m
0	No	0.00	0.00	0.00	0.00
1	Si	17567.50	-3.10	1.40	0.78

Piano	Rigido	Massa daN	X m	Y m	Z m
0	No	0.00	0.00	0.00	0.00
1	Si	17567.50	-2.80	1.52	0.78

Piano	Rigido	Massa daN	X m	Y m	Z m
0	No	0.00	0.00	0.00	0.00
1	Si	17567.50	-3.10	1.64	0.78

Piano	Rigido	Massa daN	X m	Y m	Z m
0	No	0.00	0.00	0.00	0.00
1	Si	17567.50	-3.40	1.52	0.78

**Verifica Degli Spostamenti Relativi**

Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

Interp.	Comb.	$\eta_{Xv}$ mm	$\eta_{Xh}$ mm	$\eta_{Yv}$ mm	$\eta_{Yh}$ mm	Nodo1	Nodo2	$\eta$ mm	$\eta_{Amm}$ mm	Cs
0-1	(31+32)-IV-4	0.04	0.00	0.10	0.01	13	113	0.12	4.00	35
0-1	(31+32)-IV-4	0.04	0.00	0.10	0.01	14	114	0.11	4.00	35
0-1	(31+32)-IV-4	0.04	0.00	0.10	0.01	15	115	0.12	4.00	35
0-1	(31+32)-IV-4	0.03	0.00	0.10	0.01	16	116	0.12	4.00	35
0-1	(31+32)-II-3	0.03	0.00	0.10	0.01	17	117	0.12	4.00	34
0-1	(31+32)-II-3	0.03	0.00	0.10	0.01	18	118	0.12	4.00	34
0-1	(31+32)-II-3	0.04	0.00	0.10	0.01	19	119	0.11	4.00	35
0-1	(31+32)-IV-4	0.04	0.00	0.06	0.01	33	133	0.07	4.00	58
0-1	(31+32)-IV-4	0.04	0.00	0.06	0.01	34	134	0.07	4.00	58
0-1	(31+32)-IV-4	0.03	0.00	0.06	0.01	35	135	0.07	4.00	58
0-1	(31+32)-IV-3	0.03	0.00	0.06	0.01	36	136	0.07	4.00	58
0-1	(31+32)-II-3	0.03	0.00	0.06	0.01	37	137	0.07	4.00	58
0-1	(31+32)-II-3	0.03	0.00	0.06	0.01	38	138	0.07	4.00	57
0-1	(31+32)-II-3	0.04	0.00	0.06	0.01	39	139	0.07	4.00	55
<b>Minimo</b>										
0-1	(31+32)-II-3	0.03	0.00	0.10	0.01	18	118	0.12	4.00	34

**Risultati Analisi Dinamica - Sollecitazioni massime per combinazione - Sigma terreno platea**

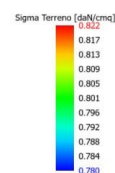
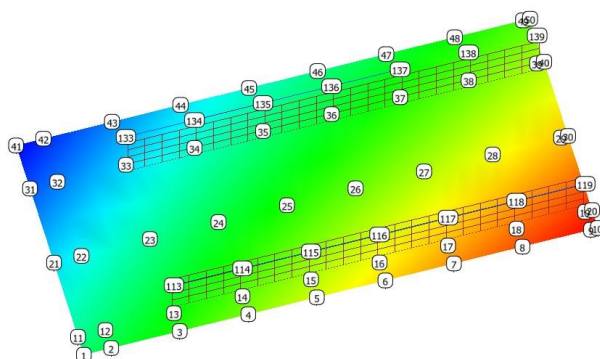
Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

Combinazione	Muro	Nodi	SigmaMax daN/cm <sup>2</sup>	SigmaMin daN/cm <sup>2</sup>
1	33	9-10-20-19	0.21	0.16
2	33	9-10-20-19	0.36	0.24
3	33	9-10-20-19	0.82	0.78
4	47	1-2-12-11	0.39	0.30
5	47	1-2-12-11	0.36	0.32
6	47	1-2-12-11	0.40	0.29
7	47	1-2-12-11	0.37	0.33
8	47	1-2-12-11	0.40	0.29
9	47	1-2-12-11	0.40	0.29
10	48	32-42-41-31	0.38	0.31
11	35	40-50-49-39	0.31	0.29
12-I-1	33	9-10-20-19	0.30	0.18
12-II-1	33	9-10-20-19	0.31	0.18
12-I-2	33	9-10-20-19	0.30	0.18
12-II-2	33	9-10-20-19	0.31	0.18
12-I-3	33	9-10-20-19	0.30	0.18
12-II-3	33	9-10-20-19	0.31	0.18
12-I-4	33	9-10-20-19	0.30	0.18
12-II-4	33	9-10-20-19	0.31	0.18
13-I-1	3	34-44-43-33	0.33	0.15
13-II-1	3	34-44-43-33	0.31	0.17
13-I-2	3	34-44-43-33	0.31	0.17
13-II-2	3	34-44-43-33	0.33	0.15
13-I-3	3	34-44-43-33	0.33	0.15
13-II-3	3	34-44-43-33	0.31	0.17
13-I-4	3	34-44-43-33	0.31	0.17



Combinazione	Muro	Nodi	SigmaMax	SigmaMin
13-II-4	3	34-44-43-33	0.33	0.15
14-I-1	33	9-10-20-19	0.31	0.13
14-II-1	33	9-10-20-19	0.31	0.13
14-I-2	33	9-10-20-19	0.31	0.13
14-II-2	33	9-10-20-19	0.31	0.13
14-I-3	33	9-10-20-19	0.31	0.13
14-II-3	33	9-10-20-19	0.31	0.13
14-I-4	33	9-10-20-19	0.31	0.13
14-II-4	33	9-10-20-19	0.31	0.14
15-I-1	35	40-50-49-39	0.30	0.14
15-II-1	35	40-50-49-39	0.29	0.16
15-I-2	35	40-50-49-39	0.29	0.16
15-II-2	35	40-50-49-39	0.30	0.14
15-I-3	35	40-50-49-39	0.30	0.14
15-II-3	35	40-50-49-39	0.29	0.16
15-I-4	35	40-50-49-39	0.29	0.16
15-II-4	35	40-50-49-39	0.30	0.14
Assoluti				
3	33	9-10-20-19	0.82	
14-I-4	33	9-10-20-19		0.13

Tipo diagramma: Tensioni medie terreno  
Combinazione corrente : Scenario ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO - C 3  
Tensioni medie terreno aste  
Tensioni medie terreno platee



**Risultati Analisi Dinamica - Spostamenti massimi - Nodi**  
Scenario di calcolo: ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	mm	mm	mm	°	°	°
1	0.00 (1)	0.00 (1)	-3.98 (3)	-0.01 (13-I-3)	0.00 (14-I-4)	0.00 (1)
2	0.00 (1)	0.00 (1)	-3.99 (3)	-0.01 (13-I-3)	0.00 (14-I-4)	0.00 (1)
3	0.00 (1)	0.00 (1)	-4.01 (3)	-0.01 (13-I-3)	0.00 (14-I-4)	0.00 (1)
4	0.00 (1)	0.00 (1)	-4.03 (3)	-0.01 (13-I-3)	0.00 (14-I-4)	0.00 (1)
5	0.00 (1)	0.00 (1)	-4.05 (3)	-0.01 (13-I-3)	0.00 (14-I-4)	0.00 (1)
6	0.00 (1)	0.00 (1)	-4.06 (3)	-0.01 (13-I-3)	0.00 (14-I-4)	0.00 (1)
7	0.00 (1)	0.00 (1)	-4.08 (3)	-0.01 (13-I-3)	0.00 (14-II-4)	0.00 (1)
8	0.00 (1)	0.00 (1)	-4.09 (3)	-0.01 (13-I-3)	0.00 (14-II-4)	0.00 (1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

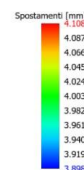
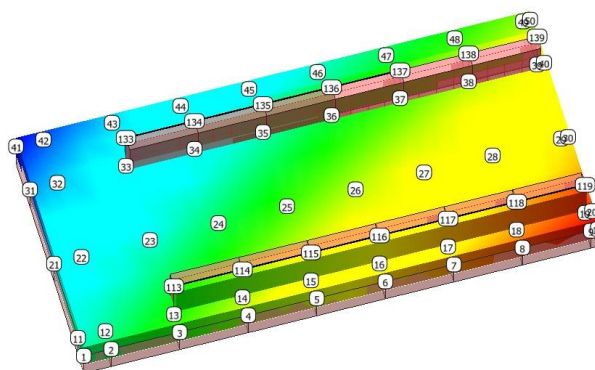
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Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
9	0.00(1)	0.00(1)	-4.11(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
10	0.00(1)	0.00(1)	-4.11(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
11	0.00(1)	0.00(1)	-3.97(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
12	0.00(1)	0.00(1)	-3.98(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
13	0.00(1)	0.00(1)	-4.00(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
14	0.00(1)	0.00(1)	-4.02(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
15	0.00(1)	0.00(1)	-4.04(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
16	0.00(1)	0.00(1)	-4.06(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
17	0.00(1)	0.00(1)	-4.07(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
18	0.00(1)	0.00(1)	-4.09(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
19	0.00(1)	0.00(1)	-4.10(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
20	0.00(1)	0.00(1)	-4.10(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
21	0.00(1)	0.00(1)	-3.94(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
22	0.00(1)	0.00(1)	-3.95(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
23	0.00(1)	0.00(1)	-3.97(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
24	0.00(1)	0.00(1)	-3.99(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
25	0.00(1)	0.00(1)	-4.01(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
26	0.00(1)	0.00(1)	-4.02(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
27	0.00(1)	0.00(1)	-4.04(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
28	0.00(1)	0.00(1)	-4.05(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
29	0.00(1)	0.00(1)	-4.07(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
30	0.00(1)	0.00(1)	-4.07(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
31	0.00(1)	0.00(1)	-3.92(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
32	0.00(1)	0.00(1)	-3.92(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
33	0.00(1)	0.00(1)	-3.94(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
34	0.00(1)	0.00(1)	-3.96(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
35	0.00(1)	0.00(1)	-3.98(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
36	0.00(1)	0.00(1)	-3.99(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
37	0.00(1)	0.00(1)	-4.01(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
38	0.00(1)	0.00(1)	-4.02(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
39	0.00(1)	0.00(1)	-4.04(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
40	0.00(1)	0.00(1)	-4.04(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
41	0.00(1)	0.00(1)	-3.90(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
42	0.00(1)	0.00(1)	-3.91(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
43	0.00(1)	0.00(1)	-3.93(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
44	0.00(1)	0.00(1)	-3.94(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
45	0.00(1)	0.00(1)	-3.96(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
46	0.00(1)	0.00(1)	-3.98(3)	-0.01(13-I-3)	0.00(14-I-4)	0.00(1)
47	0.00(1)	0.00(1)	-3.99(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
48	0.00(1)	0.00(1)	-4.01(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
49	0.00(1)	0.00(1)	-4.02(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
50	0.00(1)	0.00(1)	-4.02(3)	-0.01(13-I-3)	0.00(14-II-4)	0.00(1)
113	0.09(14-II-4)	0.36(13-I-4)	-4.00(3)	-0.05(13-I-4)	0.03(14-I-4)	0.00(13-II-4)
114	0.08(14-II-4)	0.35(13-I-4)	-4.02(3)	-0.04(13-I-4)	0.02(14-II-4)	0.00(12-I-4)
115	0.07(14-II-4)	0.35(13-I-4)	-4.04(3)	-0.04(13-I-4)	0.02(14-II-4)	0.00(12-II-4)
116	0.07(14-I-4)	0.35(13-I-3)	-4.06(3)	-0.04(13-I-4)	0.02(14-I-4)	0.00(12-I-1)
117	0.07(14-II-4)	0.36(13-I-2)	-4.07(3)	-0.04(13-I-2)	0.02(14-II-4)	0.00(12-I-2)
118	0.08(14-II-4)	0.36(13-I-2)	-4.09(3)	-0.05(13-I-2)	0.02(14-II-4)	0.00(12-I-2)
119	0.10(14-I-4)	0.37(13-I-2)	-4.10(3)	-0.05(13-I-2)	0.03(14-II-2)	0.00(12-I-2)
133	0.09(14-II-4)	0.40(13-I-4)	-3.94(3)	-0.06(13-I-4)	0.03(14-I-4)	0.00(13-II-4)
134	0.07(14-II-4)	0.40(13-I-3)	-3.96(3)	-0.05(13-I-3)	0.02(14-II-4)	-0.00(14-II-4)
135	0.07(14-II-4)	0.40(13-I-3)	-3.98(3)	-0.05(13-I-3)	0.02(14-II-4)	-0.00(14-II-4)
136	0.07(14-I-4)	0.40(13-I-3)	-3.99(3)	-0.05(13-I-3)	0.02(14-I-4)	-0.00(14-I-3)
137	0.07(14-II-4)	0.40(13-I-3)	-4.01(3)	-0.05(13-I-3)	0.02(14-II-4)	-0.00(14-I-2)
138	0.08(14-II-4)	0.40(13-I-3)	-4.02(3)	-0.05(13-I-3)	0.02(14-II-4)	-0.00(14-I-2)
139	0.10(14-I-4)	0.41(13-I-3)	-4.04(3)	-0.06(13-I-3)	0.03(14-II-2)	-0.00(15-II-2)

Tipo diagramma: Deformata  
Combinazione corrente : Scenario ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO - C 3



**Risultati Analisi Dinamica - Reazioni massime - Nodi**  
Scenario di calcolo: ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO

Nodo	Rx daN	Ry daN	Rz daN	Mx daN*m	My daN*m	Mz daN*m
1	-5.92 (2)	-2.76 (2)	0	0	0	0
2	-112.91 (2)	-19.82 (2)	0	0	0	-1.32 (15-I-4)
3	-209.83 (2)	-9.01 (2)	0	0	0	4.70 (15-I-4)
4	101.20 (13-II-2)	-14.21 (2)	0	0	0	0
5	79.41 (13-II-2)	-13.87 (2)	0	0	0	0
6	66.01 (15-II-2)	-13.82 (2)	0	0	0	0
7	51.15 (15-II-2)	-13.70 (2)	0	0	0	0
8	-61.99 (12-II-2)	-13.64 (2)	0	0	0	0
9	-12.20 (13-I-2)	-9.24 (14-II-1)	0	0	0	0
10	0	-1.99 (15-I-2)	0	0	0	0
11	-27.96 (2)	35.40 (13-II-2)	0	0	0	3.15 (11)
12	-418.44 (2)	67.04 (13-II-2)	0	0	0	33.91 (11)
13	-651.62 (2)	-261.19 (15-I-4)	0	0	0	27.36 (2)
14	422.87 (9)	-621.73 (15-I-4)	0	0	0	-44.94 (9)
15	214.56 (15-II-2)	-548.05 (15-I-4)	0	0	0	-18.48 (11)
16	-144.41 (12-I-1)	-522.70 (15-I-3)	0	0	0	8.61 (12-I-1)
17	-202.08 (12-I-1)	-512.70 (15-I-2)	0	0	0	14.70 (12-I-1)
18	-316.03 (12-I-2)	-527.39 (15-I-2)	0	0	0	23.19 (12-I-2)
19	-90.98 (12-I-2)	-253.16 (15-I-2)	0	0	0	27.40 (15-I-2)
20	0	67.73 (12-II-1)	0	0	0	-2.17 (13-I-2)
21	-45.49 (2)	189.13 (13-II-2)	0	0	0	-2.36 (13-II-2)
22	-597.48 (11)	399.05 (13-I-2)	0	0	0	5.61 (13-II-4)
23	-763.81 (11)	615.41 (13-I-4)	0	0	0	-24.73 (13-I-4)
24	674.38 (9)	704.96 (13-I-4)	0	0	0	-2.08 (14-II-1)
25	426.19 (11)	724.39 (13-I-4)	0	0	0	4.20 (13-II-2)
26	268.61 (11)	720.22 (13-I-3)	0	0	0	3.15 (13-II-2)
27	183.11 (11)	723.94 (13-I-2)	0	0	0	2.04 (13-II-2)
28	-164.52 (12-II-2)	705.76 (13-I-2)	0	0	0	4.59 (13-II-2)
29	54.89 (9)	341.91 (13-I-2)	0	0	0	-4.53 (13-II-2)
30	4.68 (9)	66.39 (15-I-2)	0	0	0	0
31	-29.23 (11)	97.41 (13-II-2)	0	0	0	-2.41 (10)
32	-451.02 (11)	158.84 (13-II-2)	0	0	0	-24.01 (2)

Nodo	Rx	Ry	Rz	Mx	My	Mz
33	-741.70 (11)	-117.99 (13-II-1)	0	0	0	-18.09 (11)
34	432.68 (9)	-788.96 (13-I-4)	0	0	0	39.02 (9)
35	199.91 (2)	-874.23 (13-I-4)	0	0	0	15.66 (9)
36	106.01 (2)	-912.51 (13-II-1)	0	0	0	-8.83 (12-I-3)
37	-147.34 (12-I-3)	-915.73 (13-II-1)	0	0	0	-13.44 (12-I-3)
38	-314.96 (12-I-2)	-931.59 (13-I-2)	0	0	0	-17.97 (12-I-2)
39	-97.68 (12-I-2)	-421.49 (13-I-4)	0	0	0	25.99 (13-I-2)
40	1.63 (15-I-2)	-59.56 (4)	0	0	0	-2.34 (13-I-2)
41	-11.58 (15-I-3)	5.65 (15-I-1)	0	0	0	0
42	-206.03 (15-I-3)	48.25 (11)	0	0	0	-5.39 (11)
43	-460.57 (15-I-3)	57.02 (15-II-4)	0	0	0	-12.19 (11)
44	-214.92 (13-II-2)	97.46 (15-II-4)	0	0	0	-2.85 (13-II-2)
45	-143.89 (13-II-2)	87.32 (15-I-3)	0	0	0	3.96 (14-II-3)
46	-105.38 (13-II-2)	85.63 (15-I-3)	0	0	0	4.18 (14-I-3)
47	-69.12 (13-II-2)	85.56 (15-I-3)	0	0	0	2.71 (2)
48	-42.90 (12-II-3)	89.10 (15-II-2)	0	0	0	-3.56 (12-II-2)
49	24.05 (15-I-2)	44.06 (15-II-2)	0	0	0	-1.41 (14-I-2)
50	1.18 (14-I-1)	6.60 (14-I-2)	0	0	0	0

**Risultati Analisi Dinamica - Spostamenti massimi - Impalcati**

Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Piano	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	mm	mm	mm	°	°	°
1	0.05 (14-II-2)	0.28 (13-II-3)	-4.03 (3-1)	0.00 (1-1)	0.00 (1-1)	0.00 (13-I-2)

**Risultati Analisi Dinamica - Spostamenti massimi - Impalcati (SLD)**

Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Piano	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	mm	mm	mm	°	°	°
1	0.03 (31-II-2)	0.09 (30-II-3)	-1.28 (20-1)	0.00 (16-1)	0.00 (16-1)	0.00 (30-I-2)

**Risultati Analisi Dinamica - Sollecitazioni Massime - Muri discretizzati**

Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
		MPa	MPa	MPa	daN*m/m	daN*m/m	daN*m/m
1	1	0.1 (2)	0.0 (2)	-0.0 (13-I-4)	-325.18 (11)	24.37 (2)	26.91 (15-I-4)
1	2	0.1 (2)	0.0 (2)	-0.0 (13-I-4)	-334.23 (11)	-48.31 (2)	111.62 (13-I-4)
1	3	0.1 (11)	0.0 (2)	-0.0 (13-II-2)	-359.74 (11)	30.96 (2)	-22.01 (13-II-2)
1	4	0.1 (11)	-0.0 (13-I-4)	-0.0 (13-II-2)	-360.59 (2)	-66.25 (2)	97.56 (13-II-2)
1	5	0.1 (11)	0.0 (2)	-0.0 (13-II-2)	-325.72 (11)	20.11 (2)	-31.92 (13-II-2)
1	6	0.1 (11)	0.0 (2)	0.0 (9)	-332.54 (2)	-51.18 (2)	85.04 (13-II-2)
1	7	0.1 (11)	0.0 (2)	-0.0 (13-II-2)	-295.12 (2)	9.65 (2)	-15.83 (9)
1	8	0.1 (11)	0.0 (2)	-0.0 (13-II-2)	-301.78 (2)	-32.83 (2)	63.32 (13-II-2)
2	1	0.1 (15-I-4)	0.1 (11)	-0.0 (14-II-1)	-311.46 (15-I-4)	-281.09 (11)	-120.94 (13-II-2)
2	2	0.0 (15-I-4)	0.1 (11)	0.0 (13-II-2)	-383.31 (15-I-4)	-366.16 (11)	-73.81 (15-II-2)
2	3	0.0 (15-I-4)	0.1 (11)	0.0 (13-II-2)	-364.81 (15-I-4)	-376.44 (11)	-73.17 (15-II-2)
2	4	0.0 (15-I-4)	0.1 (11)	0.0 (13-I-2)	-244.98 (15-I-4)	-290.02 (11)	90.39 (9)
2	5	-0.0 (9)	0.1 (11)	-0.0 (14-II-1)	198.14 (9)	-256.50 (11)	-143.81 (13-II-2)
2	6	0.0 (15-I-4)	0.1 (11)	0.0 (13-II-2)	213.79 (9)	-318.95 (11)	-90.41 (13-II-2)
2	7	0.0 (15-I-4)	0.1 (11)	0.0 (13-II-2)	191.08 (9)	-312.92 (11)	-66.09 (13-II-2)
2	8	-0.0 (9)	0.1 (11)	0.0 (13-II-2)	136.10 (9)	-226.72 (2)	61.90 (2)
3	1	0.0 (15-II-4)	0.1 (2)	0.0 (13-II-2)	-150.50 (15-II-4)	-310.09 (11)	-149.11 (13-II-2)
3	2	0.0 (15-II-4)	0.1 (2)	0.0 (13-II-2)	-205.88 (15-II-4)	-319.41 (11)	-157.46 (13-II-2)
3	3	0.0 (15-II-4)	0.1 (2)	0.0 (13-II-2)	-199.98 (15-II-4)	-311.05 (2)	-169.15 (13-II-2)
3	4	0.0 (15-II-4)	0.1 (11)	0.0 (13-I-3)	-103.21 (15-II-4)	-246.31 (2)	-125.03 (13-II-2)
3	5	0.0 (15-II-4)	0.1 (2)	0.0 (13-II-2)	26.87 (11)	-292.73 (11)	-76.06 (13-II-2)
3	6	0.0 (15-II-4)	0.1 (2)	0.0 (13-II-2)	80.89 (15-II-4)	-279.70 (11)	-37.26 (13-II-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
3	7	0.0 (15-II-4)	0.1 (2)	0.0 (13-II-2)	89.33 (15-II-4)	-270.11 (2)	-25.92 (13-II-2)
3	8	0.0 (15-II-4)	0.1 (11)	0.0 (13-I-3)	53.95 (15-I-3)	-208.57 (2)	-27.56 (13-I-4)
4	1	-0.0 (10)	0.1 (2)	0.0 (13-II-2)	183.79 (9)	-249.24 (11)	-122.71 (13-II-2)
4	2	-0.0 (13-II-1)	0.1 (2)	0.0 (13-II-2)	200.90 (9)	-314.42 (11)	-93.49 (13-II-2)
4	3	-0.0 (13-II-1)	0.1 (2)	0.0 (13-II-2)	177.80 (9)	-309.90 (11)	-93.80 (13-II-2)
4	4	-0.0 (10)	0.1 (2)	0.0 (13-II-2)	123.17 (9)	-228.40 (11)	-77.06 (13-II-2)
4	5	-0.0 (13-I-4)	0.1 (2)	0.0 (13-II-2)	217.34 (13-I-4)	-251.92 (2)	-143.12 (13-II-2)
4	6	-0.0 (13-II-1)	0.1 (2)	0.0 (13-II-2)	228.70 (13-I-4)	-326.51 (2)	-129.99 (13-II-2)
4	7	-0.0 (13-II-1)	0.1 (2)	0.0 (13-II-2)	204.23 (13-I-4)	-334.72 (2)	-123.73 (13-II-2)
4	8	-0.0 (13-I-4)	0.1 (2)	0.0 (13-II-2)	134.72 (13-I-4)	-257.88 (2)	-122.10 (13-II-2)
5	1	-0.0 (14-I-2)	-0.3 (14-I-2)	0.0 (12-II-2)	-112.48 (15-I-2)	-1405.14 (15-I-2)	-70.33 (15-I-2)
5	2	-0.0 (14-II-2)	-0.3 (14-II-2)	0.1 (12-II-2)	-59.70 (15-I-2)	-1344.80 (15-I-2)	-24.14 (14-II-2)
5	3	-0.2 (14-II-2)	-0.3 (14-II-2)	0.2 (12-II-2)	-147.17 (15-I-2)	-1455.62 (15-I-2)	242.06 (13-I-2)
5	4	-0.2 (14-II-2)	0.7 (12-I-2)	0.1 (9)	116.28 (12-I-2)	-2077.50 (15-II-2)	897.58 (13-II-2)
5	5	-0.0 (14-II-2)	-0.1 (14-II-2)	0.0 (12-II-2)	-163.23 (15-I-2)	-1427.20 (15-I-2)	-16.31 (15-I-2)
5	6	-0.1 (14-II-2)	-0.1 (11)	0.0 (4)	-120.85 (15-I-2)	-1281.43 (15-I-2)	-17.95 (14-II-2)
5	7	-0.1 (14-II-2)	0.1 (12-I-2)	-0.1 (14-I-2)	-170.51 (15-I-2)	-974.24 (15-I-2)	122.57 (13-II-2)
5	8	0.3 (12-I-3)	0.0 (9)	-0.1 (14-I-2)	-220.40 (15-I-2)	-169.78 (15-I-2)	191.98 (13-II-2)
5	9	-0.0 (11)	-0.1 (14-II-2)	-0.0 (11)	-169.21 (15-I-2)	-1424.63 (15-I-2)	15.36 (13-II-2)
5	10	-0.0 (9)	-0.1 (14-II-2)	-0.1 (14-I-2)	-129.90 (15-I-2)	-1265.18 (15-I-2)	19.04 (13-II-2)
5	11	-0.0 (14-II-3)	-0.1 (14-II-3)	-0.2 (14-I-2)	-183.36 (15-I-2)	-954.46 (15-I-2)	-82.28 (15-I-2)
5	12	0.1 (12-I-3)	0.0 (12-II-2)	-0.1 (14-I-2)	-234.50 (15-I-2)	-188.56 (15-I-2)	-142.55 (15-I-2)
5	13	0.0 (12-II-3)	-0.1 (14-II-2)	-0.0 (11)	-182.72 (15-I-2)	-1403.29 (15-I-2)	16.42 (13-II-2)
5	14	0.1 (12-II-3)	-0.2 (14-II-2)	-0.0 (11)	-188.07 (15-I-3)	-1309.78 (15-I-2)	22.83 (13-II-2)
5	15	0.2 (12-II-2)	-0.4 (14-II-3)	-0.1 (9)	-110.31 (15-II-2)	-1367.76 (15-I-2)	-118.25 (15-I-2)
5	16	-0.1 (9)	-1.4 (14-II-3)	-0.3 (14-I-2)	-86.30 (14-I-2)	-1883.58 (15-II-2)	-892.55 (15-I-3)
6	1	-0.3 (14-I-1)	-0.0 (14-I-2)	0.0 (12-II-2)	1167.62 (15-I-2)	95.20 (15-I-2)	51.60 (15-I-2)
6	2	-0.1 (14-II-1)	-0.0 (14-II-1)	0.0 (12-II-2)	1174.79 (15-I-2)	136.95 (15-I-2)	-10.54 (12-II-2)
6	3	-0.1 (14-II-1)	-0.0 (2)	-0.0 (14-I-2)	1167.02 (15-I-2)	140.15 (15-I-2)	-12.69 (13-II-2)
6	4	-0.1 (14-II-1)	0.0 (12-II-1)	-0.0 (2)	1149.45 (15-I-2)	148.71 (15-I-2)	-13.00 (13-II-2)
6	5	-0.3 (14-II-2)	-0.0 (14-II-1)	0.1 (12-II-2)	1090.09 (15-I-2)	50.65 (15-I-2)	-23.92 (12-I-2)
6	6	-0.1 (2)	-0.1 (14-II-1)	0.0 (10)	1036.10 (15-I-2)	105.65 (15-I-2)	-17.40 (12-II-2)
6	7	-0.1 (14-II-1)	-0.0 (9)	-0.1 (14-I-2)	1018.60 (15-I-2)	110.07 (15-I-2)	-17.45 (13-II-2)
6	8	-0.2 (14-II-1)	0.0 (12-II-1)	-0.0 (2)	1050.51 (15-I-2)	147.82 (15-I-2)	-18.78 (13-II-2)
6	9	-0.3 (14-II-2)	-0.2 (14-II-2)	0.2 (12-II-2)	1150.04 (15-I-2)	119.47 (15-I-2)	-204.07 (13-I-2)
6	10	0.1 (12-I-2)	-0.1 (14-II-2)	-0.1 (14-I-2)	775.00 (15-I-2)	147.35 (15-I-2)	-107.57 (13-II-2)
6	11	-0.1 (14-II-1)	-0.0 (14-II-1)	-0.2 (14-I-2)	753.98 (15-I-2)	152.95 (15-I-2)	60.06 (15-I-2)
6	12	-0.4 (14-II-1)	0.2 (12-II-1)	-0.1 (9)	1063.44 (15-I-2)	83.48 (15-II-2)	89.83 (15-I-2)
6	13	0.7 (12-I-2)	-0.2 (14-II-2)	0.1 (9)	1603.13 (15-II-2)	116.73 (14-I-2)	-706.90 (13-II-2)
6	14	0.0 (9)	0.3 (12-I-1)	-0.1 (14-I-2)	136.50 (15-I-2)	189.71 (15-I-2)	-160.74 (13-II-2)
6	15	0.0 (12-II-2)	0.1 (12-I-1)	-0.1 (14-I-2)	151.28 (15-I-2)	195.17 (15-I-2)	105.61 (15-I-2)
6	16	-1.4 (14-II-1)	-0.0 (9)	-0.3 (14-I-2)	1413.63 (15-II-2)	-85.30 (12-I-2)	667.63 (15-I-2)
7	1	-0.1 (9)	-0.0 (14-I-1)	-0.0 (14-I-2)	1140.80 (15-I-2)	147.93 (15-I-2)	-3.93 (12-II-2)
7	2	-0.1 (9)	-0.0 (2)	-0.1 (14-I-2)	1141.53 (15-I-2)	137.86 (15-I-2)	4.30 (15-I-2)
7	3	-0.1 (14-I-1)	-0.0 (9)	-0.1 (14-I-2)	1136.77 (15-I-2)	137.15 (15-I-2)	-12.22 (13-II-2)
7	4	-0.1 (14-I-2)	0.0 (12-I-2)	-0.0 (14-I-2)	1126.06 (15-I-2)	145.83 (15-I-2)	-11.53 (13-II-2)
7	5	-0.2 (9)	-0.0 (14-I-2)	0.0 (12-II-2)	1043.36 (15-I-2)	147.42 (15-I-2)	-10.18 (12-II-2)
7	6	-0.1 (9)	-0.0 (14-I-2)	-0.1 (14-I-2)	997.10 (15-I-2)	110.53 (15-I-3)	-9.20 (13-II-2)
7	7	-0.1 (14-I-2)	0.1 (12-II-2)	-0.1 (14-I-2)	993.45 (15-I-2)	109.52 (15-I-2)	-11.52 (13-II-2)
7	8	-0.2 (14-I-2)	0.1 (12-I-2)	-0.0 (2)	1031.99 (15-I-2)	144.69 (15-I-2)	-12.61 (13-II-2)
7	9	-0.2 (9)	-0.1 (14-I-2)	0.1 (12-II-2)	1058.88 (15-I-2)	83.17 (15-II-2)	-117.58 (13-II-2)
7	10	-0.1 (9)	0.1 (12-II-2)	-0.1 (14-I-2)	737.75 (15-I-2)	152.96 (15-I-3)	-88.99 (13-II-2)
7	11	-0.1 (14-I-2)	-0.0 (2)	-0.2 (14-I-2)	735.45 (15-I-2)	151.28 (15-I-2)	72.27 (15-I-2)
7	12	-0.4 (14-I-2)	0.2 (12-I-2)	-0.1 (9)	1051.51 (15-I-2)	78.81 (15-II-2)	99.90 (15-I-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
7	13	1.1 (14-I-2)	0.1 (12-I-2)	-0.2 (14-I-2)	1413.12 (15-II-2)	85.93 (14-I-2)	-692.04 (13-II-2)
7	14	-0.0 (12-II-2)	0.1 (12-II-2)	-0.0 (14-I-2)	143.55 (15-I-2)	193.42 (15-I-3)	-135.08 (13-II-2)
7	15	0.0 (12-II-2)	0.0 (12-II-2)	-0.1 (14-I-2)	142.97 (15-I-2)	191.10 (15-I-2)	119.80 (15-I-3)
7	16	-1.4 (14-I-2)	-0.1 (2)	-0.3 (14-I-2)	1408.69 (15-I-2)	-98.93 (12-I-2)	674.93 (15-I-1)
8	1	-0.0 (12-I-2)	-0.1 (4)	0.0 (12-II-1)	3.19 (10)	280.16 (4)	21.30 (12-I-1)
8	2	0.0 (13-I-2)	0.0 (15-I-2)	0.0 (13-I-2)	-3.22 (13-I-2)	-156.79 (15-I-2)	21.88 (10)
8	3	-0.0 (4)	-0.1 (4)	-0.0 (9)	7.16 (12-I-2)	278.47 (4)	-38.02 (12-II-1)
8	4	0.0 (12-II-1)	0.0 (15-I-2)	0.0 (15-I-2)	-7.88 (15-I-2)	-166.63 (15-I-2)	-48.82 (13-I-2)
9	1	-0.0 (14-II-2)	-0.1 (9)	-0.0 (14-I-3)	-179.15 (15-I-3)	-1374.40 (15-II-1)	-6.62 (15-II-2)
9	2	-0.0 (14-II-2)	-0.2 (9)	0.0 (12-II-3)	-184.91 (15-I-3)	-1289.33 (15-I-3)	-8.14 (14-II-3)
9	3	-0.2 (14-II-2)	-0.2 (9)	0.1 (12-II-3)	-106.06 (15-I-3)	-1356.59 (15-I-3)	137.30 (13-I-2)
9	4	-0.1 (11)	1.1 (14-I-3)	-0.2 (14-I-3)	81.70 (12-I-3)	-1880.93 (15-I-3)	908.16 (13-I-3)
9	5	-0.0 (11)	-0.1 (9)	-0.1 (14-I-3)	-165.65 (15-I-3)	-1386.13 (15-I-3)	-6.66 (15-II-2)
9	6	-0.1 (14-I-2)	-0.1 (9)	-0.1 (14-I-3)	-130.77 (15-I-3)	-1236.96 (15-I-3)	3.84 (12-I-3)
9	7	-0.1 (11)	-0.1 (9)	-0.1 (14-I-3)	-184.69 (15-I-3)	-935.43 (15-I-3)	103.04 (13-II-1)
9	8	0.1 (12-II-2)	-0.0 (12-II-3)	-0.0 (14-I-3)	-234.29 (15-I-3)	-179.93 (15-I-3)	164.48 (13-II-1)
9	9	-0.0 (11)	-0.1 (12-I-3)	-0.1 (14-I-3)	-165.77 (15-I-3)	-1386.83 (15-I-3)	15.70 (13-I-3)
9	10	-0.1 (11)	-0.1 (12-I-3)	-0.1 (14-I-3)	-130.84 (15-I-3)	-1237.52 (15-I-3)	12.19 (13-II-4)
9	11	-0.1 (11)	-0.1 (12-I-3)	-0.2 (14-I-3)	-184.69 (15-I-3)	-935.83 (15-I-3)	-96.10 (15-I-4)
9	12	-0.1 (11)	0.0 (12-I-4)	-0.1 (14-I-3)	-234.23 (15-I-3)	-180.02 (15-I-3)	-158.94 (15-I-4)
9	13	-0.0 (11)	-0.1 (12-I-3)	-0.0 (14-I-3)	-179.48 (15-I-3)	-1376.19 (15-I-3)	15.57 (13-II-4)
9	14	-0.0 (11)	-0.2 (12-I-3)	-0.0 (2)	-185.17 (15-I-3)	-1291.11 (15-I-3)	15.14 (13-II-4)
9	15	0.2 (12-II-2)	-0.4 (12-I-3)	-0.1 (9)	-106.06 (15-II-4)	-1357.78 (15-I-3)	-130.97 (15-I-4)
9	16	-0.1 (11)	-1.4 (12-I-3)	-0.3 (14-I-3)	-99.67 (14-II-4)	-1880.88 (15-I-3)	-903.37 (15-I-4)
10	1	-0.0 (14-I-2)	-0.1 (9)	-0.0 (14-I-3)	-179.56 (15-I-3)	-1376.84 (15-I-3)	-7.58 (15-II-2)
10	2	-0.0 (14-II-2)	-0.2 (9)	0.0 (12-II-3)	-185.20 (15-I-3)	-1291.46 (15-I-3)	-8.32 (14-I-3)
10	3	-0.1 (14-II-2)	-0.2 (9)	0.1 (12-II-3)	-106.15 (15-II-2)	-1357.91 (15-I-3)	139.33 (13-I-2)
10	4	-0.1 (11)	1.1 (14-I-3)	-0.2 (14-I-3)	81.72 (12-I-2)	-1880.90 (15-I-3)	909.40 (13-I-2)
10	5	-0.0 (11)	-0.1 (9)	-0.1 (14-I-3)	-165.84 (15-I-3)	-1387.34 (15-I-3)	-7.74 (15-II-2)
10	6	-0.1 (14-II-2)	-0.1 (9)	-0.1 (14-I-3)	-130.90 (15-I-3)	-1237.84 (15-I-3)	-4.34 (15-II-2)
10	7	-0.1 (11)	-0.1 (9)	-0.1 (14-I-3)	-184.71 (15-I-3)	-935.94 (15-I-3)	104.49 (13-I-2)
10	8	0.1 (12-II-2)	-0.0 (12-II-2)	-0.0 (14-I-3)	-234.27 (15-I-3)	-180.05 (15-I-3)	165.82 (13-I-2)
10	9	-0.0 (11)	-0.1 (12-II-2)	-0.1 (14-I-3)	-165.75 (15-I-3)	-1386.64 (15-I-3)	14.74 (13-I-2)
10	10	-0.1 (11)	-0.1 (12-II-2)	-0.1 (14-I-3)	-130.84 (15-I-3)	-1237.19 (15-I-3)	11.77 (13-I-2)
10	11	-0.1 (11)	-0.1 (12-I-3)	-0.2 (14-I-3)	-184.78 (15-I-3)	-935.54 (15-I-3)	-94.39 (15-I-4)
10	12	-0.0 (11)	0.0 (12-II-3)	-0.1 (14-I-3)	-234.33 (15-I-3)	-179.93 (15-I-3)	-157.29 (15-I-3)
10	13	0.0 (12-I-2)	-0.1 (12-I-2)	-0.0 (14-I-3)	-179.20 (15-I-3)	-1374.85 (15-II-1)	14.53 (13-I-2)
10	14	0.1 (12-I-2)	-0.2 (12-I-2)	-0.0 (2)	-184.94 (15-I-3)	-1289.42 (15-I-3)	14.55 (13-I-2)
10	15	0.2 (12-I-2)	-0.4 (12-I-2)	-0.1 (9)	-106.10 (15-I-3)	-1356.64 (15-I-3)	-128.73 (15-I-4)
10	16	-0.1 (11)	-1.4 (14-I-2)	-0.3 (14-I-3)	-99.50 (14-I-3)	-1880.92 (15-I-3)	-901.73 (15-I-3)
11	1	-0.1 (9)	-0.0 (14-I-2)	-0.0 (14-I-1)	1124.53 (15-I-3)	145.58 (15-I-3)	4.97 (15-II-2)
11	2	-0.1 (9)	-0.0 (2)	-0.1 (14-I-1)	1131.64 (15-I-3)	136.35 (15-I-3)	5.30 (15-II-2)
11	3	-0.1 (12-II-2)	-0.0 (2)	-0.1 (14-I-1)	1131.64 (15-I-3)	136.28 (15-I-3)	-11.39 (13-I-2)
11	4	-0.1 (12-I-2)	0.0 (12-I-2)	-0.0 (14-I-1)	1124.30 (15-I-3)	145.40 (15-I-3)	-11.01 (13-I-2)
11	5	-0.2 (9)	-0.0 (14-II-2)	0.0 (12-II-1)	1029.96 (15-I-3)	144.13 (15-I-2)	-6.31 (12-I-2)
11	6	-0.1 (9)	-0.1 (14-II-2)	-0.1 (14-I-1)	988.48 (15-I-3)	108.23 (15-I-3)	6.54 (14-I-1)
11	7	-0.1 (12-I-1)	-0.1 (2)	-0.1 (14-I-1)	988.36 (15-I-3)	108.01 (15-I-3)	9.42 (14-I-1)
11	8	-0.2 (12-I-2)	0.1 (12-I-2)	-0.0 (11)	1029.40 (15-I-3)	144.05 (15-II-1)	-10.21 (13-I-2)
11	9	-0.2 (9)	-0.2 (14-II-2)	0.1 (12-II-1)	1050.33 (15-I-2)	77.78 (15-II-2)	-110.94 (13-I-2)
11	10	-0.1 (9)	-0.1 (2)	-0.1 (14-I-1)	731.78 (15-I-3)	149.03 (15-I-3)	-83.92 (13-I-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
11	11	-0.1 (12-I-1)	-0.1 (2)	-0.2 (14-I-1)	731.66 (15-I-3)	149.03 (15-II-1)	74.73 (15-I-4)
11	12	-0.4 (12-I-2)	0.2 (12-I-2)	-0.1 (9)	1048.67 (15-I-3)	77.86 (15-II-1)	101.47 (15-I-4)
11	13	1.1 (14-I-1)	-0.1 (2)	-0.2 (14-I-1)	1408.34 (15-I-2)	81.97 (14-I-2)	-684.78 (13-I-2)
11	14	-0.0 (12-II-2)	0.1 (12-I-2)	-0.0 (14-I-1)	142.13 (15-I-3)	188.21 (15-I-3)	-130.27 (13-I-2)
11	15	0.0 (12-II-1)	-0.0 (2)	-0.1 (14-I-1)	142.06 (15-I-3)	188.29 (15-II-1)	122.39 (15-I-4)
11	16	-1.4 (14-I-2)	-0.1 (2)	-0.3 (14-I-1)	1407.29 (15-I-1)	-99.62 (12-I-1)	677.26 (15-I-4)
12	1	-0.0 (14-I-2)	-0.1 (9)	-0.0 (14-I-2)	-182.06 (15-I-2)	-1394.11 (15-I-2)	-6.10 (14-II-2)
12	2	-0.0 (14-I-2)	-0.2 (9)	0.0 (12-II-2)	-188.51 (15-I-3)	-1303.17 (15-I-2)	-11.74 (14-II-2)
12	3	-0.1 (14-I-2)	-0.2 (9)	0.1 (12-II-2)	-111.46 (15-II-2)	-1363.99 (15-I-3)	146.05 (13-II-2)
12	4	0.1 (12-I-2)	1.1 (14-I-2)	-0.2 (14-I-2)	84.98 (12-I-2)	-1883.41 (15-II-2)	916.42 (13-II-2)
12	5	-0.0 (11)	-0.1 (9)	-0.1 (14-I-2)	-167.67 (15-I-2)	-1398.65 (15-I-2)	-6.77 (15-I-2)
12	6	-0.0 (14-I-2)	-0.1 (9)	-0.1 (14-I-2)	-133.61 (15-I-3)	-1245.86 (15-I-3)	6.99 (13-II-2)
12	7	0.1 (12-II-2)	-0.1 (9)	-0.1 (14-I-2)	-188.79 (15-I-3)	-940.43 (15-I-3)	109.92 (13-II-2)
12	8	0.1 (12-II-2)	-0.0 (12-II-2)	-0.0 (14-I-2)	-239.47 (15-I-3)	-181.16 (15-I-3)	170.83 (13-II-2)
12	9	-0.0 (9)	-0.1 (14-I-2)	-0.1 (14-I-2)	-166.91 (15-I-3)	-1393.65 (15-I-3)	15.40 (13-II-2)
12	10	0.1 (12-II-2)	-0.1 (14-I-2)	-0.1 (14-I-2)	-132.54 (15-I-3)	-1242.72 (15-I-3)	15.02 (13-II-2)
12	11	-0.0 (11)	-0.1 (14-I-2)	-0.2 (14-I-2)	-187.25 (15-I-3)	-938.82 (15-I-3)	-92.31 (15-I-2)
12	12	0.0 (12-II-2)	0.0 (12-II-2)	-0.1 (14-I-2)	-237.40 (15-I-3)	-180.72 (15-I-3)	-155.08 (15-I-2)
12	13	0.0 (12-I-2)	-0.1 (14-I-2)	-0.0 (14-I-2)	-179.91 (15-I-3)	-1378.87 (15-I-3)	14.69 (13-II-2)
12	14	0.1 (12-I-2)	-0.2 (14-I-2)	-0.0 (11)	-185.74 (15-I-3)	-1293.05 (15-I-3)	16.85 (13-II-2)
12	15	0.2 (12-I-2)	-0.4 (14-I-2)	-0.1 (9)	-107.31 (15-II-2)	-1358.87 (15-I-3)	-127.63 (15-II-1)
12	16	-0.1 (11)	-1.4 (14-I-2)	-0.3 (14-I-2)	-98.99 (14-I-2)	-1881.11 (15-I-3)	-899.86 (15-I-3)
13	1	-0.1 (9)	-0.0 (14-II-2)	-0.0 (14-I-1)	1123.96 (15-I-3)	145.39 (15-I-3)	4.60 (15-II-2)
13	2	-0.1 (9)	-0.0 (2)	-0.1 (14-I-1)	1130.53 (15-I-3)	136.20 (15-I-3)	4.94 (15-II-2)
13	3	-0.1 (12-I-2)	-0.0 (2)	-0.1 (14-I-1)	1129.77 (13-I-3)	136.19 (13-I-3)	-11.27 (13-II-2)
13	4	-0.1 (12-I-1)	-0.0 (2)	-0.0 (14-I-1)	1123.81 (13-I-4)	145.57 (13-I-4)	-10.89 (13-II-4)
13	5	-0.2 (9)	-0.0 (14-II-2)	0.0 (12-II-1)	1029.18 (15-I-3)	144.09 (15-II-1)	-5.89 (12-II-1)
13	6	-0.1 (9)	-0.1 (14-I-2)	-0.1 (14-I-1)	987.67 (13-I-3)	108.07 (15-I-3)	7.01 (14-I-1)
13	7	-0.1 (12-I-1)	-0.1 (2)	-0.1 (14-I-1)	987.34 (13-I-3)	108.36 (13-I-3)	10.05 (14-I-1)
13	8	-0.2 (12-I-2)	-0.0 (2)	-0.0 (11)	1030.17 (13-I-4)	144.43 (13-I-4)	-9.86 (13-II-4)
13	9	-0.2 (9)	-0.2 (14-II-2)	0.1 (12-II-1)	1048.61 (15-I-3)	77.88 (15-II-1)	-108.36 (13-I-2)
13	10	-0.1 (9)	-0.1 (2)	-0.1 (14-I-1)	731.37 (13-I-3)	149.19 (13-II-1)	-81.49 (13-I-3)
13	11	-0.1 (12-I-1)	-0.1 (2)	-0.2 (14-I-1)	731.75 (13-I-4)	149.43 (13-I-3)	77.14 (15-I-4)
13	12	-0.4 (12-I-1)	0.2 (12-II-2)	-0.1 (9)	1050.27 (13-I-4)	77.96 (13-II-4)	104.41 (15-I-4)
13	13	1.1 (14-II-4)	-0.1 (2)	-0.2 (14-I-1)	1407.23 (15-I-1)	82.05 (14-I-1)	-682.13 (13-I-2)
13	14	-0.0 (12-II-1)	0.1 (12-II-2)	-0.0 (14-I-1)	142.01 (13-I-3)	188.50 (13-II-1)	-128.04 (13-I-3)
13	15	0.0 (12-I-4)	-0.1 (2)	-0.1 (14-I-1)	142.11 (13-I-4)	188.73 (13-I-3)	124.63 (15-I-4)
13	16	-1.4 (12-I-1)	-0.1 (2)	-0.3 (14-I-1)	1407.96 (13-I-4)	-99.56 (14-I-4)	679.78 (15-I-4)
14	1	0.0 (2)	-0.1 (13-II-1)	-0.0 (13-II-2)	-121.24 (2)	243.65 (13-I-4)	119.53 (13-II-2)
14	2	0.0 (2)	-0.0 (10)	-0.0 (13-II-2)	-93.00 (11)	270.04 (9)	108.09 (13-II-2)
14	3	0.1 (2)	-0.0 (13-II-1)	-0.0 (13-I-2)	-188.17 (2)	262.23 (13-I-4)	126.10 (13-II-2)
14	4	0.0 (2)	-0.0 (10)	-0.0 (13-II-2)	-147.06 (11)	307.47 (9)	88.22 (13-II-2)
14	5	0.1 (2)	-0.0 (13-II-1)	-0.0 (13-II-2)	-249.09 (2)	254.96 (13-I-4)	128.99 (13-II-2)
14	6	0.0 (2)	-0.0 (13-II-1)	-0.0 (13-II-2)	-214.16 (11)	279.31 (9)	87.96 (13-II-2)
14	7	0.1 (2)	-0.0 (13-I-4)	-0.0 (13-II-2)	-328.97 (2)	215.00 (13-I-4)	121.29 (10)
14	8	0.1 (2)	-0.0 (10)	-0.0 (13-II-2)	-317.14 (2)	194.66 (9)	76.68 (10)
15	1	0.0 (11)	-0.1 (4)	0.0 (14-II-1)	105.05 (12-II-2)	317.29 (4)	144.13 (13-II-2)
15	2	0.0 (11)	0.0 (15-I-3)	0.0 (14-II-1)	85.04 (12-II-2)	-305.44 (15-I-3)	126.15 (13-II-2)
15	3	0.0 (11)	-0.0 (4)	-0.0 (13-II-2)	85.57 (12-II-2)	370.53 (4)	88.26 (13-II-2)
15	4	0.0 (11)	0.0 (15-I-3)	-0.0 (13-II-2)	-139.09 (11)	-395.95 (15-I-3)	56.20 (13-II-2)
15	5	0.0 (11)	-0.0 (9)	-0.0 (13-II-2)	-115.87 (2)	358.62 (4)	71.92 (13-II-2)
15	6	0.0 (11)	0.0 (15-I-4)	-0.0 (13-II-2)	-181.69 (11)	-398.78 (15-I-3)	-53.33 (14-II-1)
15	7	0.0 (11)	-0.1 (9)	-0.0 (13-II-2)	-182.65 (11)	284.26 (9)	-63.04 (14-II-1)
15	8	0.0 (11)	0.0 (15-I-4)	-0.0 (13-II-2)	-223.33 (11)	-317.15 (15-I-3)	-75.48 (12-II-1)
16	1	0.0 (11)	-0.0 (9)	0.0 (14-II-1)	-91.15 (2)	278.73 (9)	151.08 (13-II-2)
16	2	0.0 (11)	0.0 (15-I-4)	0.0 (14-II-1)	-127.08 (11)	-303.64 (15-I-4)	122.74 (13-II-2)
16	3	0.0 (11)	-0.0 (9)	-0.0 (13-II-2)	-143.45 (2)	310.37 (9)	101.12 (13-II-2)
16	4	0.1 (11)	0.0 (15-I-4)	-0.0 (13-II-2)	-201.94 (11)	-390.10 (13-I-4)	-66.12 (14-II-1)
16	5	0.1 (11)	-0.0 (9)	-0.0 (13-II-2)	-212.31 (2)	283.36 (9)	86.05 (13-II-2)
16	6	0.1 (11)	0.0 (15-I-4)	-0.0 (13-II-2)	-269.23 (11)	-394.87 (13-I-4)	-78.18 (14-II-1)
16	7	0.1 (11)	-0.0 (9)	-0.0 (13-II-2)	-326.55 (11)	205.19 (9)	-62.34 (12-II-1)
16	8	0.1 (11)	0.1 (15-I-4)	-0.0 (13-II-2)	-355.43 (11)	-324.46 (15-I-4)	-91.11 (12-II-1)
17	1	0.0 (2)	-0.1 (13-II-1)	-0.0 (13-II-2)	86.59 (12-II-2)	247.06 (13-II-1)	85.29 (13-II-2)



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
17	2	0.0(2)	-0.1(10)	-0.0(13-II-2)	109.98(12-II-2)	311.08(4)	84.54(13-II-2)
17	3	0.0(2)	-0.1(13-II-1)	-0.0(13-II-2)	-132.96(2)	261.50(13-II-1)	89.07(13-II-2)
17	4	0.0(2)	-0.0(10)	-0.0(13-II-2)	87.49(12-II-2)	371.41(4)	74.09(13-II-2)
17	5	0.0(2)	-0.1(13-II-1)	-0.0(13-II-2)	-173.17(2)	257.98(13-II-1)	92.70(13-II-2)
17	6	0.0(2)	-0.0(10)	-0.0(13-II-2)	-121.20(11)	359.08(4)	79.50(13-II-2)
17	7	0.0(2)	-0.1(13-II-1)	-0.0(13-II-2)	-213.08(2)	234.82(13-II-1)	101.31(10)
17	8	0.0(2)	-0.1(10)	-0.0(13-II-2)	-179.25(11)	277.12(9)	84.48(10)
18	1	-0.0(12-II-2)	-0.1(13-I-2)	-0.0(9)	50.22(12-I-2)	252.41(13-I-2)	-51.46(4)
18	2	-0.0(12-II-2)	-0.1(10)	-0.0(9)	65.12(12-I-2)	322.75(4)	-54.24(14-II-1)
18	3	-0.0(12-II-2)	-0.1(13-II-1)	-0.0(13-II-2)	69.58(12-II-2)	268.98(13-I-2)	39.39(13-II-2)
18	4	-0.0(12-II-2)	-0.1(10)	-0.0(13-II-2)	104.20(12-II-2)	392.97(4)	37.79(13-II-2)
18	5	-0.0(12-II-2)	-0.1(13-II-1)	-0.0(13-II-2)	73.19(12-II-2)	267.50(13-I-2)	41.06(13-II-2)
18	6	-0.0(12-II-2)	-0.1(10)	-0.0(13-II-2)	118.44(12-II-2)	393.26(4)	42.89(13-II-2)
18	7	-0.0(12-II-2)	-0.1(13-II-1)	-0.0(13-II-2)	83.85(12-II-2)	249.10(13-II-1)	72.58(9)
18	8	-0.0(12-II-2)	-0.1(10)	-0.0(13-II-2)	109.77(12-II-2)	321.96(4)	70.81(9)
19	1	-0.0(12-II-2)	-0.1(4)	0.0(14-II-1)	61.35(12-I-2)	327.63(4)	111.18(13-II-2)
19	2	-0.0(12-II-2)	0.0(15-I-2)	0.0(12-II-1)	49.05(12-I-1)	-304.83(15-I-2)	104.18(13-II-2)
19	3	-0.0(12-II-2)	-0.1(4)	0.0(14-II-1)	102.65(12-I-2)	391.05(4)	52.91(13-II-2)
19	4	-0.0(12-II-2)	-0.0(4)	0.0(14-II-1)	73.33(12-II-2)	-395.96(15-I-2)	42.17(13-II-2)
19	5	-0.0(12-II-2)	-0.1(4)	-0.0(13-II-2)	119.29(12-II-2)	391.33(4)	-39.06(14-II-1)
19	6	-0.0(12-II-2)	-0.0(4)	-0.0(13-II-2)	79.80(12-II-2)	-397.73(15-I-2)	-34.66(14-II-1)
19	7	-0.0(12-II-2)	-0.1(4)	-0.0(13-II-2)	114.40(12-II-2)	327.05(4)	-63.54(12-II-1)
19	8	-0.0(12-II-2)	0.0(15-I-2)	-0.0(13-II-2)	92.50(12-II-2)	-310.44(15-I-3)	-65.25(12-II-1)
20	1	-0.0(12-II-2)	-0.1(13-II-1)	-0.0(9)	99.75(12-II-2)	250.21(13-II-1)	60.54(13-II-2)
20	2	-0.0(12-II-2)	-0.1(10)	-0.0(10)	119.15(12-II-2)	323.57(4)	63.74(13-II-2)
20	3	-0.0(12-II-2)	-0.1(13-II-1)	-0.0(13-II-2)	-81.66(2)	264.69(13-II-1)	61.44(13-II-2)
20	4	-0.0(12-II-2)	-0.1(10)	-0.0(13-II-2)	118.46(12-II-2)	392.16(4)	55.00(13-II-2)
20	5	0.0(2)	-0.1(13-II-1)	-0.0(13-II-2)	-112.24(2)	262.35(13-II-1)	64.24(13-II-2)
20	6	-0.0(12-II-2)	-0.1(10)	-0.0(13-II-2)	101.61(12-II-2)	388.47(4)	60.88(13-II-2)
20	7	0.0(2)	-0.1(13-II-1)	-0.0(13-II-2)	-138.09(2)	243.67(13-II-1)	83.16(9)
20	8	-0.0(12-II-2)	-0.1(10)	-0.0(13-II-2)	-105.10(11)	311.97(4)	77.08(9)
21	1	-0.0(12-II-2)	-0.1(4)	0.0(14-II-1)	115.30(12-II-2)	328.85(4)	129.59(13-II-2)
21	2	-0.0(12-II-2)	0.0(15-I-3)	0.0(12-II-1)	99.72(12-I-2)	-305.24(15-I-3)	118.15(13-II-2)
21	3	-0.0(12-II-2)	-0.0(4)	-0.0(13-II-2)	117.12(12-II-2)	390.32(4)	71.37(13-II-2)
21	4	-0.0(12-II-2)	-0.0(4)	-0.0(13-II-2)	-86.84(11)	-396.97(15-I-3)	52.16(13-II-2)
21	5	-0.0(12-II-2)	-0.0(4)	-0.0(13-II-2)	102.95(12-II-2)	386.72(4)	55.85(13-II-2)
21	6	0.0(11)	-0.0(4)	-0.0(13-II-2)	-118.34(11)	-399.41(15-I-3)	-40.94(14-II-1)
21	7	-0.0(12-II-2)	-0.1(4)	-0.0(13-II-2)	-105.08(11)	317.75(4)	-60.20(12-II-1)
21	8	0.0(11)	0.0(15-I-3)	-0.0(13-II-2)	-143.87(11)	-313.81(15-I-3)	-66.09(12-II-1)
22	1	0.0(2)	0.0(2)	-0.0(13-II-2)	-179.98(2)	8.49(14-II-4)	-6.69(2)
22	2	0.0(2)	0.0(2)	-0.0(13-II-2)	-183.81(2)	-25.74(2)	53.67(13-II-2)
22	3	0.0(2)	0.0(2)	-0.0(13-II-2)	-152.19(2)	15.01(2)	-19.75(15-II-2)
22	4	0.0(2)	0.0(2)	-0.0(13-II-2)	-160.49(2)	-30.01(2)	74.79(13-II-2)
22	5	0.0(2)	0.0(2)	-0.0(13-II-2)	-133.13(2)	14.85(2)	-18.04(15-II-2)
22	6	0.0(2)	0.0(2)	0.0(14-I-1)	-141.52(2)	-30.73(2)	60.48(13-II-2)
22	7	0.0(2)	0.0(2)	-0.0(13-II-2)	-116.26(2)	8.92(2)	-6.63(2)
22	8	0.0(2)	0.0(2)	-0.0(13-II-2)	-119.31(2)	-24.72(2)	48.97(13-II-2)
23	1	0.0(11)	0.0(15-I-3)	-0.0(13-II-2)	93.48(12-II-2)	25.29(15-II-4)	39.02(15-II-2)
23	2	0.0(11)	0.0(15-I-3)	-0.0(13-II-2)	94.38(12-II-2)	-112.88(15-II-2)	63.84(13-II-2)
23	3	0.0(11)	0.0(15-I-3)	-0.0(13-II-2)	85.48(12-II-2)	64.55(15-I-3)	20.86(15-II-2)
23	4	0.0(11)	0.0(15-I-3)	-0.0(13-II-2)	-101.70(11)	-151.94(15-I-3)	58.07(13-II-2)
23	5	0.0(11)	0.0(15-I-3)	-0.0(13-II-2)	-95.96(11)	65.24(15-I-3)	20.47(15-II-2)
23	6	0.0(11)	0.0(15-I-3)	-0.0(13-II-2)	-120.65(11)	-151.46(15-I-3)	65.73(13-II-2)
23	7	0.0(11)	0.0(15-I-3)	-0.0(13-II-2)	-128.02(2)	27.01(15-II-2)	12.65(13-II-2)
23	8	0.0(11)	0.0(15-I-3)	-0.0(13-II-2)	-137.56(11)	-111.83(15-I-3)	46.18(13-II-2)
24	1	0.0(11)	0.0(15-II-4)	-0.0(13-II-2)	-196.12(11)	22.57(11)	60.15(13-II-2)
24	2	0.0(11)	0.0(15-I-4)	-0.0(13-II-2)	-206.82(11)	-122.65(15-I-3)	110.81(13-II-2)
24	3	0.1(11)	0.0(15-I-4)	-0.0(13-II-2)	-206.31(11)	65.72(15-II-4)	37.12(13-II-2)
24	4	0.1(11)	0.0(15-I-4)	-0.0(13-II-2)	-230.98(11)	-164.64(15-I-4)	112.97(13-II-2)
24	5	0.1(11)	0.0(15-II-4)	-0.0(13-II-2)	-227.00(2)	70.19(15-I-3)	40.24(10)
24	6	0.1(11)	0.0(15-II-4)	-0.0(13-II-2)	-251.01(11)	-166.83(15-II-4)	124.01(13-II-2)
24	7	0.1(11)	0.0(15-II-4)	-0.0(13-II-2)	-266.84(2)	30.82(15-II-2)	36.47(13-II-2)
24	8	0.1(11)	0.0(15-II-4)	-0.0(13-II-2)	-272.99(2)	-126.31(15-II-4)	95.97(13-II-2)
25	1	0.1(2)	0.0(2)	-0.0(13-II-2)	-280.87(11)	11.04(14-I-4)	-13.88(9)
25	2	0.1(2)	0.0(2)	0.0(14-I-1)	-280.96(11)	-26.56(2)	58.81(13-II-2)
25	3	0.1(2)	0.0(2)	-0.0(13-II-2)	-234.73(2)	14.82(2)	-27.67(13-II-2)
25	4	0.1(2)	0.0(2)	0.0(14-I-1)	-243.23(2)	-30.57(2)	84.27(13-II-2)
25	5	0.1(2)	0.0(2)	-0.0(13-II-2)	-207.51(2)	14.30(2)	-24.16(13-II-2)
25	6	0.1(2)	0.0(2)	0.0(14-II-1)	-216.60(2)	-31.62(2)	70.67(13-II-2)
25	7	0.0(2)	0.0(2)	-0.0(13-II-2)	-187.05(2)	8.38(2)	-9.11(2)
25	8	0.0(2)	0.0(2)	-0.0(13-II-2)	-191.56(2)	-25.73(2)	56.24(13-II-2)
26	1	0.0(2)	0.0(2)	-0.0(13-II-2)	-116.06(2)	8.22(14-II-1)	-4.82(2)



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
26	2	0.0(2)	0.0(2)	-0.0(13-II-2)	-118.95(2)	-25.35(2)	45.61(13-II-2)
26	3	0.0(2)	0.0(2)	-0.0(13-II-2)	-89.85(2)	14.69(2)	-15.79(15-II-2)
26	4	0.0(2)	0.0(2)	-0.0(13-II-2)	-97.72(2)	-28.92(2)	62.85(13-II-2)
26	5	0.0(2)	0.0(2)	-0.0(13-II-2)	86.52(12-I-2)	14.67(2)	-14.01(15-II-2)
26	6	0.0(2)	0.0(2)	0.0(14-II-1)	84.55(12-I-2)	-29.05(2)	47.92(15-II-2)
26	7	-0.0(12-II-2)	0.0(2)	-0.0(13-II-2)	80.67(12-II-2)	8.96(2)	-5.19(2)
26	8	-0.0(12-II-2)	0.0(2)	-0.0(13-II-2)	82.48(12-II-2)	-23.29(2)	38.85(13-II-2)
27	1	-0.0(12-II-2)	0.0(2)	-0.0(13-II-2)	90.38(12-II-2)	8.78(14-I-1)	-3.23(2)
27	2	-0.0(12-II-2)	0.0(2)	-0.0(13-II-2)	87.94(12-II-2)	-24.06(2)	34.54(15-II-2)
27	3	-0.0(12-II-2)	0.0(2)	-0.0(15-II-2)	85.71(12-II-2)	14.19(2)	-11.24(11)
27	4	-0.0(12-II-2)	0.0(2)	-0.0(13-II-2)	79.25(12-II-2)	-27.09(2)	46.95(15-II-2)
27	5	-0.0(12-II-2)	0.0(2)	0.0(12-II-1)	92.54(12-II-2)	13.98(2)	8.38(12-II-2)
27	6	-0.0(12-II-2)	0.0(2)	0.0(14-I-1)	89.43(12-II-2)	-26.50(2)	-45.52(12-II-1)
27	7	-0.0(12-I-2)	0.0(2)	0.0(12-I-1)	57.51(12-I-1)	8.26(2)	5.65(12-II-2)
27	8	-0.0(12-I-2)	0.0(2)	-0.0(13-II-2)	56.94(12-I-1)	-21.59(2)	-27.48(14-II-1)
28	1	0.0(15-II-2)	-0.0(12-I-2)	-0.0(14-II-1)	-115.71(15-II-2)	56.66(14-I-2)	-43.75(13-II-2)
28	2	0.0(15-II-2)	-0.0(12-II-2)	0.0(13-II-2)	-153.69(15-II-2)	80.16(12-II-2)	-34.47(13-II-2)
28	3	0.0(15-II-2)	-0.0(12-II-2)	0.0(13-II-2)	-151.78(15-II-2)	77.05(12-II-2)	-42.16(13-II-2)
28	4	0.0(15-I-2)	-0.0(12-II-2)	0.0(13-II-2)	-111.59(15-I-3)	-85.11(11)	-25.69(13-II-2)
28	5	0.0(15-II-2)	-0.0(12-II-2)	-0.0(14-II-1)	26.12(15-II-4)	55.38(14-I-2)	-30.44(15-II-2)
28	6	0.0(15-II-2)	-0.0(12-II-2)	0.0(15-I-2)	65.61(15-I-3)	83.58(12-II-2)	-14.50(15-II-2)
28	7	0.0(15-II-2)	-0.0(12-II-2)	0.0(13-II-2)	65.32(15-II-2)	89.38(12-II-2)	-14.41(15-II-2)
28	8	0.0(15-II-2)	-0.0(12-II-2)	0.0(13-II-2)	26.31(15-II-2)	82.66(12-II-2)	13.64(14-II-1)
29	1	0.0(11)	0.0(15-I-3)	-0.0(13-II-2)	-124.89(11)	24.01(15-II-4)	47.58(15-II-2)
29	2	0.0(11)	0.0(15-I-3)	-0.0(13-II-2)	-135.18(11)	-115.96(15-I-3)	85.16(13-II-2)
29	3	0.0(11)	0.0(15-I-3)	-0.0(13-II-2)	-136.62(11)	64.35(15-I-3)	26.89(15-II-2)
29	4	0.0(11)	0.0(15-I-3)	-0.0(13-II-2)	-161.25(11)	-155.18(15-I-3)	82.97(13-II-2)
29	5	0.0(11)	0.0(15-I-3)	-0.0(13-II-2)	-156.24(11)	66.03(15-I-3)	27.06(13-II-2)
29	6	0.0(11)	0.0(15-I-4)	-0.0(13-II-2)	-181.26(11)	-154.22(15-I-3)	91.51(13-II-2)
29	7	0.0(11)	0.0(15-I-3)	-0.0(13-II-2)	-192.75(2)	28.04(15-II-2)	23.32(13-II-2)
29	8	0.0(11)	0.0(15-I-4)	-0.0(13-II-2)	-198.66(2)	-114.16(15-II-4)	69.02(13-II-2)
30	1	-0.0(12-I-2)	-0.0(13-I-2)	-0.0(4)	-49.85(12-I-2)	216.44(13-I-2)	-57.78(12-II-1)
30	2	-0.0(13-I-4)	-0.1(10)	-0.0(4)	21.02(9)	317.26(4)	-59.97(12-II-1)
30	3	0.0(9)	-0.1(13-II-1)	-0.0(4)	-31.97(12-II-3)	253.12(13-I-2)	-18.72(14-II-1)
30	4	-0.0(12-I-2)	-0.1(10)	-0.0(9)	33.37(12-I-2)	383.77(4)	19.63(13-II-2)
30	5	0.0(9)	-0.1(13-II-1)	-0.0(13-II-2)	-35.64(9)	261.78(13-I-2)	21.30(13-II-2)
30	6	-0.0(12-I-2)	-0.1(10)	0.0(14-II-1)	73.11(12-I-2)	388.90(4)	28.40(13-II-2)
30	7	-0.0(12-I-2)	-0.1(13-I-2)	-0.0(13-II-2)	78.41(12-I-2)	250.46(13-I-2)	63.28(4)
30	8	-0.0(12-I-2)	-0.1(10)	0.0(14-II-1)	102.61(12-I-2)	321.59(4)	63.07(4)
31	1	0.0(15-I-2)	-0.1(4)	0.0(13-I-2)	32.80(15-I-4)	320.89(4)	76.59(13-I-4)
31	2	-0.0(12-I-2)	0.0(15-I-2)	0.0(12-II-1)	-52.84(12-I-2)	-254.19(15-I-2)	64.55(10)
31	3	-0.0(12-I-2)	-0.1(4)	0.0(14-II-1)	35.91(10)	379.10(4)	36.35(13-II-2)
31	4	0.0(15-I-2)	-0.0(4)	0.0(12-II-1)	-40.43(13-I-2)	-365.57(15-I-2)	24.92(13-II-2)
31	5	-0.0(12-I-2)	-0.1(4)	-0.0(13-II-2)	72.43(12-I-2)	385.48(4)	-51.12(14-II-1)
31	6	0.0(15-I-2)	-0.0(4)	-0.0(13-II-2)	-51.51(15-I-2)	-383.38(15-I-2)	-35.65(14-II-1)
31	7	-0.0(12-I-2)	-0.1(4)	-0.0(13-II-2)	104.71(12-I-2)	325.99(4)	-80.55(12-II-1)
31	8	-0.0(12-I-2)	0.0(15-I-2)	-0.0(13-II-2)	80.77(12-I-2)	-304.43(15-I-2)	-82.43(12-II-1)
32	1	0.0(14-I-2)	-0.0(13-I-2)	-0.0(12-I-3)	-3.32(12-II-2)	176.46(13-I-2)	-21.86(4)
32	2	-0.0(12-I-2)	-0.1(10)	-0.0(12-II-3)	3.00(4)	268.93(4)	-20.73(12-I-3)
32	3	0.0(14-II-3)	-0.0(13-I-2)	0.0(15-I-2)	-6.77(14-II-3)	185.25(13-I-2)	34.48(12-II-3)
32	4	-0.0(12-II-2)	-0.1(10)	0.0(12-II-1)	6.94(12-I-2)	267.32(4)	29.61(4)
33	1	0.0(15-I-2)	0.0(15-I-2)	0.0(15-I-2)	-4.84(10)	-4.31(13-I-2)	-4.60(13-II-2)
33	2	0.0(12-I-1)	0.0(15-I-2)	0.0(13-I-2)	-12.41(12-I-1)	-43.25(15-I-2)	-31.21(13-I-2)
33	3	0.0(13-II-2)	0.0(15-I-2)	0.0(13-I-2)	1.56(2)	-7.93(13-I-2)	-7.75(15-I-2)
33	4	-0.0(15-I-2)	0.0(15-I-2)	0.0(10)	3.34(15-I-2)	-62.66(15-I-2)	-13.00(14-I-2)
34	1	0.0(15-II-2)	0.0(11)	-0.0(15-I-2)	-90.52(15-II-2)	-38.03(12-I-3)	-23.76(14-II-3)
34	2	0.0(15-II-2)	0.0(9)	-0.0(14-II-1)	-156.41(15-II-2)	-33.64(13-II-2)	-7.40(9)
34	3	0.0(15-II-2)	0.0(9)	-0.0(14-II-1)	-162.43(15-II-2)	-42.13(15-II-2)	-14.13(13-II-2)
34	4	0.0(15-II-2)	-0.0(12-I-2)	0.0(13-II-2)	-119.69(15-II-2)	68.86(12-I-2)	27.81(14-II-1)
34	5	0.0(15-II-2)	-0.0(12-I-2)	-0.0(15-II-4)	27.94(15-I-3)	18.32(15-I-2)	-18.56(15-II-2)
34	6	0.0(15-II-2)	0.0(9)	-0.0(15-I-2)	62.93(15-II-2)	10.10(14-II-1)	17.24(12-I-2)
34	7	0.0(15-II-2)	-0.0(12-I-2)	0.0(13-II-2)	66.49(15-II-2)	36.98(14-I-2)	26.90(12-I-2)
34	8	0.0(15-II-2)	-0.0(12-I-2)	0.0(13-II-2)	26.02(15-II-2)	73.65(12-I-2)	29.64(14-II-1)
35	1	0.0(14-II-3)	0.0(13-I-2)	0.0(9)	-63.95(14-II-2)	-4.17(13-I-2)	-14.31(14-II-2)
35	2	0.0(14-II-3)	0.0(10)	0.0(12-II-3)	-57.91(14-II-3)	-9.17(13-II-2)	19.55(15-I-2)
35	3	0.0(14-II-2)	-0.0(15-II-2)	-0.0(15-II-2)	3.39(13-I-2)	1.32(11)	-7.68(14-I-2)
35	4	0.0(14-II-3)	-0.0(14-II-1)	-0.0(13-I-2)	-2.78(14-II-3)	2.80(15-II-2)	12.28(14-I-2)
36	1	-0.0(12-I-1)	0.0(14-II-1)	0.0(14-II-1)	69.50(12-I-2)	11.04(14-II-1)	13.55(12-II-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
36	2	-0.0(12-I-1)	0.0(14-I-1)	-0.0(13-II-2)	65.69(12-I-2)	-22.38(2)	-27.65(12-II-1)
36	3	0.0(9)	0.0(14-II-1)	0.0(12-II-1)	-23.97(9)	17.20(14-II-1)	28.38(12-I-2)
36	4	0.0(9)	0.0(14-I-1)	-0.0(13-II-2)	-27.19(9)	-35.56(14-II-1)	-40.99(12-II-1)
36	5	0.0(11)	-0.0(13-II-2)	0.0(12-I-2)	-23.23(10)	22.90(14-II-1)	19.88(12-I-2)
36	6	0.0(9)	-0.0(13-II-2)	0.0(14-II-1)	-33.13(14-II-1)	-44.86(14-II-1)	-32.12(12-II-1)
36	7	0.0(10)	0.0(14-I-2)	0.0(13-I-2)	-22.88(12-II-1)	11.52(14-II-2)	-12.12(15-I-4)
36	8	0.0(12-II-1)	0.0(14-I-2)	0.0(13-I-2)	-41.72(12-II-1)	-38.50(14-I-2)	-29.75(12-II-1)
37	1	0.0(2)	0.0(15-II-4)	0.0(2)	-29.59(15-II-2)	6.49(2)	37.61(2)
37	2	0.0(11)	0.0(15-I-4)	-0.0(15-II-2)	-49.49(15-II-2)	-16.73(15-I-4)	-75.65(2)
37	3	0.0(11)	0.0(15-I-4)	-0.0(13-I-4)	-232.96(2)	-4.69(9)	51.85(11)
37	4	0.0(11)	0.0(15-I-4)	-0.0(15-I-4)	-221.78(2)	-31.81(15-I-4)	75.26(13-I-4)
38	1	0.0(2)	0.0(2)	0.0(13-I-2)	-46.02(2)	-223.72(11)	-113.78(13-I-3)
38	2	-0.0(13-I-4)	0.0(2)	0.0(13-II-2)	29.15(13-I-4)	48.01(13-II-2)	-84.26(13-I-3)
38	3	0.0(2)	0.0(2)	0.0(13-I-1)	5.97(15-I-1)	-228.42(11)	-36.96(13-I-2)
38	4	-0.0(13-I-4)	0.0(2)	0.0(13-I-3)	25.74(15-II-4)	42.99(13-II-2)	38.62(2)
39	1	-0.0(10)	0.0(2)	0.0(13-II-2)	84.66(9)	-251.88(2)	-99.40(13-II-2)
39	2	-0.0(10)	0.0(2)	0.0(13-II-2)	84.91(9)	-9.88(12-II-3)	-66.37(13-II-2)
39	3	-0.0(13-I-4)	0.0(2)	0.0(13-II-2)	77.65(13-I-4)	-248.26(2)	-127.87(13-II-2)
39	4	-0.0(13-I-4)	0.0(2)	0.0(13-II-2)	63.45(13-I-4)	19.48(15-II-2)	-61.56(13-II-2)
40	1	0.0(15-I-4)	0.0(11)	-0.0(2)	-134.57(15-I-4)	-280.45(11)	-80.49(13-I-1)
40	2	-0.0(9)	0.0(11)	-0.0(2)	-51.07(13-I-4)	15.75(2)	-45.74(15-I-1)
40	3	-0.0(9)	0.0(11)	0.0(13-II-2)	93.23(9)	-269.71(11)	-60.77(13-II-2)
40	4	-0.0(9)	0.0(11)	0.0(13-II-2)	91.78(9)	13.06(11)	56.62(2)
41	1	-0.1(9)	-0.0(14-I-2)	-0.0(12-II-4)	1126.59(13-I-4)	146.04(13-I-4)	5.41(15-II-4)
41	2	-0.1(9)	-0.0(14-I-2)	-0.1(12-II-4)	1137.53(13-I-4)	137.39(13-I-4)	6.37(15-II-4)
41	3	-0.1(12-II-1)	-0.0(2)	-0.1(12-II-4)	1142.48(13-I-4)	138.08(13-I-4)	-9.66(13-I-4)
41	4	-0.1(12-I-1)	-0.0(2)	-0.0(12-II-4)	1142.27(13-I-4)	148.21(13-I-4)	-8.52(13-II-2)
41	5	-0.2(9)	-0.1(14-I-2)	0.0(14-I-4)	1032.29(13-I-4)	145.11(13-I-4)	6.74(15-II-4)
41	6	-0.1(9)	-0.1(14-I-2)	-0.1(12-II-4)	993.95(13-I-4)	110.02(13-I-4)	6.53(14-I-4)
41	7	-0.1(12-II-1)	-0.1(2)	-0.1(12-II-4)	997.93(13-I-4)	110.96(13-I-4)	8.91(14-II-4)
41	8	-0.2(12-II-4)	-0.0(2)	0.0(14-I-4)	1044.64(13-I-4)	147.94(13-I-4)	-5.49(12-I-4)
41	9	-0.2(9)	-0.2(14-I-2)	0.1(14-I-4)	1051.63(13-I-4)	79.01(13-II-4)	-105.78(13-I-3)
41	10	-0.1(9)	-0.1(2)	-0.1(12-II-4)	735.79(13-I-4)	152.00(13-I-4)	-77.91(13-I-4)
41	11	-0.1(12-I-4)	-0.1(14-II-1)	-0.2(12-II-4)	738.09(13-I-4)	153.63(13-I-3)	83.69(15-II-4)
41	12	-0.4(12-II-4)	0.2(12-I-2)	0.1(14-I-4)	1059.26(13-I-4)	83.87(13-II-4)	112.83(15-II-4)
41	13	1.1(14-II-4)	-0.2(2)	-0.2(12-II-4)	1408.24(13-I-4)	81.01(12-II-4)	-679.04(13-I-1)
41	14	-0.0(14-I-4)	-0.1(2)	-0.0(12-II-4)	143.06(13-I-4)	191.97(13-I-4)	-124.36(13-I-4)
41	15	0.0(14-I-4)	-0.1(14-I-4)	-0.1(12-II-4)	143.69(13-I-4)	194.31(13-I-3)	130.69(15-II-4)
41	16	-1.4(12-II-4)	-0.2(14-II-4)	-0.3(12-II-4)	1411.95(13-II-4)	-103.33(14-II-4)	687.96(15-II-4)
42	1	-0.0(14-I-2)	-0.1(9)	-0.0(12-II-4)	-179.78(15-I-3)	-1378.17(15-I-4)	-6.50(15-II-4)
42	2	-0.1(14-I-2)	-0.2(9)	0.0(14-I-4)	-185.72(15-I-3)	-1292.77(15-I-3)	-8.80(15-II-4)
42	3	-0.2(14-I-2)	-0.2(9)	0.1(14-I-4)	-107.23(15-II-4)	-1358.80(15-I-3)	135.81(13-II-1)
42	4	-0.1(11)	1.1(14-II-4)	-0.2(12-II-4)	80.76(12-II-4)	-1881.16(15-I-3)	906.17(13-I-3)
42	5	-0.0(14-II-3)	-0.1(9)	-0.1(12-II-4)	-166.93(15-I-4)	-1393.91(15-I-4)	-7.11(15-II-4)
42	6	-0.1(14-II-3)	-0.1(9)	-0.1(12-II-4)	-132.59(15-I-4)	-1242.85(15-I-4)	-7.12(15-II-4)
42	7	-0.1(11)	-0.1(9)	-0.1(12-II-4)	-187.47(15-I-3)	-939.00(15-I-3)	100.23(13-I-4)
42	8	-0.1(11)	-0.0(14-I-4)	-0.0(12-II-4)	-237.80(15-I-3)	-180.81(13-I-3)	161.52(13-I-4)
42	9	-0.0(11)	-0.1(12-II-3)	-0.1(12-II-4)	-167.89(13-I-4)	-1400.12(13-I-4)	15.21(13-I-4)
42	10	-0.1(11)	-0.1(12-II-3)	-0.1(12-II-4)	-133.88(13-I-3)	-1247.18(13-I-4)	8.53(13-I-4)
42	11	-0.1(14-II-3)	-0.1(12-I-4)	-0.2(12-II-4)	-189.35(13-I-3)	-941.05(13-I-4)	-102.47(15-II-4)
42	12	-0.1(14-I-4)	0.0(14-I-4)	-0.1(12-II-4)	-240.20(13-I-3)	-181.34(13-I-4)	-164.85(15-II-4)
42	13	-0.0(11)	-0.1(12-I-3)	-0.0(12-II-4)	-182.53(13-I-4)	-1396.93(13-I-4)	13.98(13-II-2)
42	14	-0.0(11)	-0.2(12-I-3)	0.0(14-I-4)	-189.18(13-I-3)	-1305.62(13-I-4)	9.29(10)
42	15	0.2(12-I-2)	-0.4(12-II-4)	0.1(14-I-4)	-112.46(13-II-4)	-1365.46(13-I-4)	-139.11(15-II-4)
42	16	-0.1(14-II-4)	-1.4(12-II-4)	-0.3(12-II-4)	-102.87(12-II-4)	-1883.96(13-II-4)	-911.53(15-II-4)
43	1	-0.1(9)	-0.0(14-II-1)	0.0(2)	1152.03(13-I-4)	149.16(13-I-4)	7.87(15-II-4)
43	2	-0.1(9)	-0.0(2)	0.1(2)	1171.45(13-I-4)	140.85(13-I-4)	7.72(15-II-4)
43	3	-0.1(9)	-0.1(9)	0.0(2)	1182.05(13-I-4)	137.94(13-I-4)	-15.11(13-I-4)
43	4	-0.3(9)	-0.1(2)	0.1(2)	1181.26(13-I-4)	96.68(13-I-4)	-56.50(13-I-4)
43	5	-0.1(9)	-0.0(14-II-2)	0.1(2)	1052.54(13-I-4)	148.55(13-I-4)	14.32(15-II-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
43	6	-0.1 (9)	-0.1 (2)	0.1 (9)	1021.91 (13-I-4)	111.07 (13-I-4)	13.49 (15-II-4)
43	7	-0.1 (2)	-0.1 (9)	0.0 (2)	1041.39 (13-I-4)	106.78 (13-I-4)	11.93 (9)
43	8	-0.3 (9)	-0.0 (9)	0.0 (14-I-4)	1097.07 (13-I-4)	51.31 (13-I-4)	14.75 (9)
43	9	-0.2 (9)	-0.2 (14-II-2)	0.1 (14-I-4)	1064.43 (13-I-4)	84.33 (13-II-4)	-94.10 (13-I-4)
43	10	0.0 (14-I-4)	-0.1 (2)	-0.1 (12-II-4)	755.80 (13-I-4)	154.44 (13-I-4)	-63.39 (13-I-4)
43	11	-0.1 (14-II-4)	-0.1 (9)	-0.1 (12-II-4)	777.39 (13-I-4)	148.84 (13-I-4)	105.10 (15-II-4)
43	12	-0.3 (9)	0.2 (12-I-4)	0.1 (14-I-4)	1152.48 (13-I-4)	120.10 (13-I-4)	202.58 (15-I-4)
43	13	1.1 (14-I-4)	-0.1 (2)	-0.2 (12-II-4)	1412.41 (13-II-4)	69.69 (12-I-4)	-669.99 (13-I-4)
43	14	-0.0 (14-I-4)	0.0 (9)	-0.1 (12-II-4)	151.71 (13-I-4)	197.06 (13-I-4)	-108.13 (13-I-4)
43	15	0.0 (14-I-4)	-0.2 (14-II-4)	-0.1 (12-II-4)	137.11 (13-I-4)	191.50 (13-I-4)	158.90 (15-II-4)
43	16	-0.9 (14-II-4)	0.2 (12-I-4)	-0.1 (12-II-4)	1600.82 (13-II-4)	-98.31 (14-II-4)	705.82 (15-II-4)
44	1	-0.0 (14-II-3)	-0.1 (9)	0.0 (11)	-183.45 (13-I-4)	-1407.80 (13-I-4)	-8.68 (15-II-4)
44	2	-0.0 (14-II-3)	-0.1 (9)	0.1 (11)	-189.14 (13-I-4)	-1313.57 (13-I-4)	-16.13 (15-II-4)
44	3	-0.2 (14-II-2)	-0.2 (9)	0.1 (14-I-4)	-111.81 (13-II-4)	-1370.18 (13-I-4)	124.62 (13-I-4)
44	4	-0.1 (11)	1.1 (14-I-4)	-0.2 (12-II-4)	70.39 (14-I-4)	-1884.26 (13-II-4)	897.27 (13-I-3)
44	5	-0.0 (11)	-0.1 (9)	0.1 (11)	-170.33 (13-I-4)	-1431.98 (13-I-4)	-7.90 (15-II-4)
44	6	-0.1 (11)	-0.1 (9)	0.1 (9)	-131.40 (13-I-4)	-1270.85 (13-I-4)	-13.10 (15-II-4)
44	7	-0.1 (11)	0.0 (14-I-4)	-0.1 (12-II-4)	-185.55 (13-I-4)	-957.72 (13-I-4)	87.39 (13-I-4)
44	8	0.0 (9)	-0.0 (14-I-4)	-0.1 (12-II-4)	-237.27 (13-I-4)	-189.33 (13-I-4)	146.50 (13-I-4)
44	9	-0.0 (9)	-0.1 (9)	0.0 (11)	-164.83 (13-I-4)	-1438.67 (13-I-4)	23.75 (13-I-4)
44	10	-0.1 (9)	-0.1 (11)	0.0 (11)	-122.58 (13-I-4)	-1289.72 (13-I-4)	15.44 (13-I-4)
44	11	-0.1 (9)	-0.1 (14-II-4)	-0.1 (12-II-4)	-172.71 (13-I-4)	-978.69 (13-I-4)	-118.58 (15-II-4)
44	12	-0.2 (14-II-4)	0.0 (14-I-4)	-0.1 (12-II-4)	-222.95 (13-I-4)	-170.77 (13-I-4)	-189.13 (15-II-4)
44	13	-0.0 (2)	-0.3 (9)	0.1 (2)	-114.47 (13-I-4)	-1423.87 (13-I-4)	77.27 (13-I-4)
44	14	-0.0 (9)	-0.3 (9)	0.0 (14-I-4)	-60.59 (13-I-4)	-1355.31 (13-I-4)	14.99 (9)
44	15	0.2 (12-I-4)	-0.3 (9)	0.1 (14-I-4)	-148.13 (13-I-4)	-1461.19 (13-I-4)	-239.41 (15-I-4)
44	16	0.2 (12-I-4)	-0.9 (14-II-4)	-0.1 (12-II-4)	-97.44 (12-II-4)	-2078.26 (13-II-4)	-896.51 (15-II-4)
45	1	-0.0 (9)	0.0 (2)	0.0 (13-II-2)	53.85 (9)	-31.80 (2)	-67.98 (13-II-2)
45	2	-0.0 (9)	0.0 (2)	0.0 (13-II-2)	60.03 (9)	13.02 (2)	-7.33 (9)
45	3	-0.0 (13-I-4)	0.0 (2)	0.0 (13-II-2)	54.81 (13-I-3)	-30.38 (2)	-63.37 (13-II-2)
45	4	-0.0 (13-I-4)	0.0 (2)	0.0 (13-II-2)	53.72 (13-I-3)	11.30 (11)	-7.97 (9)
46	1	-0.0 (9)	0.0 (15-II-2)	-0.0 (2)	31.21 (2)	-32.12 (11)	-36.06 (13-II-2)
46	2	-0.0 (9)	0.0 (15-II-2)	-0.0 (2)	33.56 (2)	12.16 (2)	9.34 (9)
46	3	-0.0 (9)	0.0 (11)	0.0 (13-II-2)	56.89 (9)	-35.18 (11)	-52.21 (13-II-2)
46	4	-0.0 (9)	0.0 (11)	0.0 (13-II-2)	62.36 (9)	12.86 (11)	8.41 (9)
47	1	0.0 (2)	0.0 (14-II-4)	0.0 (2)	7.91 (2)	2.06 (2)	4.64 (2)
47	2	0.0 (2)	-0.0 (9)	0.0 (2)	8.60 (2)	4.97 (9)	-8.45 (2)
47	3	0.0 (9)	-0.0 (9)	0.0 (2)	-19.38 (2)	-1.17 (13-II-2)	2.27 (9)
47	4	0.0 (13-II-2)	-0.0 (2)	0.0 (2)	-16.12 (11)	9.08 (9)	-22.55 (2)
48	1	-0.0 (13-I-3)	0.0 (2)	0.0 (13-II-2)	24.21 (13-I-4)	-22.73 (2)	-39.17 (13-II-2)
48	2	-0.0 (13-I-4)	0.0 (2)	0.0 (13-II-2)	18.12 (13-I-4)	9.34 (11)	-11.26 (13-I-3)
48	3	-0.0 (13-I-4)	0.0 (2)	0.0 (13-II-2)	11.01 (13-II-2)	-22.98 (2)	-13.93 (13-II-2)
48	4	-0.0 (13-I-4)	0.0 (11)	0.0 (13-II-2)	10.09 (13-II-2)	9.69 (11)	3.01 (2)

**Risultati Analisi Dinamica - Sollecitazioni massime per combinazione - Sigma terreno platea - S.L.E**  
Scenario di calcolo: ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO

Combinazione	Muro	Nodi	SigmaMax daN/cm <sup>2</sup>	SigmaMin daN/cm <sup>2</sup>
16	47	1-2-12-11	0.26	0.24
17	47	1-2-12-11	0.28	0.21
18	48	32-42-41-31	0.27	0.23
19	47	1-2-12-11	0.29	0.21
20	47	1-2-12-11	0.29	0.22
21	47	1-2-12-11	0.26	0.24
22	33	9-10-20-19	0.23	0.21
23	47	1-2-12-11	0.27	0.21
24	47	1-2-12-11	0.28	0.21

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
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Combinazione	Muro	Nodi	SigmaMax	SigmaMin
25	47	1-2-12-11	0.28	0.21
26	47	1-2-12-11	0.27	0.22
27	33	9-10-20-19	0.26	0.18
28	1	3-4-14-13	0.27	0.21
29-I-1	33	9-10-20-19	0.28	0.20
29-II-1	33	9-10-20-19	0.28	0.20
29-I-2	33	9-10-20-19	0.28	0.20
29-II-2	33	9-10-20-19	0.28	0.20
29-I-3	36	8-9-19-18	0.28	0.20
29-II-3	33	9-10-20-19	0.28	0.20
29-I-4	33	9-10-20-19	0.28	0.20
29-II-4	33	9-10-20-19	0.28	0.20
30-I-1	3	34-44-43-33	0.27	0.21
30-II-1	3	34-44-43-33	0.26	0.22
30-I-2	3	34-44-43-33	0.26	0.22
30-II-2	3	34-44-43-33	0.27	0.21
30-I-3	3	34-44-43-33	0.27	0.21
30-II-3	3	34-44-43-33	0.26	0.22
30-I-4	3	34-44-43-33	0.26	0.22
30-II-4	3	34-44-43-33	0.27	0.21
31-I-1	33	9-10-20-19	0.28	0.16
31-II-1	33	9-10-20-19	0.28	0.16
31-I-2	33	9-10-20-19	0.28	0.16
31-II-2	33	9-10-20-19	0.28	0.16
31-I-3	33	9-10-20-19	0.28	0.16
31-II-3	33	9-10-20-19	0.28	0.16
31-I-4	33	9-10-20-19	0.28	0.16
31-II-4	33	9-10-20-19	0.28	0.16
32-I-1	35	40-50-49-39	0.24	0.20
32-II-1	35	40-50-49-39	0.23	0.21
32-I-2	35	40-50-49-39	0.23	0.21
32-II-2	35	40-50-49-39	0.24	0.20
32-I-3	35	40-50-49-39	0.24	0.20
32-II-3	35	40-50-49-39	0.23	0.21
32-I-4	35	40-50-49-39	0.23	0.21
32-II-4	35	40-50-49-39	0.24	0.20
Assoluti				
20	47	1-2-12-11	0.29	
31-I-4	33	9-10-20-19		0.16

**Risultati Analisi Dinamica - Spostamenti massimi - Nodi - S.I.E.**  
Scenario di calcolo: **ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	mm	mm	mm	°	°	°
1	0.00 (16)	0.00 (16)	-1.44 (20)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
2	0.00 (16)	0.00 (16)	-1.43 (20)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
3	0.00 (16)	0.00 (16)	-1.42 (20)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
4	0.00 (16)	0.00 (16)	-1.41 (20)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
5	0.00 (16)	0.00 (16)	-1.39 (20)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
6	0.00 (16)	0.00 (16)	-1.37 (20)	0.01 (31-I-2)	0.00 (31-I-4)	0.00 (16)
7	0.00 (16)	0.00 (16)	-1.37 (29-I-3)	0.01 (31-I-2)	0.00 (31-II-4)	0.00 (16)
8	0.00 (16)	0.00 (16)	-1.38 (31-I-3)	0.01 (31-I-2)	0.00 (31-II-4)	0.00 (16)
9	0.00 (16)	0.00 (16)	-1.42 (31-II-4)	0.01 (31-I-2)	0.00 (31-II-4)	0.00 (16)
10	0.00 (16)	0.00 (16)	-1.42 (31-II-4)	0.01 (31-I-2)	0.00 (31-II-4)	0.00 (16)
11	0.00 (16)	0.00 (16)	-1.42 (20)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
12	0.00 (16)	0.00 (16)	-1.41 (20)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
13	0.00 (16)	0.00 (16)	-1.40 (20)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
14	0.00 (16)	0.00 (16)	-1.39 (20)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
15	0.00 (16)	0.00 (16)	-1.37 (20)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
16	0.00 (16)	0.00 (16)	-1.35 (20)	0.01 (31-I-2)	0.00 (31-I-4)	0.00 (16)
17	0.00 (16)	0.00 (16)	-1.34 (29-I-3)	0.01 (31-I-2)	0.00 (31-II-4)	0.00 (16)
18	0.00 (16)	0.00 (16)	-1.36 (29-I-3)	0.01 (31-I-2)	0.00 (31-II-4)	0.00 (16)
19	0.00 (16)	0.00 (16)	-1.39 (31-II-3)	0.01 (31-I-2)	0.00 (31-II-4)	0.00 (16)
20	0.00 (16)	0.00 (16)	-1.39 (31-II-4)	0.01 (31-I-2)	0.00 (31-II-4)	0.00 (16)
21	0.00 (16)	0.00 (16)	-1.34 (20)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
22	0.00 (16)	0.00 (16)	-1.33 (20)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
23	0.00 (16)	0.00 (16)	-1.32 (20)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
24	0.00 (16)	0.00 (16)	-1.31 (20)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
25	0.00 (16)	0.00 (16)	-1.28 (20)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
26	0.00 (16)	0.00 (16)	-1.26 (20)	0.01 (31-II-1)	0.00 (31-I-4)	0.00 (16)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
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Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
27	0.00 (16)	0.00 (16)	-1.25 (29-I-2)	0.01 (31-I-2)	0.00 (31-II-4)	0.00 (16)
28	0.00 (16)	0.00 (16)	-1.27 (29-II-2)	0.01 (31-II-2)	0.00 (31-II-4)	0.00 (16)
29	0.00 (16)	0.00 (16)	-1.28 (29-II-2)	0.01 (31-II-2)	0.00 (31-II-4)	0.00 (16)
30	0.00 (16)	0.00 (16)	-1.29 (29-II-2)	0.01 (31-II-2)	0.00 (31-II-4)	0.00 (16)
31	0.00 (16)	0.00 (16)	-1.32 (18)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
32	0.00 (16)	0.00 (16)	-1.32 (18)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
33	0.00 (16)	0.00 (16)	-1.31 (18)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
34	0.00 (16)	0.00 (16)	-1.30 (18)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
35	0.00 (16)	0.00 (16)	-1.29 (18)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
36	0.00 (16)	0.00 (16)	-1.28 (18)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
37	0.00 (16)	0.00 (16)	-1.26 (18)	0.01 (31-II-2)	0.00 (31-II-4)	0.00 (16)
38	0.00 (16)	0.00 (16)	-1.24 (30-I-3)	0.01 (31-II-2)	0.00 (31-II-4)	0.00 (16)
39	0.00 (16)	0.00 (16)	-1.23 (30-I-3)	0.01 (31-II-2)	0.00 (31-II-4)	0.00 (16)
40	0.00 (16)	0.00 (16)	-1.23 (30-I-3)	0.01 (31-II-2)	0.00 (31-II-4)	0.00 (16)
41	0.00 (16)	0.00 (16)	-1.34 (18)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
42	0.00 (16)	0.00 (16)	-1.34 (18)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
43	0.00 (16)	0.00 (16)	-1.34 (18)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
44	0.00 (16)	0.00 (16)	-1.33 (30-I-3)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
45	0.00 (16)	0.00 (16)	-1.32 (30-I-3)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
46	0.00 (16)	0.00 (16)	-1.31 (30-I-3)	0.01 (31-I-1)	0.00 (31-I-4)	0.00 (16)
47	0.00 (16)	0.00 (16)	-1.30 (30-I-3)	0.01 (31-II-2)	0.00 (31-II-4)	0.00 (16)
48	0.00 (16)	0.00 (16)	-1.29 (30-I-3)	0.01 (31-II-2)	0.00 (31-II-4)	0.00 (16)
49	0.00 (16)	0.00 (16)	-1.28 (30-I-3)	0.01 (31-II-2)	0.00 (31-II-4)	0.00 (16)
50	0.00 (16)	0.00 (16)	-1.28 (30-I-3)	0.01 (31-II-2)	0.00 (31-II-4)	0.00 (16)
113	0.04 (31-II-4)	0.10 (30-I-4)	-1.42 (20)	-0.01 (30-I-4)	0.01 (31-I-4)	-0.00 (19)
114	0.04 (31-II-4)	0.10 (30-I-4)	-1.40 (20)	-0.01 (30-I-4)	0.01 (31-II-4)	0.00 (29-I-4)
115	0.04 (31-II-4)	0.10 (30-I-4)	-1.38 (20)	-0.01 (30-I-4)	0.01 (31-II-4)	0.00 (29-II-4)
116	0.04 (31-I-4)	0.11 (30-I-3)	-1.36 (20)	-0.01 (30-I-4)	0.01 (31-I-4)	0.00 (29-I-1)
117	0.03 (31-II-4)	0.11 (30-I-2)	-1.35 (29-I-3)	-0.01 (30-I-2)	0.01 (31-II-4)	0.00 (29-I-2)
118	0.04 (31-II-4)	0.11 (30-I-2)	-1.37 (29-I-3)	-0.01 (30-I-2)	0.01 (31-II-4)	0.00 (29-I-2)
119	0.05 (31-I-4)	0.11 (30-I-2)	-1.42 (31-I-3)	-0.01 (30-I-2)	0.02 (31-II-2)	0.00 (29-I-2)
133	0.04 (31-II-4)	0.15 (30-I-4)	-1.35 (18)	-0.02 (30-I-4)	0.01 (31-I-4)	0.00 (30-II-4)
134	0.04 (31-II-4)	0.15 (30-I-3)	-1.34 (18)	-0.02 (30-I-3)	0.01 (31-II-4)	-0.00 (31-II-4)
135	0.04 (31-II-4)	0.15 (30-I-3)	-1.32 (18)	-0.02 (30-I-3)	0.01 (31-II-4)	-0.00 (31-II-4)
136	0.03 (31-I-4)	0.15 (30-I-3)	-1.31 (18)	-0.02 (30-I-3)	0.01 (31-I-4)	-0.00 (31-I-3)
137	0.03 (31-II-4)	0.15 (30-I-3)	-1.29 (30-I-3)	-0.02 (30-I-3)	0.01 (31-II-4)	-0.00 (31-I-2)
138	0.03 (31-II-4)	0.15 (30-I-3)	-1.28 (30-I-3)	-0.02 (30-I-3)	0.01 (31-II-4)	-0.00 (31-I-2)
139	0.05 (31-I-4)	0.15 (30-I-3)	-1.27 (30-I-3)	-0.02 (30-I-3)	0.02 (31-II-2)	-0.00 (32-II-2)

**Risultati Analisi Dinamica - Reazioni massime - Nodi - S.L.E**  
Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

Nodo	Rx	Ry	Rz	Mx	My	Mz
	daN	daN	daN	daN*m	daN*m	daN*m
1	-3.82 (27)	-1.80 (27)	0	0	0	0
2	-72.41 (27)	-12.97 (27)	0	0	0	0
3	-129.94 (27)	-6.06 (27)	0	0	0	2.28 (32-I-4)
4	45.27 (30-II-2)	-9.15 (31-I-4)	0	0	0	0
5	39.09 (30-II-2)	-9.51 (31-I-2)	0	0	0	0
6	34.85 (32-II-2)	-9.70 (31-II-2)	0	0	0	0
7	28.65 (32-II-2)	-9.90 (31-I-3)	0	0	0	0
8	-24.19 (29-II-2)	-10.60 (31-I-1)	0	0	0	0
9	5.30 (19)	-7.54 (31-II-1)	0	0	0	0
10	0	-1.24 (32-I-2)	0	0	0	0
11	-18.38 (27)	-17.13 (31-II-4)	0	0	0	2.16 (32-I-4)
12	-280.26 (27)	39.73 (30-II-2)	0	0	0	23.51 (32-I-4)
13	-435.03 (27)	109.56 (19)	0	0	0	18.23 (27)
14	299.41 (32-II-2)	247.63 (19)	0	0	0	-30.17 (19)
15	144.04 (32-II-2)	312.23 (20)	0	0	0	-13.01 (32-II-2)
16	80.91 (32-II-2)	340.54 (17)	0	0	0	-5.86 (32-II-2)
17	-77.37 (29-I-1)	346.50 (17)	0	0	0	5.68 (29-I-1)
18	-149.96 (29-I-2)	366.94 (29-I-1)	0	0	0	11.79 (29-I-2)
19	-50.27 (29-I-2)	176.27 (29-I-2)	0	0	0	11.04 (32-I-2)
20	0	49.12 (29-II-1)	0	0	0	-1.21 (30-I-2)
21	-30.58 (27)	63.00 (30-II-2)	0	0	0	0
22	-406.37 (32-I-1)	139.80 (30-I-2)	0	0	0	-2.69 (31-I-1)
23	-519.89 (32-II-1)	237.78 (30-I-4)	0	0	0	-9.85 (30-I-4)
24	447.72 (19)	275.75 (30-I-4)	0	0	0	0
25	306.77 (31-II-4)	279.70 (30-I-4)	0	0	0	1.79 (30-II-2)
26	216.10 (31-II-3)	277.81 (30-I-3)	0	0	0	1.37 (30-II-2)
27	129.87 (32-I-1)	279.41 (30-I-2)	0	0	0	0
28	66.49 (32-II-1)	269.87 (30-I-2)	0	0	0	2.00 (30-II-2)
29	38.40 (19)	124.37 (30-I-2)	0	0	0	-2.28 (30-II-2)

Nodo	Rx	Ry	Rz	Mx	My	Mz
30	3.20 (19)	23.43 (32-I-2)	0	0	0	0
31	-20.75 (32-I-3)	34.83 (30-II-2)	0	0	0	-1.77 (30-II-2)
32	-308.46 (32-II-4)	47.11 (30-II-2)	0	0	0	-15.95 (27)
33	-519.43 (32-II-4)	63.48 (27)	0	0	0	-12.63 (32-II-4)
34	291.03 (19)	-423.06 (30-I-4)	0	0	0	26.28 (19)
35	130.45 (27)	-522.56 (30-I-4)	0	0	0	10.56 (19)
36	69.48 (27)	-557.22 (30-II-1)	0	0	0	3.31 (19)
37	-52.67 (29-I-3)	-562.60 (30-II-1)	0	0	0	-5.57 (29-I-3)
38	-149.62 (29-I-2)	-565.53 (30-I-2)	0	0	0	-9.70 (29-I-2)
39	-52.99 (29-I-2)	-255.14 (30-I-2)	0	0	0	10.22 (30-I-2)
40	0	-44.03 (29-II-3)	0	0	0	0
41	-8.31 (32-I-3)	2.85 (32-I-1)	0	0	0	0
42	-143.42 (32-I-3)	34.78 (32-II-4)	0	0	0	-3.87 (32-II-1)
43	-282.88 (32-I-3)	40.98 (32-II-4)	0	0	0	-8.49 (32-II-4)
44	-102.05 (30-II-2)	63.41 (32-II-4)	0	0	0	1.78 (19)
45	-60.59 (30-II-2)	56.63 (32-I-3)	0	0	0	3.09 (31-II-3)
46	59.09 (31-I-3)	55.48 (32-I-3)	0	0	0	3.09 (31-I-3)
47	42.83 (31-I-3)	54.96 (32-I-3)	0	0	0	2.01 (31-II-3)
48	20.53 (32-I-2)	56.18 (32-II-2)	0	0	0	1.37 (32-I-2)
49	15.89 (32-I-2)	29.29 (32-II-2)	0	0	0	0
50	0	4.42 (31-I-2)	0	0	0	0

**Risultati Analisi Dinamica - Sollecitazioni Massime - Muri discretizzati - S.L.E**  
Scenario di calcolo: **ScenarioNT\_ 2018 A2\_SLV\_SLD\_STR\_GEO**

Muro	Pann.	Sxx MPa	Syy MPa	Sxy MPa	Mxx daN*m/m	Myy daN*m/m	Mxy daN*m/m
1	1	0.1 (32-I-4)	0.0 (27)	0.0 (31-I-4)	-227.49 (32-II-2)	15.85 (27)	14.18 (32-I-4)
1	2	0.1 (32-I-4)	0.0 (27)	0.0 (31-I-4)	-233.20 (32-II-2)	-31.44 (27)	-40.83 (31-I-4)
1	3	0.1 (32-I-4)	0.0 (27)	0.0 (31-I-2)	-249.43 (32-I-4)	20.32 (27)	-10.46 (30-II-2)
1	4	0.1 (32-I-4)	0.0 (19)	0.0 (19)	-248.32 (32-I-4)	-41.47 (27)	-57.56 (31-II-3)
1	5	0.1 (32-I-4)	0.0 (27)	0.0 (31-II-4)	-225.46 (32-I-4)	12.87 (27)	-17.87 (30-II-2)
1	6	0.1 (32-I-4)	0.0 (27)	0.0 (19)	-225.88 (27)	-32.33 (27)	-44.95 (31-II-4)
1	7	0.0 (32-I-4)	0.0 (27)	0.0 (31-II-4)	-199.93 (27)	6.38 (27)	-10.59 (19)
1	8	0.0 (32-I-4)	0.0 (27)	0.0 (31-I-1)	-203.54 (27)	-21.95 (31-I-1)	-30.72 (31-II-4)
2	1	0.0 (32-I-4)	0.1 (32-I-4)	-0.0 (31-II-1)	-130.26 (32-I-4)	-196.86 (32-I-4)	-47.04 (30-II-2)
2	2	0.0 (32-I-4)	0.1 (32-I-4)	-0.0 (31-II-1)	-179.21 (32-I-4)	-254.80 (32-I-4)	49.02 (29-II-1)
2	3	0.0 (32-I-4)	0.1 (32-I-4)	-0.0 (31-II-1)	-176.42 (32-I-4)	-261.18 (32-I-4)	46.86 (29-II-1)
2	4	0.0 (32-I-4)	0.1 (32-I-4)	0.0 (30-I-2)	-115.75 (32-I-4)	-200.58 (32-II-2)	62.38 (19)
2	5	-0.0 (19)	0.1 (32-I-1)	-0.0 (31-II-1)	135.62 (19)	-177.34 (32-II-1)	-67.04 (30-II-2)
2	6	-0.0 (19)	0.0 (32-I-1)	-0.0 (31-II-1)	146.96 (19)	-217.93 (32-I-1)	-35.23 (30-II-2)
2	7	-0.0 (19)	0.0 (32-II-1)	0.0 (30-II-2)	131.65 (19)	-213.03 (32-I-1)	38.45 (31-II-1)
2	8	-0.0 (19)	0.0 (32-II-1)	0.0 (30-II-2)	93.98 (19)	-154.27 (32-II-2)	41.12 (31-II-3)
3	1	0.0 (32-II-4)	0.0 (27)	0.0 (30-II-2)	-96.92 (32-II-4)	-219.87 (32-I-3)	-86.73 (30-II-2)
3	2	0.0 (32-II-4)	0.0 (27)	0.0 (30-II-2)	-135.31 (32-II-4)	-222.37 (32-II-4)	-89.41 (30-II-2)
3	3	0.0 (32-II-4)	0.0 (32-II-4)	0.0 (30-II-2)	-132.39 (32-II-4)	-211.52 (27)	-93.76 (30-II-2)
3	4	0.0 (32-II-4)	0.0 (32-II-4)	0.0 (30-I-3)	-71.77 (32-II-4)	-163.44 (27)	-56.06 (30-II-2)
3	5	0.0 (32-II-4)	0.0 (27)	0.0 (30-II-2)	19.19 (32-II-4)	-206.71 (32-I-3)	-47.27 (30-II-2)
3	6	0.0 (32-II-4)	0.0 (27)	0.0 (30-II-2)	58.08 (32-II-4)	-193.19 (32-II-4)	-23.83 (30-II-2)
3	7	0.0 (32-II-4)	0.0 (27)	0.0 (30-II-2)	65.18 (32-II-4)	-182.21 (27)	-12.79 (30-II-2)
3	8	0.0 (32-II-4)	0.0 (32-II-4)	0.0 (30-I-3)	38.51 (32-I-3)	-137.02 (27)	16.78 (31-I-3)
4	1	-0.0 (30-II-1)	0.0 (27)	0.0 (30-II-2)	125.86 (19)	-171.67 (32-I-1)	-45.01 (30-II-2)
4	2	-0.0 (30-II-1)	0.0 (32-I-1)	0.0 (30-II-2)	138.32 (19)	-215.06 (32-I-1)	-41.59 (30-II-2)
4	3	-0.0 (30-II-1)	0.0 (27)	0.0 (30-II-2)	122.77 (19)	-211.58 (32-I-1)	-48.56 (30-II-2)
4	4	-0.0 (30-II-1)	0.0 (27)	0.0 (30-II-2)	85.20 (19)	-156.46 (32-II-1)	-50.52 (30-II-2)
4	5	-0.0 (30-I-4)	0.0 (27)	0.0 (30-II-2)	77.18 (30-I-4)	-171.41 (27)	-66.32 (30-II-2)
4	6	-0.0 (30-II-1)	0.0 (27)	0.0 (30-II-2)	-65.22 (19)	-220.26 (27)	-73.96 (30-II-2)
4	7	-0.0 (30-II-1)	0.0 (27)	0.0 (30-II-2)	-74.02 (19)	-225.16 (27)	-70.72 (30-II-2)
4	8	-0.0 (30-I-4)	0.0 (27)	0.0 (30-II-2)	-47.27 (27)	-173.47 (27)	-79.09 (30-II-2)
5	1	-0.0 (31-I-2)	-0.2 (31-I-2)	0.0 (29-II-2)	-51.26 (32-I-2)	-649.88 (32-I-2)	-36.68 (32-I-2)
5	2	-0.0 (31-II-2)	-0.2 (31-II-2)	0.0 (29-II-2)	-26.63 (32-I-2)	-627.95 (32-I-2)	-12.88 (31-II-2)
5	3	-0.1 (31-II-2)	-0.2 (31-II-2)	0.1 (29-II-2)	-67.62 (32-I-2)	-680.44 (32-I-2)	103.51 (30-I-2)
5	4	-0.1 (31-II-2)	0.3 (29-I-2)	0.1 (19)	51.89 (29-I-2)	-968.19 (32-II-2)	410.48 (30-II-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

Pagina 234 di 262

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
5	5	-0.0 (31-II-2)	-0.1 (31-II-2)	0.0 (29-II-2)	-75.11 (32-I-2)	-666.31 (32-I-2)	-10.39 (32-I-2)
5	6	-0.1 (31-II-2)	-0.1 (31-II-2)	0.0 (29-II-2)	-54.02 (32-I-2)	-602.89 (32-I-2)	-11.74 (32-I-2)
5	7	-0.0 (31-II-2)	-0.0 (19)	-0.0 (31-I-2)	-77.33 (32-I-2)	-460.14 (32-I-2)	45.25 (30-II-2)
5	8	0.2 (29-I-3)	0.0 (19)	-0.1 (31-I-2)	-101.31 (32-I-2)	-81.73 (32-I-2)	77.66 (30-II-2)
5	9	-0.0 (31-II-2)	-0.1 (31-II-2)	-0.0 (32-II-2)	-79.09 (32-I-2)	-670.28 (32-I-2)	6.10 (30-II-2)
5	10	-0.0 (19)	-0.1 (31-II-2)	-0.0 (31-I-2)	-59.70 (32-I-2)	-602.63 (32-I-2)	4.27 (30-II-2)
5	11	-0.0 (31-II-3)	-0.1 (31-II-3)	-0.1 (31-I-2)	-84.80 (32-I-2)	-461.56 (32-I-2)	-51.27 (32-I-2)
5	12	0.1 (29-I-3)	0.0 (29-II-2)	-0.0 (31-I-2)	-107.82 (32-I-2)	-88.83 (32-I-2)	-81.97 (32-I-2)
5	13	-0.0 (19)	-0.1 (31-II-2)	-0.0 (32-II-2)	-86.78 (32-I-2)	-663.46 (32-I-2)	6.74 (30-II-2)
5	14	0.0 (29-II-3)	-0.1 (31-II-2)	-0.0 (32-II-2)	-91.31 (32-I-3)	-630.15 (32-I-2)	7.32 (30-II-2)
5	15	0.1 (29-II-2)	-0.2 (31-II-3)	-0.0 (19)	-53.34 (32-II-2)	-676.04 (32-II-2)	-65.73 (32-I-2)
5	16	-0.0 (19)	-0.7 (31-II-3)	-0.2 (31-I-2)	-38.99 (31-I-2)	-959.09 (32-II-2)	-460.60 (32-I-3)
6	1	-0.2 (31-I-1)	-0.0 (31-II-2)	0.0 (29-II-2)	408.78 (32-I-2)	33.66 (32-I-2)	17.65 (32-I-2)
6	2	-0.1 (31-II-2)	-0.0 (31-II-1)	0.0 (29-II-2)	410.86 (32-I-2)	48.51 (32-I-2)	-6.29 (29-II-2)
6	3	-0.1 (31-II-1)	-0.0 (31-II-1)	-0.0 (31-I-2)	409.98 (32-I-2)	49.77 (32-I-2)	-3.61 (30-II-2)
6	4	-0.1 (31-II-1)	-0.0 (19)	-0.0 (27)	407.18 (32-I-2)	52.50 (32-I-2)	-3.37 (30-II-2)
6	5	-0.2 (31-II-2)	-0.0 (31-II-2)	0.0 (29-II-2)	370.12 (32-I-2)	17.45 (32-I-2)	-12.86 (29-I-2)
6	6	-0.1 (31-II-2)	-0.1 (31-II-1)	0.0 (18)	354.74 (32-I-2)	38.62 (32-I-2)	-9.71 (29-II-2)
6	7	-0.1 (31-II-1)	-0.0 (19)	-0.0 (31-I-2)	353.47 (32-I-2)	39.74 (32-I-2)	-2.75 (30-II-2)
6	8	-0.1 (31-II-1)	0.0 (29-II-1)	-0.0 (27)	368.37 (32-I-2)	50.88 (32-I-2)	-3.33 (30-II-2)
6	9	-0.2 (31-II-2)	-0.1 (31-II-2)	0.1 (29-II-2)	371.43 (32-I-2)	39.64 (32-I-2)	-65.17 (30-I-2)
6	10	-0.0 (19)	-0.0 (31-II-2)	-0.0 (31-I-2)	258.65 (32-I-2)	53.92 (32-I-2)	-30.11 (30-II-2)
6	11	-0.1 (31-II-1)	-0.0 (31-II-1)	-0.1 (31-I-2)	259.03 (32-I-2)	54.20 (32-I-2)	28.94 (32-I-2)
6	12	-0.2 (31-II-1)	0.1 (29-II-2)	-0.0 (19)	368.95 (32-I-2)	26.59 (32-II-2)	37.18 (32-I-2)
6	13	0.3 (29-I-2)	-0.1 (31-II-2)	0.1 (19)	489.95 (32-II-2)	52.05 (31-I-2)	-218.17 (30-II-2)
6	14	0.0 (19)	0.2 (29-I-1)	-0.1 (31-I-2)	48.06 (32-I-2)	70.34 (32-I-2)	-46.15 (30-II-2)
6	15	0.0 (29-II-2)	0.1 (29-I-1)	-0.0 (31-I-2)	51.11 (32-I-2)	68.24 (32-I-2)	44.90 (32-I-2)
6	16	-0.7 (31-II-1)	-0.0 (19)	-0.2 (31-I-2)	485.36 (32-II-2)	-38.63 (29-I-2)	234.33 (32-I-2)
7	1	-0.1 (19)	-0.0 (31-I-2)	-0.0 (31-I-2)	407.01 (32-I-2)	52.41 (32-I-2)	-2.46 (29-II-2)
7	2	-0.1 (19)	-0.0 (31-I-1)	-0.0 (31-I-2)	409.02 (32-I-2)	49.41 (32-I-2)	2.28 (32-I-2)
7	3	-0.1 (31-I-1)	-0.0 (19)	-0.0 (31-I-2)	408.83 (32-I-2)	49.38 (32-I-2)	-4.04 (30-II-2)
7	4	-0.1 (31-I-2)	-0.0 (19)	-0.0 (31-I-2)	406.45 (32-I-2)	52.33 (32-I-2)	-3.97 (30-II-2)
7	5	-0.1 (19)	-0.0 (31-I-2)	0.0 (29-II-2)	368.20 (32-I-2)	50.64 (32-I-2)	-5.16 (29-II-2)
7	6	-0.1 (19)	-0.0 (31-I-2)	-0.0 (31-I-2)	353.42 (32-I-2)	39.19 (32-I-2)	-2.31 (30-II-2)
7	7	-0.1 (31-I-2)	-0.0 (19)	-0.1 (31-I-2)	353.24 (32-I-2)	39.14 (32-I-2)	4.62 (31-I-2)
7	8	-0.1 (31-I-2)	0.0 (29-I-2)	-0.0 (32-II-1)	367.62 (32-I-2)	50.45 (32-I-2)	-3.82 (30-II-2)
7	9	-0.1 (19)	-0.1 (31-I-2)	0.1 (29-II-2)	368.94 (32-I-2)	26.46 (32-II-2)	-38.33 (30-II-2)
7	10	-0.0 (19)	-0.0 (19)	-0.1 (31-I-2)	258.85 (32-I-2)	53.33 (32-I-3)	-29.54 (30-II-2)
7	11	-0.1 (31-I-2)	-0.0 (27)	-0.1 (31-I-2)	258.62 (32-I-2)	53.18 (32-I-2)	27.62 (32-I-2)
7	12	-0.2 (31-I-2)	0.1 (29-I-2)	-0.0 (19)	368.19 (32-I-2)	25.98 (32-II-2)	36.65 (32-I-3)
7	13	0.4 (31-I-2)	-0.0 (19)	0.1 (19)	485.38 (32-II-2)	28.94 (31-I-2)	-235.92 (30-II-2)
7	14	-0.0 (29-II-2)	0.1 (29-II-2)	-0.0 (31-I-2)	50.52 (32-I-2)	67.23 (32-I-3)	-45.67 (30-II-2)
7	15	0.0 (29-II-2)	0.0 (29-II-2)	-0.0 (31-I-2)	50.49 (32-I-2)	66.99 (32-I-2)	43.84 (32-I-3)
7	16	-0.7 (31-I-2)	-0.1 (27)	-0.2 (31-I-2)	484.04 (32-I-2)	-44.93 (29-I-2)	233.34 (32-I-1)
8	1	-0.0 (29-I-2)	-0.0 (29-I-2)	0.0 (29-II-1)	2.34 (29-II-1)	205.44 (29-I-2)	15.94 (29-I-1)
8	2	0.0 (30-I-2)	-0.0 (19)	0.0 (30-I-2)	-2.31 (30-I-2)	63.64 (19)	16.84 (29-II-1)
8	3	-0.0 (29-I-2)	-0.0 (29-I-2)	-0.0 (19)	4.93 (29-I-2)	204.30 (29-I-2)	-24.85 (29-II-1)
8	4	0.0 (29-II-1)	-0.0 (19)	0.0 (32-I-2)	-5.16 (32-I-2)	64.82 (19)	-29.74 (30-I-2)
9	1	-0.0 (31-II-2)	-0.1 (19)	-0.0 (31-I-3)	-86.46 (32-I-3)	-660.11 (32-I-3)	-3.69 (32-II-2)
9	2	-0.0 (31-II-2)	-0.1 (19)	0.0 (29-II-3)	-91.66 (32-I-3)	-629.64 (32-I-3)	-4.19 (31-II-3)
9	3	-0.1 (31-II-2)	-0.1 (19)	0.1 (29-II-3)	-54.52 (32-I-3)	-676.82 (32-I-3)	68.11 (30-I-2)
9	4	-0.1 (32-II-2)	0.4 (31-I-3)	0.1 (19)	27.30 (29-I-3)	-959.30 (32-I-3)	462.34 (30-I-3)
9	5	-0.0 (31-I-2)	-0.1 (19)	-0.0 (31-I-3)	-79.17 (32-I-3)	-666.69 (32-I-3)	-3.58 (32-II-2)
9	6	-0.1 (31-I-2)	-0.1 (19)	-0.0 (31-I-3)	-62.06 (32-I-3)	-603.59 (32-I-3)	-2.40 (32-II-2)
9	7	-0.1 (32-II-2)	-0.0 (19)	-0.1 (31-I-3)	-89.06 (32-I-3)	-462.97 (32-I-3)	51.21 (30-I-2)
9	8	-0.1 (32-I-2)	-0.0 (29-II-3)	-0.0 (31-I-3)	-113.27 (32-I-3)	-88.45 (32-I-3)	82.18 (30-II-1)
9	9	-0.0 (32-I-3)	-0.1 (29-I-3)	-0.0 (31-I-3)	-79.19 (32-I-3)	-666.77 (32-I-3)	8.59 (30-II-2)
9	10	-0.0 (32-II-4)	-0.1 (29-I-3)	-0.1 (31-I-3)	-62.02 (32-I-3)	-603.63 (32-I-3)	7.44 (30-II-4)
9	11	-0.1 (31-I-2)	-0.1 (29-I-3)	-0.1 (31-I-3)	-88.96 (32-I-3)	-463.01 (32-I-3)	-46.62 (32-I-4)
9	12	-0.1 (31-I-2)	0.0 (29-I-4)	-0.0 (31-I-3)	-113.09 (32-I-3)	-88.45 (32-I-3)	-78.45 (32-I-4)
9	13	-0.0 (32-II-4)	-0.1 (29-I-3)	-0.0 (31-I-3)	-86.47 (32-I-3)	-660.20 (32-I-3)	8.71 (30-II-4)
9	14	-0.0 (32-I-2)	-0.1 (29-I-3)	-0.0 (27)	-91.54 (32-I-3)	-629.74 (32-I-3)	9.26 (30-II-4)
9	15	0.1 (29-II-2)	-0.2 (29-I-3)	-0.0 (19)	-54.14 (32-II-4)	-676.91 (32-I-3)	-63.59 (32-I-4)
9	16	-0.1 (32-II-4)	-0.7 (29-I-3)	-0.2 (31-I-3)	-45.02 (31-II-4)	-959.17 (32-I-3)	-458.92 (32-I-4)
10	1	-0.0 (31-I-2)	-0.1 (19)	-0.0 (31-I-3)	-86.55 (32-I-3)	-660.71 (32-I-3)	-4.50 (32-II-2)
10	2	-0.0 (31-II-2)	-0.1 (19)	0.0 (29-II-3)	-91.64 (32-I-3)	-630.03 (32-I-3)	-5.04 (32-II-2)
10	3	-0.1 (31-II-2)	-0.1 (19)	0.1 (29-II-3)	-54.28 (32-II-2)	-677.03 (32-I-3)	67.91 (30-I-2)
10	4	-0.1 (32-II-2)	0.4 (31-I-3)	0.1 (19)	27.16 (29-I-2)	-959.19 (32-I-3)	462.03 (30-I-2)
10	5	-0.0 (31-I-2)	-0.1 (19)	-0.0 (31-I-3)	-79.25 (32-I-3)	-667.16 (32-I-3)	-4.44 (32-II-2)
10	6	-0.0 (31-II-2)	-0.1 (19)	-0.0 (31-I-3)	-62.11 (32-I-3)	-603.88 (32-I-3)	-3.32 (32-II-2)
10	7	-0.0 (32-II-2)	-0.0 (19)	-0.1 (31-I-3)	-89.04 (32-I-3)	-463.11 (32-I-3)	50.94 (30-I-2)
10	8	0.0 (29-I-2)	-0.0 (29-II-2)	-0.0 (31-I-3)	-113.20 (32-I-3)	-88.48 (32-I-3)	81.99 (30-I-2)



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
10	9	-0.0 (32-I-3)	-0.1 (29-II-2)	-0.0 (31-I-3)	-79.24 (32-I-3)	-667.05 (32-I-3)	7.67 (30-I-2)
10	10	-0.0 (32-II-2)	-0.1 (29-II-2)	-0.1 (31-I-3)	-62.14 (32-I-3)	-603.77 (32-I-3)	6.48 (30-I-2)
10	11	-0.1 (32-II-2)	-0.1 (29-I-3)	-0.1 (31-I-3)	-89.16 (32-I-3)	-463.05 (32-I-3)	-46.78 (32-I-4)
10	12	-0.0 (32-I-2)	0.0 (29-II-3)	-0.0 (31-I-3)	-113.35 (32-I-3)	-88.46 (32-I-3)	-78.53 (32-I-4)
10	13	-0.0 (32-II-2)	-0.1 (29-I-2)	-0.0 (31-I-3)	-86.50 (32-I-3)	-660.28 (32-I-3)	7.70 (30-I-2)
10	14	-0.0 (32-I-2)	-0.1 (29-I-2)	-0.0 (32-II-4)	-91.70 (32-I-3)	-629.71 (32-I-3)	8.11 (30-I-2)
10	15	0.1 (29-I-2)	-0.2 (29-I-2)	-0.0 (19)	-54.56 (32-I-3)	-676.85 (32-I-3)	-63.69 (32-I-4)
10	16	-0.1 (32-II-2)	-0.7 (31-I-2)	-0.2 (31-I-3)	-44.98 (31-I-3)	-959.29 (32-I-3)	-459.02 (32-I-3)
11	1	-0.1 (19)	-0.0 (31-I-2)	-0.0 (31-I-1)	406.22 (32-I-3)	52.32 (32-I-3)	-1.88 (29-I-2)
11	2	-0.1 (19)	-0.0 (31-I-2)	-0.0 (31-I-1)	408.82 (32-I-3)	49.44 (32-I-3)	-2.01 (19)
11	3	-0.1 (29-II-2)	-0.0 (27)	-0.0 (31-I-1)	409.11 (32-I-3)	49.46 (32-I-3)	-4.20 (30-I-2)
11	4	-0.1 (29-I-2)	-0.0 (19)	-0.0 (31-I-1)	407.14 (32-I-3)	52.43 (32-I-3)	-4.03 (30-I-2)
11	5	-0.1 (19)	-0.0 (31-II-2)	0.0 (29-II-1)	367.36 (32-I-2)	50.44 (32-I-2)	-3.69 (29-I-2)
11	6	-0.1 (19)	-0.0 (31-II-2)	-0.0 (31-I-1)	352.82 (32-I-3)	39.24 (32-I-3)	-2.77 (30-I-2)
11	7	-0.1 (29-II-2)	-0.0 (27)	-0.1 (31-I-1)	353.04 (32-I-3)	39.24 (32-I-3)	4.97 (31-I-1)
11	8	-0.1 (29-I-2)	-0.0 (27)	-0.0 (32-I-4)	367.68 (32-I-3)	50.72 (32-II-1)	-3.59 (30-I-2)
11	9	-0.1 (19)	-0.1 (31-II-2)	0.1 (29-II-1)	368.07 (32-I-2)	25.90 (32-II-2)	-39.09 (30-I-2)
11	10	-0.0 (19)	-0.0 (27)	-0.1 (31-I-1)	258.19 (32-I-2)	53.23 (32-I-3)	-29.93 (30-I-2)
11	11	-0.1 (29-I-1)	-0.1 (31-II-2)	-0.1 (31-I-1)	258.16 (32-I-3)	53.42 (32-II-1)	27.02 (32-I-4)
11	12	-0.2 (29-I-2)	0.1 (29-I-2)	-0.0 (19)	367.60 (32-I-3)	26.44 (32-II-1)	36.25 (32-I-4)
11	13	0.4 (31-I-1)	-0.1 (27)	0.1 (19)	483.97 (32-I-2)	27.24 (31-I-2)	-235.71 (30-I-2)
11	14	-0.0 (29-II-2)	0.0 (29-I-2)	-0.0 (31-I-1)	50.38 (32-I-2)	67.02 (32-I-3)	-45.93 (30-I-2)
11	15	0.0 (29-II-1)	-0.0 (31-II-2)	-0.0 (31-I-1)	50.39 (32-I-3)	67.31 (32-II-1)	43.47 (32-I-4)
11	16	-0.7 (31-I-2)	-0.1 (27)	-0.2 (31-I-1)	483.61 (32-I-1)	-44.97 (29-I-1)	233.42 (32-I-4)
12	1	-0.0 (31-I-2)	-0.1 (19)	-0.0 (31-I-2)	-86.82 (32-I-2)	-662.67 (32-I-2)	-4.59 (32-I-2)
12	2	-0.0 (31-I-2)	-0.1 (19)	0.0 (29-II-2)	-91.88 (32-I-3)	-630.40 (32-I-2)	-5.67 (31-II-2)
12	3	-0.1 (31-I-2)	-0.1 (19)	0.1 (29-II-2)	-54.66 (32-II-2)	-676.69 (32-I-3)	67.10 (30-II-2)
12	4	-0.0 (19)	0.4 (31-I-2)	0.1 (19)	28.60 (29-I-2)	-959.40 (32-II-2)	462.00 (30-II-2)
12	5	-0.0 (31-I-2)	-0.1 (19)	-0.0 (31-I-2)	-79.47 (32-I-2)	-668.46 (32-I-2)	-4.77 (32-I-2)
12	6	-0.0 (31-I-2)	-0.1 (19)	-0.0 (31-I-2)	-62.40 (32-I-3)	-604.35 (32-I-3)	-3.48 (32-I-2)
12	7	-0.0 (19)	-0.0 (19)	-0.1 (31-I-2)	-89.40 (32-I-3)	-463.15 (32-I-3)	50.70 (30-II-2)
12	8	0.1 (29-II-2)	-0.0 (29-II-2)	-0.0 (31-I-2)	-113.57 (32-I-3)	-88.44 (32-I-3)	81.78 (30-II-2)
12	9	-0.0 (19)	-0.1 (31-I-2)	-0.0 (31-I-2)	-79.40 (32-I-3)	-667.93 (32-I-3)	7.30 (30-II-2)
12	10	-0.0 (19)	-0.1 (31-I-2)	-0.1 (31-I-2)	-62.29 (32-I-3)	-604.29 (32-I-3)	6.57 (30-II-2)
12	11	-0.0 (32-II-2)	-0.1 (31-I-2)	-0.1 (31-I-2)	-89.27 (32-I-3)	-463.26 (32-I-3)	-47.60 (32-I-2)
12	12	0.0 (29-II-2)	0.0 (29-II-2)	-0.0 (31-I-2)	-113.44 (32-I-3)	-88.49 (32-I-3)	-79.11 (32-I-2)
12	13	-0.0 (19)	-0.1 (31-I-2)	-0.0 (31-I-2)	-86.60 (32-I-3)	-660.98 (32-I-3)	7.24 (30-II-2)
12	14	0.0 (29-I-2)	-0.1 (31-I-2)	-0.0 (32-II-2)	-91.70 (32-I-3)	-630.18 (32-I-3)	8.11 (30-II-2)
12	15	0.1 (29-I-2)	-0.2 (31-I-2)	-0.0 (19)	-54.50 (32-II-2)	-677.10 (32-I-3)	-64.43 (32-II-1)
12	16	-0.1 (32-I-2)	-0.7 (31-I-2)	-0.2 (31-I-2)	-44.95 (31-I-2)	-959.20 (32-I-3)	-459.26 (32-I-3)
13	1	-0.1 (19)	-0.0 (31-II-2)	-0.0 (31-I-1)	407.09 (32-I-3)	52.44 (32-I-3)	1.64 (32-II-2)
13	2	-0.1 (19)	-0.0 (31-I-2)	-0.0 (31-I-1)	408.86 (32-I-3)	49.47 (32-I-3)	1.84 (32-II-2)
13	3	-0.1 (29-I-2)	-0.0 (27)	-0.0 (31-I-1)	408.29 (30-I-3)	49.43 (30-I-3)	4.14 (31-I-1)
13	4	-0.1 (29-I-1)	-0.0 (27)	-0.0 (31-I-1)	406.73 (30-I-4)	52.46 (30-I-4)	-3.89 (30-II-2)
13	5	-0.1 (19)	-0.0 (31-II-2)	0.0 (29-II-1)	367.63 (32-I-3)	50.76 (32-II-1)	-3.37 (29-II-1)
13	6	-0.1 (19)	-0.1 (31-I-2)	-0.0 (31-I-1)	352.86 (30-I-3)	39.36 (32-I-4)	2.50 (31-I-1)
13	7	-0.1 (29-I-1)	-0.0 (27)	-0.1 (31-I-1)	352.80 (30-I-4)	39.40 (30-I-3)	5.52 (31-I-1)
13	8	-0.1 (29-I-2)	-0.0 (27)	-0.0 (32-I-4)	367.76 (30-I-4)	50.72 (30-I-4)	-3.77 (30-II-4)
13	9	-0.1 (19)	-0.1 (31-II-2)	0.1 (29-II-1)	367.60 (32-I-3)	26.48 (32-II-1)	-38.77 (30-I-2)
13	10	-0.0 (19)	-0.1 (27)	-0.1 (31-I-1)	258.10 (30-I-3)	53.58 (30-I-4)	-29.47 (30-I-2)
13	11	-0.1 (29-I-1)	-0.1 (31-I-2)	-0.1 (31-I-1)	258.32 (30-I-4)	53.55 (30-I-3)	27.53 (32-I-4)
13	12	-0.2 (29-I-1)	0.1 (29-II-2)	-0.0 (19)	368.17 (30-I-4)	26.18 (30-II-4)	36.86 (32-I-4)
13	13	0.4 (31-II-4)	-0.1 (27)	0.1 (19)	483.59 (32-I-1)	27.48 (31-I-1)	-235.17 (30-I-2)
13	14	-0.0 (29-II-1)	-0.0 (27)	-0.0 (31-I-1)	50.38 (30-I-3)	67.50 (30-II-1)	-45.49 (30-I-2)
13	15	0.0 (29-I-4)	-0.1 (31-I-2)	-0.0 (31-I-1)	50.43 (30-I-4)	67.42 (30-I-3)	43.92 (32-I-4)
13	16	-0.7 (29-I-1)	-0.1 (31-II-4)	-0.2 (31-I-1)	483.80 (30-I-4)	-44.83 (31-II-4)	233.98 (32-I-4)
14	1	0.0 (27)	-0.0 (30-II-1)	-0.0 (30-II-2)	-84.52 (27)	98.51 (30-I-4)	48.47 (30-II-2)
14	2	0.0 (27)	-0.0 (30-II-1)	-0.0 (30-II-2)	-67.75 (32-II-2)	183.82 (19)	-35.69 (31-II-1)
14	3	0.0 (27)	-0.0 (30-II-1)	-0.0 (30-II-2)	-128.75 (27)	80.52 (30-I-4)	77.88 (30-II-2)
14	4	0.0 (32-I-1)	-0.0 (30-II-1)	-0.0 (30-II-2)	-104.29 (32-II-1)	209.85 (19)	37.08 (30-II-2)
14	5	0.0 (27)	-0.0 (30-II-1)	-0.0 (30-II-2)	-169.13 (27)	74.26 (30-I-4)	86.48 (30-II-2)
14	6	0.0 (32-I-1)	-0.0 (30-II-1)	-0.0 (30-II-2)	-148.99 (32-II-1)	190.96 (19)	42.00 (30-II-2)
14	7	0.0 (27)	-0.0 (30-I-4)	-0.0 (30-II-2)	-222.32 (27)	71.62 (30-I-4)	84.55 (30-II-2)
14	8	0.0 (27)	-0.0 (30-II-1)	-0.0 (30-II-2)	-217.05 (32-II-1)	133.28 (19)	55.10 (30-II-2)
15	1	0.0 (32-II-1)	-0.0 (17)	0.0 (31-II-1)	46.55 (29-II-2)	215.24 (17)	82.60 (30-II-2)
15	2	0.0 (32-II-1)	-0.0 (17)	0.0 (31-II-1)	-60.65 (32-II-1)	-120.47 (32-I-3)	71.47 (30-II-2)
15	3	0.0 (32-II-1)	-0.0 (17)	0.0 (31-II-1)	-53.37 (27)	251.83 (17)	44.48 (30-II-2)
15	4	0.0 (32-II-1)	-0.0 (17)	-0.0 (30-II-2)	-100.72 (32-II-1)	-180.05 (32-I-3)	-26.97 (31-II-1)
15	5	0.0 (32-II-1)	-0.0 (19)	-0.0 (30-II-2)	-80.96 (27)	244.04 (17)	30.56 (30-II-2)
15	6	0.0 (32-II-1)	-0.0 (19)	-0.0 (30-II-2)	-130.23 (32-I-4)	-182.59 (32-I-3)	-36.55 (31-II-1)



**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
15	7	0.0 (32-II-1)	-0.0 (19)	-0.0 (30-II-2)	-128.43 (32-II-2)	193.59 (19)	-46.71 (31-II-1)
15	8	0.0 (32-II-1)	-0.0 (19)	-0.0 (30-II-2)	-158.20 (32-I-4)	-131.25 (32-I-4)	-57.56 (29-II-1)
16	1	0.0 (32-II-1)	-0.0 (19)	0.0 (31-II-1)	-64.55 (27)	189.82 (19)	79.88 (30-II-2)
16	2	0.0 (32-I-4)	-0.0 (19)	0.0 (31-II-1)	-92.10 (32-II-1)	-118.70 (32-I-4)	59.23 (30-II-2)
16	3	0.0 (32-II-1)	-0.0 (19)	0.0 (31-II-1)	-99.37 (27)	211.84 (19)	48.27 (30-II-2)
16	4	0.0 (32-I-4)	-0.0 (19)	0.0 (31-II-1)	-143.99 (32-I-4)	-173.33 (30-I-4)	-48.89 (31-II-1)
16	5	0.0 (32-II-1)	-0.0 (19)	0.0 (31-II-1)	-146.38 (32-I-1)	193.72 (19)	36.34 (30-II-2)
16	6	0.0 (32-I-4)	-0.0 (19)	-0.0 (30-II-2)	-189.58 (32-I-4)	-177.80 (30-I-4)	-59.84 (31-II-1)
16	7	0.0 (32-II-1)	-0.0 (19)	-0.0 (30-II-2)	-224.33 (32-II-2)	140.53 (19)	-45.04 (29-II-1)
16	8	0.0 (32-I-4)	0.0 (32-I-4)	-0.0 (30-II-2)	-246.69 (32-I-4)	-138.83 (32-I-4)	-72.06 (29-II-1)
17	1	0.0 (32-II-1)	-0.0 (30-II-1)	-0.0 (30-II-2)	-56.33 (27)	101.19 (30-II-1)	-34.40 (31-II-1)
17	2	0.0 (27)	-0.0 (30-II-1)	-0.0 (30-II-2)	48.35 (29-II-2)	210.83 (17)	-45.21 (31-II-1)
17	3	0.0 (27)	-0.0 (30-II-1)	-0.0 (30-II-2)	-91.41 (27)	79.06 (30-II-1)	48.61 (30-II-2)
17	4	0.0 (32-II-1)	-0.0 (30-II-1)	-0.0 (30-II-2)	-59.87 (32-II-2)	252.33 (17)	30.84 (30-II-2)
17	5	0.0 (27)	-0.0 (30-II-1)	-0.0 (30-II-2)	-118.61 (27)	75.82 (30-II-1)	57.45 (30-II-2)
17	6	0.0 (32-II-1)	-0.0 (30-II-1)	-0.0 (30-II-2)	-86.77 (32-II-1)	244.30 (17)	40.62 (30-II-2)
17	7	0.0 (32-I-1)	-0.0 (30-II-1)	-0.0 (30-II-2)	-145.82 (27)	89.16 (30-II-1)	71.03 (30-II-2)
17	8	0.0 (27)	-0.0 (30-II-1)	-0.0 (30-II-2)	-125.50 (32-II-1)	188.56 (19)	59.91 (30-II-2)
18	1	-0.0 (29-II-2)	-0.0 (30-I-2)	-0.0 (19)	-18.20 (19)	106.28 (30-I-2)	-41.17 (29-II-1)
18	2	-0.0 (29-II-2)	-0.0 (30-II-1)	-0.0 (19)	36.97 (29-I-2)	225.08 (29-I-2)	-44.01 (31-II-1)
18	3	-0.0 (29-II-2)	-0.0 (30-II-1)	-0.0 (30-II-2)	-33.51 (19)	86.03 (30-I-2)	16.53 (30-II-2)
18	4	-0.0 (29-II-2)	-0.0 (30-II-1)	-0.0 (30-II-2)	57.35 (29-II-2)	273.27 (29-I-2)	-13.90 (31-II-1)
18	5	-0.0 (29-II-2)	-0.0 (30-II-1)	-0.0 (30-II-2)	-41.72 (27)	84.71 (30-I-2)	23.32 (30-II-2)
18	6	-0.0 (29-II-2)	-0.0 (30-II-1)	-0.0 (30-II-2)	60.24 (29-II-2)	270.75 (29-I-2)	23.08 (30-II-2)
18	7	-0.0 (29-II-2)	-0.0 (30-II-1)	0.0 (31-II-1)	-53.44 (27)	103.13 (30-II-1)	49.23 (19)
18	8	-0.0 (29-II-2)	-0.0 (30-II-1)	0.0 (31-II-1)	45.84 (29-II-2)	219.43 (29-I-2)	47.88 (19)
19	1	-0.0 (29-II-2)	-0.0 (29-I-2)	0.0 (31-II-1)	35.82 (29-I-2)	230.15 (29-I-2)	69.47 (30-II-2)
19	2	-0.0 (29-II-2)	-0.0 (29-I-2)	0.0 (29-II-1)	18.70 (29-I-1)	-116.95 (32-I-2)	65.88 (30-II-2)
19	3	-0.0 (29-II-2)	-0.0 (29-I-2)	0.0 (31-II-1)	56.88 (29-I-2)	273.14 (29-I-2)	29.35 (30-II-2)
19	4	-0.0 (29-II-2)	-0.0 (29-II-2)	0.0 (31-II-1)	-37.01 (32-I-2)	-177.52 (32-I-2)	21.52 (30-II-2)
19	5	-0.0 (29-II-2)	-0.0 (29-II-2)	-0.0 (30-II-2)	60.80 (29-II-2)	-123.63 (29-I-2)	-16.84 (31-II-1)
19	6	-0.0 (29-II-2)	-0.0 (29-II-2)	-0.0 (30-II-2)	-51.66 (32-I-2)	-179.86 (32-I-2)	-18.48 (31-II-1)
19	7	-0.0 (29-II-2)	-0.0 (29-I-2)	-0.0 (30-II-2)	48.36 (29-II-2)	224.28 (29-I-2)	-43.95 (29-II-1)
19	8	-0.0 (29-II-2)	-0.0 (29-II-2)	-0.0 (30-II-2)	-61.00 (32-II-1)	-123.63 (32-I-2)	-45.95 (29-II-1)
20	1	0.0 (27)	-0.0 (30-II-1)	-0.0 (30-II-2)	34.99 (29-II-2)	104.29 (30-II-1)	-40.47 (31-II-1)
20	2	0.0 (27)	-0.0 (30-II-1)	-0.0 (30-II-2)	57.87 (29-II-2)	219.51 (29-II-2)	-47.41 (31-II-1)
20	3	0.0 (27)	-0.0 (30-II-1)	-0.0 (30-II-2)	-55.81 (27)	82.10 (30-II-1)	29.84 (30-II-2)
20	4	0.0 (27)	-0.0 (30-II-1)	-0.0 (30-II-2)	57.50 (29-II-2)	265.98 (17)	21.52 (30-II-2)
20	5	0.0 (27)	-0.0 (30-II-1)	-0.0 (30-II-2)	-76.97 (27)	79.89 (30-II-1)	37.66 (30-II-2)
20	6	0.0 (32-II-2)	-0.0 (30-II-1)	-0.0 (30-II-2)	-44.71 (32-I-2)	263.70 (17)	31.55 (30-II-2)
20	7	0.0 (32-II-2)	-0.0 (30-II-1)	0.0 (31-II-1)	-95.31 (27)	97.63 (30-II-1)	56.18 (19)
20	8	0.0 (27)	-0.0 (30-II-1)	0.0 (31-II-1)	-75.21 (32-II-1)	211.66 (17)	51.92 (19)
21	1	0.0 (32-I-2)	-0.0 (29-I-2)	0.0 (31-II-1)	56.89 (29-II-2)	223.82 (29-II-2)	77.92 (30-II-2)
21	2	0.0 (32-II-1)	-0.0 (29-I-2)	0.0 (29-II-1)	37.88 (29-I-2)	-119.44 (32-I-3)	71.73 (30-II-2)
21	3	0.0 (32-II-2)	-0.0 (17)	0.0 (31-II-1)	57.10 (29-II-2)	264.89 (17)	37.90 (30-II-2)
21	4	0.0 (32-II-1)	-0.0 (17)	-0.0 (30-II-2)	-64.27 (32-I-2)	-180.53 (32-I-3)	23.78 (30-II-2)
21	5	0.0 (32-II-1)	-0.0 (17)	-0.0 (30-II-2)	44.31 (29-II-2)	262.62 (17)	24.63 (30-II-2)
21	6	0.0 (32-II-1)	-0.0 (17)	-0.0 (30-II-2)	-86.34 (32-II-1)	-182.98 (32-I-3)	-24.76 (31-II-1)
21	7	0.0 (32-II-1)	-0.0 (17)	-0.0 (30-II-2)	-75.58 (32-II-2)	215.71 (17)	-43.49 (29-II-1)
21	8	0.0 (32-II-1)	-0.0 (17)	-0.0 (30-II-2)	-103.73 (32-I-4)	-127.74 (32-I-3)	-48.82 (29-II-1)
22	1	0.0 (27)	0.0 (31-I-2)	-0.0 (30-II-2)	-125.99 (32-I-4)	6.64 (31-II-4)	-5.27 (31-I-4)
22	2	0.0 (27)	0.0 (31-I-2)	0.0 (31-II-1)	-126.83 (27)	-18.86 (31-II-1)	23.36 (30-II-2)
22	3	0.0 (27)	0.0 (31-I-2)	-0.0 (30-II-2)	-104.70 (27)	11.42 (31-I-2)	-13.78 (32-II-2)
22	4	0.0 (27)	0.0 (31-I-2)	0.0 (31-II-1)	-110.19 (27)	-22.08 (31-I-2)	34.70 (30-II-2)
22	5	0.0 (27)	0.0 (31-I-2)	-0.0 (30-II-2)	-91.58 (27)	9.64 (27)	-11.79 (32-II-2)
22	6	0.0 (27)	0.0 (31-I-2)	0.0 (31-I-1)	-97.12 (27)	-20.97 (31-I-2)	27.34 (30-II-2)
22	7	0.0 (27)	0.0 (31-I-2)	-0.0 (30-II-2)	-79.13 (27)	5.94 (27)	-5.24 (31-I-1)
22	8	0.0 (27)	0.0 (31-I-2)	-0.0 (30-II-2)	-80.89 (27)	-16.96 (31-I-4)	22.26 (30-II-2)
23	1	0.0 (32-I-2)	0.0 (32-I-3)	0.0 (31-II-1)	-51.60 (32-II-2)	18.13 (32-II-4)	22.71 (32-II-2)
23	2	0.0 (32-I-2)	0.0 (32-I-3)	-0.0 (30-II-2)	-59.69 (32-II-2)	-71.03 (32-II-2)	31.98 (30-II-2)
23	3	0.0 (32-II-2)	0.0 (32-II-3)	-0.0 (30-II-2)	-57.40 (32-II-2)	42.54 (32-II-3)	13.54 (32-II-2)
23	4	0.0 (32-II-2)	0.0 (32-I-3)	-0.0 (30-II-2)	-75.92 (32-II-2)	-96.68 (32-I-3)	27.99 (30-II-2)
23	5	0.0 (32-II-2)	0.0 (32-I-3)	-0.0 (30-II-2)	-69.75 (32-I-2)	42.10 (32-I-3)	14.00 (32-II-2)
23	6	0.0 (32-II-2)	0.0 (32-I-3)	-0.0 (30-II-2)	-88.07 (32-II-2)	-97.28 (32-I-3)	30.93 (30-II-2)
23	7	0.0 (32-II-2)	0.0 (32-I-3)	-0.0 (30-II-2)	-91.34 (32-I-2)	16.52 (32-II-2)	6.30 (30-II-2)
23	8	0.0 (32-II-2)	0.0 (32-I-3)	-0.0 (30-II-2)	-99.06 (32-I-2)	-73.48 (32-I-3)	22.55 (30-II-2)
24	1	0.0 (32-I-2)	0.0 (32-II-4)	-0.0 (30-II-2)	-142.40 (32-II-2)	16.62 (32-II-4)	36.74 (30-II-2)
24	2	0.0 (32-I-2)	0.0 (32-I-4)	-0.0 (30-II-2)	-150.64 (32-II-2)	-78.52 (32-I-3)	60.83 (30-II-2)
24	3	0.0 (32-II-1)	0.0 (32-I-4)	-0.0 (30-II-2)	-145.44 (32-II-1)	43.36 (32-II-4)	26.12 (30-II-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

Maggio 2021

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
24	4	0.0 (32-II-1)	0.0 (32-I-4)	-0.0 (30-II-2)	-163.76 (32-I-2)	-106.19 (32-I-4)	60.98 (30-II-2)
24	5	0.0 (32-I-1)	0.0 (32-II-4)	-0.0 (30-II-2)	-156.49 (32-I-2)	45.14 (32-I-3)	28.38 (30-II-2)
24	6	0.0 (32-I-1)	0.0 (32-II-4)	-0.0 (30-II-2)	-175.63 (32-II-4)	-108.08 (32-II-4)	66.99 (30-II-2)
24	7	0.0 (32-I-1)	0.0 (32-II-4)	-0.0 (30-II-2)	-180.53 (27)	18.61 (32-II-2)	23.00 (30-II-2)
24	8	0.0 (32-I-1)	0.0 (32-II-4)	-0.0 (30-II-2)	-185.54 (27)	-83.29 (32-II-4)	54.30 (30-II-2)
25	1	0.0 (27)	0.0 (31-II-1)	0.0 (31-I-1)	-195.91 (32-I-4)	7.78 (31-I-4)	-9.26 (19)
25	2	0.0 (27)	0.0 (31-I-1)	0.0 (31-I-1)	-195.60 (32-I-4)	-19.08 (31-I-1)	-22.19 (31-II-1)
25	3	0.0 (27)	0.0 (31-I-1)	-0.0 (30-II-2)	-160.63 (27)	11.95 (31-II-1)	-19.12 (30-II-2)
25	4	0.0 (27)	0.0 (31-I-1)	0.0 (31-I-1)	-166.10 (27)	-23.93 (31-II-1)	33.97 (30-II-2)
25	5	0.0 (27)	0.0 (31-I-1)	-0.0 (30-II-2)	-142.11 (27)	9.42 (31-I-1)	-15.64 (30-II-2)
25	6	0.0 (27)	0.0 (31-I-1)	0.0 (31-II-1)	-148.03 (27)	-22.94 (31-II-1)	28.18 (30-II-2)
25	7	0.0 (27)	0.0 (31-II-1)	-0.0 (30-II-2)	-127.17 (27)	5.58 (27)	-6.34 (31-I-4)
25	8	0.0 (27)	0.0 (31-I-1)	0.0 (31-II-1)	-129.86 (27)	-18.64 (31-I-2)	22.59 (30-II-2)
26	1	0.0 (27)	0.0 (31-I-4)	-0.0 (30-II-2)	-80.63 (27)	6.39 (31-II-1)	-3.74 (31-I-1)
26	2	0.0 (27)	0.0 (27)	-0.0 (30-II-2)	-82.28 (27)	-17.90 (31-II-2)	22.04 (30-II-2)
26	3	0.0 (27)	0.0 (31-II-2)	-0.0 (30-II-2)	-61.91 (27)	11.14 (31-I-4)	-11.62 (32-II-2)
26	4	0.0 (27)	0.0 (27)	-0.0 (30-II-2)	-67.13 (27)	-20.51 (31-II-2)	31.56 (30-II-2)
26	5	0.0 (27)	0.0 (31-I-4)	-0.0 (30-II-2)	-51.38 (27)	9.52 (27)	-9.53 (32-II-2)
26	6	0.0 (27)	0.0 (31-I-4)	0.0 (31-II-1)	-56.55 (27)	-19.06 (31-I-4)	23.49 (32-II-2)
26	7	0.0 (27)	0.0 (27)	-0.0 (30-II-2)	-41.24 (27)	5.94 (27)	-3.90 (31-II-2)
26	8	0.0 (27)	0.0 (31-I-2)	-0.0 (30-II-2)	-42.52 (27)	-15.69 (31-I-1)	18.76 (30-II-2)
27	1	0.0 (27)	0.0 (31-I-1)	-0.0 (30-II-2)	-44.38 (27)	6.55 (31-I-1)	-2.21 (27)
27	2	0.0 (27)	0.0 (27)	-0.0 (30-II-2)	-45.53 (27)	-16.19 (31-I-1)	17.53 (32-II-2)
27	3	0.0 (27)	0.0 (31-II-1)	-0.0 (32-II-2)	28.22 (29-II-2)	10.77 (31-I-1)	-8.46 (32-II-2)
27	4	0.0 (27)	0.0 (27)	-0.0 (30-II-2)	-32.82 (27)	-18.56 (31-I-1)	24.26 (32-II-2)
27	5	0.0 (19)	0.0 (31-II-1)	-0.0 (32-II-2)	33.06 (29-II-2)	9.03 (27)	-5.92 (32-II-2)
27	6	0.0 (19)	0.0 (31-II-1)	0.0 (31-I-1)	29.64 (29-II-2)	-16.78 (27)	-17.18 (29-II-1)
27	7	0.0 (19)	0.0 (31-I-1)	-0.0 (32-II-2)	-22.76 (19)	5.41 (27)	-2.27 (27)
27	8	0.0 (19)	0.0 (31-II-1)	-0.0 (30-II-2)	-22.69 (19)	-15.51 (31-II-1)	11.48 (30-II-2)
28	1	0.0 (32-II-2)	0.0 (32-I-2)	-0.0 (31-II-1)	-70.78 (32-II-2)	-28.04 (30-II-2)	-21.56 (30-II-2)
28	2	0.0 (32-II-2)	0.0 (32-II-2)	0.0 (30-II-2)	-95.32 (32-II-2)	-41.77 (32-II-2)	-16.16 (30-II-2)
28	3	0.0 (32-II-2)	0.0 (32-II-2)	0.0 (30-II-2)	-95.39 (32-II-2)	-52.39 (32-I-2)	-18.78 (30-II-2)
28	4	0.0 (32-II-2)	0.0 (32-II-2)	0.0 (30-II-2)	-71.69 (32-I-3)	-62.75 (32-I-2)	14.85 (31-II-1)
28	5	0.0 (32-II-2)	0.0 (32-I-2)	-0.0 (31-II-1)	18.03 (32-II-4)	-24.32 (19)	-17.91 (32-II-2)
28	6	0.0 (32-II-2)	0.0 (32-II-2)	0.0 (30-II-2)	42.33 (32-I-3)	28.73 (29-II-2)	-9.23 (32-II-2)
28	7	0.0 (32-II-2)	0.0 (32-II-2)	0.0 (30-II-2)	41.73 (32-II-2)	-33.73 (32-I-2)	-9.86 (32-II-2)
28	8	0.0 (32-II-2)	0.0 (32-II-2)	0.0 (30-II-2)	16.33 (32-II-2)	-54.82 (32-I-2)	8.33 (31-II-1)
29	1	0.0 (32-I-2)	0.0 (32-I-3)	-0.0 (30-II-2)	-93.52 (32-II-2)	17.56 (32-II-4)	27.82 (32-II-2)
29	2	0.0 (32-I-2)	0.0 (32-I-3)	-0.0 (30-II-2)	-101.44 (32-II-2)	-73.85 (32-I-3)	44.37 (30-II-2)
29	3	0.0 (32-I-2)	0.0 (32-I-3)	-0.0 (30-II-2)	-98.66 (32-II-2)	42.65 (32-I-3)	17.75 (32-II-2)
29	4	0.0 (32-II-2)	0.0 (32-I-3)	-0.0 (30-II-2)	-117.03 (32-II-2)	-99.84 (32-I-3)	42.15 (30-II-2)
29	5	0.0 (32-II-2)	0.0 (32-I-3)	-0.0 (30-II-2)	-111.00 (32-I-2)	42.60 (32-I-3)	18.79 (30-II-2)
29	6	0.0 (32-II-2)	0.0 (32-I-4)	-0.0 (30-II-2)	-129.32 (32-I-2)	-100.02 (32-I-3)	46.02 (30-II-2)
29	7	0.0 (32-II-2)	0.0 (32-I-3)	-0.0 (30-II-2)	-132.79 (27)	16.86 (32-II-2)	13.55 (30-II-2)
29	8	0.0 (32-II-2)	0.0 (32-I-4)	-0.0 (30-II-2)	-138.88 (32-I-2)	-75.84 (32-II-4)	36.61 (30-II-2)
30	1	-0.0 (29-I-2)	-0.0 (30-I-2)	-0.0 (29-II-3)	-29.83 (29-I-2)	90.41 (30-I-2)	-45.34 (29-II-1)
30	2	0.0 (19)	-0.0 (30-II-1)	-0.0 (29-I-1)	14.72 (19)	231.60 (29-I-2)	-47.54 (29-II-1)
30	3	0.0 (19)	-0.0 (30-II-1)	-0.0 (29-I-1)	-25.34 (29-II-3)	-87.58 (31-II-2)	-11.62 (31-II-1)
30	4	-0.0 (29-I-2)	-0.0 (30-II-1)	-0.0 (19)	25.87 (29-I-2)	283.80 (29-I-2)	-9.87 (31-II-1)
30	5	0.0 (19)	-0.0 (30-II-1)	-0.0 (30-II-2)	-24.87 (19)	83.28 (30-I-2)	12.54 (30-II-2)
30	6	-0.0 (29-I-2)	-0.0 (30-II-1)	0.0 (31-II-1)	44.18 (29-I-2)	285.38 (29-I-2)	16.75 (30-II-2)
30	7	-0.0 (29-I-2)	-0.0 (30-I-2)	0.0 (31-II-1)	27.29 (29-I-2)	105.30 (30-I-2)	46.01 (29-I-1)
30	8	-0.0 (29-I-2)	-0.0 (30-II-1)	0.0 (31-II-1)	50.81 (29-I-2)	231.54 (29-I-2)	44.88 (29-I-1)
31	1	0.0 (32-I-2)	-0.0 (29-I-2)	0.0 (30-I-2)	21.44 (32-I-4)	239.68 (29-I-2)	53.91 (30-I-4)
31	2	-0.0 (29-I-2)	-0.0 (19)	0.0 (29-II-1)	-30.68 (29-I-2)	-94.50 (32-I-2)	45.49 (30-I-4)
31	3	-0.0 (29-I-2)	-0.0 (29-I-2)	0.0 (31-II-1)	25.44 (30-I-4)	287.91 (29-I-2)	22.38 (30-II-2)
31	4	0.0 (32-I-2)	-0.0 (29-I-2)	0.0 (29-II-1)	-26.61 (30-I-2)	-160.70 (32-I-2)	16.33 (30-II-2)
31	5	-0.0 (29-I-2)	-0.0 (29-I-2)	-0.0 (30-II-2)	43.77 (29-I-2)	288.34 (29-II-2)	-22.56 (31-II-1)
31	6	0.0 (32-I-2)	-0.0 (29-I-2)	-0.0 (30-II-2)	-32.05 (32-I-2)	-169.87 (32-I-2)	-16.35 (31-II-1)
31	7	-0.0 (29-I-2)	-0.0 (29-I-2)	-0.0 (30-II-2)	52.24 (29-I-2)	237.99 (29-I-2)	-50.87 (29-II-1)
31	8	-0.0 (29-I-2)	-0.0 (29-I-2)	-0.0 (30-II-2)	30.43 (29-I-2)	-117.08 (32-I-2)	-52.22 (29-II-1)
32	1	0.0 (31-I-2)	-0.0 (30-I-2)	-0.0 (29-I-3)	-2.45 (29-II-2)	93.34 (30-I-2)	-17.80 (29-II-3)
32	2	-0.0 (29-I-2)	-0.0 (29-I-2)	-0.0 (29-II-3)	2.27 (29-II-3)	193.96 (29-I-2)	-16.24 (29-I-3)
32	3	0.0 (31-II-3)	-0.0 (30-I-2)	0.0 (32-I-2)	-4.95 (31-II-3)	97.37 (30-I-2)	26.26 (29-II-3)
32	4	-0.0 (29-II-2)	-0.0 (29-I-2)	0.0 (29-II-1)	4.79 (29-I-2)	193.08 (29-I-2)	23.38 (29-II-3)
33	1	0.0 (32-I-2)	0.0 (32-I-2)	0.0 (32-I-2)	-3.45 (30-I-4)	-2.42 (30-I-2)	-1.99 (30-II-2)
33	2	0.0 (29-I-1)	0.0 (32-I-2)	0.0 (30-I-2)	-9.25 (29-I-1)	-24.60 (32-I-2)	-17.99 (30-I-2)
33	3	0.0 (32-II-2)	0.0 (32-I-2)	0.0 (30-I-2)	1.06 (19)	-3.39 (30-I-2)	-4.20 (32-I-2)
33	4	0.0 (29-I-2)	0.0 (32-I-2)	0.0 (29-II-2)	-1.51 (19)	-35.06 (32-I-2)	-9.40 (31-I-2)
34	1	0.0 (32-II-2)	0.0 (32-II-2)	0.0 (19)	-58.94 (32-II-2)	-22.52 (29-I-3)	-17.45 (31-II-3)
34	2	0.0 (32-II-2)	0.0 (19)	0.0 (19)	-94.46 (32-II-2)	-23.65 (30-II-2)	-4.73 (19)
34	3	0.0 (32-II-2)	0.0 (19)	0.0 (30-II-2)	-98.73 (32-II-2)	-28.92 (32-II-2)	7.20 (31-II-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

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Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
34	4	0.0 (32-II-2)	0.0 (32-II-2)	0.0 (30-II-2)	-73.44 (32-II-2)	-33.35 (32-II-2)	16.00 (31-II-1)
34	5	0.0 (32-II-2)	0.0 (19)	-0.0 (32-II-4)	17.75 (32-I-3)	10.92 (32-II-2)	-13.15 (32-II-2)
34	6	0.0 (32-II-2)	0.0 (19)	-0.0 (32-I-2)	41.23 (32-II-2)	-5.56 (19)	-8.05 (19)
34	7	0.0 (32-II-2)	0.0 (19)	0.0 (30-II-2)	43.00 (32-II-2)	-14.46 (19)	9.89 (29-I-2)
34	8	0.0 (32-II-2)	0.0 (19)	0.0 (30-II-2)	16.87 (32-II-2)	-26.96 (19)	16.29 (31-II-1)
35	1	0.0 (31-II-2)	0.0 (30-I-2)	0.0 (19)	-45.21 (31-II-2)	-2.41 (30-I-2)	-10.54 (31-II-2)
35	2	0.0 (31-II-3)	0.0 (29-I-2)	0.0 (29-II-3)	-41.16 (31-II-2)	-6.14 (30-II-2)	6.54 (32-I-2)
35	3	0.0 (31-II-2)	-0.0 (32-II-2)	-0.0 (32-II-2)	1.82 (30-I-2)	0	-4.97 (31-I-2)
35	4	0.0 (31-II-3)	-0.0 (31-II-1)	-0.0 (30-I-2)	-2.31 (31-II-3)	1.24 (32-II-2)	8.20 (31-I-2)
36	1	0.0 (19)	0.0 (31-II-1)	0.0 (31-II-1)	-27.80 (19)	7.51 (31-II-1)	6.06 (29-II-2)
36	2	0.0 (19)	0.0 (31-I-1)	-0.0 (30-II-2)	-26.99 (19)	-17.14 (31-II-1)	-10.12 (29-II-1)
36	3	0.0 (19)	0.0 (31-II-1)	0.0 (29-II-1)	-16.85 (19)	13.09 (31-II-1)	12.27 (29-I-2)
36	4	0.0 (19)	0.0 (31-I-1)	-0.0 (30-II-2)	-19.14 (19)	-26.39 (31-II-1)	-14.68 (29-II-1)
36	5	0.0 (32-I-2)	0.0 (31-II-1)	0.0 (29-I-2)	-17.32 (30-I-2)	16.55 (31-II-1)	8.28 (29-I-2)
36	6	0.0 (19)	0.0 (31-I-1)	0.0 (31-II-1)	-25.30 (31-II-1)	-30.51 (31-II-1)	-11.97 (29-II-1)
36	7	0.0 (30-I-2)	0.0 (31-I-2)	0.0 (30-I-2)	-13.45 (29-II-1)	8.71 (31-II-2)	-8.16 (32-I-4)
36	8	0.0 (29-II-1)	0.0 (31-I-2)	0.0 (30-I-2)	-26.58 (29-II-1)	-24.84 (31-I-2)	-16.00 (29-II-1)
37	1	0.0 (27)	-0.0 (19)	0.0 (27)	-17.20 (32-II-2)	4.25 (27)	24.88 (27)
37	2	0.0 (32-II-2)	0.0 (32-I-4)	0.0 (29-I-2)	-26.34 (32-II-2)	6.68 (19)	-47.74 (27)
37	3	0.0 (32-II-2)	0.0 (32-I-4)	0.0 (31-I-4)	-156.78 (27)	-3.26 (19)	37.08 (32-I-4)
37	4	0.0 (32-II-2)	0.0 (32-I-4)	-0.0 (32-I-4)	-151.91 (32-I-4)	-20.03 (32-I-4)	-43.23 (31-I-4)
38	1	0.0 (27)	0.0 (27)	0.0 (30-I-2)	-30.72 (27)	-153.90 (32-II-4)	-49.36 (30-I-2)
38	2	-0.0 (30-I-4)	0.0 (27)	-0.0 (31-II-1)	9.77 (30-I-4)	21.55 (30-II-2)	-43.51 (30-II-2)
38	3	0.0 (27)	0.0 (27)	0.0 (30-I-3)	3.49 (32-I-1)	-157.70 (32-II-4)	21.90 (27)
38	4	0.0 (27)	0.0 (27)	0.0 (30-I-3)	17.40 (32-II-4)	20.27 (30-II-2)	24.73 (27)
39	1	-0.0 (30-II-1)	0.0 (27)	0.0 (30-II-2)	58.76 (19)	-170.31 (27)	-49.38 (30-II-2)
39	2	-0.0 (30-II-1)	0.0 (27)	0.0 (30-II-2)	58.90 (19)	6.14 (27)	-37.21 (30-II-2)
39	3	-0.0 (30-I-4)	0.0 (27)	0.0 (30-II-2)	-38.14 (27)	-166.53 (27)	-65.64 (30-II-2)
39	4	-0.0 (30-I-4)	0.0 (27)	0.0 (30-II-2)	24.77 (30-I-4)	11.74 (32-II-2)	-28.77 (30-II-2)
40	1	0.0 (32-I-4)	0.0 (32-II-2)	-0.0 (19)	-64.41 (32-I-4)	-194.32 (32-II-2)	43.52 (19)
40	2	-0.0 (19)	0.0 (32-II-2)	-0.0 (31-II-3)	14.94 (31-I-4)	10.43 (31-I-1)	23.67 (19)
40	3	-0.0 (19)	0.0 (32-II-2)	0.0 (30-II-2)	64.45 (19)	-185.16 (32-II-1)	37.11 (31-I-2)
40	4	-0.0 (19)	0.0 (32-I-2)	0.0 (30-II-2)	63.42 (19)	9.53 (32-I-4)	35.48 (27)
41	1	-0.1 (19)	-0.0 (31-I-2)	-0.0 (29-II-4)	407.30 (30-I-4)	52.56 (30-I-4)	1.97 (32-II-4)
41	2	-0.1 (19)	-0.0 (31-I-2)	-0.0 (29-II-4)	409.80 (30-I-4)	49.63 (30-I-4)	2.32 (32-II-4)
41	3	-0.1 (29-II-1)	-0.0 (32-I-4)	-0.0 (29-II-4)	409.90 (30-I-4)	49.62 (30-I-4)	4.73 (31-II-4)
41	4	-0.1 (29-I-1)	-0.0 (27)	0.0 (27)	407.91 (30-I-4)	52.61 (30-I-4)	-3.41 (30-II-2)
41	5	-0.1 (19)	-0.0 (31-I-2)	0.0 (31-I-4)	368.08 (30-I-4)	50.84 (30-I-4)	-3.01 (29-II-4)
41	6	-0.1 (19)	-0.1 (31-I-2)	-0.0 (29-II-4)	353.77 (30-I-4)	39.57 (30-I-4)	2.66 (31-I-4)
41	7	-0.1 (29-II-1)	-0.0 (27)	-0.0 (29-II-4)	354.02 (30-I-4)	39.57 (30-I-4)	5.39 (31-II-4)
41	8	-0.1 (29-II-4)	-0.0 (27)	0.0 (31-I-4)	368.84 (30-I-4)	51.00 (30-I-4)	3.55 (19)
41	9	-0.1 (19)	-0.1 (31-I-2)	0.1 (31-I-4)	368.39 (30-I-4)	26.32 (30-II-4)	-38.52 (30-I-3)
41	10	-0.0 (19)	-0.1 (27)	-0.0 (29-II-4)	258.91 (30-I-4)	53.75 (30-I-4)	-29.31 (30-I-4)
41	11	-0.1 (29-I-4)	-0.1 (31-II-2)	-0.1 (29-II-4)	259.07 (30-I-4)	53.84 (30-I-3)	28.03 (32-II-4)
41	12	-0.2 (29-II-4)	0.1 (29-I-2)	-0.0 (19)	369.07 (30-I-4)	26.91 (30-II-4)	37.09 (32-II-4)
41	13	0.4 (31-II-4)	-0.1 (27)	0.1 (19)	483.84 (30-I-4)	27.14 (29-II-4)	-234.61 (30-I-1)
41	14	-0.0 (31-I-4)	-0.1 (27)	-0.0 (29-II-4)	50.55 (30-I-4)	67.65 (30-I-4)	-45.20 (30-I-4)
41	15	0.0 (31-I-4)	-0.1 (31-I-4)	-0.0 (29-II-4)	50.59 (30-I-4)	67.85 (30-I-3)	44.38 (32-II-4)
41	16	-0.7 (29-II-4)	-0.1 (31-II-4)	-0.2 (29-II-4)	484.78 (30-II-4)	-46.31 (31-II-4)	234.70 (32-II-4)
42	1	-0.0 (31-I-2)	-0.1 (19)	-0.0 (29-II-4)	-86.48 (32-I-3)	-660.32 (32-I-3)	-2.99 (32-II-4)
42	2	-0.0 (31-I-2)	-0.1 (19)	0.0 (31-I-4)	-91.60 (32-I-3)	-629.92 (32-I-3)	-4.21 (31-II-4)
42	3	-0.1 (31-I-2)	-0.1 (19)	0.1 (31-I-4)	-54.35 (32-II-4)	-677.02 (32-I-3)	68.82 (30-II-1)
42	4	-0.1 (32-II-4)	0.4 (31-II-4)	0.1 (19)	26.86 (29-II-4)	-959.21 (32-I-3)	462.61 (30-I-3)
42	5	-0.0 (31-II-3)	-0.1 (19)	-0.0 (29-II-4)	-79.33 (32-I-4)	-667.70 (32-I-4)	-2.95 (32-II-4)
42	6	-0.1 (31-II-3)	-0.1 (19)	-0.0 (29-II-4)	-62.23 (32-I-3)	-604.21 (32-I-3)	-2.45 (32-II-4)
42	7	-0.1 (32-II-4)	-0.0 (19)	-0.0 (29-II-4)	-89.28 (32-I-3)	-463.31 (32-I-3)	51.87 (30-I-4)
42	8	-0.1 (32-I-2)	-0.0 (31-I-4)	-0.0 (29-II-4)	-113.52 (32-I-3)	-88.53 (30-I-3)	82.58 (30-I-4)
42	9	-0.0 (32-II-4)	-0.1 (29-II-3)	-0.0 (29-II-4)	-79.56 (30-I-4)	-669.10 (30-I-4)	9.45 (30-I-4)
42	10	-0.0 (32-II-4)	-0.1 (29-II-3)	-0.0 (29-II-4)	-62.49 (30-I-3)	-604.91 (30-I-4)	7.75 (30-I-4)
42	11	-0.1 (31-II-3)	-0.1 (29-I-4)	-0.1 (29-II-4)	-89.63 (30-I-3)	-463.44 (30-I-4)	-46.81 (32-II-4)
42	12	-0.1 (31-I-4)	0.0 (31-I-4)	-0.0 (29-II-4)	-113.88 (30-I-3)	-88.52 (30-I-4)	-78.66 (32-II-4)
42	13	-0.0 (32-II-4)	-0.1 (29-I-3)	0.0 (32-II-4)	-87.07 (30-I-4)	-664.18 (30-I-4)	9.28 (30-II-2)
42	14	-0.0 (32-II-1)	-0.1 (29-I-3)	0.0 (31-I-4)	-92.22 (30-I-3)	-631.68 (30-I-4)	9.12 (30-II-2)
42	15	0.1 (29-I-2)	-0.2 (29-II-4)	-0.0 (19)	-55.18 (30-II-4)	-677.46 (30-I-4)	-63.47 (32-II-4)
42	16	-0.1 (31-II-4)	-0.7 (29-II-4)	-0.2 (29-II-4)	-46.33 (29-II-4)	-959.70 (30-II-4)	-459.45 (32-II-4)
43	1	-0.1 (30-I-4)	-0.0 (31-II-1)	0.0 (27)	408.33 (30-I-4)	52.74 (30-I-4)	2.35 (32-II-4)
43	2	-0.1 (19)	-0.0 (32-I-4)	0.0 (27)	411.38 (30-I-4)	50.03 (30-I-4)	2.76 (32-II-4)
43	3	-0.1 (19)	-0.0 (19)	0.0 (27)	412.50 (30-I-4)	48.74 (30-I-4)	6.92 (19)
43	4	-0.2 (19)	-0.0 (32-I-4)	0.0 (32-I-4)	411.60 (30-I-4)	33.96 (30-I-4)	-18.49 (30-I-4)
43	5	-0.1 (19)	-0.0 (31-II-2)	0.0 (31-I-4)	369.08 (30-I-4)	51.26 (30-I-4)	-4.64 (29-I-4)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
43	6	-0.0 (19)	-0.0 (31-II-4)	0.0 (19)	354.36 (30-I-4)	40.13 (30-I-4)	-2.59 (30-I-4)
43	7	-0.1 (32-I-4)	-0.1 (19)	0.0 (27)	355.95 (30-I-4)	38.92 (30-I-4)	8.00 (19)
43	8	-0.2 (19)	-0.0 (19)	0.0 (31-I-4)	371.60 (30-I-4)	17.59 (30-I-4)	9.87 (19)
43	9	-0.1 (19)	-0.1 (31-II-2)	0.1 (31-I-4)	369.21 (30-I-4)	26.99 (30-II-4)	-38.24 (30-I-4)
43	10	-0.0 (19)	-0.0 (32-I-4)	0.1 (19)	259.49 (30-I-4)	54.73 (30-I-4)	-29.70 (30-I-4)
43	11	-0.1 (31-II-4)	-0.0 (19)	0.0 (19)	259.11 (30-I-4)	54.33 (30-I-4)	29.60 (32-II-4)
43	12	-0.2 (19)	-0.1 (19)	-0.1 (19)	371.69 (30-I-4)	39.78 (30-I-4)	64.91 (32-I-4)
43	13	0.4 (31-I-4)	-0.1 (31-I-1)	0.1 (19)	484.71 (30-II-4)	22.94 (29-I-4)	-234.76 (30-I-4)
43	14	-0.0 (31-I-4)	0.0 (19)	0.0 (19)	51.21 (30-I-4)	68.88 (30-I-4)	-45.49 (30-I-4)
43	15	0.0 (31-I-4)	0.1 (19)	0.0 (19)	48.20 (30-I-4)	70.84 (30-I-4)	45.73 (32-II-4)
43	16	-0.4 (31-II-4)	0.1 (29-I-4)	-0.1 (29-II-4)	488.65 (30-II-4)	-33.54 (31-II-4)	217.83 (32-II-4)
44	1	-0.0 (31-II-3)	-0.1 (30-II-4)	0.0 (32-II-4)	-87.19 (30-I-4)	-665.98 (30-I-4)	-3.07 (31-I-4)
44	2	-0.0 (31-II-3)	-0.1 (19)	0.0 (31-I-4)	-91.91 (30-I-4)	-632.23 (30-I-4)	-6.10 (31-I-4)
44	3	-0.1 (31-II-2)	-0.1 (19)	0.1 (31-I-4)	-54.18 (30-II-4)	-677.35 (30-I-4)	69.22 (30-I-4)
44	4	-0.1 (31-I-3)	0.4 (31-I-4)	0.1 (19)	23.07 (31-I-4)	-959.46 (30-II-4)	463.18 (30-I-3)
44	5	-0.0 (32-II-4)	-0.1 (19)	0.0 (32-II-4)	-79.73 (30-I-4)	-674.41 (30-I-4)	-2.49 (31-I-4)
44	6	-0.0 (31-II-4)	-0.0 (19)	0.0 (19)	-60.56 (30-I-4)	-605.76 (30-I-4)	3.64 (30-I-4)
44	7	-0.0 (32-II-4)	-0.0 (19)	0.1 (19)	-86.03 (30-I-4)	-463.33 (30-I-4)	54.09 (30-I-4)
44	8	0.0 (19)	-0.0 (31-I-4)	0.0 (19)	-109.36 (30-I-4)	-89.24 (30-I-4)	84.15 (30-I-4)
44	9	-0.0 (19)	-0.1 (19)	0.0 (32-I-1)	-76.02 (30-I-4)	-672.75 (30-I-4)	14.48 (30-I-4)
44	10	-0.1 (19)	-0.1 (32-II-4)	0.0 (32-II-1)	-55.01 (30-I-4)	-607.44 (30-I-4)	14.55 (30-I-4)
44	11	-0.0 (19)	-0.1 (31-II-4)	-0.0 (29-II-4)	-78.57 (30-I-4)	-462.57 (30-I-4)	-43.17 (32-II-4)
44	12	0.1 (19)	0.0 (31-I-4)	0.0 (19)	-102.76 (30-I-4)	-82.27 (30-I-4)	-76.17 (32-II-4)
44	13	-0.0 (32-II-4)	-0.2 (19)	0.0 (27)	-52.33 (30-I-4)	-660.03 (30-I-4)	40.41 (30-I-4)
44	14	-0.0 (19)	-0.2 (19)	0.0 (31-I-4)	-27.13 (30-I-4)	-633.69 (30-I-4)	12.84 (30-II-4)
44	15	-0.1 (19)	-0.2 (19)	-0.1 (19)	-68.15 (30-I-4)	-683.47 (30-I-4)	-102.13 (32-I-4)
44	16	0.1 (29-I-4)	-0.4 (31-II-4)	-0.1 (29-II-4)	-33.15 (29-II-4)	-968.68 (30-II-4)	-409.91 (32-II-4)
45	1	-0.0 (19)	0.0 (27)	0.0 (30-II-2)	37.50 (19)	-21.45 (27)	-26.32 (30-II-2)
45	2	-0.0 (19)	0.0 (27)	0.0 (30-II-2)	41.70 (19)	8.57 (27)	-5.03 (19)
45	3	-0.0 (30-I-4)	0.0 (27)	0.0 (30-II-2)	27.26 (30-I-3)	-19.93 (27)	-25.94 (30-II-2)
45	4	-0.0 (30-I-4)	0.0 (27)	0.0 (30-II-2)	28.74 (30-I-3)	7.79 (32-I-1)	-5.53 (19)
46	1	-0.0 (19)	0.0 (32-II-2)	-0.0 (19)	21.47 (19)	-23.18 (32-II-2)	18.87 (31-I-2)
46	2	-0.0 (19)	0.0 (32-II-2)	-0.0 (31-I-2)	23.02 (19)	8.15 (27)	6.48 (19)
46	3	-0.0 (19)	0.0 (32-II-2)	-0.0 (31-I-2)	39.45 (19)	-24.32 (32-II-2)	19.56 (31-II-1)
46	4	-0.0 (19)	0.0 (32-I-1)	-0.0 (31-II-1)	43.15 (19)	9.03 (32-II-2)	5.86 (19)
47	1	0.0 (27)	0.0 (31-II-4)	0.0 (27)	5.20 (27)	1.35 (27)	2.99 (27)
47	2	0.0 (27)	-0.0 (19)	0.0 (27)	5.53 (27)	3.43 (19)	-5.55 (27)
47	3	0.0 (19)	-0.0 (19)	0.0 (27)	-12.74 (19)	0	1.64 (30-II-2)
47	4	0.0 (30-II-2)	-0.0 (19)	0.0 (27)	-11.64 (32-II-2)	6.32 (19)	-14.10 (27)
48	1	-0.0 (30-I-3)	0.0 (27)	0.0 (30-II-2)	11.46 (30-I-4)	-14.92 (27)	-17.20 (30-II-2)
48	2	-0.0 (30-I-4)	0.0 (27)	0.0 (30-II-2)	9.41 (30-I-4)	6.63 (32-I-3)	-5.87 (30-I-3)
48	3	-0.0 (30-I-4)	0.0 (27)	0.0 (30-II-2)	4.24 (30-II-2)	-15.47 (27)	-4.97 (30-II-2)
48	4	-0.0 (30-I-4)	0.0 (32-I-2)	0.0 (30-II-2)	4.64 (30-II-2)	6.95 (32-I-3)	1.98 (27)

Verifiche stato limite ultimo

Verifica dei Muri in calcestruzzo

Scenario di calcolo: ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO

Simbologia:

Muro	Indice del muro in verifica
Nodi	[n1-n2-n3-n4...] Indici dei nodi di attacco del muro
Pann.X	Numero di pannelli in direzione locale X del muro(per muri a pannelli)
Pann.Y	Numero di pannelli in direzione locale Y del muro(per muri a pannelli)
Pann	Numero totale di pannelli (per muri a mesh)
Spess [cm]	Spessore del muro
Criterio	Criterio di verifica adottato per la verifica
Pannello	Indice del pannello
Nx [daN]	Sforzo in direzione x locale per metro lineare (Nx=sxx*spessore)
Ny [daN]	Sforzo in direzione y locale per metro lineare (Ny=syy*spessore)
Nxy [daN]	Sforzo tagliante locale per metro lineare (Nxy=sxy*spessore)
Mx [daN*m]	Momento in direzione x locale per metro lineare
My [daN*m]	Momento in direzione y locale per metro lineare
Mxy [daN*m]	Momento torcente locale per metro lineare
Ax [m^2]	Armatura totale pannello in direzione x locale (¹)
Ay [m^2]	Armatura totale pannello in direzione y locale (¹)
εc	Deformazione nel cls (²)
εf	Deformazione nell'acciaio (²)
Massimi	Armature massime riscontrate nel muro
Massimo	massima sigma ideale riscontrata nel muro

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E  
DEL RECAPITO FINALE DI SQUINZANO (LE)  
PROGETTO DEFINITIVO  
Tabulati di calcolo strutturale-Basamenti BTK1-BTK2-  
BTK3**

**R.37.13**

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$\sigma_{id+}, \sigma_{id-}$  [MPa]  $(\sigma_x^2 + \sigma_y^2 - \sigma_x \sigma_y + 3 \tau_{xy}^2)^{1/2}$  Tensioni ideali ai lembi della lastra (Acciaio)  
 $\sigma_{id+}, \sigma_{id-}$  [MPa]  $(\sigma_x^2 + \sigma_y^2 - \sigma_x \sigma_y + 3 \tau_{xy}^2)^{1/2}$  Tensioni ideali ai lembi della lastra (Legno)  
 Fatt.Ampl.Sisma Fattore moltiplicativo di gruppo per le azioni sismiche (solo se diverso da 1.0)  
 Cs Coefficiente di sicurezza definito dal rapporto  $|M_r(N)|/|M_d|$  ( $M_r(N)$ =Momento resistente corrispondente allo sforzo normale N,  $M_d$ =momento agente), quando richiesto dal criterio di verifica  
 $\zeta_e$  Livello di sicurezza sismico definito come rapporto tra l'accelerazione sopportabile e l'accelerazione di progetto, quando richiesto dal criterio di verifica

Note Verifica muri:  
 (1): Le armature  $A_x$  ed  $A_y$  vanno intese come a metro lineare di pannello.  
 (2): Le deformazioni sono stampate a meno del fattore  $10^{-3}$ ; esse si riferiscono alla verifica considerando quali sollecitazioni di progetto  $M_x, d=M_x \pm |M_{xy}|, M_y, d=M_y \pm |M_{xy}|$  scegliendo il segno in modo tale da rendere massimo in valore assoluto il relativo momento flettente, le sollecitazioni stampate si riferiscono alle sollecitazioni in una data combinazione riferite al sistema locale del pannello

Muro [Platea]: 1 - Nodi: [3-4-14-13]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=250.380$  [(12+13)-VIII-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	3991.06	197.55	364.11	-360.59	-66.25	-72.60	31.42	31.42	2	56
1	3990.73	126.14	-68.21	-325.18	18.64	18.08	31.42	31.42	11	71

Muro [Platea]: 2 - Nodi: [14-24-23-13]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=142.228$  [(12+13)-IV-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
3	-368.08	3715.00	-549.47	-61.03	-356.48	43.80	31.42	31.42	2	61
1	1028.70	3688.07	-239.73	-152.67	-281.09	-42.87	31.42	31.42	11	75

Muro [Platea]: 3 - Nodi: [34-44-43-33]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=682.300$  [(14+15)-VII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
2	593.21	3285.31	619.51	-179.74	-319.41	-95.37	31.42	31.42	11	59
1	760.95	3175.04	568.60	-127.49	-310.09	-97.20	31.42	31.42	11	60

Muro [Platea]: 4 - Nodi: [24-34-33-23]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=360.726$  [(12+13)-VIII-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
7	-447.74	3329.54	763.07	3.25	-315.64	-57.11	31.42	31.42	11	65
1	-920.10	3461.46	629.30	93.81	-249.24	-35.73	31.42	31.42	11	85

Muro : 5 - Nodi: [39-38-138-139], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=94.648$  [(12+13)-II-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
16	-690.38	-	-	-21.14	-	-553.11	31.42	31.42	11	4.6
		4074.10	2047.12		1156.14					
1	-290.54	-	-	-60.03	-765.96	-42.05	31.42	31.42	11	9.7
		3574.85	-16.64							

Muro : 6 - Nodi: [19-119-118-18], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=85.351$  [(12+13)-VI-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
13	-	15.28	1198.87	456.71	14.45	-207.64	31.42	31.42	10	12
	2319.49									
1	-	-248.64	59.66	436.23	36.60	14.49	31.42	31.42	10	17
	3416.81									

Muro : 7 - Nodi: [18-118-117-17], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=102.658$  [(12+13)-II-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
13	-4079.30	-659.40	1823.75	440.99	-3.13	-214.98	31.42	31.42	10	12
1	-2528.99	-171.76	-193.96	429.01	55.00	0.60	31.42	31.42	11	18

Muro [Platea]: 8 - Nodi: [30-29-19-20] Pann=4 Spess.=50 cm, Terreno=Terreno1, , Criterio=CLS\_Platee\_ND, Materiale=C35/45,  $\zeta_e=621.259$  [(14+15)-II-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
3	-41.57	3281.72	-50.82	4.92	278.47	-22.11	31.42	31.42	4	85
1	-39.85	3304.42	100.39	3.09	280.16	18.06	31.42	31.42	4	86

Muro : 9 - Nodi: [36-35-135-136], Pann.X=4, Pann.Y=4 Spess.=20 cm, Terreno=--, Criterio=CLS\_Muri\_ND, Materiale=C35/45,  $\zeta_e=117.368$  [(14+15)-IV-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	1625.75	4085.67	1846.41	-22.59	1156.37	557.02	31.42	31.42	10	4.6
1	-402.55	2596.05	-159.62	-101.63	-773.84	-3.58	31.42	31.42	11	10.0

Muro : 10 - Nodi: [37-36-136-137], Pann.X=4, Pann.Y=4 Spess.=20 cm, Terreno=--, Criterio=CLS\_Muri\_ND, Materiale=C35/45,  $\zeta_e=124.445$  [(14+15)-II-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	1286.76	4085.52	1848.57	-23.09	1156.45	556.59	31.42	31.42	10	4.6
1	-308.71	2614.95	-206.25	-101.82	-774.80	-4.39	31.42	31.42	11	10.0

Muro : 11 - Nodi: [17-117-116-16], Pann.X=4, Pann.Y=4 Spess.=20 cm, Terreno=--, Criterio=CLS\_Muri\_ND, Materiale=C35/45,  $\zeta_e=112.530$  [(14+15)-II-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
13	4086.29	-999.56	1852.45	440.81	-3.75	-214.65	31.42	31.42	10	12
1	2625.33	-281.47	-166.10	428.35	54.89	0.34	31.42	31.42	11	18

Muro : 12 - Nodi: [38-37-137-138], Pann.X=4, Pann.Y=4 Spess.=20 cm, Terreno=--, Criterio=CLS\_Muri\_ND, Materiale=C35/45,  $\zeta_e=113.352$  [(12+13)-II-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	-835.02	4077.86	1804.00	-23.03	1156.50	556.66	31.42	31.42	10	4.6
1	-189.27	2526.21	-272.69	-102.46	-779.30	-4.38	31.42	31.42	11	9.9

Muro : 13 - Nodi: [16-116-115-15], Pann.X=4, Pann.Y=4 Spess.=20 cm, Terreno=--, Criterio=CLS\_Muri\_ND, Materiale=C35/45,  $\zeta_e=101.909$  [(14+15)-IV-1] : **Verificato**

Armatura a maglia doppia

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Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
13	4085.85	1358.02	1837.40	440.85	-3.41	-214.57	31.42	31.42	10	12
1	2608.24	-376.94	-161.86	428.89	55.02	0.37	31.42	31.42	11	18

Muro [Platea]: 14 - Nodi: [35-34-24-25]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=536.445$  [(14+15)-VIII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
7	2626.40	-22.64	14.04	-328.97	-69.17	77.54	31.42	31.42	2	60
1	1142.04	1709.41	-941.22	-21.75	112.10	54.15	31.42	31.42	10	>100

Muro [Platea]: 15 - Nodi: [26-25-15-16]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=128.608$  [(12+13)-VI-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
3	303.90	1199.82	-200.15	17.20	352.24	53.20	31.42	31.42	10	62
1	449.68	1834.99	151.95	27.28	274.00	108.09	31.42	31.42	10	67

Muro [Platea]: 16 - Nodi: [25-24-14-15]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=110.622$  [(12+13)-II-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
8	2806.42	848.59	-464.78	-355.43	-164.11	-61.31	31.42	31.42	11	59
1	1191.09	1451.28	176.06	15.01	237.07	102.17	31.42	31.42	10	75

Muro [Platea]: 17 - Nodi: [36-35-25-26]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=295.479$  [(12+13)-II-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
6	504.09	1962.96	-271.47	-28.85	358.43	26.88	31.42	31.42	9	66
1	-523.53	-741.20	-29.75	83.84	7.31	-51.61	31.42	31.42	(12+13)-II-3	>100

Muro [Platea]: 18 - Nodi: [38-37-27-28]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=276.569$  [(12+13)-VI-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
6	-186.91	2287.41	-29.67	35.55	393.26	16.14	31.42	31.42	4	62
1	-58.01	2126.82	-430.20	-0.65	123.95	-16.81	31.42	31.42	10	>100

Muro [Platea]: 19 - Nodi: [28-27-17-18]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=411.535$  [(14+15)-II-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs



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Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
3	15.09	-2456.44	-83.20	20.45	385.72	26.68	31.42	31.42	9	62
1	126.28	-2857.43	187.92	14.31	322.17	67.26	31.42	31.42	9	66

Muro [Platea]: 20 - Nodi: [37-36-26-27]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45, $\zeta_e=190.364$  [(12+13)-VIII-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
6	218.63	-2182.63	-148.40	-0.69	386.41	23.82	31.42	31.42	9	62
1	1017.20	-906.25	-38.39	98.51	16.09	-56.69	31.42	31.42	(12+13)-II-3	>100

Muro [Platea]: 21 - Nodi: [27-26-16-17]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45, $\zeta_e=140.392$  [(14+15)-II-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
3	-44.90	1366.88	-192.31	37.77	371.35	45.36	31.42	31.42	10	61
1	293.99	-2869.93	216.84	5.33	325.75	67.03	31.42	31.42	9	65

Muro [Platea]: 22 - Nodi: [5-6-16-15]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45, $\zeta_e=376.140$  [(12+13)-VII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
2	1885.52	81.56	-60.05	-179.67	-20.36	21.40	31.42	31.42	11	>100
1	2062.20	73.30	32.58	-179.98	7.57	-6.69	31.42	31.42	2	>100

Muro [Platea]: 23 - Nodi: [47-46-36-37]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45, $\zeta_e=823.447$  [(14+15)-V-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
8	1431.44	619.24	-426.78	-137.56	-96.20	8.58	31.42	31.42	11	>100
1	-876.80	68.12	92.01	93.90	9.50	3.92	31.42	31.42	(12+13)-V-3	>100

Muro [Platea]: 24 - Nodi: [45-44-34-35]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45, $\zeta_e=671.681$  [(14+15)-V-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
6	2840.59	559.37	-712.58	-251.01	-141.61	62.48	31.42	31.42	11	78
1	2415.14	265.23	-173.05	-196.12	22.57	44.37	31.42	31.42	11	>100

Muro [Platea]: 25 - Nodi: [4-5-15-14]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45, $\zeta_e=645.629$  [(14+15)-III-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
2	3061.65	80.51	39.95	-280.96	-20.03	14.87	31.42	31.42	11	83
1	3078.28	45.72	-53.29	-280.87	3.24	-11.36	31.42	31.42	11	84

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Muro [Platea]: 26 - Nodi: [6-7-17-16]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,  $\zeta_e=805.064$  [(14+15)-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
2	1079.35	78.98	-91.69	-110.89	-19.80	22.77	31.42	31.42	11	>100
1	1269.32	71.14	-4.08	-116.06	7.24	-4.82	31.42	31.42	2	>100

Muro [Platea]: 27 - Nodi: [7-8-18-17]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,  $\zeta_e=1154.411$  [(14+15)-VI-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
6	-960.71	39.00	175.54	88.06	-6.81	-47.89	31.42	31.42	(12+13)-I-3	>100
1	-917.23	32.59	109.94	89.65	6.59	0.48	31.42	31.42	(12+13)-III-4	>100

Muro [Platea]: 28 - Nodi: [38-48-47-37]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,  $\zeta_e=1010.665$  [(12+13)-II-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
3	454.51	670.14	202.03	-123.21	-69.54	-6.85	31.42	31.42	11	>100
1	601.25	496.14	8.24	-90.56	-33.52	-20.71	31.42	31.42	11	>100

Muro [Platea]: 29 - Nodi: [46-45-35-36]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,  $\zeta_e=433.581$  [(12+13)-VII-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
8	2206.75	659.58	-608.75	-196.82	-99.71	24.95	31.42	31.42	11	>100
1	1653.32	249.07	-57.02	-124.89	23.64	34.68	31.42	31.42	11	>100

Muro [Platea]: 30 - Nodi: [39-38-28-29]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,  $\zeta_e=203.234$  [(12+13)-VI-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
6	-214.85	2298.86	23.75	36.57	388.90	14.58	31.42	31.42	4	63
1	-156.59	34.68	-399.40	-46.90	-87.67	-58.24	31.42	31.42	(14+15)-VI-4	>100

Muro [Platea]: 31 - Nodi: [29-28-18-19]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,  $\zeta_e=115.423$  [(12+13)-II-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
5	-515.57	1691.20	164.93	70.78	342.86	-55.08	31.42	31.42	(12+13)-II-3	64
1	37.68	2988.00	251.60	15.89	320.89	57.45	31.42	31.42	4	68

Muro [Platea]: 32 - Nodi: [40-39-29-30]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45,  $\zeta_e=376.602$  [(12+13)-V-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
4	-37.04	3138.21	12.53	4.84	267.32	29.61	31.42	31.42	4	86
1	5.57	1504.76	-59.81	-0.80	121.38	-16.82	31.42	31.42	10	>100

Muro [Platea]: 33 - Nodi: [9-10-20-19]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=2416.787$  [(14+15)-II-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	-3.95	506.59	90.93	0.51	-45.46	-11.94	31.42	31.42	11	>100
1	36.83	59.77	60.92	-4.84	-3.30	-2.69	31.42	31.42	10	>100

Muro [Platea]: 34 - Nodi: [39-49-48-38]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=980.674$  [(12+13)-II-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
3	461.24	282.83	99.75	-126.59	-37.42	1.54	31.42	31.42	11	>100
1	468.34	124.85	-60.20	-81.15	-36.49	-26.29	31.42	31.42	(14+15)-VI-4	>100

Muro [Platea]: 35 - Nodi: [40-50-49-39]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=1196.849$  [(14+15)-VI-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
1	769.81	11.78	28.33	-68.01	-1.10	-14.80	31.42	31.42	(14+15)-VI-4	>100

Muro [Platea]: 36 - Nodi: [8-9-19-18]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=271.689$  [(12+13)-II-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
2	-361.66	93.89	111.28	65.13	-14.98	-29.62	31.42	31.42	(12+13)-VI-3	>100
1	-430.69	60.89	129.06	69.33	9.36	13.36	31.42	31.42	(12+13)-V-3	>100

Muro [Platea]: 37 - Nodi: [2-3-13-12]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=352.211$  [(14+15)-II-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	2081.51	76.51	45.80	-221.78	-17.17	-64.68	31.42	31.42	2	86
1	688.66	-2.29	216.31	-21.53	5.61	32.64	31.42	31.42	11	>100

Muro [Platea]: 38 - Nodi: [33-43-42-32]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=1134.388$  [(12+13)-VI-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
3	80.24	1806.88	36.57	2.58	-224.45	36.57	31.42	31.42	2	95
1	122.28	1586.35	85.94	-42.75	-223.72	-37.23	31.42	31.42	11	95

Muro [Platea]: 39 - Nodi: [23-33-32-22]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=563.842$  [(14+15)-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
1	-425.15	1780.51	241.33	30.92	-248.04	-45.55	31.42	31.42	11	84

Muro [Platea]: 40 - Nodi: [13-23-22-12]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=288.647$  [(14+15)-VIII-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
1	-128.54	1808.00	-797.65	-21.53	-261.02	61.85	31.42	31.42	2	76

Muro : 41 - Nodi: [15-115-114-14], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=104.328$  [(14+15)-IV-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	4058.82	2821.94	1775.68	441.12	-2.28	214.10	31.42	31.42	11	12
1	2467.56	-424.82	8.96	429.75	55.20	0.93	31.42	31.42	11	18

Muro : 42 - Nodi: [35-34-134-135], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=115.557$  [(14+15)-VIII-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
4	1970.96	4084.03	1854.26	-23.31	1156.53	557.25	31.42	31.42	10	4.6
1	-436.48	2454.81	55.22	-101.79	-774.88	-2.55	31.42	31.42	11	10.0

Muro : 43 - Nodi: [14-114-113-13], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=75.335$  [(12+13)-IV-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
16	2365.65	-67.94	1109.61	456.89	14.63	207.44	31.42	31.42	10	12
1	1747.81	-368.87	792.57	431.16	55.44	1.93	31.42	31.42	11	18

Muro : 44 - Nodi: [34-33-133-134], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND,  
Materiale=C35/45, $\zeta_e=84.182$  [(12+13)-VIII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
4	1590.22	4060.26	2101.88	-22.71	1156.51	556.47	31.42	31.42	10	4.6
1	-364.38	1828.29	813.50	-102.93	-783.96	-2.52	31.42	31.42	11	9.8

Muro [Platea]: 45 - Nodi: [22-32-31-21]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=527.025$  [(14+15)-VII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx daN	Ny daN	Nxy daN	Mx daN*m	My daN*m	Mxy daN*m	Ax cmq	Ay cmq	C	Cs
2	-628.88	97.33	-25.17	60.03	11.13	-7.33	31.42	31.42	9	>100
1	-529.69	111.99	213.73	35.10	-27.05	-29.93	31.42	31.42	10	>100

Muro [Platea]: 46 - Nodi: [12-22-21-11]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=606.288$  [(14+15)-I-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
3	-714.79	138.56	-148.57	56.89	-30.87	16.54	31.42	31.42	9	>100
1	-337.75	120.37	-282.84	31.21	-25.45	28.90	31.42	31.42	2	>100

Muro [Platea]: 47 - Nodi: [1-2-12-11]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=2545.674$  [(14+15)-VII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
4	10.70	-112.08	167.95	-13.77	8.15	-22.55	31.42	31.42	2	>100
1	51.83	6.18	24.82	7.91	2.06	4.64	31.42	31.42	2	>100

Muro [Platea]: 48 - Nodi: [32-42-41-31]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND,  
Materiale=C35/45, $\zeta_e=1654.166$  [(12+13)-IV-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	daN	daN	daN	daN*m	daN*m	daN*m	cmq	cmq		
1	-217.47	16.34	189.70	14.49	-12.53	-20.78	31.42	31.42	10	>100

#### Verifiche stato limite di esercizio

##### Verifica dei Muri (Stati limite esercizio)

Scenario di calcolo: **ScenarioNT\_2018 A2\_SLV\_SLD\_STR\_GEO**

#### Simbologia

P.	Numero pannello
Nx [MPa]	Sforzo normale in direzione x
Ny [MPa]	Sforzo normale in direzione y
Nxy [MPa]	Sforzo tagliante in direzione xy
Mx [daN]	Momento flettente in direzione x
My [daN]	Momento flettente in direzione y
Mxy [daN]	Momento torcente
Afx [cmq/m]	Area acciaio in direzione x per metro lineare
Afy [cmq/m]	Area acciaio in direzione y per metro lineare
$\sigma_c$ [MPa]	Tensione nel calcestruzzo compresso
$\sigma_f$ [MPa]	Tensione nell'acciaio
$\sigma_{ct}$ [MPa]	Tensione nel calcestruzzo teso
$\sigma_{sct}$ [MPa]	Tensione nel calcestruzzo teso (quando richiesto dalla verifica)
$\sigma_{sca}$ [MPa]	Tensione ammissibile nel calcestruzzo
$\sigma_{sfa}$ [MPa]	Tensione ammissibile nell'acciaio
$\sigma_{scta}$ [MPa]	Tensione ammissibile nel calcestruzzo teso
Cbc	Combinazione generatore della tensione nel cls compresso
Cbct	Combinazione generatore della tensione nel cls teso
Cbf	Combinazione generatore della tensione nell'acciaio
Cb	Combinazione
$\sigma_{fmed}$ [MPa]	Tensione media dell'acciaio
Wd [mm]	Apertura delle fessure
Wk [mm]	Apertura caratteristica delle fessure
Wamm_Freq [mm]	Apertura ammissibile delle fessure per combinazione Frequente
Wamm_Qp [mm]	Apertura ammissibile delle fessure per combinazione Quasi Permanente
Wamm_Rara [mm]	Apertura ammissibile delle fessure per combinazione Rara
Cs	Coefficiente di sicurezza definito come minimo di $\sigma_{Amm}/\sigma$ tra acciaio e calcestruzzo oppure Wamm/Wk

Muro [Platea]: 1 - Nodi: [3-4-14-13]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.01	12.72	22	22	Si	28
3	31.42	31.42	-0.01	13.04	22	22	Si	28

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.01	10.32	28	28	Si	35

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
2	0.0	0.0	0.0	-172.95	-27.50	-30.30	10.11	0.017	0.017	28 (Qp)	Si	12
2	0.0	0.0	0.0	-171.53	-25.49	-20.71	9.87	0.017	0.017	26 (Fr)	Si	18

Muro [Platea]: 2 - Nodi: [14-24-23-13]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.04	12.45	22	22	Si	29
3	31.42	31.42	-0.04	12.53	22	22	Si	29

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.05	8.28	28	28	Si	43
3	31.42	31.42	-0.02	9.63	28	28	Si	37

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
3	-0.0	0.0	-0.0	-39.10	-200.40	37.41	9.63	0.015	0.015	28 (Qp)	Si	13
3	-0.0	0.0	-0.0	-38.68	-195.18	38.31	9.33	0.015	0.015	23 (Fr)	Si	20

Muro [Platea]: 3 - Nodi: [34-44-43-33]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.03	10.74	22	22	Si	34

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.02	8.50	28	28	Si	42

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	0.0	0.0	0.0	-39.38	-128.99	-5.30	7.95	0.014	0.014	28 (Qp)	Si	14
4	0.0	0.0	0.0	-38.05	-124.16	-6.99	7.69	0.013	0.013	23 (Fr)	Si	22

Muro [Platea]: 4 - Nodi: [24-34-33-23]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	31.42	31.42	-0.03	10.31	22	22	Si	35
2	31.42	31.42	-0.02	10.87	22	22	Si	33

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.04	8.06	28	28	Si	45
7	31.42	31.42	-0.03	8.79	28	28	Si	41

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σfmed	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
6	-0.0	0.0	0.0	-62.64	-169.72	-31.81	8.59	0.014	0.014	28 (Qp)	Si	14
6	-0.0	0.0	0.0	-43.06	-160.51	-40.12	8.17	0.013	0.013	26 (Fr)	Si	23

Muro : 5 - Nodi: [39-38-138-139], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σca[MPa]=22.41 σfa[MPa]=360.00

P.	Afx	Afy	σc	σf	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-1.99	35.81	22	22	Si	10

Combinazione QP: σca[MPa]=16.81 σfa[MPa]=360.00

P.	Afx	Afy	σc	σf	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.59	7.46	28	28	Si	28

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σfmed	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	0.0	-0.1	0.0	5.01	-240.79	99.10	5.18	0.004	0.004	25 (Fr)	Si	80
8	0.1	0.0	-0.0	-15.52	-17.00	15.97	4.86	0.006	0.006	28 (Qp)	Si	33

Muro : 6 - Nodi: [19-119-118-18], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σca[MPa]=22.41 σfa[MPa]=360.00

P.	Afx	Afy	σc	σf	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
13	31.42	31.42	-0.76	10.73	22	22	Si	30

Combinazione QP: σca[MPa]=16.81 σfa[MPa]=360.00

P.	Afx	Afy	σc	σf	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
13	31.42	31.42	-0.59	7.46	28	28	Si	28

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σfmed	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
14	0.0	0.1	-0.0	-17.05	-15.71	15.81	4.88	0.006	0.006	28 (Qp)	Si	33
14	0.0	0.0	-0.0	-17.31	-17.13	16.16	4.26	0.005	0.005	25 (Fr)	Si	60

Muro : 7 - Nodi: [18-118-117-17], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σca[MPa]=22.41 σfa[MPa]=360.00

P.	Afx	Afy	σc	σf	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.71	10.10	22	22	Si	31

Combinazione QP: σca[MPa]=16.81 σfa[MPa]=360.00

P.	Afx	Afy	σc	σf	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
13	31.42	31.42	-0.56	3.94	28	28	Si	30

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	σfmed	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
9	-0.1	0.0	0.0	-77.38	-8.24	6.57	0.45	0.000	0.000	26 (Fr)	Si	>100
13	-0.1	-0.0	0.1	-238.85	-8.84	113.70	3.94	0.003	0.003	28 (Qp)	Si	72

Muro [Platea]: 8 - Nodi: [30-29-19-20]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σca[MPa]=22.41 σfa[MPa]=360.00

P.	Afx	Afy	σc	σf	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	31.42	31.42	-0.05	-0.00	22	22	Si	>100
4	31.42	31.42	-0.00	1.22	22	22	Si	>100

Combinazione QP: σca[MPa]=16.81 σfa[MPa]=360.00

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P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	31.42	31.42	-0.08	-0.00	28	28	Si	>100
4	31.42	31.42	-0.03	0.13	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	0.0	-0.0	-0.0	-3.12	57.21	-16.17	0.13	0.000	0.000	28 (Qp)	Si	>100
4	0.0	-0.0	-0.0	-3.00	59.73	-15.42	0.13	0.000	0.000	25 (Fr)	Si	>100

Muro : 9 - Nodi: [36-35-135-136], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	31.42	31.42	-1.94	31.10	22	22	Si	12
4	31.42	31.42	-1.94	31.11	22	22	Si	12

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	31.42	31.42	-0.56	3.92	28	28	Si	30
4	31.42	31.42	-0.56	3.93	28	28	Si	30

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.1	-0.1	0.1	-8.72	-238.84	114.41	3.93	0.003	0.003	28 (Qp)	Si	72
16	-0.1	-0.1	-0.1	-8.75	-238.85	-112.74	3.92	0.003	0.003	23 (Fr)	Si	>100

Muro : 10 - Nodi: [37-36-136-137], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-1.94	31.11	22	22	Si	12

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.56	3.93	28	28	Si	30

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.0	-0.1	0.1	-8.93	-238.87	114.22	3.93	0.003	0.003	28 (Qp)	Si	72
16	-0.1	-0.1	-0.1	-8.74	-238.84	-112.99	3.92	0.003	0.003	24 (Fr)	Si	>100

Muro : 11 - Nodi: [17-117-116-16], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.71	10.03	22	22	Si	31

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
13	31.42	31.42	-0.56	3.93	28	28	Si	30

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
10	-0.0	-0.0	0.0	-48.90	-7.38	4.65	0.37	0.000	0.000	26 (Fr)	Si	>100
13	-0.1	-0.0	0.1	-238.89	-9.03	113.73	3.93	0.003	0.003	28 (Qp)	Si	72

Muro : 12 - Nodi: [38-37-137-138], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00



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P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-1.94	31.13	22	22	Si	12

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	31.42	31.42	-0.56	3.92	28	28	Si	30
4	31.42	31.42	-0.56	3.94	28	28	Si	30

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.0	-0.1	0.1	-8.62	-238.82	114.03	3.94	0.003	0.003	28 (Qp)	Si	72
16	-0.0	-0.1	-0.1	-8.99	-238.88	-113.14	3.92	0.003	0.003	23 (Fr)	Si	>100

Muro : 13 - Nodi: [16-116-115-15], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.71	10.20	22	22	Si	31

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
13	31.42	31.42	-0.56	3.93	28	28	Si	30

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
11	-0.0	-0.0	-0.0	-48.68	-7.08	-4.60	0.36	0.000	0.000	26 (Fr)	Si	>100
13	-0.1	-0.1	0.1	-238.83	-8.68	113.89	3.93	0.003	0.003	28 (Qp)	Si	72

Muro [Platea]: 14 - Nodi: [35-34-24-25]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.04	5.98	22	22	Si	60
7	31.42	31.42	-0.02	9.18	22	22	Si	39

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.07	3.59	28	28	Si	>100
7	31.42	31.42	-0.01	6.62	28	28	Si	54

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
7	0.0	-0.0	-0.0	-174.67	-32.15	68.02	6.62	0.009	0.009	28 (Qp)	Si	21
8	0.0	-0.0	-0.0	-154.37	124.12	42.01	5.90	0.008	0.008	26 (Fr)	Si	36

Muro [Platea]: 15 - Nodi: [26-25-15-16]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.07	3.84	22	22	Si	94
8	31.42	31.42	-0.03	6.33	22	22	Si	57

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.08	1.26	28	28	Si	>100
8	31.42	31.42	-0.02	3.40	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			

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P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
6	0.0	-0.0	-0.0	-69.27	-21.71	-18.23	3.09	0.005	0.005	28 (Qp)	Si	42
6	0.0	-0.0	-0.0	-63.41	-21.53	-17.52	2.78	0.004	0.004	23 (Fr)	Si	71

Muro [Platea]: 16 - Nodi: [25-24-14-15]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.05	6.74	22	22	Si	53
8	31.42	31.42	-0.02	10.10	22	22	Si	36

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.07	3.64	28	28	Si	99
8	31.42	31.42	-0.01	6.99	28	28	Si	51

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	-0.0	0.0	-181.73	1.48	-57.75	6.99	0.010	0.010	28 (Qp)	Si	20
8	0.0	-0.0	0.0	-175.71	2.19	-58.16	6.64	0.009	0.009	23 (Fr)	Si	32

Muro [Platea]: 17 - Nodi: [36-35-25-26]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.06	3.88	22	22	Si	93
7	31.42	31.42	-0.02	6.01	22	22	Si	60

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.09	1.30	28	28	Si	>100
7	31.42	31.42	-0.01	3.47	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
5	0.0	-0.0	-0.0	-73.53	-58.16	30.76	3.27	0.005	0.005	28 (Qp)	Si	40
5	0.0	-0.0	-0.0	-65.74	-37.01	35.06	2.89	0.004	0.004	26 (Fr)	Si	68

Muro [Platea]: 18 - Nodi: [38-37-27-28]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.06	0.41	22	22	Si	>100
7	31.42	31.42	-0.03	1.68	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.09	0.62	28	28	Si	>100
5	31.42	31.42	-0.03	0.90	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
7	0.0	-0.0	0.0	-26.83	-3.79	45.45	0.68	0.001	0.001	28 (Qp)	Si	>100
7	0.0	-0.0	0.0	-22.00	14.20	45.28	0.51	0.001	0.001	26 (Fr)	Si	>100

Muro [Platea]: 19 - Nodi: [28-27-17-18]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.08	1.50	22	22	Si	>100

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
8	31.42	31.42	-0.03	2.31	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.09	0.43	28	28	Si	>100
6	31.42	31.42	-0.03	0.63	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	-0.0	-0.0	-22.06	23.33	-31.36	0.47	0.001	0.001	28 (Qp)	Si	>100
8	0.0	-0.0	-0.0	-18.49	24.55	-31.43	0.32	0.000	0.000	24 (Fr)	Si	>100

Muro [Platea]: 20 - Nodi: [37-36-26-27]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.06	1.82	22	22	Si	>100
7	31.42	31.42	-0.03	3.65	22	22	Si	99

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.09	0.66	28	28	Si	>100
5	31.42	31.42	-0.03	1.81	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
5	0.0	-0.0	-0.0	-45.12	-54.45	17.96	1.81	0.003	0.003	28 (Qp)	Si	76
5	0.0	-0.0	-0.0	-39.06	-33.06	20.89	1.53	0.002	0.002	26 (Fr)	Si	>100

Muro [Platea]: 21 - Nodi: [27-26-16-17]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.07	1.76	22	22	Si	>100
8	31.42	31.42	-0.03	3.82	22	22	Si	94

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.09	0.46	28	28	Si	>100
6	31.42	31.42	-0.03	1.55	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	0.0	-0.0	-0.0	-24.13	-18.53	3.91	1.06	0.002	0.002	24 (Fr)	Si	>100
6	0.0	-0.0	-0.0	-39.41	-20.48	-6.33	1.55	0.002	0.002	28 (Qp)	Si	90

Muro [Platea]: 22 - Nodi: [5-6-16-15]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	5.60	22	22	Si	64
2	31.42	31.42	-0.00	6.23	22	22	Si	58

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	3.55	28	28	Si	>100
2	31.42	31.42	-0.00	4.06	28	28	Si	89

Verifica aperture fessure:Wamm\_Freq[mm]=0.300 Wamm\_Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
2	0.0	0.0	0.0	-79.15	-13.13	0.04	4.06	0.007	0.007	28 (Qp)	Si	30
2	0.0	0.0	0.0	-72.56	-11.85	3.39	3.64	0.006	0.006	26 (Fr)	Si	51

Muro [Platea]: 23 - Nodi: [47-46-36-37]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.02	4.20	22	22	Si	86
8	31.42	31.42	-0.00	4.75	22	22	Si	76

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.01	2.18	28	28	Si	>100
8	31.42	31.42	-0.00	2.46	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	0.0	-0.0	-50.53	-30.55	4.99	2.46	0.004	0.004	28 (Qp)	Si	51
8	0.0	0.0	-0.0	-45.14	-28.80	6.38	2.23	0.004	0.004	24 (Fr)	Si	84

Muro [Platea]: 24 - Nodi: [45-44-34-35]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.02	9.05	22	22	Si	40
8	31.42	31.42	0.00	9.70	16	22	Si	37

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.01	6.14	28	28	Si	59
8	31.42	31.42	-0.00	6.87	28	28	Si	52

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
7	0.0	0.0	-0.0	-131.48	7.26	12.50	6.84	0.011	0.011	28 (Qp)	Si	18
7	0.0	0.0	-0.0	-125.05	6.98	13.31	6.51	0.011	0.011	23 (Fr)	Si	28

Muro [Platea]: 25 - Nodi: [4-5-15-14]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	8.78	22	22	Si	41
1	31.42	31.42	0.00	9.87	16	22	Si	36

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	6.37	28	28	Si	56
2	31.42	31.42	-0.00	7.42	28	28	Si	48

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
2	0.0	0.0	0.0	-140.98	-14.52	-9.84	7.42	0.012	0.012	28 (Qp)	Si	16
2	0.0	0.0	0.0	-135.60	-13.20	-5.34	7.04	0.012	0.012	26 (Fr)	Si	26

Muro [Platea]: 26 - Nodi: [6-7-17-16]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
4	31.42	31.42	-0.00	3.25	22	22	Si	>100
1	31.42	31.42	0.00	3.74	16	22	Si	96

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	1.94	28	28	Si	>100
2	31.42	31.42	-0.00	2.22	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	-0.0	-44.52	3.27	-2.27	2.21	0.004	0.004	28 (Qp)	Si	56
1	0.0	0.0	-0.0	-39.16	2.62	-2.05	1.87	0.003	0.003	26 (Fr)	Si	>100

Muro [Platea]: 27 - Nodi: [7-8-18-17]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	1.46	22	22	Si	>100
1	31.42	31.42	-0.00	1.82	18	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	0.99	28	28	Si	>100
1	31.42	31.42	0.00	1.14	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	-0.0	-24.48	3.12	-1.21	1.14	0.002	0.002	28 (Qp)	Si	>100
1	0.0	0.0	-0.0	-20.94	2.52	-1.02	0.93	0.001	0.001	26 (Fr)	Si	>100

Muro [Platea]: 28 - Nodi: [38-48-47-37]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.02	2.32	22	22	Si	>100
4	31.42	31.42	-0.00	2.73	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.01	1.21	28	28	Si	>100
4	31.42	31.42	-0.00	1.37	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	0.0	0.0	0.0	-27.36	-29.11	-1.60	1.37	0.002	0.002	28 (Qp)	Si	93
4	0.0	0.0	0.0	-25.59	-25.88	-2.76	1.25	0.002	0.002	24 (Fr)	Si	>100

Muro [Platea]: 29 - Nodi: [46-45-35-36]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.02	6.48	22	22	Si	56
8	31.42	31.42	-0.00	7.09	22	22	Si	51

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.01	3.73	28	28	Si	97
8	31.42	31.42	-0.00	4.20	28	28	Si	86

Verifica aperture fessure:Wamm\_Freq[mm]=0.300 Wamm\_Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
8	0.0	0.0	-0.0	-83.91	-34.26	11.79	4.20	0.007	0.007	28 (Qp)	Si	30
8	0.0	0.0	-0.0	-77.18	-32.67	13.33	3.89	0.006	0.006	24 (Fr)	Si	48

Muro [Platea]: 30 - Nodi: [39-38-28-29]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.07	0.15	22	22	Si	>100
3	31.42	31.42	-0.03	0.50	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.09	0.58	28	28	Si	>100
3	31.42	31.42	-0.03	0.75	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
6	-0.0	-0.0	0.0	22.85	255.26	8.32	0.58	0.001	0.001	28 (Qp)	Si	>100
6	-0.0	-0.0	0.0	22.96	253.64	9.73	0.47	0.000	0.000	26 (Fr)	Si	>100

Muro [Platea]: 31 - Nodi: [29-28-18-19]Pann=8Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
5	31.42	31.42	-0.07	1.33	22	22	Si	>100
8	31.42	31.42	-0.03	2.12	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
5	31.42	31.42	-0.09	0.40	28	28	Si	>100
4	31.42	31.42	-0.02	0.62	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	-0.0	0.0	11.66	211.00	38.06	0.28	0.000	0.000	28 (Qp)	Si	>100
1	0.0	-0.0	0.0	11.47	214.90	38.69	0.27	0.000	0.000	24 (Fr)	Si	>100

Muro [Platea]: 32 - Nodi: [40-39-29-30]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.06	-0.00	22	22	Si	>100
3	31.42	31.42	-0.02	0.09	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.07	-0.00	28	28	Si	>100
3	31.42	31.42	-0.02	0.14	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
3	0.0	-0.0	-0.0	-3.44	35.30	20.31	0.14	0.000	0.000	28 (Qp)	Si	>100
3	0.0	-0.0	0.0	-3.11	46.75	18.76	0.13	0.000	0.000	26 (Fr)	Si	>100

Muro [Platea]: 33 - Nodi: [9-10-20-19]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
1	31.42	31.42	-0.00	0.18	20	22	Si	>100
4	31.42	31.42	-0.00	1.60	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	31.42	31.42	-0.00	0.10	28	28	Si	>100
4	31.42	31.42	0.00	0.67	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	0.0	0.0	0.0	-1.42	-12.67	-6.45	0.67	0.001	0.001	28 (Qp)	Si	>100
4	0.0	0.0	0.0	-1.45	-11.60	-6.20	0.62	0.001	0.001	25 (Fr)	Si	>100

Muro [Platea]: 34 - Nodi: [39-49-48-38]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.02	2.36	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.01	0.92	28	28	Si	>100
4	31.42	31.42	-0.00	0.93	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
3	0.0	0.0	0.0	-34.98	-16.75	-0.58	0.92	0.001	0.001	28 (Qp)	Si	>100
3	0.0	0.0	0.0	-32.72	-16.42	-1.17	0.86	0.001	0.001	23 (Fr)	Si	>100

Muro [Platea]: 35 - Nodi: [40-50-49-39]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.00	0.06	22	22	Si	>100
2	31.42	31.42	0.00	1.47	16	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.00	0.03	28	28	Si	>100
1	31.42	31.42	0.00	1.16	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	0.0	0.0	0.0	-21.95	-1.19	-6.78	1.16	0.002	0.002	28 (Qp)	Si	>100
1	0.0	0.0	0.0	-19.86	-1.20	-6.46	1.05	0.002	0.002	25 (Fr)	Si	>100

Muro [Platea]: 36 - Nodi: [8-9-19-18]Pann=8Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
8	31.42	31.42	-0.00	0.77	22	22	Si	>100
5	31.42	31.42	-0.00	0.95	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
6	31.42	31.42	-0.00	0.87	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			

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P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
8	0.0	0.0	0.0	-15.30	-9.10	-5.70	0.87	0.001	0.001	28 (Qp)	Si	>100
8	0.0	0.0	0.0	-14.66	-13.93	-6.93	0.83	0.001	0.001	27 (Fr)	Si	>100

Muro [Platea]: 37 - Nodi: [2-3-13-12]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.00	2.10	20	22	Si	>100
3	31.42	31.42	-0.00	7.39	20	22	Si	49

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.00	1.50	28	28	Si	>100
3	31.42	31.42	-0.00	6.11	28	28	Si	59

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
3	0.0	0.0	0.0	-131.38	-2.81	22.96	6.11	0.010	0.010	28 (Qp)	Si	21
3	0.0	0.0	0.0	-128.06	-2.79	22.29	5.96	0.009	0.009	23 (Fr)	Si	32

Muro [Platea]: 38 - Nodi: [33-43-42-32]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	31.42	31.42	-0.01	5.94	22	22	Si	61
3	31.42	31.42	-0.00	6.16	18	22	Si	58

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	31.42	31.42	-0.01	4.88	28	28	Si	74
3	31.42	31.42	0.00	5.05	28	28	Si	71

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
3	0.0	0.0	0.0	1.18	-123.34	15.63	5.05	0.007	0.007	28 (Qp)	Si	27
3	0.0	0.0	0.0	1.41	-120.19	11.19	4.82	0.007	0.007	26 (Fr)	Si	43

Muro [Platea]: 39 - Nodi: [23-33-32-22]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.01	2.54	22	22	Si	>100
1	31.42	31.42	-0.01	6.61	22	22	Si	54

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
1	31.42	31.42	-0.02	5.53	28	28	Si	65

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
1	-0.0	0.0	0.0	49.78	-137.67	-11.99	5.53	0.008	0.008	28 (Qp)	Si	25
1	-0.0	0.0	0.0	49.41	-133.01	-18.34	5.37	0.008	0.008	26 (Fr)	Si	38

Muro [Platea]: 40 - Nodi: [13-23-22-12]Pann=4Spess.=50 cm, Terreno=Terreno1, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.01	2.92	22	22	Si	>100
1	31.42	31.42	-0.01	7.32	22	22	Si	49



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Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.02	5.69	28	28	Si	63

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
3	-0.0	0.0	-0.0	54.61	-142.75	29.83	5.69	0.008	0.008	28 (Qp)	Si	24
3	-0.0	0.0	-0.0	56.54	-138.62	28.98	5.55	0.008	0.008	23 (Fr)	Si	37

Muro : 41 - Nodi: [15-115-114-14], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.72	11.03	22	22	Si	31

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	31.42	31.42	-0.56	3.97	28	28	Si	30

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
11	-0.0	-0.0	-0.0	-48.75	-7.06	-4.08	0.49	0.000	0.000	26 (Fr)	Si	>100
16	-0.1	-0.1	-0.1	-238.84	-8.50	-112.88	3.97	0.003	0.003	28 (Qp)	Si	71

Muro : 42 - Nodi: [35-34-134-135], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	31.42	31.42	-1.94	31.17	22	22	Si	12

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	31.42	31.42	-0.56	3.97	28	28	Si	30

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
16	-0.1	-0.1	-0.1	-8.97	-238.89	-112.76	3.97	0.003	0.003	28 (Qp)	Si	71
16	-0.1	-0.1	-0.1	-8.98	-238.90	-112.71	3.96	0.003	0.003	23 (Fr)	Si	>100

Muro : 43 - Nodi: [14-114-113-13], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	31.42	31.42	-0.76	10.59	22	22	Si	30
2	31.42	31.42	-0.73	12.09	22	22	Si	30

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	31.42	31.42	-0.59	7.37	28	28	Si	28

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
15	0.0	0.0	0.0	-7.53	-3.61	-6.08	2.50	0.004	0.004	27 (Fr)	Si	79
16	-0.1	-0.0	-0.0	-241.34	9.19	-96.67	7.37	0.006	0.006	28 (Qp)	Si	36

Muro : 44 - Nodi: [34-33-133-134], Pann.X=4, Pann.Y=4Spess.=20 cm, Terreno=--,Criterio=CLS\_Muri\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

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P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	31.42	31.42	-1.99	35.71	22	22	Si	10

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
16	31.42	31.42	-0.59	7.38	28	28	Si	28

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
16	-0.0	-0.1	-0.0	9.18	-241.33	-96.67	7.38	0.006	0.006	28 (Qp)	Si	36
16	-0.0	-0.1	-0.0	9.17	-241.34	-96.66	7.39	0.006	0.006	23 (Fr)	Si	54

Muro [Platea]: 45 - Nodi: [22-32-31-21]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.01	0.34	22	22	Si	>100
1	31.42	31.42	-0.01	0.63	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
2	31.42	31.42	-0.01	0.32	28	28	Si	>100
1	31.42	31.42	-0.01	0.60	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
2	-0.0	0.0	-0.0	36.22	7.38	-4.16	0.32	0.000	0.000	28 (Qp)	Si	>100
2	-0.0	0.0	-0.0	35.15	6.96	-4.16	0.31	0.000	0.000	26 (Fr)	Si	>100

Muro [Platea]: 46 - Nodi: [12-22-21-11]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.01	0.37	22	22	Si	>100
3	31.42	31.42	-0.01	0.74	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.02	0.32	28	28	Si	>100
3	31.42	31.42	-0.01	0.59	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.0	0.0	-0.0	37.17	6.80	5.29	0.32	0.001	0.001	28 (Qp)	Si	>100
4	-0.0	0.0	-0.0	37.93	6.70	5.33	0.32	0.000	0.000	23 (Fr)	Si	>100

Muro [Platea]: 47 - Nodi: [1-2-12-11]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	0.32	20	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
4	31.42	31.42	-0.00	0.15	28	28	Si	>100
3	31.42	31.42	-0.00	0.38	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			

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P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
1	0.0	0.0	0.0	4.65	0.91	2.76	0.18	0.000	0.000	28 (Qp)	Si	>100
4	0.0	-0.0	0.0	-8.05	5.68	-12.54	0.15	0.000	0.000	24 (Fr)	Si	>100

Muro [Platea]: 48 - Nodi: [32-42-41-31]Pann=4Spess.=50 cm, Terreno=Terrenol, ,Criterio=CLS\_Platee\_ND, Materiale=C35/45

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara:  $\sigma_{ca}$ [MPa]=22.41  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.00	0.42	22	22	Si	>100

Combinazione QP:  $\sigma_{ca}$ [MPa]=16.81  $\sigma_{fa}$ [MPa]=360.00

P.	Afx	Afy	$\sigma_c$	$\sigma_f$	Cbc	Cbf	Ver	Cs
	cmq/m	cmq/m	MPa	MPa				
3	31.42	31.42	-0.00	0.38	28	28	Si	>100

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

P.	Nx	Ny	Nxy	Mx	My	Mxy	$\sigma_{fmed}$	Wd	Wk	Cb	Ver	Cs
	MPa	MPa	MPa	daN	daN	daN	MPa	mm	mm			
4	-0.0	0.0	0.0	0.60	4.92	1.33	0.20	0.000	0.000	28 (Qp)	Si	>100
4	-0.0	0.0	0.0	0.71	4.84	1.25	0.19	0.000	0.000	23 (Fr)	Si	>100

Il Progettista